

Thermodynamic Potentials (Free energies)

- Enthalpy $H(U, P, N)$
- Helmholtz free energy $F(T, V, N)$
- Gibbs free energy $G(T, P, N)$
- Maxwell relations
- Phase transitions
- Clausius - Clapeyron Eqn.
- Mixtures
- Osmotic pressure

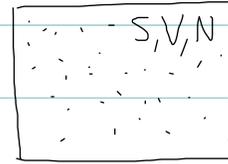
Thermodynamic Potentials

1. $U(S, V, N)$ - internal energy

→ isolated system w/ fixed S, V, N

→ state determined by maximum S

$$\rightarrow dU = Tds - PdV + \mu dN$$



2. $H(S, P, N)$ - Enthalpy

$$\rightarrow H = U + PV$$

→ fixed S, P, N

→ energy to make system in vacuum (U) +
work to make room for it (PV)



→ recall C_v vs $C_p = \left. \frac{\partial H}{\partial T} \right|_p$

$$\rightarrow dH = dU + PdV + VdP = Tds + VdP + \mu dN$$

$$\Rightarrow H(S, \underline{P}, N)$$

$$T = \left. \frac{\partial H}{\partial S} \right|_{P, N}, \quad V = \left. \frac{\partial H}{\partial P} \right|_{S, N}$$

} Legendre transform:

cf Hamilt \leftrightarrow Lagr.

$$L = p\dot{q} - H$$

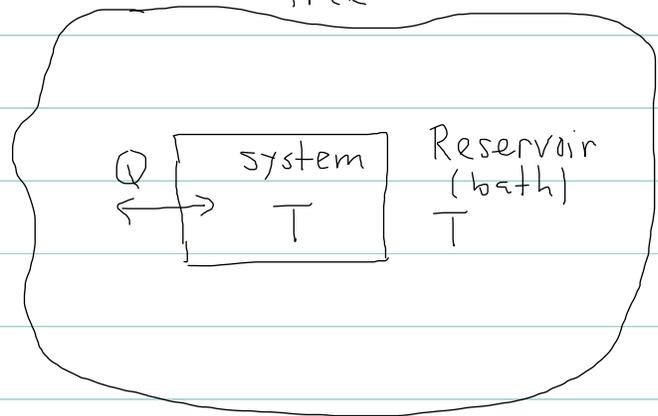
3. $F(T, V, N)$ - Helmholtz free energy

$$\rightarrow F(T, V, N) = U(S, V, N) - TS$$

\rightarrow fixed T, V, N

energy to
create isolated
system

heat that enters
from reservoir for
free



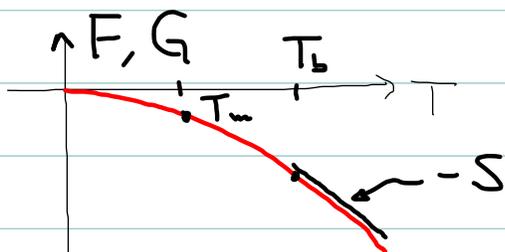
(reversible) $TdS - PdV + \mu dN$

$$\rightarrow dF = dU - TdS - dTS$$

\uparrow
minimize $= -SdT - PdV + \mu dN \Rightarrow F(T, V, N)$

$$= \underbrace{Q - TdS + W}_{\leq 0} \leq W = W_{\text{other}} (\text{const } V)$$

$$\Rightarrow \left. \frac{\partial F}{\partial T} \right|_{V, N} = -S, \quad \left. \frac{\partial F}{\partial V} \right|_{T, N} = -P, \quad \left. \frac{\partial F}{\partial N} \right|_{T, V} = \mu$$



4. $G(T, P, N)$ - Gibbs free energy

$$\rightarrow G(T, P) = F(T, V) + PV$$

$$= H(S, P) - TS$$

$$= U(S, V) + PV - TS$$

$$\rightarrow dG = dU + PdV + VdP - Tds - dTS$$

$$= VdP - SdT + \underbrace{\mu dN}_{\text{if many species}} \leq W_{\text{other}} \left(\text{const}_{T, P} \right)$$

$$\Rightarrow \mu = \left. \frac{\partial G}{\partial N} \right|_{T, P}$$

$$+ \mu_1 dN_1 + \mu_2 dN_2 + \dots$$

$$\Rightarrow \underline{G = \mu N}$$

summary:

