

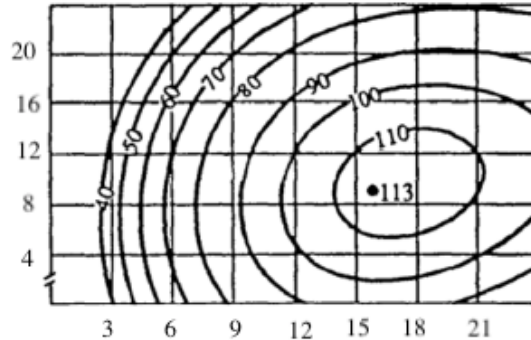
APPM 2350—Final Exam

Saturday, Dec 11th 7:30am-10am 2021

Show all your work and simplify your answers. Answers with no justification will receive no points. You are allowed one 8.5×11-in page of notes (TWO sided). You may NOT use a calculator, smartphone, smartwatch, the Internet or any other electronic device.

Problem 1 (35 points)

Use the portion of the level curve graph of $g(x, y)$ shown below to answer the following questions. You can assume $g(x, y)$ is a continuous function with continuous partial derivatives.



Do NOT try to find an expression for the actual function $g(x, y)$ (no credit will be given). Use ONLY the information provided on the level curve plot to answer the following questions:

- Estimate $g_y(9, 16)$. For credit, *show work* justifying your estimate.
- Estimate the derivative of $g(x, y)$ at the point $(9, 16)$ in the direction $-3\mathbf{i} + 4\mathbf{j}$. For credit, *show work* justifying/explaining your estimate.
- Estimate \mathbf{n} , a unit vector that is normal to the surface $z = g(x, y)$ at the point $(9, 16, 80)$. For credit, *show work* justifying your estimate.
- Based on the level curves shown, are there any points in the domain where $\nabla g = \vec{0}$? If not, explain why. If so, give the value of $g(x, y)$ at the point(s).
- Let C be the level curve defined by $g(x, y) = 110$ and oriented counter-clockwise. Determine whether the work done by $\mathbf{G} = \nabla g$ around C is positive, zero or negative. Justify your answer.
- Let C be the level curve defined by $g(x, y) = 110$. Determine whether the total outward flux of $\mathbf{G} = \nabla g$ through C is positive, zero or negative. Justify your answer.
- Evaluate** $\int_{C_1} \nabla g \cdot d\mathbf{r}$, where C_1 is the straight line path from $(x, y) = (21, 12)$ to $(x, y) = (9, 20)$.

SOLUTION:

(a) $g_y \approx \frac{\Delta g}{\Delta y}$

There are multiple acceptable answers, as long as you justify your reasoning.

Option 1: Using a forward difference at the point $(9, 16)$:

$$g_y(9, 16) \approx \frac{g(9, 20) - g(9, 16)}{20 - 16} = \frac{70 - 80}{4} = -\frac{5}{2}$$

Option 2: Based on the level curves shown we can approximate $g(9, 12) \approx 85$ (or any other number between 85 and 90) and use a centered difference:

$$g_y(9, 16) \approx \frac{g(9, 20) - g(9, 12)}{20 - 12} = \frac{70 - 85}{8} = -\frac{15}{8}$$

(b)

$$D_{\mathbf{u}}g = \frac{dg}{ds} = \nabla g(9, 16) \cdot \mathbf{u} \text{ where } \mathbf{u} = \frac{-3\mathbf{i} + 4\mathbf{j}}{\sqrt{3^2 + 4^2}} = -\frac{3}{5}\mathbf{i} + \frac{4}{5}\mathbf{j}$$

There are multiple acceptable ways to approximate this, as long as you justify your reasoning.

