



# STOUT

Spectropolarimeter  
Telescope  
Observatory for  
Ultraviolet  
Transmissions

Presenters:

1. Andrew Arnold
2. Caleb Beavers
3. Darin Brock
4. Matt Funk
5. Ian Geraghty
6. Andrew Lux
7. Dawson Stokely

Team Members:

1. Zach Allen
2. Joshua Bruski-Hyland
3. Ryan Lynch
4. Matthew Normile

Customer:

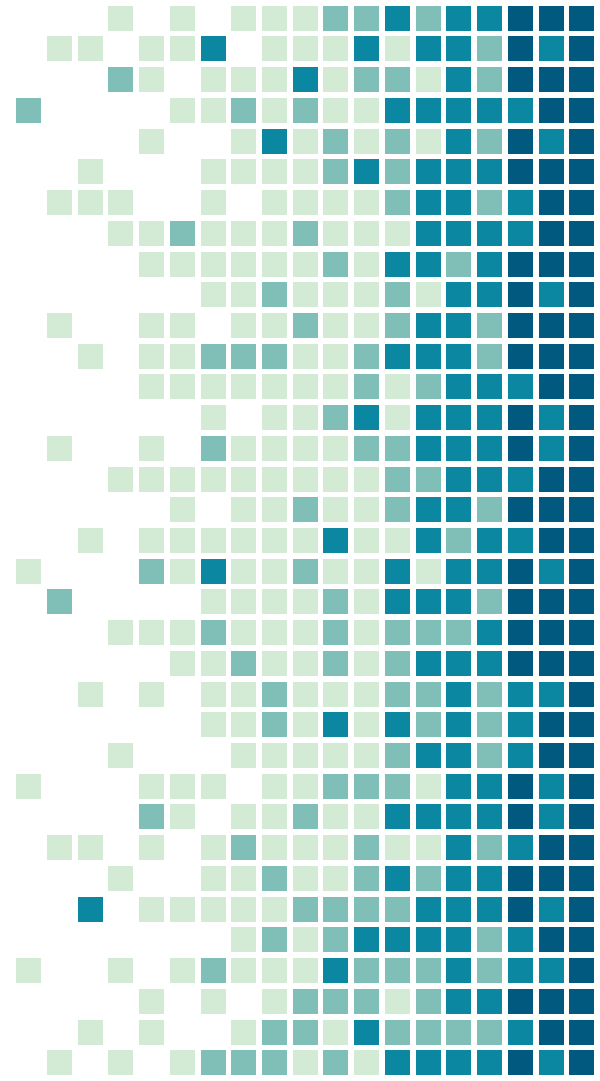
NCAR High Altitude  
Observatory

Advisor:

Francisco López Jiménez

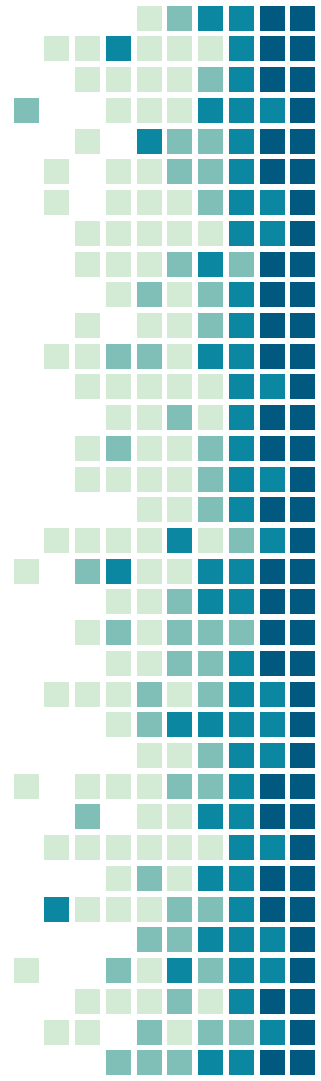
1. Phil Oakley
2. Scott Sewell

# Project Purpose / Objectives



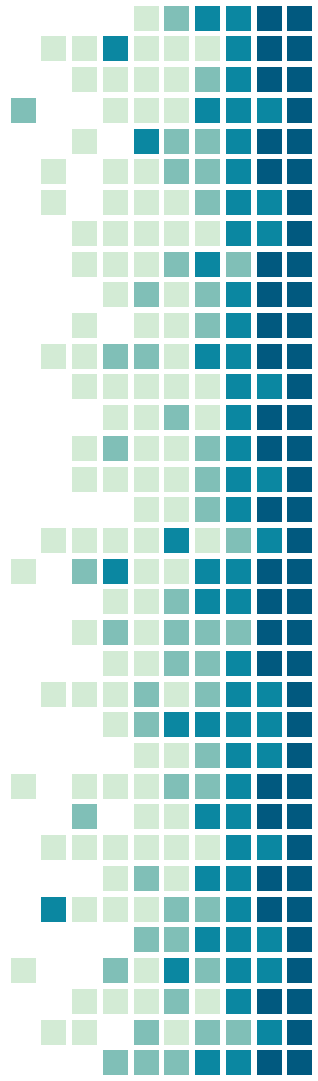
# Motivation

- Solar phenomena present catastrophic risks to ground and space based systems
- Models can be used to determine preconditions in the magnetic structure that lead to solar phenomena
- Solar photosphere and transition region (solar atmosphere) emit UV light
- UV light passes through the sun's magnetic field and is polarized to align with the field vector
- Measurements of UV spectra at varying polarization angles can be used to model solar magnetic field structure

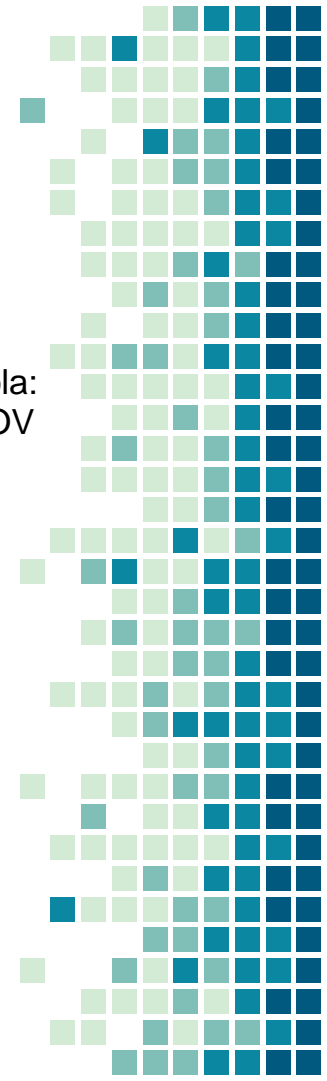
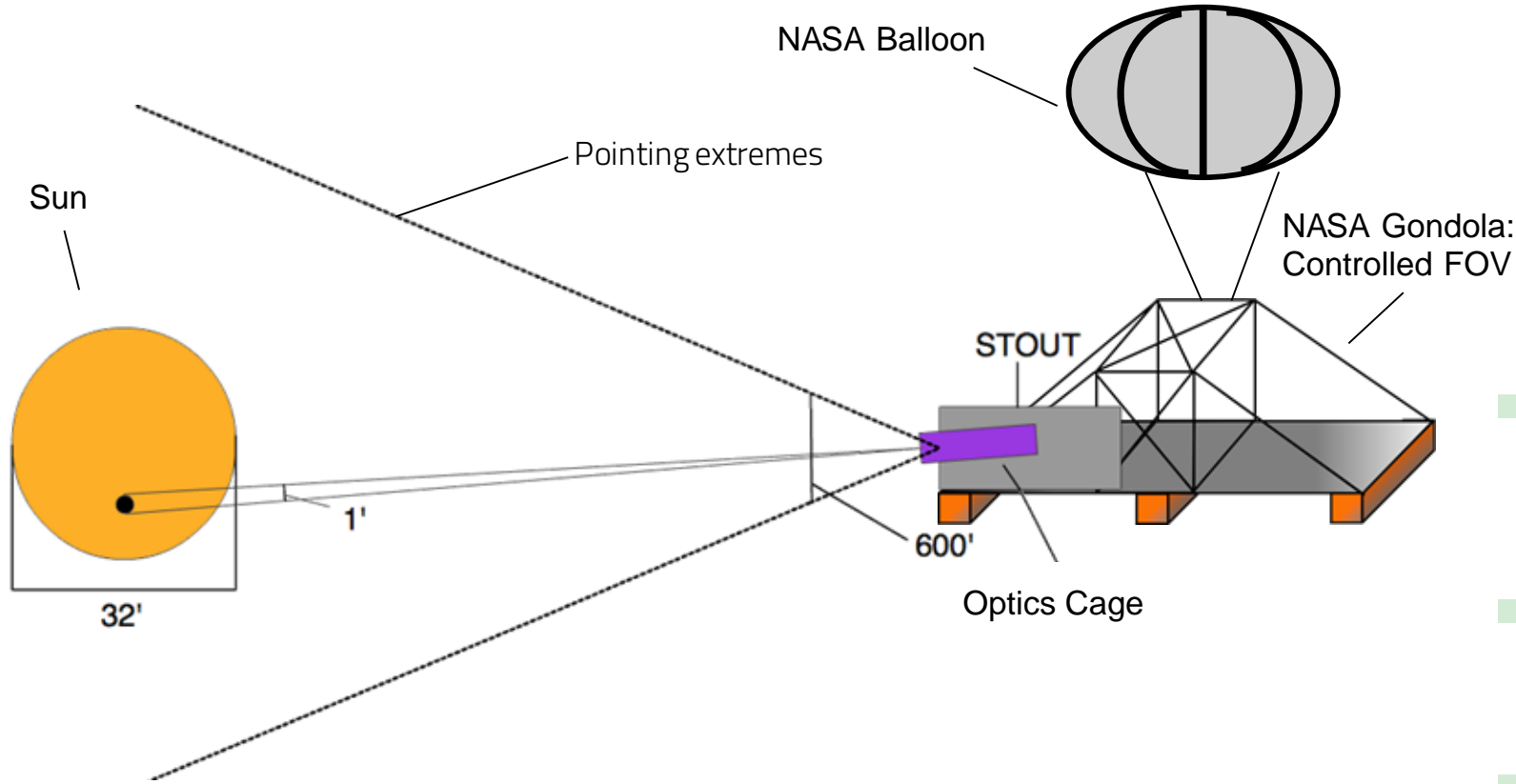


# Mission Statement

STOUT will design and manufacture a 3U CubeSat-style payload capable of high-altitude balloon flight, which integrates with last year's RADIANCE project. The module will scan the body of the sun to measure sunlight intensity as a function of position on the sun, polarization angle, and wavelength. Ambient atmospheric data, pointing attitude information, and images will be recorded as well. The team will utilize a variety of ground tests that simulate the expected high altitude environment in order to calibrate the module's data collection systems and verify the payload's flight readiness.