	→ -TS				
↓	<table border="1" style="border-collapse: collapse; text-align: center;"> <tr> <td>U</td> <td>F</td> </tr> <tr> <td>H</td> <td>G</td> </tr> </table>	U	F	H	G
U	F				
H	G				
+PV					

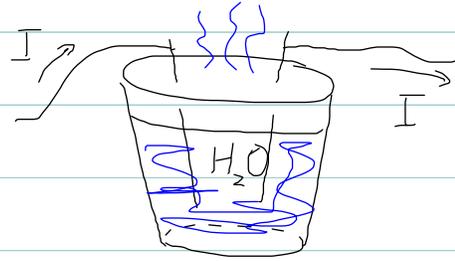
- U - energy of syst. in isolation
- H - net energy including PV work against pressure
- F - net energy for system in contact w/ reservoir @ T
- $G = U - TS + PV$

heat entering
from bath

work
against P

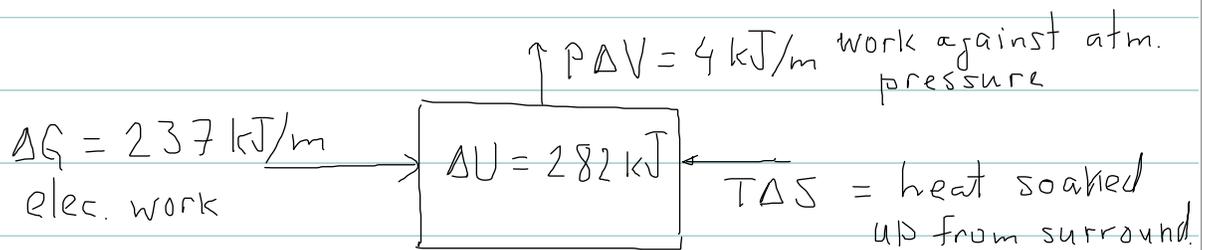
Electrolysis: separate $H_2O \rightarrow H_2 + \frac{1}{2}O_2$
via electrical current

How much energy/mole
is required?



At T_{room} , done slowly @ const p , the electrical
energy: $\Delta G = \Delta U + p\Delta V - T\Delta S$

$$= 282 \text{ kJ} + 4 \text{ kJ} - 49 \text{ kJ} = 237 \text{ kJ/mol}$$

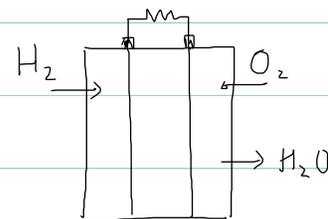
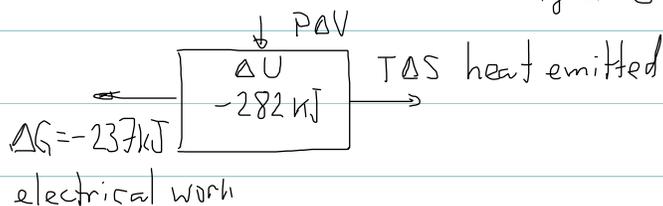


note: for isolated system (S, V, N fixed) \Rightarrow

$$W_{elect.} = \Delta U = 282 \text{ kJ/m}$$

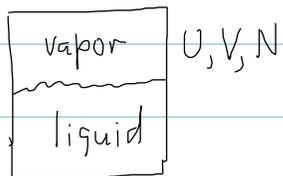
↓ lower S

Fuel cell (battery): $H_2 + \frac{1}{2}O_2 \rightarrow H_2O$
higher S



(in battery no gases involved: $\Delta V = 0 \Rightarrow \Delta U \approx \Delta H$; $\Delta F \approx \Delta G$)

- S maximized for isolated system (fixed U, V, N):