Option 1: Approximate $\nabla g(9, 16)$ using forward differences:

From part (a) we have $g_y \approx -\frac{5}{2}$

Using a forward difference at the point $(9, 16)$:

$$g_x(9, 16) \approx \frac{g(12, 16) - g(9, 16)}{12 - 9} = \frac{90 - 80}{3} = \frac{10}{3}$$

Thus using forward differences, $\nabla g(9, 16) \approx \langle \frac{10}{3}, -\frac{5}{2} \rangle$

Thus

$$D_{\mathbf{u}}g = \nabla g(9, 16) \cdot \mathbf{u} \approx \langle \frac{10}{3}, -\frac{5}{2} \rangle \cdot \langle -\frac{3}{5}, \frac{4}{5} \rangle = -2 - 2 = -4$$

Option 2: Approximate $\frac{dg}{ds}$ in the direction \mathbf{u} directly on the level curve plot using forward differences. Starting at the point $(9, 16)$ and moving in the direction $\langle -3, 4 \rangle$ (i.e. a distance of 5 diagonally across one of the boxes) we see:

$$\frac{dg}{ds} \approx \frac{\Delta g}{\Delta s} = \frac{g(6, 20) - g(9, 16)}{5} = \frac{50 - 80}{5} = -6$$

Note that a more accurate forward approximation would use just the closest level curve in the direction $\langle -3, 4 \rangle$, i.e.:

$$\frac{dg}{ds} \approx \frac{\Delta g}{\Delta s} = \frac{70 - 80}{2} = -5$$

Other approximations (including centered differences of the above calculations) are also acceptable as long as you show work justifying your steps.

(c) Let

$$f(x, y, z) = g(x, y) - z$$

The surface $z = g(x, y)$ is one level surface of $f(x, y, z)$, thus ∇f is normal to this surface.

$$\nabla f(x, y, z) = \langle g_x(x, y), g_y(x, y), -1 \rangle$$

Thus

$$\mathbf{n} = \frac{\nabla f(9, 16, 80)}{\|\nabla f(9, 16, 80)\|}$$

is normal to the graph of the surface at the point $(9, 16, 80)$.

Using our estimates from part (a) and (b):

$$\nabla f(9, 16, 80) = \langle g_x(9, 16), g_y(9, 16), -1 \rangle \approx \langle \frac{10}{3}, -\frac{5}{2}, -1 \rangle$$

Thus

$$\mathbf{n} \approx \frac{\langle \frac{10}{3}, -\frac{5}{2}, -1 \rangle}{\sqrt{(10/3)^2 + (-5/2)^2 + 1}}$$

(d) Yes, there is a critical point when $g(x, y) = 113$

(e) Since ∇g is a conservative field, the work done around any closed curve is zero. Since $g(x, y) = 110$ is a closed curve, the work done is zero.

(f) The total flux is $\oint_C \nabla g \cdot \mathbf{n} ds$ where \mathbf{n} is the outward pointing unit normal. Since ∇g points in the direction of greatest increase, for this function it points inward to the level curves and thus $\mathbf{n} = -\frac{\nabla g}{\|\nabla g\|}$ is the outward unit normal to the level curve $g(x, y) = 110$. Thus the total flux is

$$\oint_C \nabla g \cdot \mathbf{n} ds = \oint_C \nabla g \cdot \left(\frac{-\nabla g}{\|\nabla g\|} \right) ds = - \oint_C \|\nabla g\| ds < 0$$

(g) We can use the Fundamental Theorem of Line Integrals:

$$\int_C \nabla g \cdot d\mathbf{r} = g(9, 20) - g(21, 12) = 70 - 110 = \boxed{-40}$$

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Problem 2 (30 points)

The following questions are not related:

(a) Given

$$\mathbf{F} = z \mathbf{i} + x \mathbf{j} - 3e^{y^2} \arctan(z^2) \mathbf{k}$$

Find the outward flux through the surface that consists of the part of the cylinder $x^2 + y^2 = 16$ that lies in the **first octant** between $z = 0$ and $z = 5$. (By outward we mean oriented away from the z -axis. Note that this surface is not closed).

(b) Evaluate

$$\int_C (2x \cos y + 3) dx - (x^2 \sin y + 2y) dy$$

where C is the path $\mathbf{r}(t) = \cos^3 t \mathbf{i} + \sin^3 t \mathbf{j}$, $0 \leq t \leq \pi/2$.

