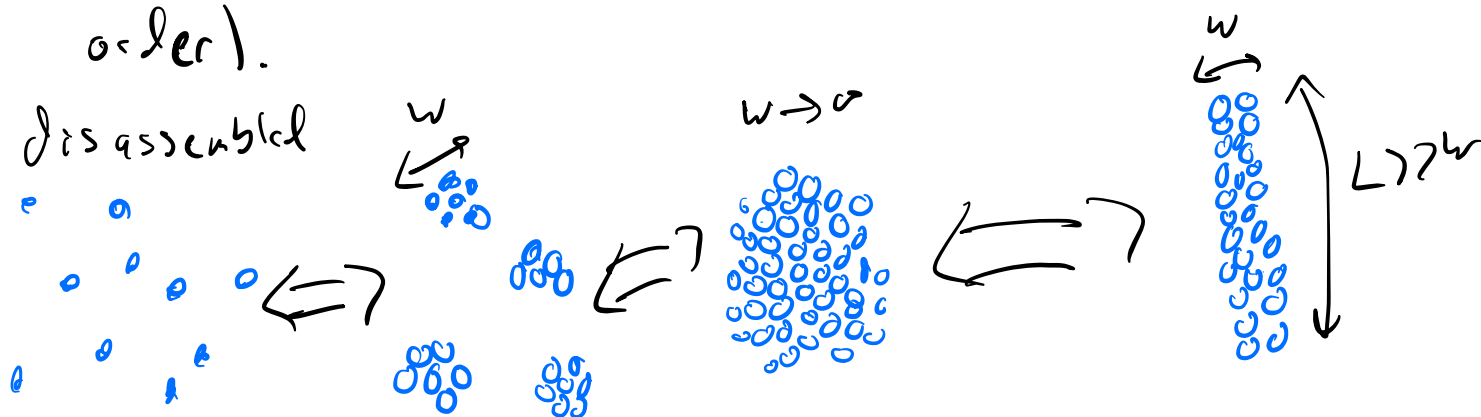


III

GFA Consequences: Shape & Size Selection

In "canonical view" of GF (see Sadoc & Mosser) the ordered domain itself is considered fixed, and usually assumed to take bulk dimensions (i.e. $L \rightarrow \infty$). In assemblies, size and shape of domain become important degrees of freedom (in addition to internal order).



Let's start with a simple assembly model, short-range, cohesive interactions = $-u_0$

Interaction energy of clusters:

$$E_{\text{int}} = -u_0 \underbrace{\frac{\langle z \rangle}{2}}_{\text{avg. \# neighbors}} \underbrace{N_p}_{\substack{\text{\# particles} \\ N_p \propto W^d}} + \frac{u_0}{2} \underbrace{\Delta z}_{\substack{\text{decrease in} \\ \text{neighbor @ surf.}}} \underbrace{N_s}_{\substack{\text{\# @ surface} \propto W^{d-1}}}$$

Canonical ensemble $\Rightarrow$ Fixed N_{tot}

For simplicity, assume n_c clusters of size W

$$N_{tot} = n_c N_p$$

$$F_{tot} = n_c E_{int}(W) = N_{tot} \left(\frac{E_{int}}{N_p} \right) = N_{tot} E_{int}(w)$$

$\hookrightarrow$ consider $T \gg 0$ energy/particle (intensive)

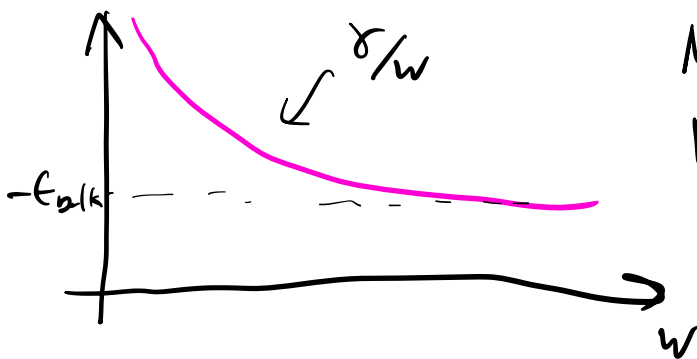
In simple model (short-range cohesion):

$$E_{int}(w) = -u_0 \frac{\langle z \rangle}{2} + \frac{u_0}{2} \Delta z \left(\frac{N_s}{N_p} \right) \sim \frac{w^{d-1}}{w^d} = \frac{1}{w}$$