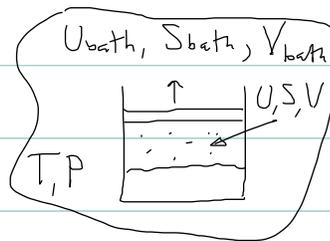


- $F = U - TS$ is minimized for system @ T - constant \Leftrightarrow

$$S_{\text{univ.}} = S_{\text{sys}} + S_{\text{bath}} \text{ is maximum: } dF = \underbrace{Q - Tds}_{\leq 0} - \underbrace{PdV}_{\substack{\text{const} \\ V}} \leq 0$$

- $G = \underbrace{U + PV}_H - TS$ is minimized for system @ T, p - constant \Leftrightarrow

S_{universe} - maximized



$$dS_{\text{univ}} = dS + dS_{\text{bath}}$$

$$= dS - \frac{dU}{T} - \frac{P}{T} dV \quad (dU_{\text{bath}} = -dU, dV_{\text{bath}} = -dV)$$

$$= -\frac{1}{T} (dU - Tds + PdV) = -\frac{1}{T} dG \Rightarrow \text{minimize } G$$

why? $G = U + PV - TS$

$$\left. \begin{aligned} \rightarrow \text{IF } U \downarrow, U_{\text{bath}} \uparrow \Rightarrow S_{\text{bath}} \uparrow \\ \rightarrow \text{IF } V \downarrow, V_{\text{bath}} \uparrow \Rightarrow S_{\text{bath}} \uparrow \\ \rightarrow S \uparrow \end{aligned} \right\} G \downarrow$$

balance: $dS_b = \frac{dU_b}{T} + \frac{P}{T} dV_b = -\frac{dU}{T} - \frac{P}{T} dV$

at low T , ΔS_{bath} big for $\Delta U, \Delta V$; high T ΔS_{bath} small.

Maxwell relations

dU, dS, dH, dF, dG - exact differential

$$\Rightarrow \frac{\partial^2 f}{\partial x \partial y} = \frac{\partial^2 f}{\partial y \partial x} \quad (\text{vanishing } \nabla \times \nabla f, \text{ partial commute, exact})$$

• $dU = TdS - PdV + \mu dN$; $\frac{\partial U}{\partial S} = T$, $\frac{\partial U}{\partial V} = -P$, ...

$$\Rightarrow \left. \frac{\partial T}{\partial V} \right|_{V,N} = - \left. \frac{\partial P}{\partial S} \right|_{V,N}, \quad \left. \frac{\partial T}{\partial N} \right|_{S,V} = \left. \frac{\partial \mu}{\partial S} \right|_{V,N}, \dots$$

• $dG = -SdT + VdP + \mu dN$; $S = - \left. \frac{\partial G}{\partial T} \right|_{P,N}$, $V = \left. \frac{\partial G}{\partial P} \right|_{T,N}$, $\mu = \left. \frac{\partial G}{\partial N} \right|_{T,P}$

$$- \left. \frac{\partial S}{\partial P} \right|_{T,N} = \left. \frac{\partial V}{\partial T} \right|_{P,N}, \quad \left. \frac{\partial V}{\partial N} \right|_{T,P} = \left. \frac{\partial \mu}{\partial P} \right|_{T,N}, \dots$$

also recall: $f(x, y, z) = \text{const.}$

$$\Rightarrow \left. \frac{\partial x}{\partial y} \right|_z \left. \frac{\partial y}{\partial z} \right|_x \left. \frac{\partial z}{\partial x} \right|_y = -1$$

proof:

$$0 = df = \frac{\partial f}{\partial x} dx + \frac{\partial f}{\partial y} dy + \frac{\partial f}{\partial z} dz$$

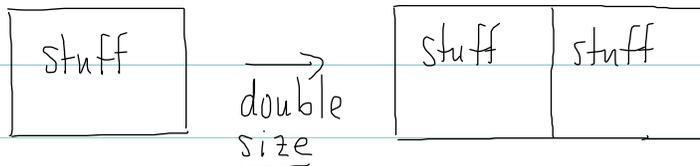
& $f(x, y, z) = c \Rightarrow z(x, y)$

$$dz = \left. \frac{\partial z}{\partial x} \right|_y dx + \left. \frac{\partial z}{\partial y} \right|_x dy$$