SOLUTION:

(a) We need to compute $\iint_S \mathbf{F} \cdot \mathbf{n} dS$, a standard vector surface (flux) integral.

$$g(x, y, z) = x^2 + y^2 \implies \nabla g = \langle 2x, 2y, 0 \rangle \quad (\text{use positive gradient for outward normal})$$

$$\mathbf{F} \cdot \nabla g = \langle z, x, -3e^{y^2} \arctan(z^2) \rangle \cdot \langle 2x, 2y, 0 \rangle = 2x(y + z)$$

project onto the yz -plane $\implies \mathbf{p} = \mathbf{i}$, $|\nabla g \cdot \mathbf{p}| = |2x| = 2x$ since $x > 0$ and

$$\mathcal{R} = \left\{ (x, y, z) \in \mathbb{R}^3 \mid x = 0, 0 \leq y \leq 4, 0 \leq z \leq 5 \right\}$$

$$\iint_S \mathbf{F} \cdot \mathbf{n} dS = \iint_{\mathcal{R}} \mathbf{F} \cdot \frac{\nabla g}{|\nabla g \cdot \mathbf{p}|} dA = \boxed{\int_0^5 \int_0^4 (y + z) dy dz = 90}$$

Note: Projecting onto the xz -plane results in an integrand of $\frac{x(y+z)}{y}$ which, using the surface to eliminate y , gives

$$\boxed{\int_0^5 \int_0^4 \left(\frac{xz}{\sqrt{16-x^2}} + x \right) dx dz = 90}$$

(b) Direct integration is not possible as the integrand will contain terms like $\cos(\sin^3 t)$. Noting that the integral can be written alternatively as $\int_C \mathbf{F} \cdot d\mathbf{r}$ with $\mathbf{F} = \langle 2x \cos y + 3, -x^2 \sin y - 2y \rangle = \langle P, Q \rangle$, we check to see if \mathbf{F} is conservative.

$$\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} = -2x \sin y - (-2x \sin y) = 0$$

Since \mathbf{F} is defined throughout \mathbb{R}^2 , which is simply connected, and $\nabla \times \mathbf{F} = \mathbf{0}$, \mathbf{F} is conservative. This means that the integral is path independent and also that a potential function, f , exists such that $\mathbf{F} = \nabla f$. This provides two options:

Option 1 - find the potential and use the Fundamental Theorem for Line Integrals

$$\frac{\partial f}{\partial x} = 2x \cos y + 3 \implies f(x, y) = x^2 \cos y + 3x + g(y)$$

$$\frac{\partial f}{\partial y} = -x^2 \sin y + g'(y) = -x \sin y - 2y \implies g'(y) = -2y \implies g(y) = -y^2 + c$$

$$f(x, y) = x^2 \cos y + 3x - y^2 + c$$

Then we have

$$\int_C (2x \cos y + 3) dx - (x^2 \sin y + 2y) dy = \int_C \mathbf{F} \cdot d\mathbf{r} = \int_C \nabla f \cdot d\mathbf{r}$$

$$\boxed{= f(0, 1) - f(1, 0) = (-1 + c) - (4 + c) = -5}$$

Option 2 - integrate along another path

To avoid more complex integrations which would occur if using the line segment between $(1, 0)$ and $(0, 1)$, we choose the path $(1, 0) \rightarrow (0, 0) \rightarrow (0, 1)$ consisting of two line segments. For the part along the x -axis we have $x = 1 - t, y = 0, 0 \leq t \leq 1$ with $dx = -dt$ and $dy = 0$ and for the part along the y -axis we use $x = 0, y = t, 0 \leq t \leq 1$ with $dx = 0$ and $dy = dt$. Then

$$\int_C (2x \cos y + 3) dx - (x^2 \sin y + 2y) dy = \int_0^1 [2(1-t) + 3] (-dt) + \int_0^1 -2t dt$$

$$= \int_0^1 (-5 + 2t) dt + \int_0^1 -2t dt = \int_0^1 -5 dt = -5$$

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Problem 3 (25 points)

A metal plate lies in the xy -plane in the region $0 \leq x \leq 4 - y^2$

(i.e the region in quadrants I and IV bounded by the y -axis and the curve $x = 4 - y^2$).

- (a) Sketch and shade the region where the plate lies. Label any intercepts.
- (b) Find the work done by

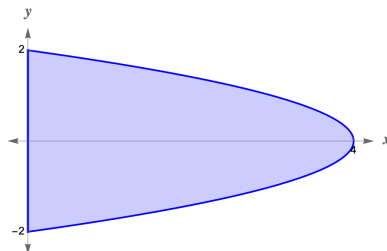
$$\mathbf{G} = \left\langle yx^2 - 3y + e^{\cos(x)}, \quad \frac{x^3}{3} - \arctan y \right\rangle$$

counterclockwise once around the boundary of the plate.