# Pointing Explanation



# NASA Gondola



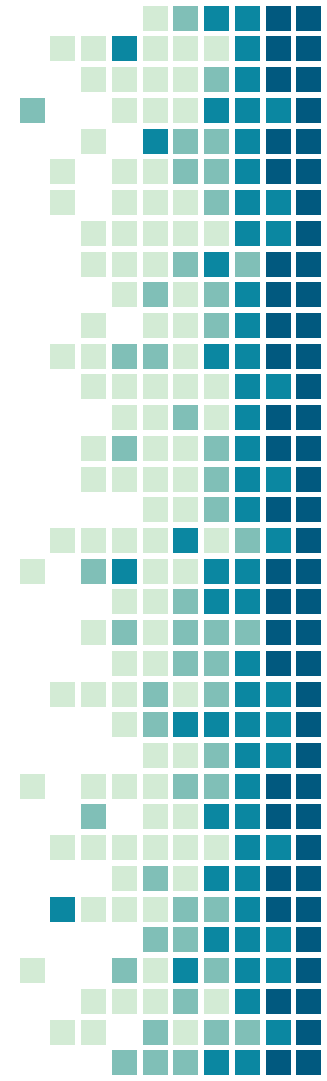
## Mission

- Ground: 8 Hours
  - Powered on and systems check
- Ascent: 2 hours
  - Launched from NM or Antarctica
- Flight: 2 weeks at 40 km
  - Gondola platform puts the system FOV within  $\pm 5^\circ$  of the Sun
  - Solar irradiance data collected
  - Polarized UV spectra collected
- Descent: 1 hr
  - Customer retrieves data

# Project Objectives

## **STOUT shall be capable of...**

1. Integrating with RADIANCE module and NASA high altitude balloon gondola
2. Enduring and collecting data during the conditions of a 40 km high-altitude balloon flight
3. Determining its attitude relative to the sun
4. Collecting variable polarization UV spectra at various points on the sun's surface
5. Capturing images of the sun in the visible spectrum
6. Surviving a descent under parachute and impacting with the ground so data is retrievable by customer



STOUT

RADIANCE

## Ascent

Power on and receive continuous power from NASA Gondola



## Float

Complete mission operations at 40 km for approximately 2 weeks. Gondola controlled to keep Sun in  $\pm 5^\circ$  FOV during daylight hours



## Descent

Power down, mission operation data storage survives 5g parachute landing, customer collect and analyze data



Mission Operations

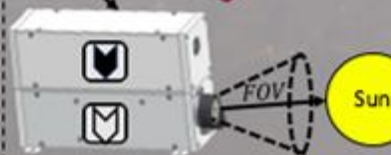
### Maintain Operational Internal Temperature

Monitor temperature and pressure, and control internal temperature



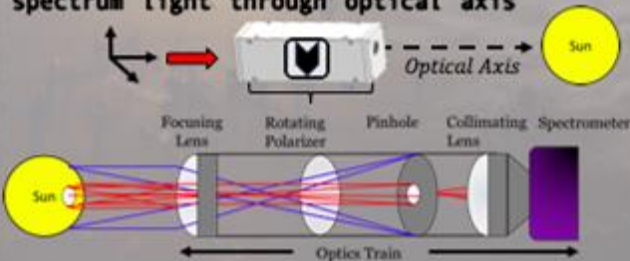
### Determine Sun-Off Angles

Using RADIANCE Sun Sensor, record and save sun-off angles within  $\pm 5^\circ$  dual axis Field of View



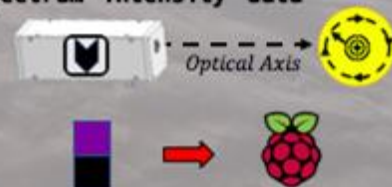
### Delimitate Light Spectrum Through Optics Train

Using STOUT optics train, obtain UV spectrum intensity data by passing whole spectrum light through optical axis



### Data Collection

Scan entirety of Sun, collecting and saving UV spectrum intensity data

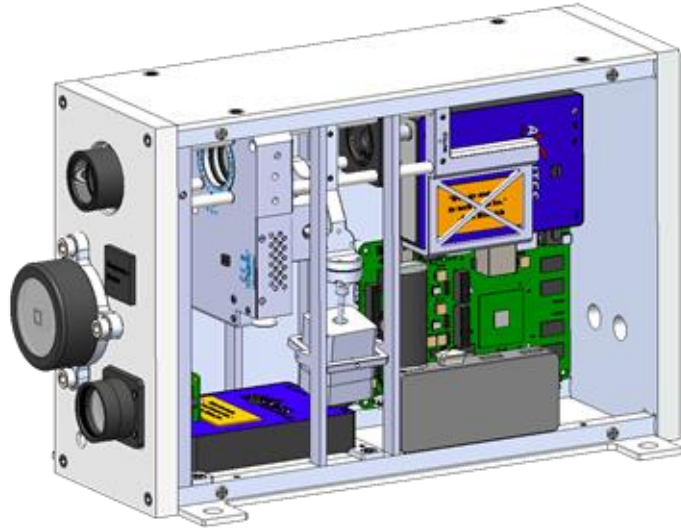




# Design Solutions



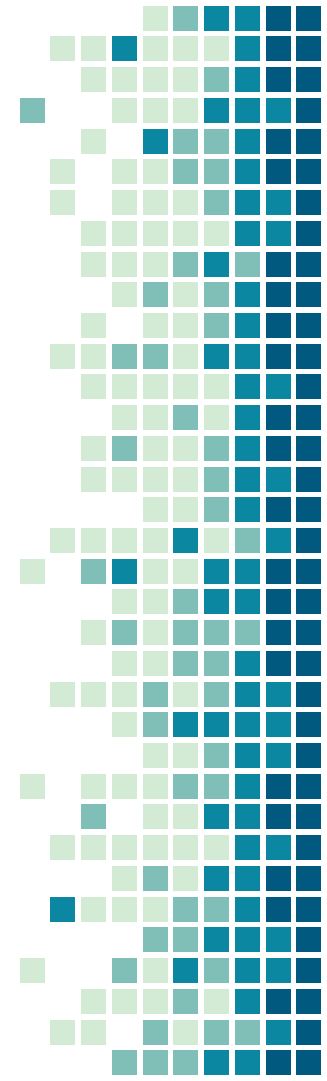
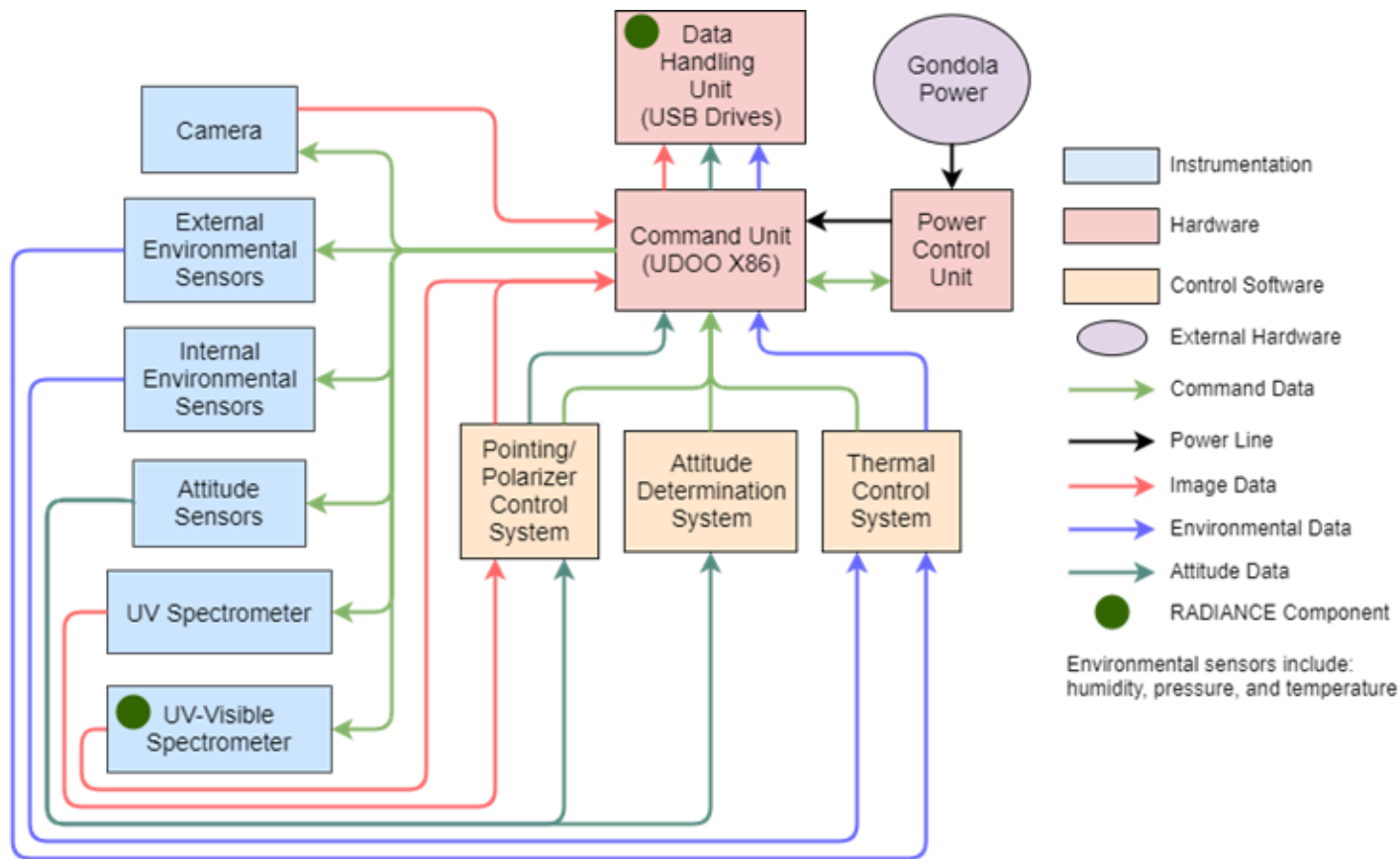
# System Overview