$$\Rightarrow 0 = \left(\frac{\partial_x f}{\partial_x} + \frac{\partial_z f}{\partial_x} \left. \frac{\partial z}{\partial x} \right|_y \right) dx + \left(\frac{\partial_y f}{\partial_y} + \frac{\partial_z f}{\partial_y} \left. \frac{\partial z}{\partial y} \right|_x \right) dy$$

$$\Rightarrow \left. \frac{\partial z}{\partial x} \right|_y = - \frac{\frac{\partial_x f}{\partial_x}}{\frac{\partial_z f}{\partial_z}} = - \frac{\frac{\partial_y f}{\partial_x}}{\frac{\partial_y f}{\partial_z}} \quad \checkmark$$

Extensive vs Intensive



$V, N \rightarrow 2V, 2N$ extensive

$T, P \rightarrow T, P$ intensive

Extensive: m, V, N, S, U, H, F, G

Intensive: T, ρ, n, μ

(intensive)(intensive) = (intensive)

(intensive)(extensive) = (extensive)

(extensive)(extensive) = (wrong, typically)

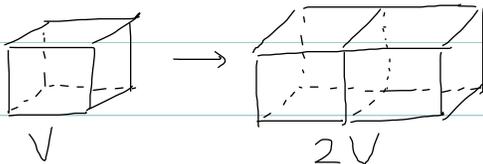
(intensive) + (intensive) = (intensive)

(extensive) + (extensive) = (extensive)

(extensive) + (intensive) = (wrong)

apple + orange

note: ignore surface effects, which are important for small syst.



, but $S \neq 2S$

Important relation: $\mu = \left. \frac{\partial G}{\partial N} \right|_{T,P} \Rightarrow \underline{G = \mu N}$

but $\mu = \left. \frac{\partial F}{\partial N} \right|_{T,V} \not\Rightarrow F = \mu N$, why?

$G(N, p, T) = \int dN \mu(T, P)$
 ↑ extensive N ← extensive μ(T, P) ← intensive
 fixed N_i const. when T, P - const (since intensive)

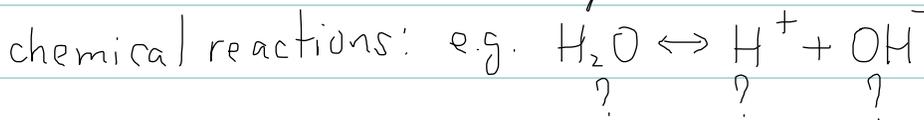
but $\mu = \left. \frac{\partial U}{\partial N} \right|_{S,V} \Leftrightarrow U(S, V, N) = \int dN \mu(S, V, N) \not\Rightarrow \cancel{U = \mu N}$
 μ ≡ const.

$\Rightarrow G = \mu_1 N_1 + \mu_2 N_2 + \dots$

mixture of diff. species, e.g. chem reaction solution, etc.

another derivation: $G(T, P, N) \Rightarrow G(T, P, \lambda N) = \lambda G(T, P, N)$

$\left. \frac{\partial}{\partial \lambda} \right|_{\lambda=1} \Rightarrow G(T, P, N) = N \left. \frac{\partial G}{\partial N} \right|_{T,P} = N \mu \quad \checkmark$



equilibrium: $0 = dG = \mu_{H_2O} dN_{H_2O} + \mu_{H^+} dN_{H^+} + \mu_{OH^-} dN_{OH^-}$
 $\Rightarrow \mu_{H_2O} = \mu_{H^+} + \mu_{OH^-}$

more generally: $\nu_1 X_1 + \nu_2 X_2 + \dots \rightarrow \nu_3 X_3 + \nu_4 X_4 + \dots$

$\Rightarrow \nu_1 \mu_1 + \nu_2 \mu_2 + \dots = \nu_3 \mu_3 + \nu_4 \mu_4 + \dots$