- (c) Let the temperature at any point on the plate be given by $T(x, y) = y^2 + x^2 - x$. Find the location(s) of the hottest and coldest points on the plate. Show work fully justifying your answer.

SOLUTION:

- (a) The region looks like this:



- (b) The boundary curve C of the region is piecewise smooth and closed, and the vector field \mathbf{G} has continuous first partial derivatives, so we should use Green's Theorem. With $\mathbf{G} = \langle P(x, y), Q(x, y) \rangle$,

$$\begin{aligned}
 \oint_C \mathbf{G} \cdot d\mathbf{r} &= \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA \\
 &= \iint_R [x^2 - (x^2 - 3)] dA \\
 &= \iint_R 3 dA \\
 &= 3 \int_{-2}^2 \int_0^{4-y^2} 1 dx dy \\
 &= 3 \int_{-2}^2 [x]_0^{4-y^2} dy \\
 &= 3 \int_{-2}^2 (4 - y^2) dy \\
 &= 3 \left[4y - \frac{y^3}{3} \right]_{-2}^2 \\
 &= 3 \left\{ \left[4(2) - \frac{(2)^3}{3} \right] - \left[4(-2) - \frac{(-2)^3}{3} \right] \right\} \\
 &= 3 \left[\left(8 - \frac{8}{3} \right) - \left(-8 + \frac{8}{3} \right) \right] \\
 &= 24 - 8 + 24 - 8 \\
 &= \boxed{32}
 \end{aligned}$$

- (c) By the Extreme Value Theorem there must exist absolute max and min temperatures on the plate. We have to optimize the temperature function $T(x, y) = y^2 + x^2 - x$ inside the plate and on the boundary of the plate.

For full credit you must find all possible max/min on the interior and boundary, and compare the temperatures at each point to find the absolute max and min.

To optimize $T(x, y)$ on the inside of the plate, note that $\nabla T(x, y) = \langle 2x - 1, 2y \rangle$, which equals $\langle 0, 0 \rangle$ when

$$2x - 1 = 0 \implies x = \frac{1}{2} \quad \text{and} \quad 2y = 0 \implies y = 0$$

Since $\nabla T(x, y)$ always exists (T is a polynomial in two variables), $(\frac{1}{2}, 0)$ is the only critical point of $T(x, y)$, which is in the interior of the metal plate. We will evaluate $T(x, y)$ at this point after we have found all points of interest.

To optimize $T(x, y)$ on the boundary of the plate, we break the curve C into two pieces, say C_1 is the line segment on the y -axis given by $x = 0$ and $-2 \leq y \leq 2$, and C_2 is the curve $x = 4 - y^2$ for $-2 \leq y \leq 2$.

On C_1 , since $x = 0$ we study the function $T_1(y) = T(0, y) = y^2$ on the interval $[-2, 2]$. Since $T_1'(y) = 2y$ which equals zero when $y = 0$, we have three points of interest (when $y = 0$ and including the endpoints $y = \pm 2$) to consider later:

$$(0, 0) \quad (0, 2) \quad (0, -2)$$

To optimize $T(x, y)$ on the curve C_2 there are two methods we could use:

Method 1: just like on C_1 , since $x = 4 - y^2$ on C_2 we study the function

$$T_2(y) = T(4 - y^2, y) = y^2 + (4 - y^2)^2 - (4 - y^2) = y^2 + 16 - 8y^2 + y^4 - 4 + y^2 = y^4 - 6y^2 + 12$$

for $-2 \leq y \leq 2$.