const. $\nearrow$

$$E_{int}(w) = -E_{bulk} + \frac{\gamma}{w}$$

γ surface energy



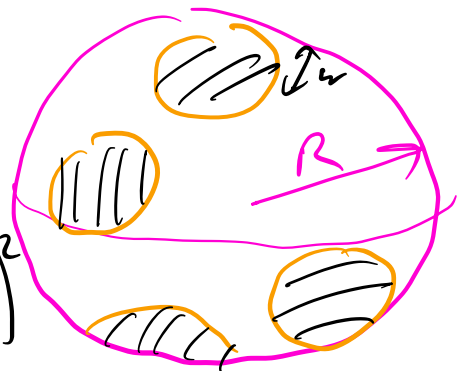
Minimal E_{tot}

$W_* \rightarrow \infty$; single, macroscopic cluster

For GFA $E_{int}(w)$ has additional terms due to accumulation of internal stress

Ex. 2D Nematic domains (defect-free) on sphere

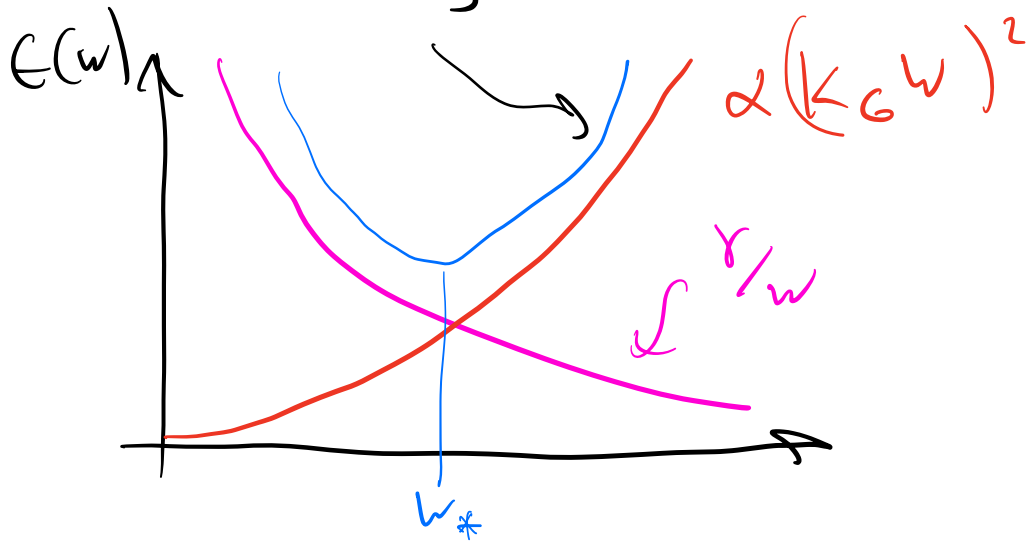
last lecture: $F_{elas} = \frac{K_F}{16} (Area) \left(\frac{w}{R^2} \right)^2$



$$\epsilon(w) = -\epsilon_{\text{bulk}} + \frac{\gamma}{w} + \frac{F_{\text{elas}}}{\rho_0 (A_{\text{ren}})}$$

$\rho_0 (A_{\text{ren}}) \rightarrow \text{density of particles}$

"excess" energy density $\rightarrow \epsilon_{\text{ex}}(w) = \frac{K_f}{16 \rho_0} \left(\frac{w}{R^2} \right)^2$



$$\frac{\partial \epsilon}{\partial w} = -\frac{\gamma}{w_*^2} + \frac{K_f w}{8 \rho_0 R^4} \Rightarrow w_* = \left(\frac{8\gamma}{K_f} \rho_0 \right)^{1/3} R^{4/3}$$

Self-limited assembly:

finite domain size w_x

subunit $\ll w_* \ll$ bulk size

Note $\lim_{K_c \rightarrow 0} w_* \rightarrow \infty$, unlimited for frustration-free limit

2nd Ex. Crystalline domains on spheres (Schneider & Gompper, EPL 2005)

$$E_{ex}(w) = \frac{\gamma}{384 \rho_s} \left(\frac{w}{R} \right)^4$$

$$\Rightarrow w_* \propto \left(\frac{\gamma \rho_s}{\gamma} \right)^{1/5} K_6^{-2/5}$$

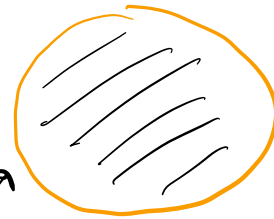
$\uparrow$ cohesion/stiffness $\nwarrow$ frustration

Shapes of domains

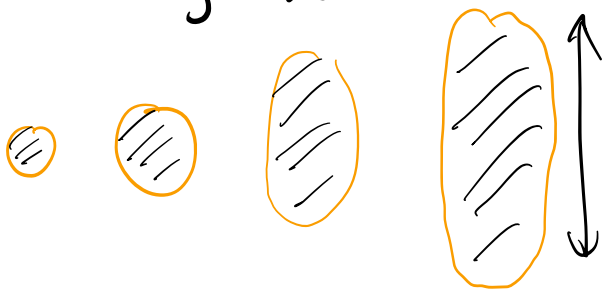
So far we have tacitly assumed compact (circular) domains. Why?