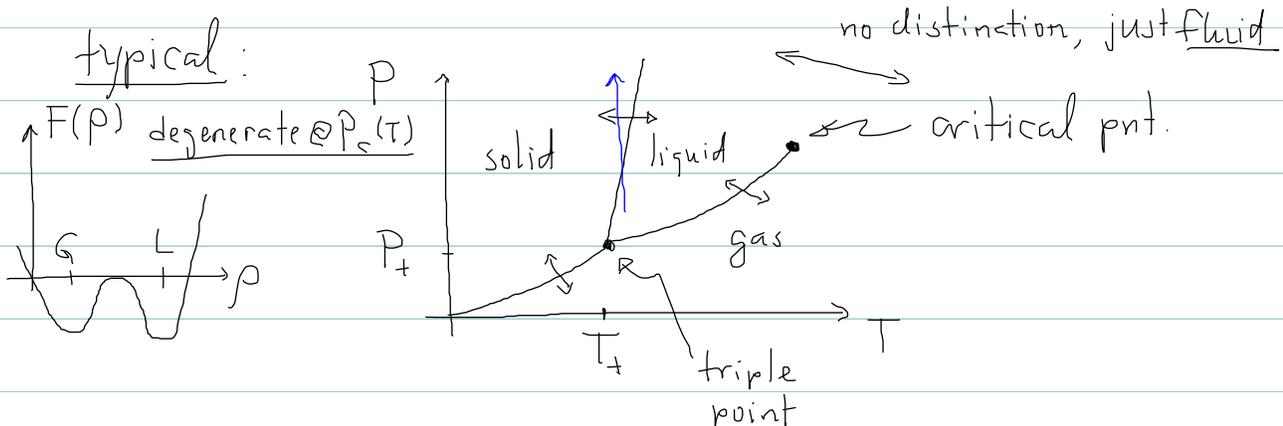
\Rightarrow partial pressures & concentrations of reactance

Phase Transitions

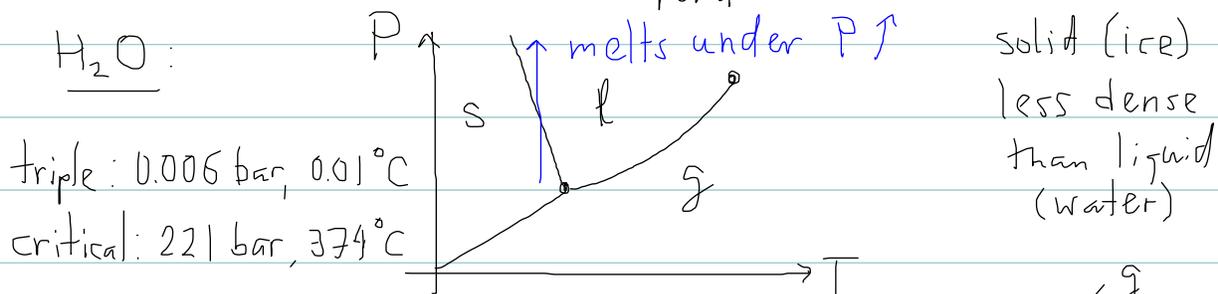
use G since usually @ fixed T, P :

Ex. gas \leftrightarrow liquid \leftrightarrow solid

typical:



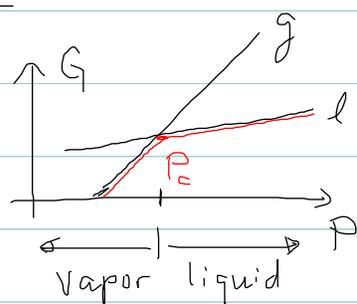
H₂O:



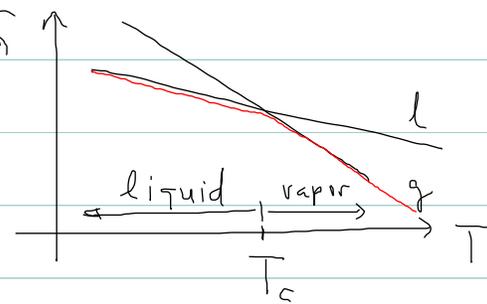
triple: 0.006 bar, 0.01 °C
critical: 221 bar, 374 °C

note: (1) $\left. \frac{\partial G}{\partial P} \right|_{T, N} = V > 0 \Rightarrow$