But

$$T_2'(y) = 4y^3 - 12y = 4y(y^2 - 3)$$

which equals zero when $y = 0, \pm\sqrt{3}$. This gives us three more points of interest to consider:

$$(4, 0) \quad (1, \sqrt{3}) \quad (1, -\sqrt{3})$$

(note that the 'endpoint' $y = \pm 2$ are the same as on C_1)

Method 2: we could use Lagrange multipliers. Let $g(x, y) = x + y^2$. Then the curve C_2 is the level curve $g(x, y) = 4$. We want to solve the system

$$\nabla T(x, y) = \lambda \nabla g(x, y) \quad \text{and} \quad g(x, y) = 4$$

or

$$\langle 2x - 1, 2y \rangle = \lambda \langle 1, 2y \rangle \quad \text{and} \quad x = 4 - y^2$$

or

$$\begin{aligned} 2x - 1 &= \lambda \\ 2y &= 2\lambda y \\ x &= 4 - y^2 \end{aligned}$$

The second equation tells us that

$$2y - 2\lambda y = 0 \quad \text{or} \quad 2y(1 - \lambda) = 0,$$

so either $y = 0$ or $\lambda = 1$. If $y = 0$, the third equation gives $x = 4$, so $(4, 0)$ is a point of interest.

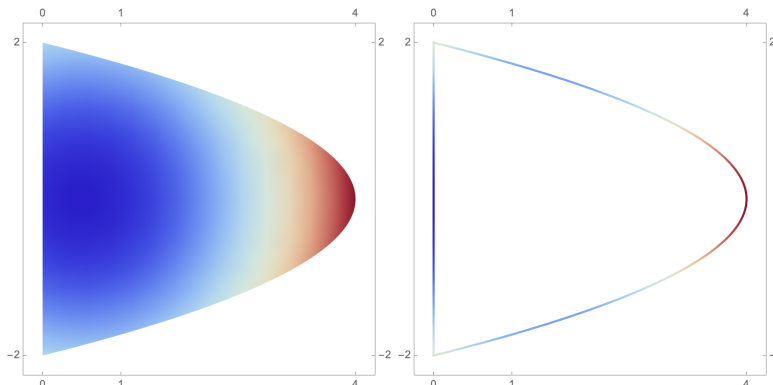
If $\lambda = 1$, then the first equation says that $2x - 1 = 1$ or $x = 1$. The third equation then gives $y = \pm\sqrt{3}$. We get the two points of interest $(1, \pm\sqrt{3})$.

To finish the problem, we evaluate $T(x, y)$ at all of the points of interest:

$$\begin{aligned} T\left(\frac{1}{2}, 0\right) &= -\frac{1}{4} \\ T(0, 0) &= 0 \\ T(0, -2) &= 4 \\ T(0, 2) &= 4 \\ T(4, 0) &= 12 \\ T(1, \sqrt{3}) &= 3 \\ T(1, -\sqrt{3}) &= 3 \end{aligned}$$

The hottest point on the plate is therefore $(4, 0)$ and the coldest point is $(\frac{1}{2}, 0)$.

For fun, this is what the temperature distribution on the inside and on the boundary of the plate looks like:



Problem 4 (35 points)

The integral

$$\int_0^{2\sqrt{2}} \int_{-\sqrt{8-y^2}}^{\sqrt{8-y^2}} \int_{\sqrt{x^2+y^2}}^{\sqrt{16-x^2-y^2}} dz dx dy$$

represents the volume of a 3D region, \mathcal{E} .

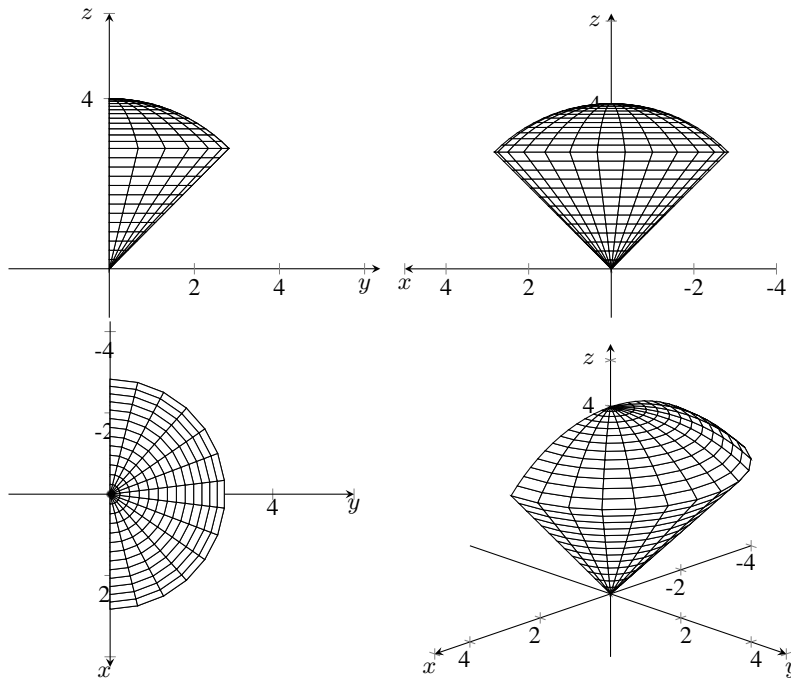
- Sketch and shade a 2D cross section of the object in the rz -plane. Label the (r, z) coordinates on all corners of the cross section.
- Sketch and shade the projection of the object onto the xy -plane. Label any intercepts.
- Set up but DO NOT EVALUATE, equivalent integral(s) to find the volume of the object using:
 - Cylindrical coordinates in the order $dz dr d\theta$
 - Spherical coordinates in the order $d\rho d\phi d\theta$
- Calculate the total outward flux of