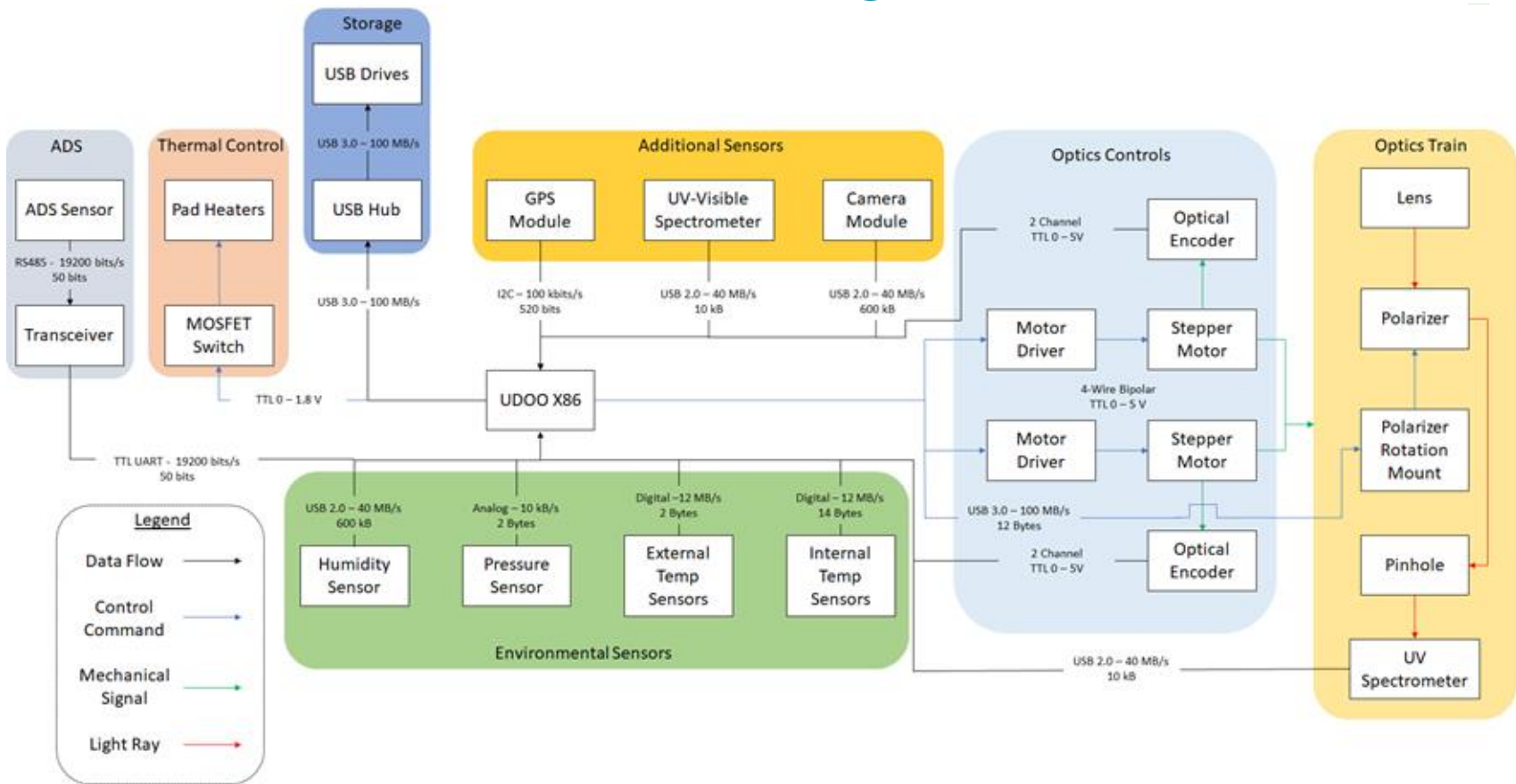
## Summary

| Parameter          | Values   |
|--------------------|--|
| Dimensions         | 10x20x30 cm  |
| Mass               | 4.4 kg   |
| Power Consumption  | 74.5 W   |
| Flight Environment | -70°C - 20°C   |
| Materials          | Aluminum 6061 (Structure)<br>Polyisocyanurate (Insulation) |

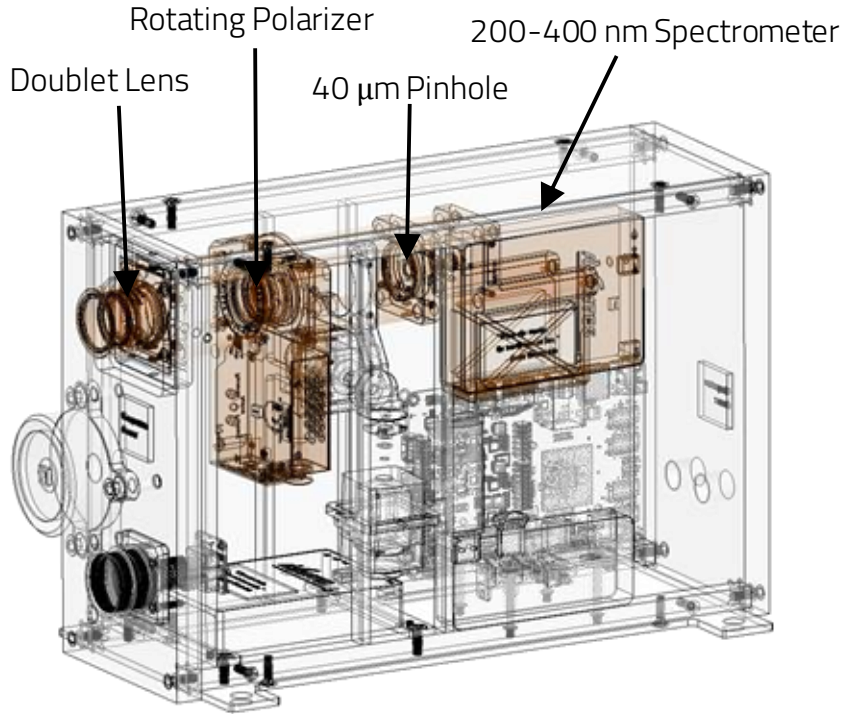
# Functional Block Diagram



# Hardware Architecture Diagram

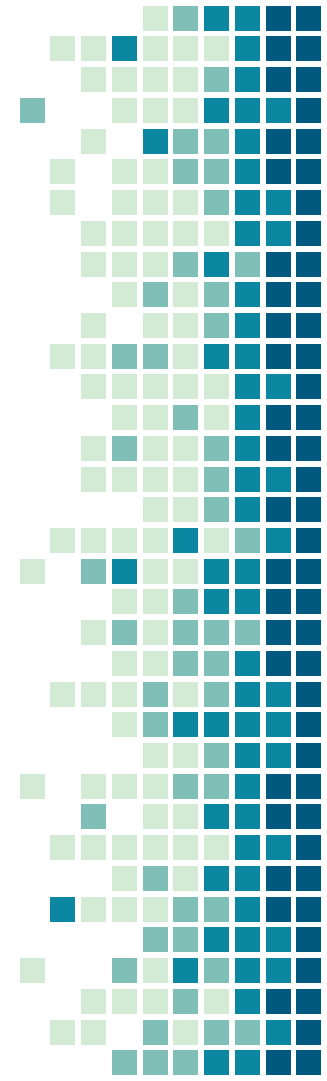


# Optics



## Components

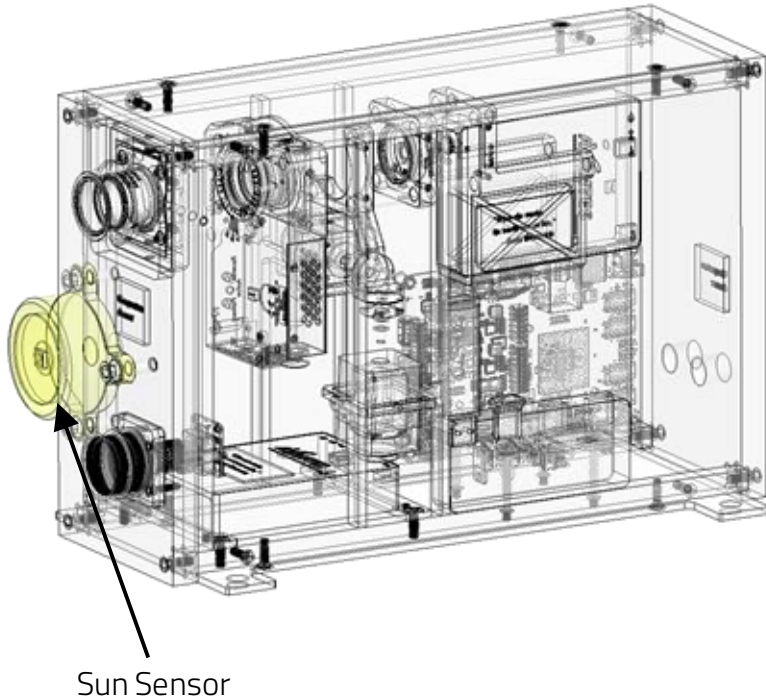
- Thorlabs UV Doublet Lens: Focus light in UV spectrum
- Thorlabs Mounted Wire Grid Polarizer: Control input light polarization angle
- Thorlabs Precision Pinhole: Isolate spot on Sun
- Avantes Collimating Lens: Feed light into spectrometer
- Avantes Spectrometer: Measure light intensity as function of wavelength
- Thorlabs Optics Cage: Mount and align optical components



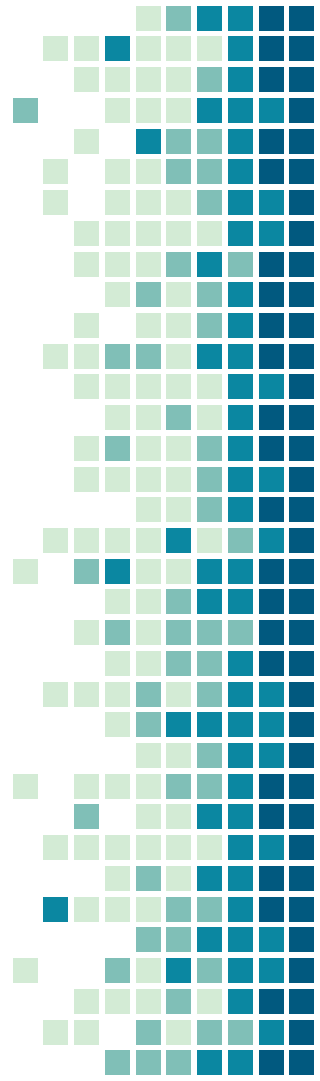
# Attitude Determination System

## Components

- Solar Mems Sun Sensor: Determines Sun's position in the system's FOV
- Quadrant photodetector used to measure off-sun angles from generated photocurrents



Sun Sensor

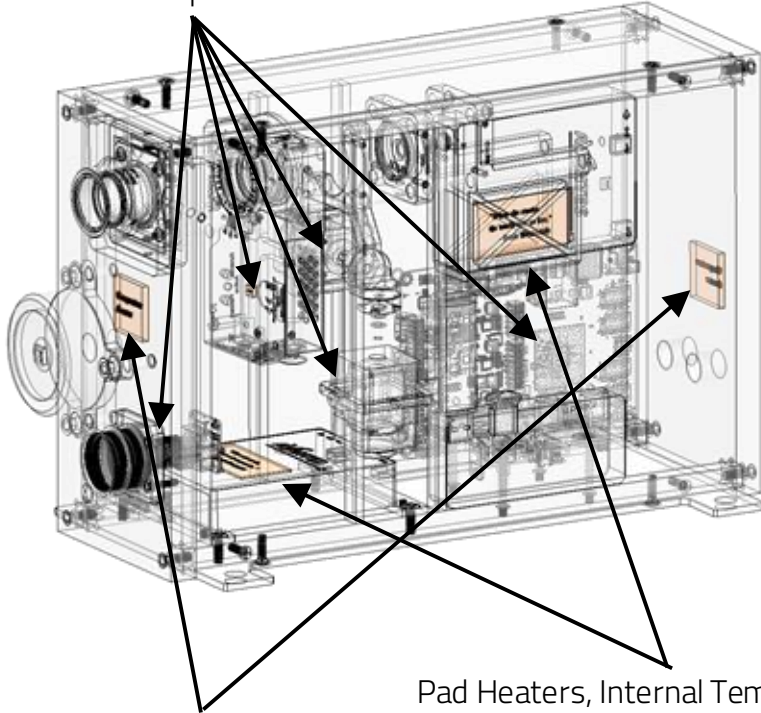


# Environmental Monitoring & Control System

## Components

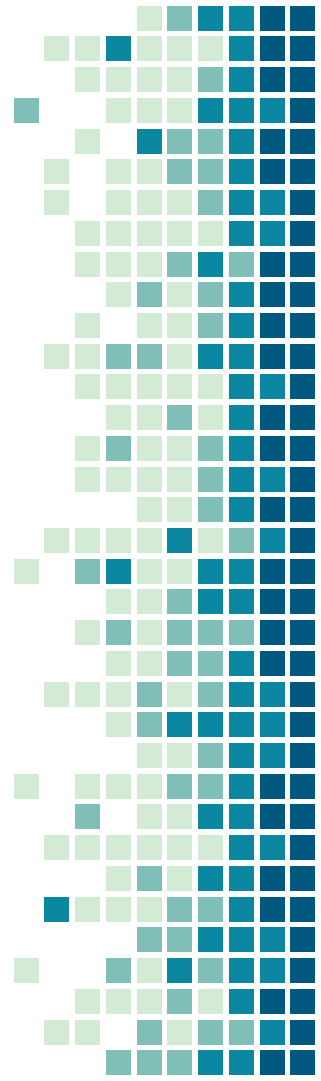
- 7 Internal Temperature Sensors: Measure internal temperature
- 2 External Temperature Sensors: Measure External Temperature
- 1 Pressure Sensor: Measure external pressure
- 3 Resistive Pads: Keep module at an operable temperature