phase w/ lower G is the stable one



(2) $\left. \frac{\partial G}{\partial T} \right|_{V, N} = -S < 0 \Rightarrow G$



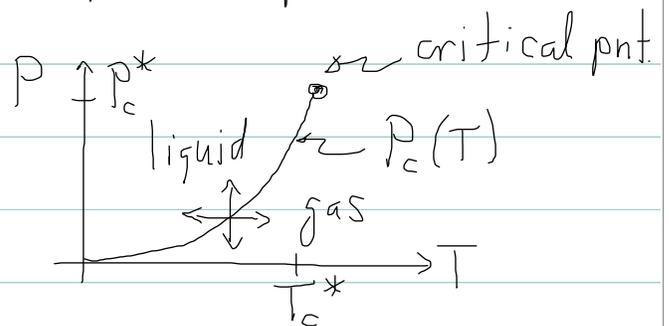
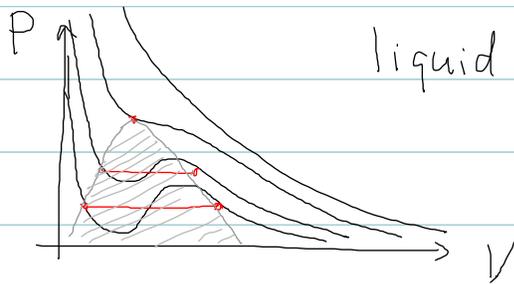
$(V_{\text{solid}}^{\text{H}_2\text{O}} > V_{\text{liquid}}^{\text{H}_2\text{O}} \Rightarrow$

$P \uparrow$ Ice melts, since G_{water} increases slower w/ P (smaller V , high n) \Rightarrow melts

van der Waals EOS:

$$\left(P + \frac{aN^2}{V^2} \right) (V - Nb) = Nk_B T$$

reduced P due to attractive interactions excluded volume



- density (V) jumps across P_c T_c

- vapor pressure $P_c(T)$ - coexistence pressure at which condensation/boiling transition takes place.

vaporization of droplet:

- self-tunes $P < P_c \rightarrow P = P_c$ as liquid evaporates

- to get $P > P_c$ need to have enclosed container & reduce volume

- under vaporization either all liquid evaporates for $P < P_c$ or $P \rightarrow P_c$.

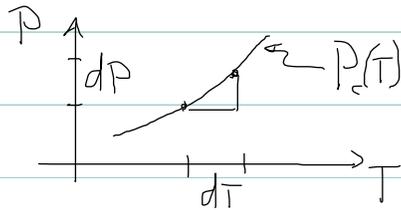
Clausius-Clapeyron Relation

phase boundary on P-T phase diagram

e.g. liquid-gas $P_c(T)$:

at $P_c(T)$: $G_l = G_g \Leftrightarrow \mu_l = \mu_g$ (maximizes S_{tot})

change ΔT , ΔP s.t. on $P_c(T)$



$$\underline{dG_l = dG_g}$$

$$-S_l dT + V_l dP = -S_g dT + V_g dP$$

$$\Rightarrow (S_g - S_l) dT = (V_g - V_l) dP \Rightarrow \left. \frac{dP}{dT} \right|_{P_c} = \frac{\Delta S}{\Delta V} = \frac{L}{T \Delta V}$$

latent heat

gives slope of $P_c(T)$

C-C relation

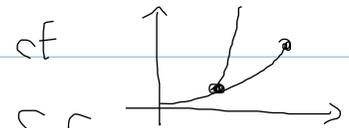
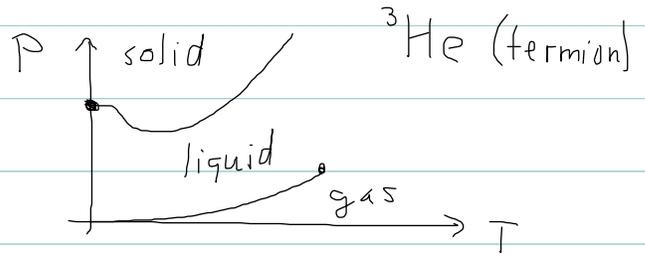
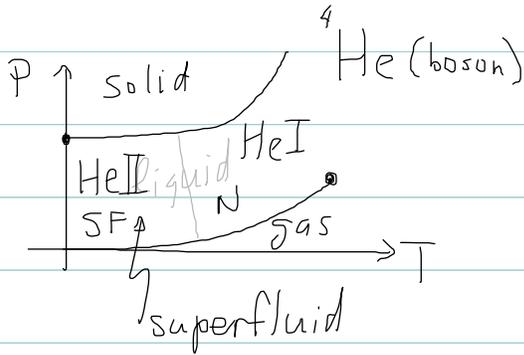
in terms of ΔS , ΔV