$$\mathbf{F} = (xz^2 + \tan(y^2z))\mathbf{i} + (yx^2 - xe^{\cos(z)})\mathbf{j} + (zy^2)\mathbf{k}$$

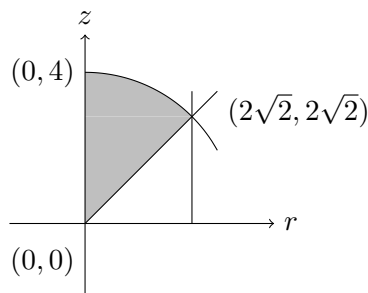
across the entire surface of \mathcal{E} .

SOLUTION:

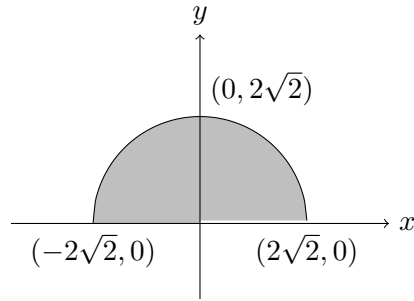
The surface looks like the figure below.



(a)



(b)



(c)

$$(i) \int_0^\pi \int_0^{2\sqrt{2}} \int_r^{\sqrt{16-r^2}} r dz dr d\theta$$

$$(ii) \int_0^\pi \int_0^{\frac{\pi}{4}} \int_0^4 \rho^2 \sin(\phi) d\rho d\phi d\theta$$

(d) Calculating

$$\begin{aligned} \int_V (\nabla \cdot \mathbf{F}) dV &= \int_V (z^2 + x^2 + y^2) dV = \int_0^\pi \int_0^{\frac{\pi}{4}} \int_0^4 (\rho^2) \rho^2 \sin(\phi) d\rho d\phi d\theta \\ &= \left(\int_0^\pi d\theta \right) \left(\int_0^{\frac{\pi}{4}} \sin(\phi) d\phi \right) \left(\int_0^4 \rho^4 d\rho \right) = \left(\theta \Big|_0^\pi \right) \left(-\cos(\phi) \Big|_0^{\frac{\pi}{4}} \right) \left(\frac{\rho^5}{5} \Big|_0^4 \right) \\ &= \pi \left(\cos(0) - \cos\left(\frac{\pi}{4}\right) \right) \frac{4^5}{5} = \pi \left(1 - \frac{\sqrt{2}}{2} \right) \frac{1024}{5}, \end{aligned}$$

by the Divergence Theorem, the outward flux is

$$\oiint \mathbf{F} \cdot \mathbf{n} dS = \int_V (\nabla \cdot \mathbf{F}) dV = \pi \left(1 - \frac{\sqrt{2}}{2} \right) \frac{1024}{5}.$$

Problem 5 (25 points)

Let \mathcal{C} be the path parameterized by

$$\mathbf{r}(t) = \langle 2 \cos t, 2 \sin t, 3 - \cos t \rangle, \quad 0 \leq t \leq 2\pi$$

(a) \mathcal{C} lies in a plane. Find the equation of that plane.