Internal Temperature Sensors

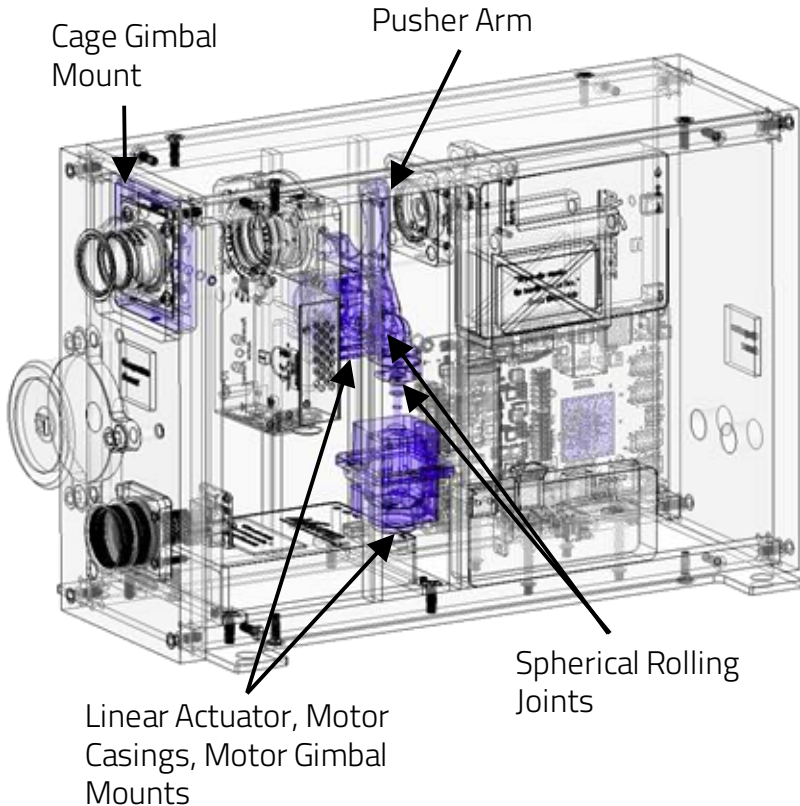


Pad Heaters, Internal Temperature Sensors

External Temperature Sensors

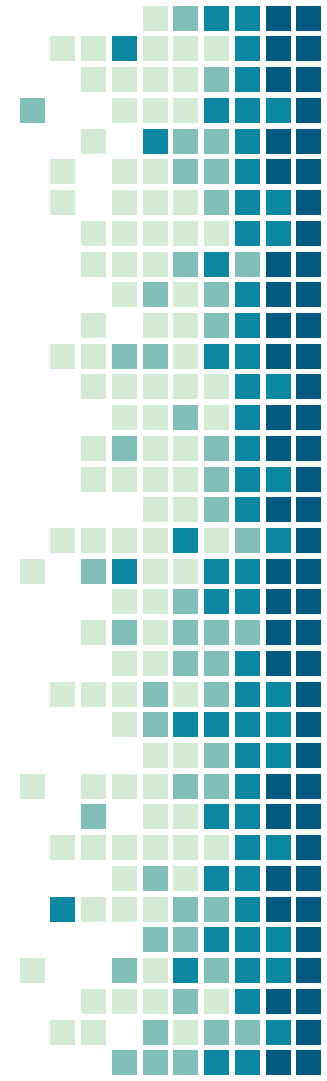


# Pointing Controls



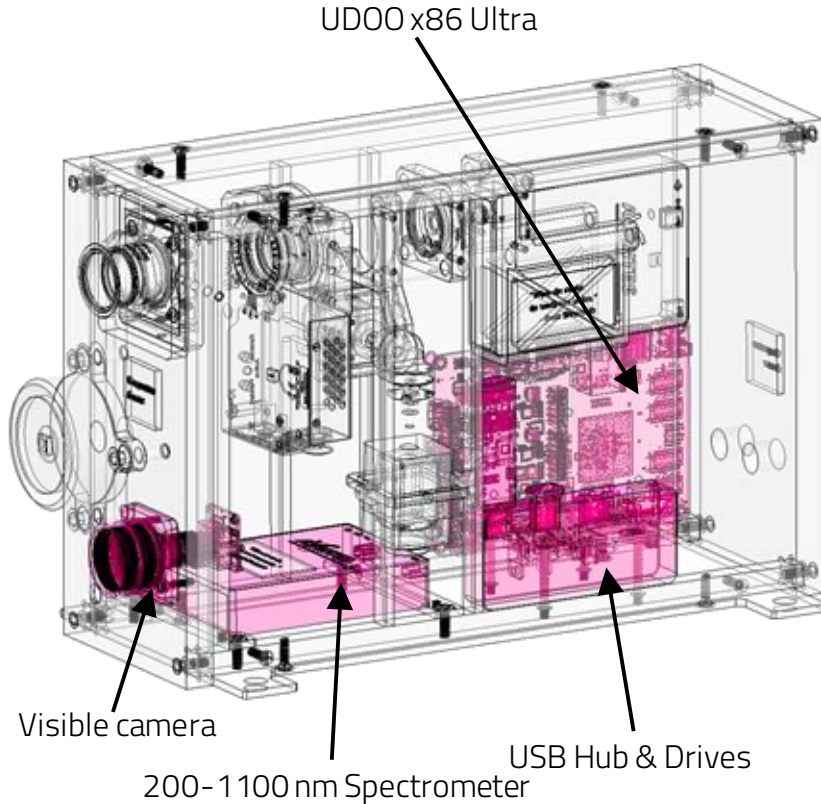
## Components

- Custom Cage System Gimbal Mount
- 2 Haydon Kerk Pittman Hybrid Stepper Motor Non Captive Linear Actuator
- Custom Motor Casings
- Custom Motor Gimbal Mounts
- Custom Cage System Pusher Arm
- Hephaist Spherical Rolling Joints



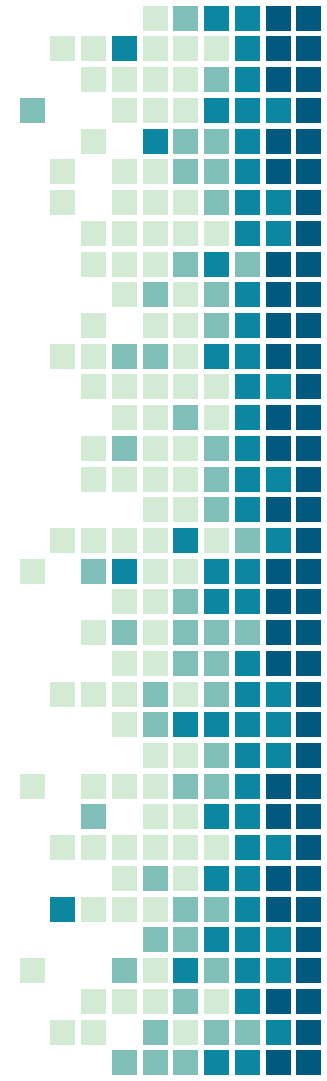


# CPU and Data Acquisition

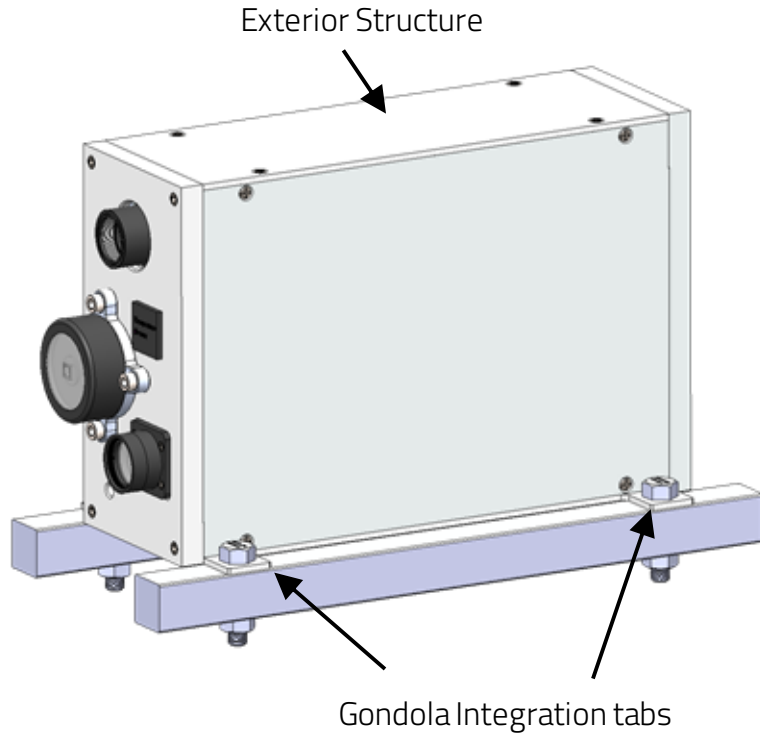


## Components

- UDOO x86 Ultra
  - 2.56 GHz Quad Core processor for control computation
  - Intel Curie Microcontroller for motor control
  - USB 3.0 for fast write rates
- USB Thumbdrives for data storage
  - One MX-ES Ultra 64 GB
  - One Samsung Fit 64 GB
- Sabrent 4 Port USB 3.0 Externally Powered Hub
- RADIANCE Spectrometer
- 2 MP Visible Camera