$$\text{liquid-gas: } \Delta S > 0, \Delta V > 0 \Rightarrow \frac{dP}{dT} > 0$$

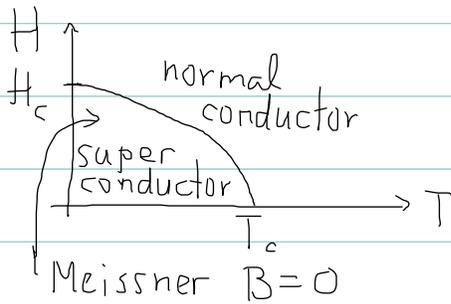
$$\text{water-ice: } S_{ice} - S_{water} < 0, V_{ice} - V_w > 0 \Rightarrow \frac{dP}{dT} < 0$$

Other Transitions

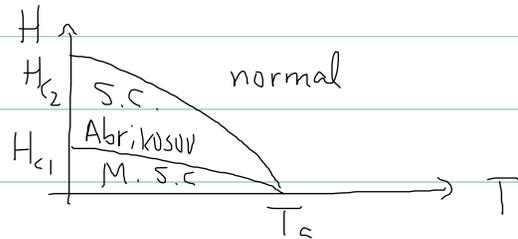
- He - only substance that remains a liquid down to $T=0$



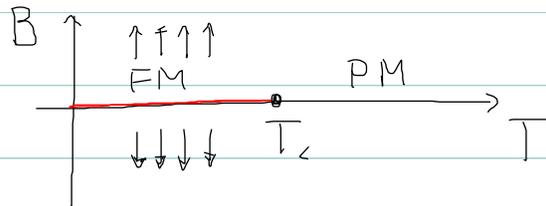
- Type I S.C.



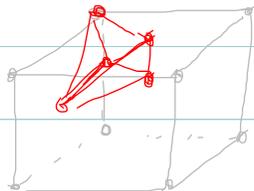
- Type II S.C.



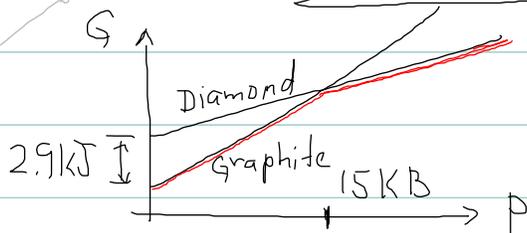
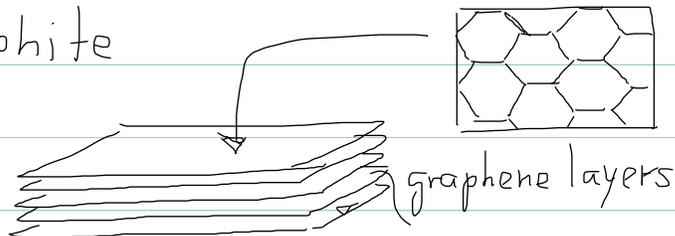
- Ferromagnet (Fe)



- diamond & graphite



vs



$$\left. \frac{\partial G}{\partial P} \right|_{T,N} = V > \text{for graphite}$$

$$\left. \frac{\partial G}{\partial T} \right|_{P,N} = -S \Rightarrow S_{gr} > S_{diam.} \Rightarrow T \uparrow \Rightarrow \text{graphite}$$