(b) Let

$$\mathbf{F}(x, y, z) = \langle e^{x^2} + 2z^2, \sinh(y^2), \cos(z^2) + zy \rangle$$

Find the circulation of $\mathbf{F}(x, y, z)$ around \mathcal{C} .

SOLUTION:

(a) To find the equation of the plane we need a point and a normal vector.

One possible point : $t = 0 \implies (x, y, z) = (2, 0, 2)$.

To find the normal vector:

Option 1: Find 3 points on the curve, create 2 vectors between them and find their cross product:

$$P_1: t = 0 \implies (x, y, z) = (2, 0, 2).$$

$$P_2: t = \pi/2 \implies (x, y, z) = (0, 2, 3).$$

$$P_3: t = \pi \implies (x, y, z) = (-2, 0, 4).$$

$$P_1 P_2 \times P_1 P_3 = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ -2 & 2 & 1 \\ -4 & 0 & 2 \end{vmatrix} = \langle 4, 0, 8 \rangle$$

Thus the plane is $4(x - 2) + 0(y - 0) + 8(z - 2) = 0$

$$\boxed{\implies x + 2z = 6}$$

Option 2:

The normal vector to the osculating plane (binormal vector of the curve) will point in the direction of $\mathbf{r}'(t) \times \mathbf{r}''(t)$:

$$\begin{aligned} & \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ -2 \sin(t) & 2 \cos(t) & \sin(t) \\ -2 \cos(t) & -2 \sin(t) & \cos(t) \end{vmatrix} \\ &= \langle 2 \cos^2(t) + 2 \sin^2(t), 2 \sin(t) \cos(t) - 2 \sin(t) \cos(t), 4 \sin^2(t) + 4 \cos^2(t) \rangle \\ &= \langle 2, 0, 4 \rangle \end{aligned}$$

Thus, the osculating plane to the curve C is constant i.e. C lies in a plane which has a normal vector that points in the direction of $\langle 2, 0, 4 \rangle$.

Thus the plane is $2(x - 2) + 0(y - 0) + 4(z - 2) = 0$

$$\boxed{\implies x + 2z = 6}$$

- (b) Note that integrating $\mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) dt$ would be impossible. We can start by checking to see if this vector field is conservative:

$$\nabla \times \mathbf{F} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ e^{x^2} + 2z^2 & \sinh(y^2) & \cos(z^2) + zy \end{vmatrix} = \langle z, 4z, 0 \rangle$$

Thus \mathbf{F} is not conservative.

However, since C is a closed curve, Stokes' theorem tells us that

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \int \int_S (\nabla \times \mathbf{F}) \cdot \hat{n} dS$$

If we model the plane by the equation $x + 2z = d$ it becomes a level surface of the function $g(x, y, z) = x + 2z$.

Thus $\nabla g(x, y, z) = \langle 1, 0, 2 \rangle$. Checking orientation, this follows the right-hand rule with the direction of C .

Projecting onto the xy -plane we get:

$$(\nabla \times \mathbf{F}) \cdot \hat{n} dS = \frac{(\nabla \times \mathbf{F}) \cdot \nabla g}{|\nabla g \cdot \hat{k}|} dA = \frac{\langle z, 4z, 0 \rangle \cdot \langle 1, 0, 2 \rangle}{2} dx dy = \frac{1}{2} z$$

Since on the plane $z = 3 - \frac{x}{2}$, we can convert the integrand to be in terms of xy :

$$\frac{1}{2} z = \frac{1}{2} \left(3 - \frac{x}{2} \right)$$

The region of integration on the xy -plane is given by the x and y coordinates of C . Since $x = 2 \cos t$ and $y = \sin t$, this traces out a circle of radius 2 centered at the origin in the xy -plane.

Thus,

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \int \int_S (\nabla \times \mathbf{F}) \cdot \hat{n} dS = \iint_R \left(\frac{3}{2} - \frac{x}{4} \right) dA$$

$$\begin{aligned} &= \int_0^{2\pi} \int_0^2 \left(\frac{3r}{2} - \frac{1}{4}r^2 \cos \theta \right) dr d\theta \\ &= \int_0^{2\pi} \left(3 - \frac{2}{3} \cos \theta \right) d\theta = 3(2\pi) - 0 = \boxed{6\pi} \end{aligned}$$

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End Of Exam