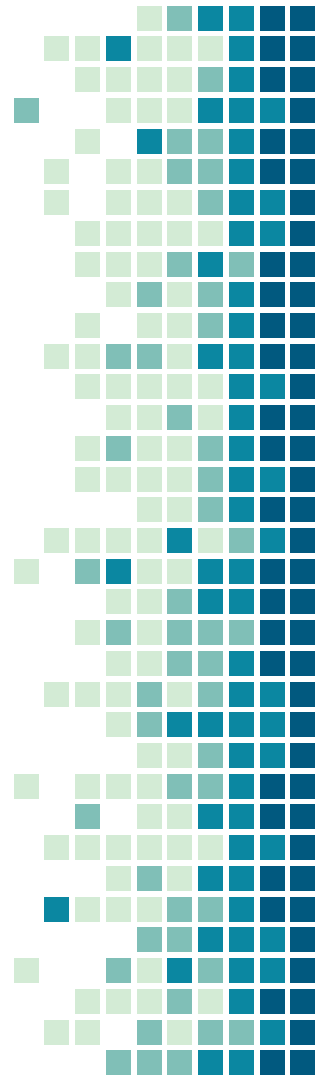


# Structure

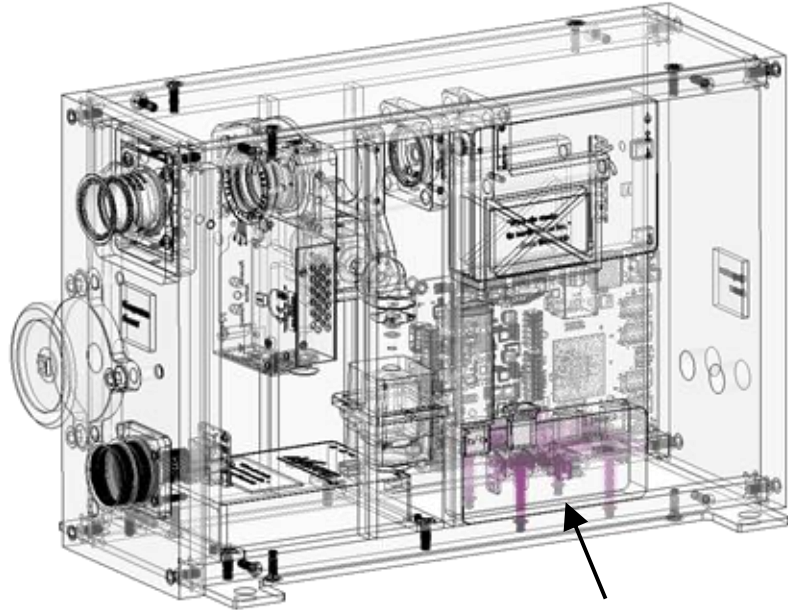


## Components

- Aluminum 6061: Exterior plates and interior struts
- Tabs attach to balloon gondola



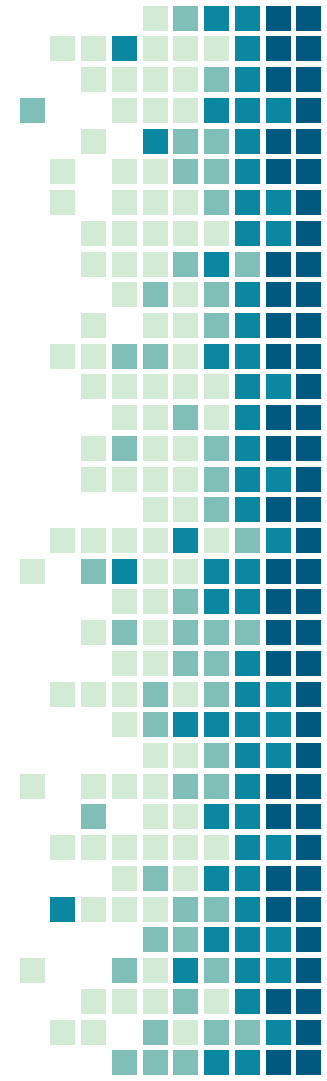
# Electrical Power System



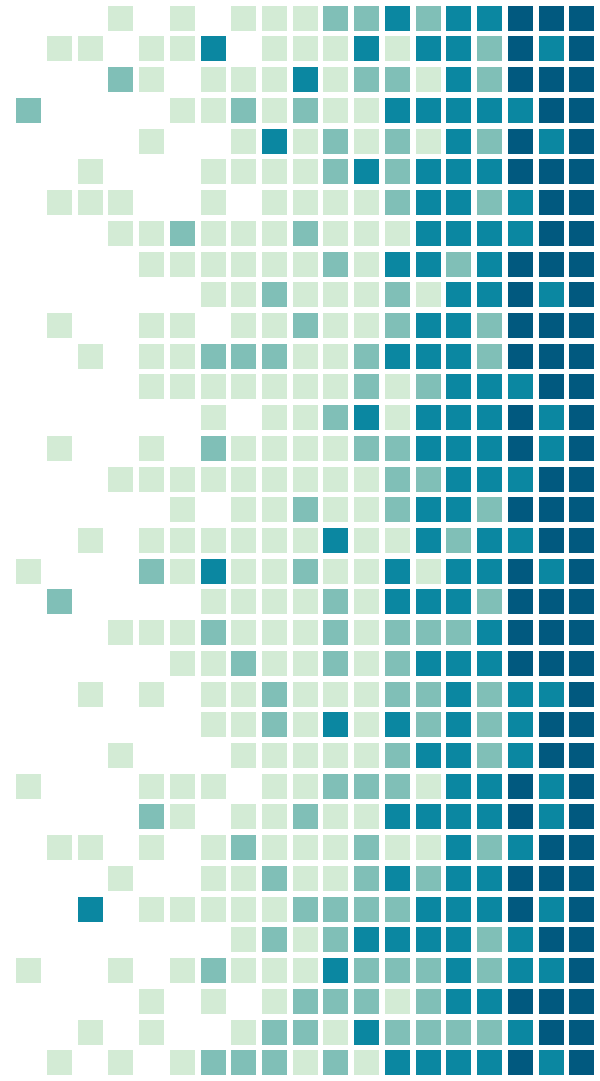
Printed Circuit Board

## Components

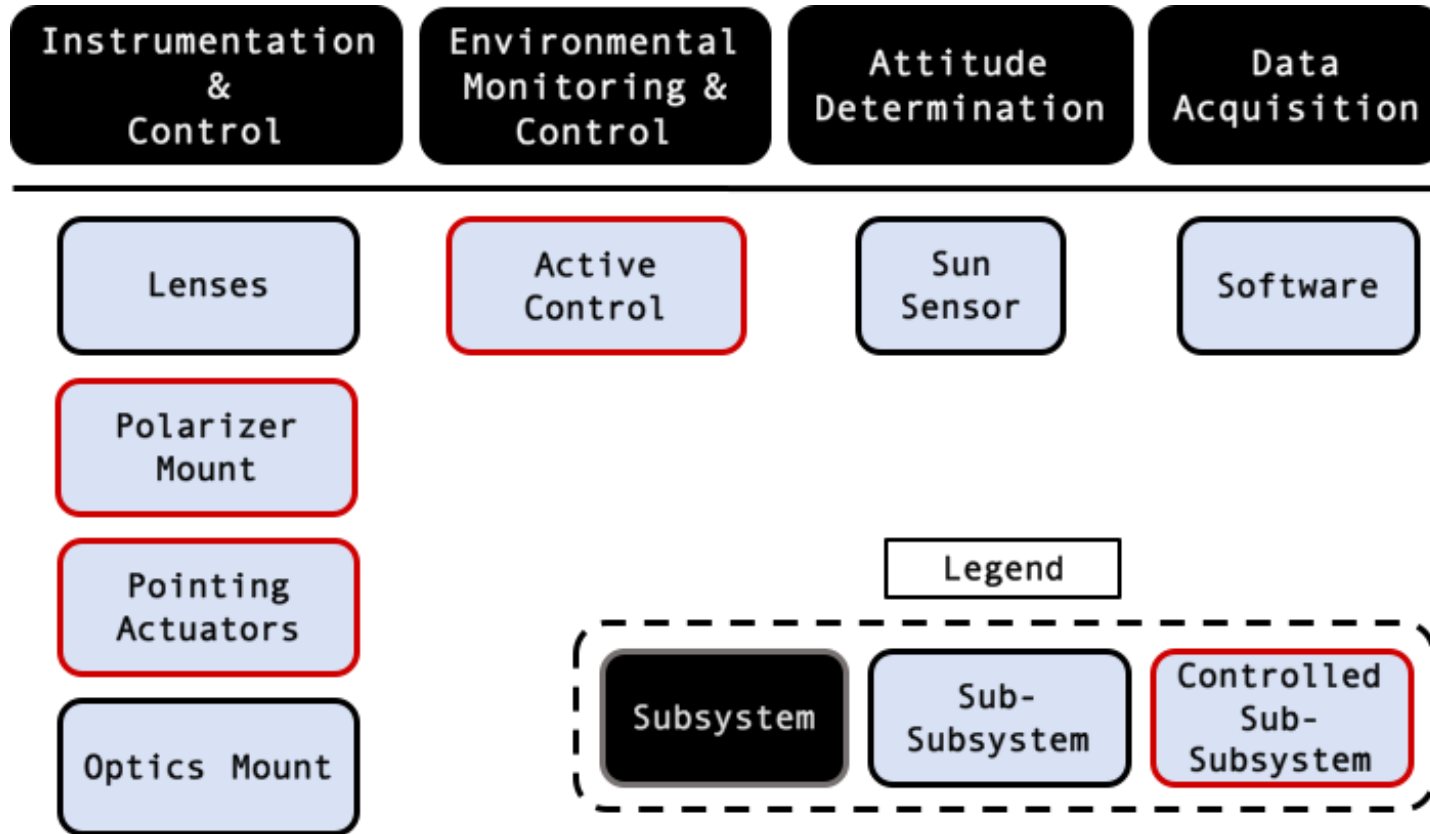
- Custom PCB to distribute power to subsystems



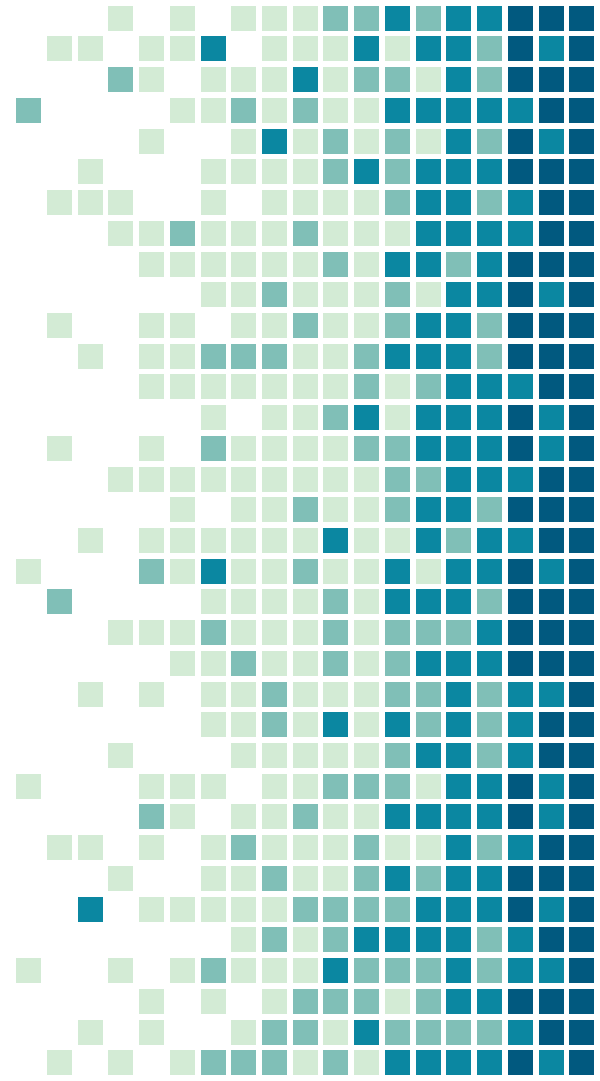
# Critical Project Elements



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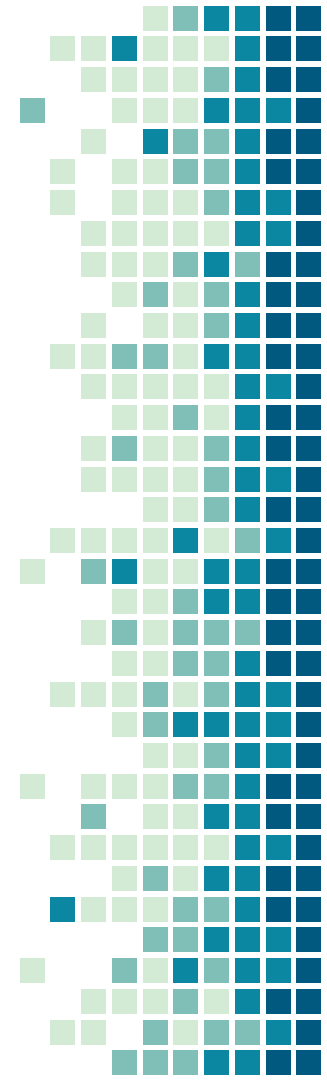