Phase transformation of mixtures

A & B molecules: $N_A + N_B = N \leftarrow$ fixed

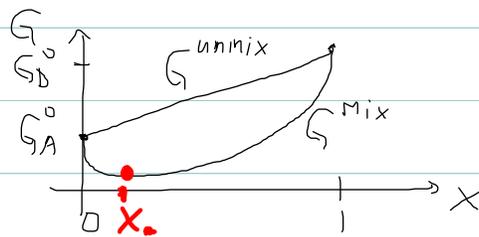
$$\left. \begin{aligned} x &\equiv \frac{N_B}{N} - \text{B fraction} \\ 1-x &= \frac{N_A}{N} - \text{A fraction} \end{aligned} \right\} \text{vary } x$$

$$G_{AB}^{\text{unmixed}} = (1-x)G_A^\circ + xG_B^\circ - \text{unmixed}$$

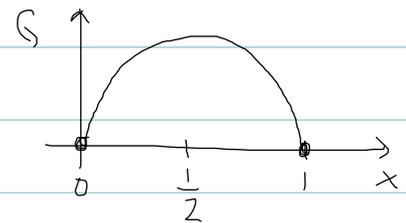
$$\text{mix A \& B: } \Delta S_{\text{mix}} = -k_B N [x \ln x + (1-x) \ln(1-x)]$$

(see prob. 2.38 & Ising PM up/down \Leftrightarrow A & B)

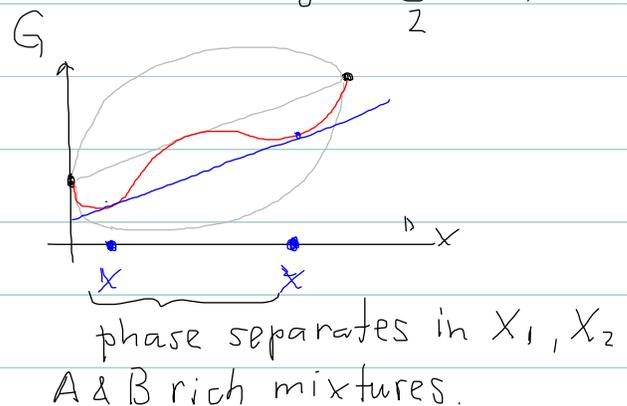
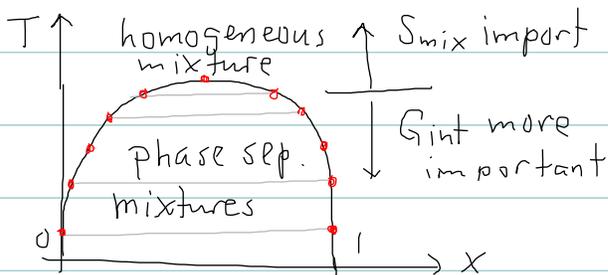
$$G_o^{\text{mix}} \approx (1-x)G_A^\circ + xG_B^\circ + \underbrace{k_B T N [x \ln x + (1-x) \ln(1-x)]}_{-TS}$$



add repulsive inter. $G_{\text{int}} = U_0 x(1-x)$



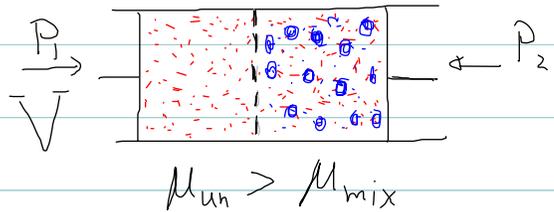
$$G_{\text{int}}^{\text{mix}} = G_o^{\text{mix}} + G_{\text{int}}$$



Osmotic Pressure

- solvent can go across membrane

- solute cannot



e.g. membrane surrounding

plant or animal cell, permeable to water & small molecules, but not large ions.

$\mu_{unmix} > \mu_{mix} \Rightarrow$ solvent moves to the right until

$$P_2 > P_1 \quad \text{s.t.} \quad \mu_{mix}(P_2, T) = \mu_{unmix}(P_1, T)$$

and flow stops

$P_{osmotic} \equiv P_2 - P_1$ (microscopically: more from L \rightarrow R than from R \rightarrow L)

\Leftrightarrow imbalanced pressure of solute

$$P_{osm} \approx \frac{N_B k_B T}{V}$$

can be huge: put cell inside pure water & osmotic pressure will build up (~ 10 Pascals) \Rightarrow animal cell will burst
plant cell are rigid & use osmosis to bring water up the stem