But E_{int} also includes elastic cost of frustration.

circular minimizes boundary



For large domains $\Rightarrow$ symmetry breaking



$L \gg w$ sometimes called "filamentation"

Why would strip be better? Consider 2D

nematic example again



$$F = \frac{K_F}{2} \int dA (\nabla_{\perp} \Theta - \vec{A})^2 \quad \text{Recall: } \vec{A} = \frac{1}{2R^2} (-y \hat{x} + x \hat{y})$$

$$\text{E.L. equation } \nabla_{\perp}^2 \Theta = 0 \quad \text{B.C. } (\partial_y \Theta - A_y) \Big|_{y=\pm \frac{w}{2}} = 0$$

$$\Theta = Ax + Bx + Cxy + D \quad = \partial_y \Theta \Big|_{y=\pm \frac{w}{2}} = \frac{x}{2R^2}$$

$$A=B=0 \quad C = -\frac{1}{2R^2} \quad \leftarrow = -Cx - \frac{x}{2R^2}$$

$$\text{strain gradient: } (\nabla_{\perp} \Theta - \vec{A}) = -2 \times \frac{1}{2R^2} y \hat{x}$$

$$\text{can check } \nabla_{\perp} \times (\nabla_{\perp} \Theta - \vec{A}) = -K_G$$

grows $\perp$ to
long direction

Frustration requires strain gradient. Energetics
selects direction of gradient

$$F = \frac{K_F}{2} L \int_{-w/2}^{+w/2} dy \left(\frac{x}{R^2} \right)^2 = \frac{K_F}{8} \underbrace{(Lw)}_{\text{Area}} \left(\frac{w}{R^2} \right)^2 \propto L w^3$$

faster growth
in $\perp$ direction

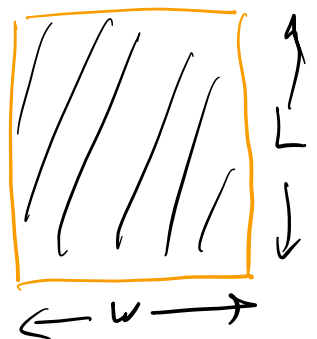
Crude model of shape selection.

$\Rightarrow$ Assume rectangular shape, fixed $N_p \propto Lw$

$$E_{\text{tot}} \propto \frac{F_{\text{tot}}}{\text{Area}} \approx -E_{\text{bulk}} + \frac{\gamma(\text{perimeter})}{Lw}$$

$$+ \frac{K_F}{8} (K_G w)^2 \quad \leftarrow \text{assume still holds for } w \lesssim L$$

$$= \text{const.} + 2\gamma \left(\frac{1}{w} + \frac{w}{\text{Area}} \right) + \frac{K_F}{8} (K_G w)^2$$