# Design Requirements and Their Satisfaction



# Functional Requirements

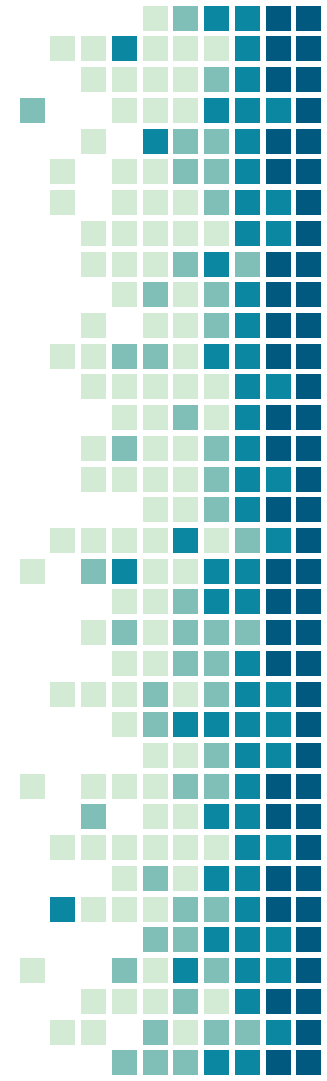
- **FR 1:** The system shall integrate with RADIANCE module
- **FR 2:** The system shall take variable polarized UV spectrum measurements at various points on the sun's surface
- **FR 3:** The system shall determine its attitude
- **FR 4:** The system shall take environmental measurements
- **FR 5:** The system shall survive the environmental conditions of a high altitude balloon flight to 40 km
- **FR 6:** The system shall record data
- **FR 7:** The system shall interface with the NASA balloon gondola



# EMCS Requirements

**FR5: The system shall survive the conditions of a high altitude balloon flight up to 40km**

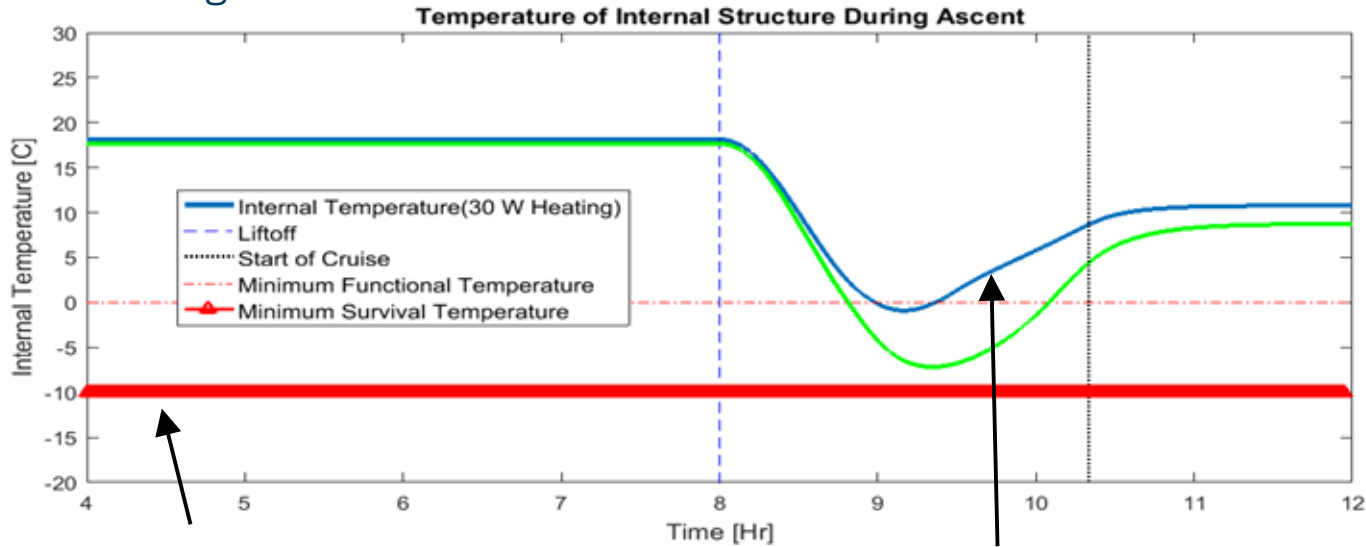
| Requirement | Description   |
|-------------|---|
| 5.1         | During ascent and descent the system shall survive external temperatures ranging from $-65^{\circ}\text{C}$ to $20^{\circ}\text{C}$ |
| 5.2         | During cruise the system shall operate under external temperatures ranging from $-25^{\circ}\text{C}$ to $-15^{\circ}\text{C}$      |
| 5.3         | The system shall operate at pressure values of 100 kPa to 10 Pa   |





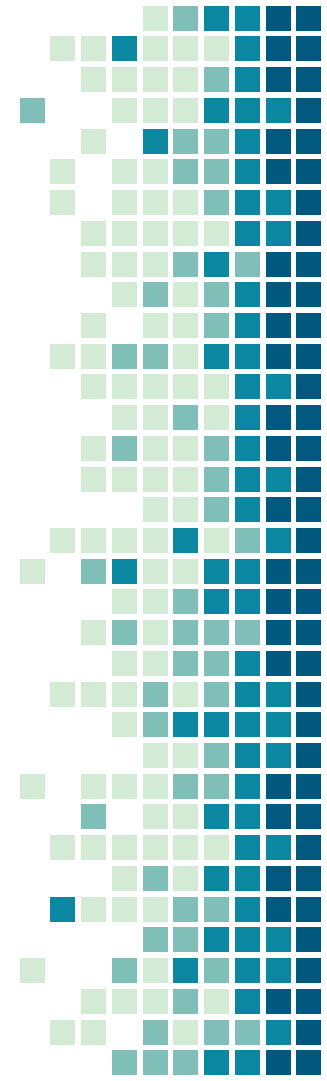
# EMCS Requirements

- EMCS proven valid during cruise and descent, however ascent operational temperature margins were too close to validate through 1D model



Survival temperature  
determined by spectrometer  
survivability temperature

Internal Temperature (20 W  
Heating)



# Design Requirements: EMCS

## Solidworks 3D Thermal Modeling

- Partial transient model simulated at harshest ascent condition of approximately  $-65^{\circ}\text{C}$  at 16 km altitude
- Assumptions
  - Perfect thermal conduction through bonded contacts
  - Convection, conduction and radiation accounted for
  - Power board, and heat pads are only notable heat sources (all other systems not operating during ascent)

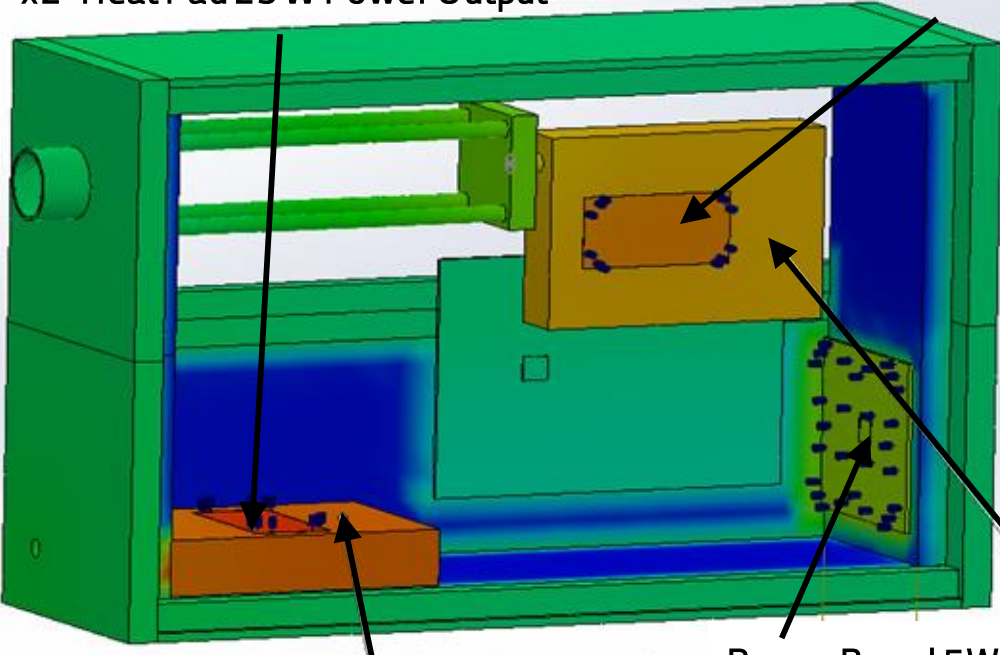
## Initial Conditions

| Item   | Value   |
|--|---|
| STOUT Internal Temp.   | $15^{\circ}\text{C}$ (STD sea level)                      |
| Ambient Temperature  | $-65^{\circ}\text{C}$ (Lower temperature limit of ascent) |
| Air Convective Heat Transfer Coefficient (External and Internal) | $\sim 5 \text{ W/m}^2\text{K}$                            |

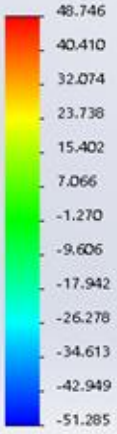
# Expected Spectrometer Temperatures at -65°C Environment

1"x2" Heat Pad 25 W Power Output

1"x2" Heat Pad 20 W Power Output



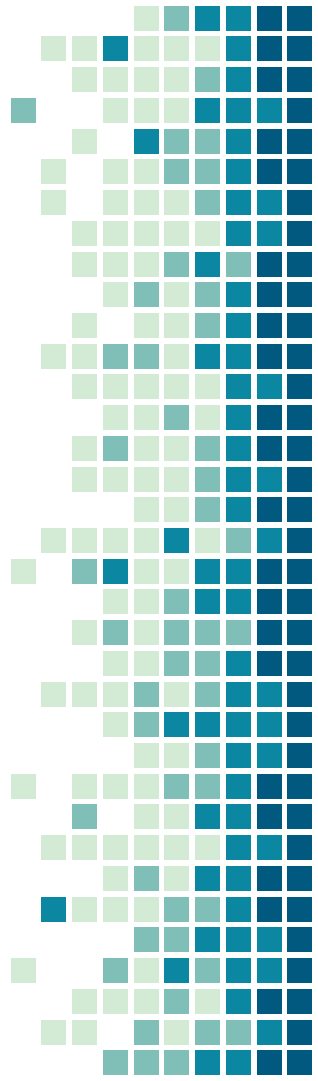
Temp (Celsius)