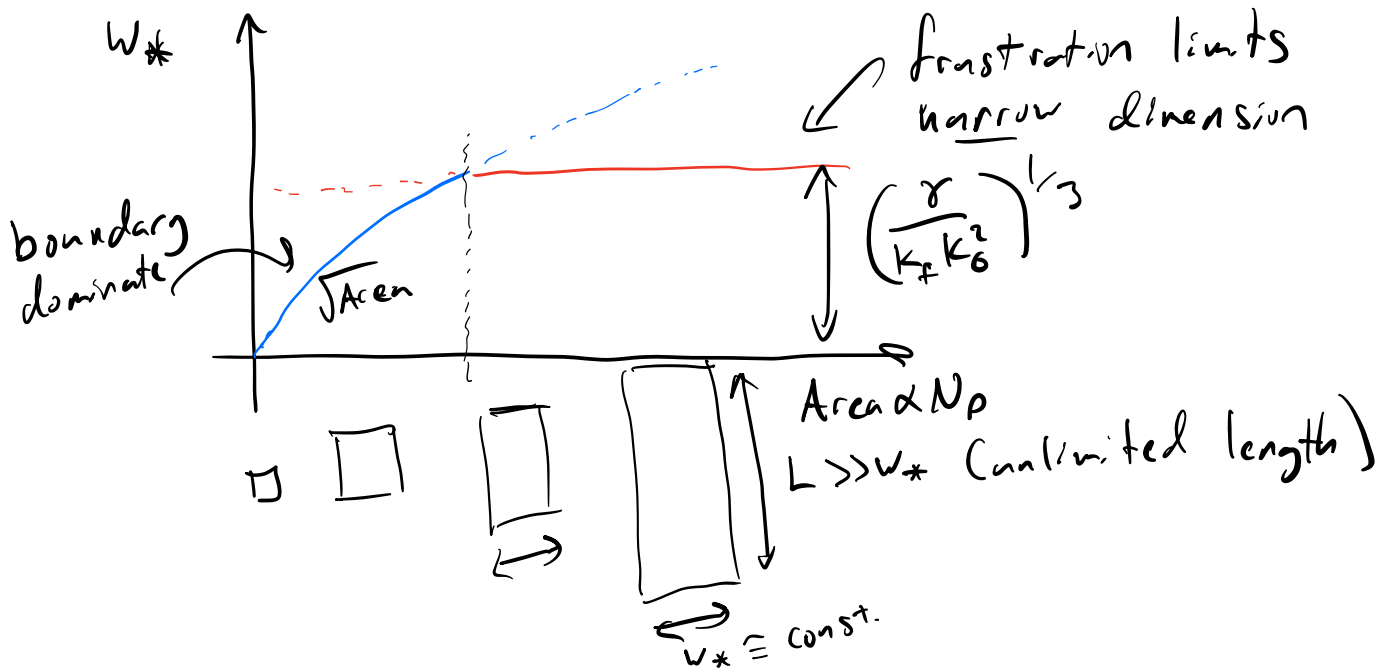
Equlibrium shape $\left. \frac{\partial E}{\partial w} \right|_{\text{Area}} = 2\gamma \left(-\frac{1}{w^2} + \frac{1}{\text{Area}} \right) + \frac{k_f}{4} k_G^2 w$

For small area, surface term dominates

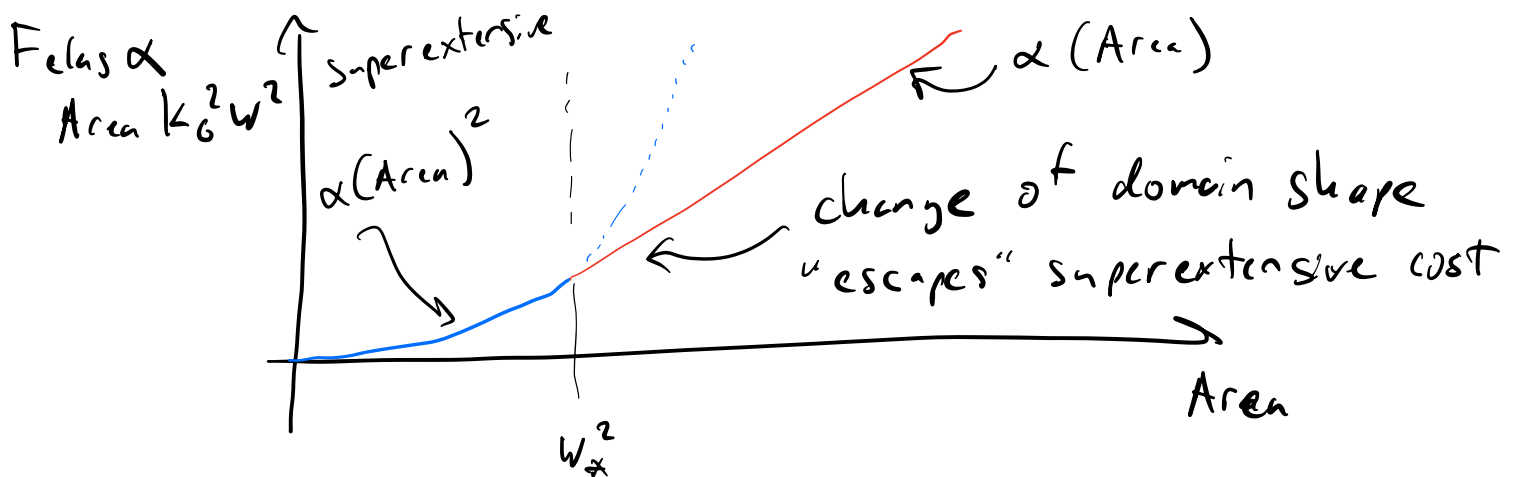
$\Rightarrow w_* \approx \sqrt{\text{Area}} = L_x$ (square)

For large area, frustration balances edge energy

$w_* \approx \left(\frac{4\gamma}{k_f k_G^2} \right)^{1/3}$ independent of Area



Notice the cross over in elastic energy v.s. area



This is the first example of "frustration escape": groundstate avoids superextensive growth of elastic energy via some morphological motif (a.k.a. mode).

Here, transition from compact to extended (a.k.a. "filamented") domain shape.