Spectrometer 1: 36°C

Power Board 5W Power Output

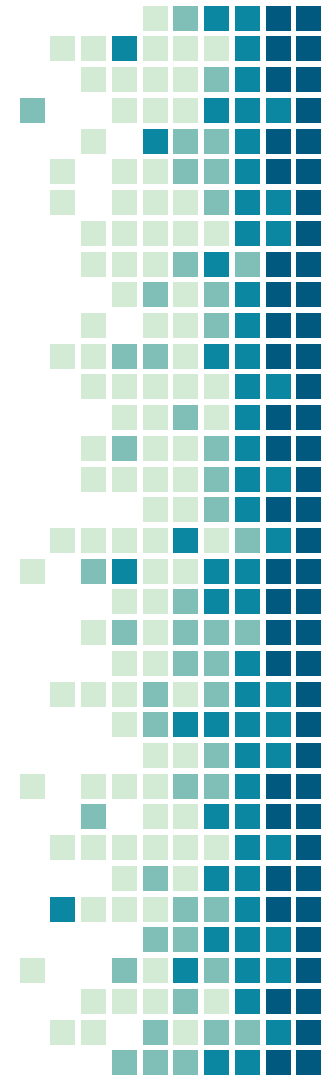
Spectrometer 2: 29°C



# Design Requirements: EMCS

## Future EMCS Development

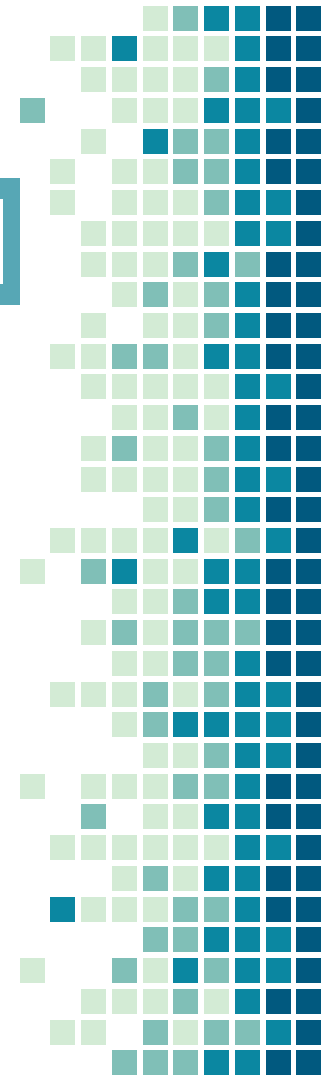
- Develop Full transient model of ascent, cruise, and descent of mission flight
  - Allows for optimization of EMCS (i.e. resistive pad placement and size, total power usage through various flight phases, etc.)
- Verification of EMCS
  - TVAC chamber testing to verify thermal system is suitable for STOUT flight
  - Possible use of environmental chamber for harsher conditions



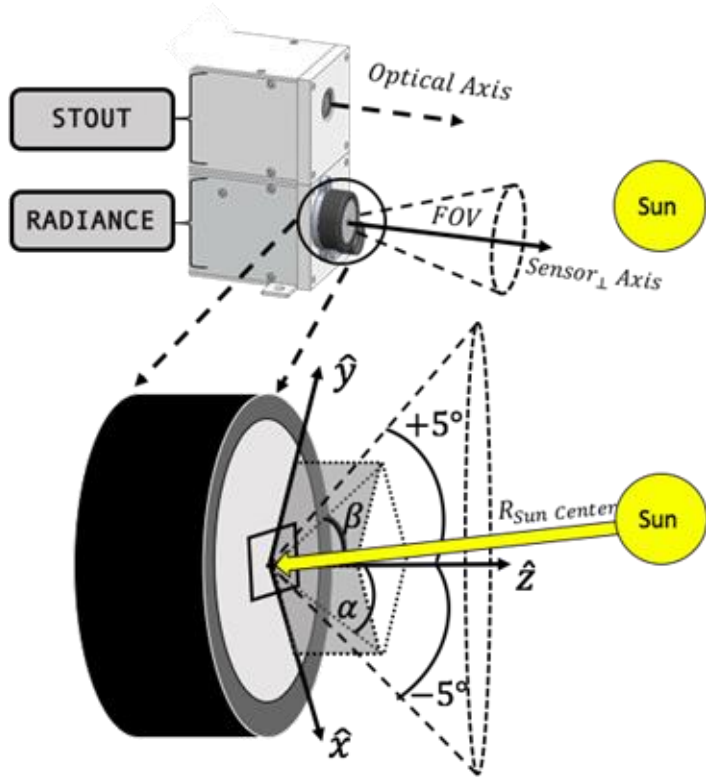
# Attitude Determination Requirements

**FR3: The system shall determine its attitude relative to the Sun center**

| Requirement | Description   |
|-------------|---|
| 3.1         | The off-light source angle attitude shall be determined to within 3' (0.05°) of light source center |
| 3.2         | Attitude data shall be recorded synchronously with instrument data                                  |
| 3.3         | Attitude data shall be interfaced with instrumentation pointing control                             |

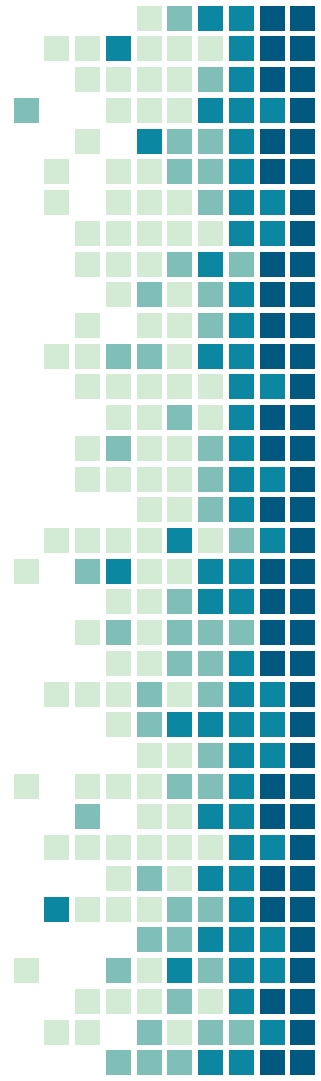


# Attitude Determination System

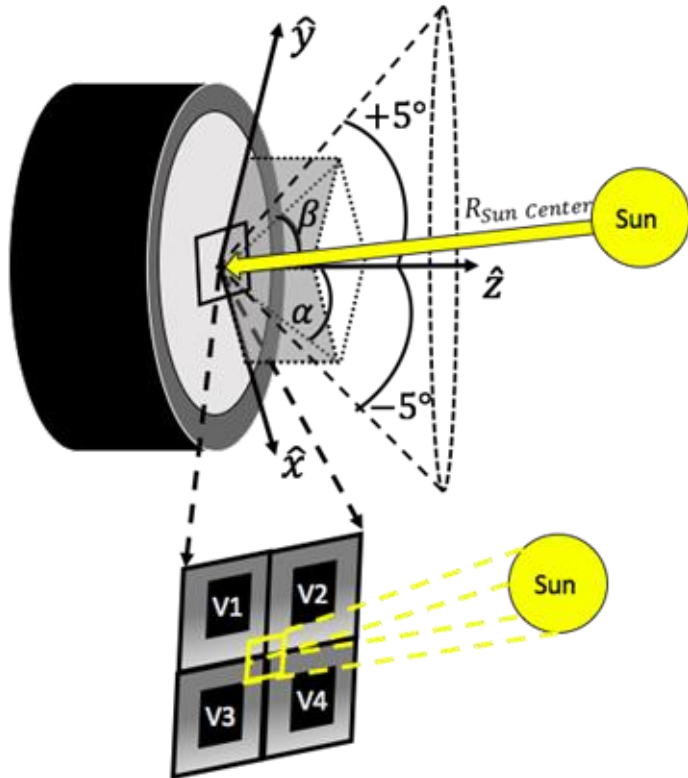


## Solar Mems Sun Sensor

- Quadrant photodetector used to measure off-sun angles from generated photocurrents for optics pointing control
- Field of View: dual axes  $\pm 15^\circ$
- Accuracy:  $\pm 0.02^\circ$
- Serial RS 485 Communication
- Output in Hex
- Requires calibration in conjunction with optical axis



# Attitude Determination System



$$x_1 = V_3 + V_4$$

$$y_1 = V_1 + V_4$$

$$x_2 = V_1 + V_2$$

$$y_2 = V_2 + V_3$$

$$F_x = \frac{x_2 - x_1}{x_2 + x_1}$$

$$F_y = \frac{y_2 - y_1}{y_2 + y_1}$$

$$\alpha = \arctan(C * F_x) \quad \beta = \arctan(C * F_y)$$

*Parametric Value (C)*

*\* Dependent on Sensor \**

## Sun Off-Angles ( $\alpha$ & $\beta$ )

- Communicates the sun's position relative to field of view to the system
- Data saved and used in optics controls

# Optical System Requirements

**FR2: Take variable polarization angle UV spectrum of multiple points on the Sun**

| Requirement | Description  | Level Met |
|-------------|--|-----------|
| 2.1         | Isolation of $\leq 1'$ ( $0.0167^\circ$ ) spot in the FOV                        | 1         |
| 2.2         | Take spectrum measurements over the 270 - 400 nm range                           | 3         |
| 2.3         | Rotate polarizer with $\leq 0.5^\circ$ accuracy                                  | 2         |
| 2.4         | Pointing capabilities of $\pm 1^\circ$ in azimuth and $\pm 5^\circ$ in elevation | 1         |



# Optical System

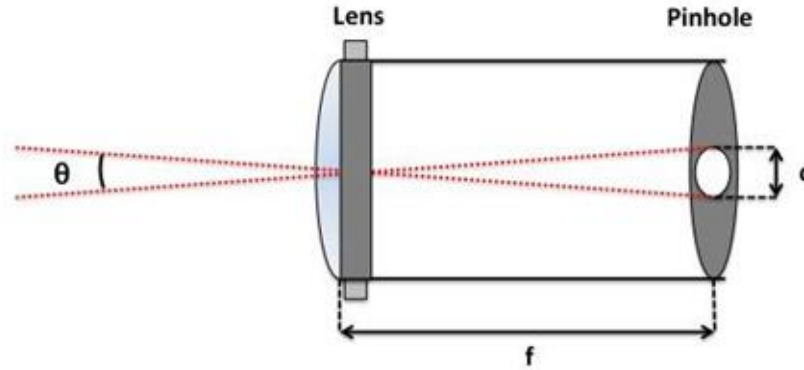
## FR 2.1: Isolation of $\leq 60''$ ( $0.0167^\circ$ ) spot in FOV

- **Relevant Components**
  - Thorlabs ACA254-UV lens with a 150 mm focal length
  - Thorlabs Precision Pinhole with a  $40 \mu\text{m}$  diameter
- **Sources of Error**
  - Manufacturing error of lens focal length ( $\pm 1.5 \text{ mm}$ )
  - Human error in placing the pinhole directly in the focal plane of the lens ( $\pm 1 \text{ mm}$ )
  - Manufacturing error of pinhole diameter ( $\pm 3 \mu\text{m}$ )

Pinhole Diameter:  $d = 40 \pm 3 \mu\text{m}$   
Lens Focal Length:  $f = 150 \pm 1.8 \text{ mm}$

### Isolated Spot Size

$$\theta = 2 \tan^{-1}(d/2f) = 55 \pm 7''$$

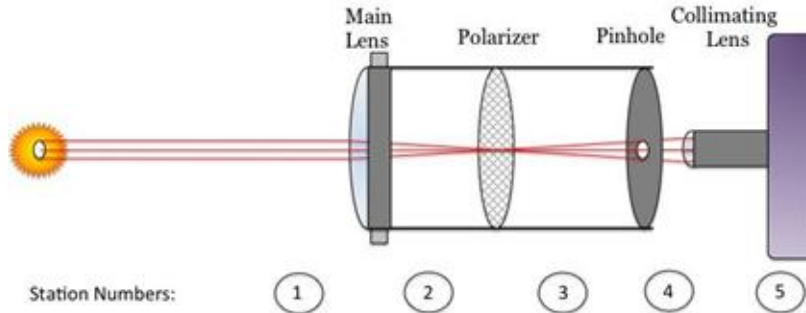


# Optical System

FR 2.2: Take spectrum measurements over the 270 - 400 nm range

- **Relevant Components**

- Avantes AvaSpec Mini 2048 Spectrometer with a 200-400 nm grating
- Avantes COL-UV/VIS Collimating Lens
- Thorlabs Precision Pinhole with 40  $\mu\text{m}$  diameter
- Thorlabs ACA254-UV Lens
- Thorlabs Ultrabroadband Wire Grid Polarizer



Power at Station 5 used to test system to set an appropriate spectrometer exposure time

## 200 - 400 nm Flux Budget

| Station | Total Power        |
|---------|--------------------|
| 1       | 41.8 mW            |
| 2       | 38.7 mW            |
| 3       | 23.7 mW            |
| 4       | 19.5 $\mu\text{W}$ |
| 5       | 18.1 $\mu\text{W}$ |

# Optical System

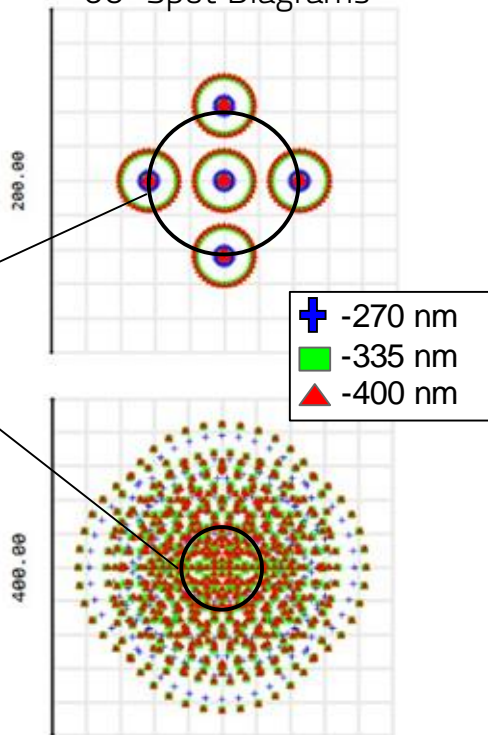
- Improper placement of the pinhole relative to the lens degrades focusing quality

60" Spot Diagrams

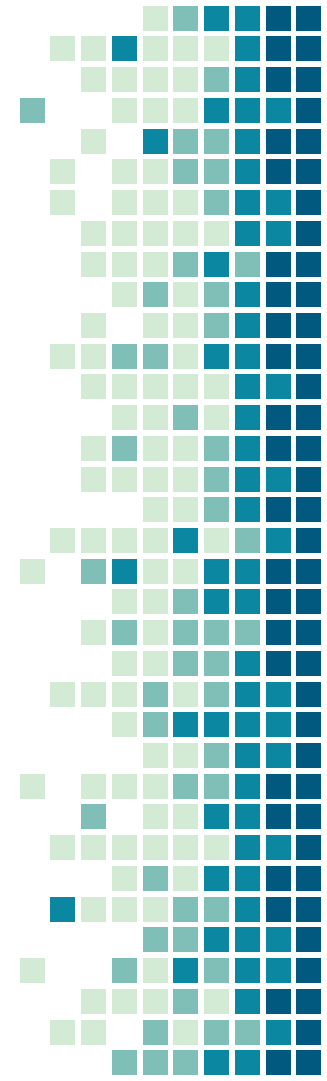
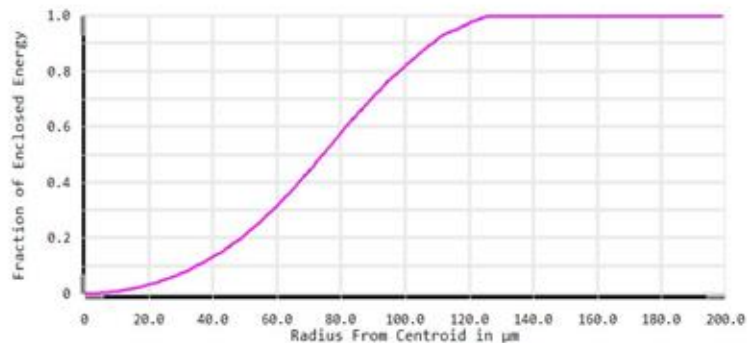
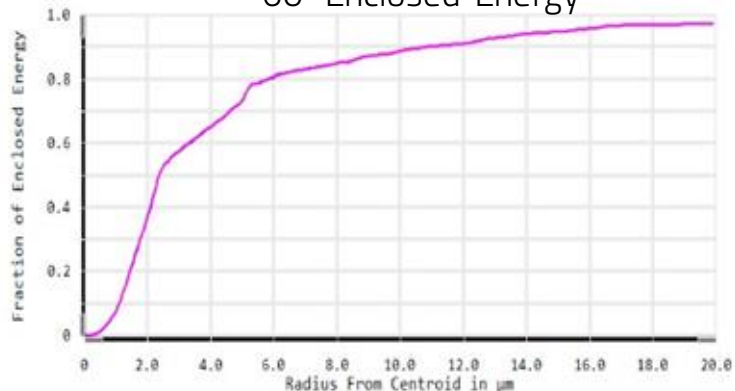
Perfectly in focal plane

40  $\mu\text{m}$  Pinhole Diameter

Including manufacturing and human error (+/- 1.8 mm)



60" Enclosed Energy



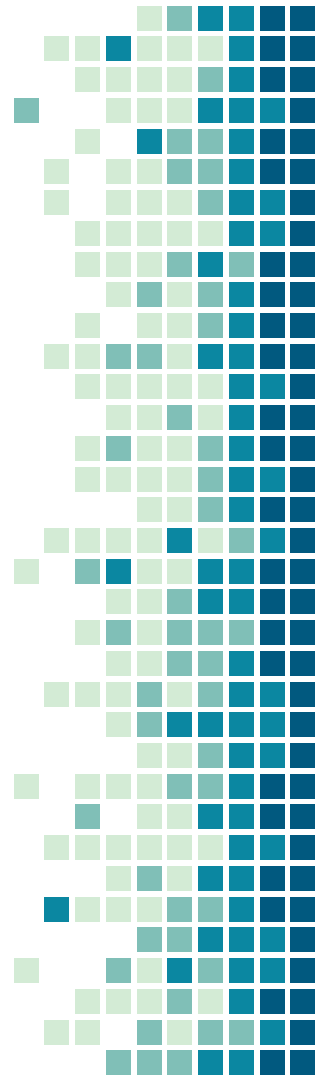
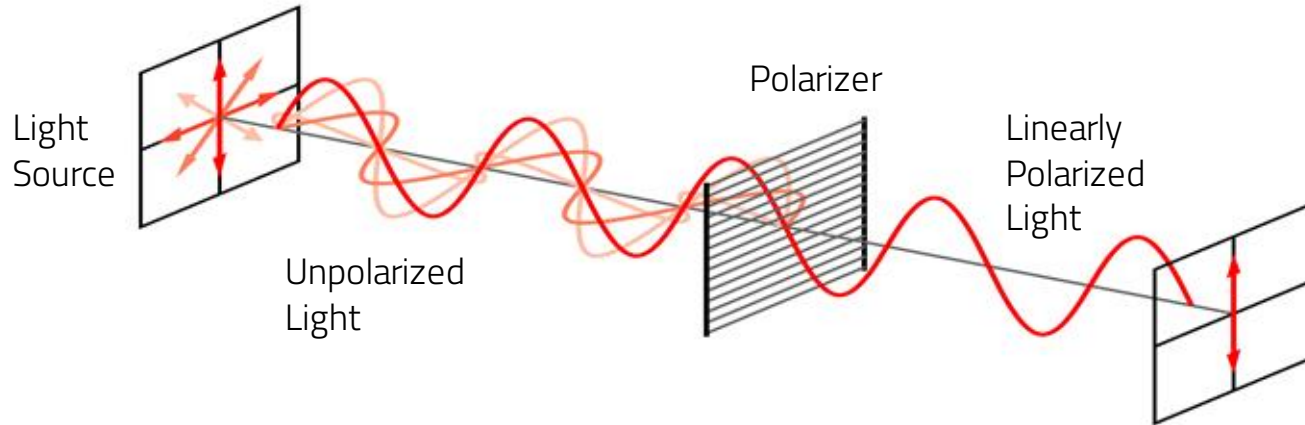
# Optical System

## FR 2.3: Rotate polarizer with $\leq 0.5^\circ$ accuracy

- Relevant Components

- Thorlabs Stepper Motor Rotation Mount

- Provides  $360^\circ$  rotation of the polarizer at a speed of  $10^\circ/\text{s}$  with an accuracy of  $\pm 0.14^\circ$



# Optical System/Pointing Control

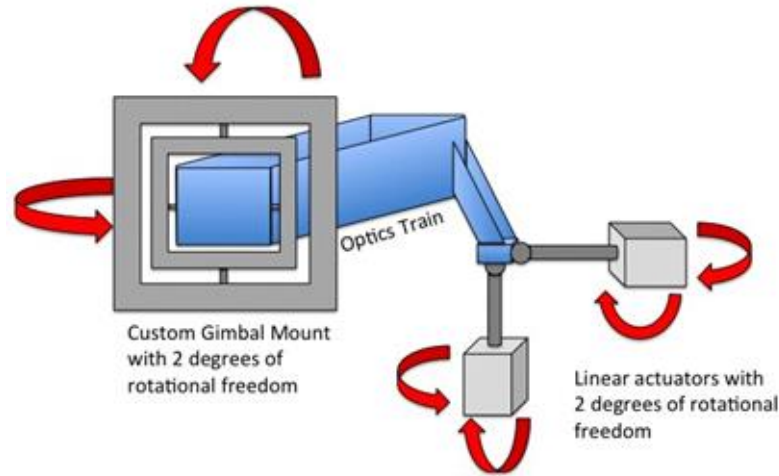
**FR 2.4:** Pointing capabilities of  $\pm 5^\circ$  in azimuth and  $\pm 1^\circ$  in elevation

## ○ Relevant Components

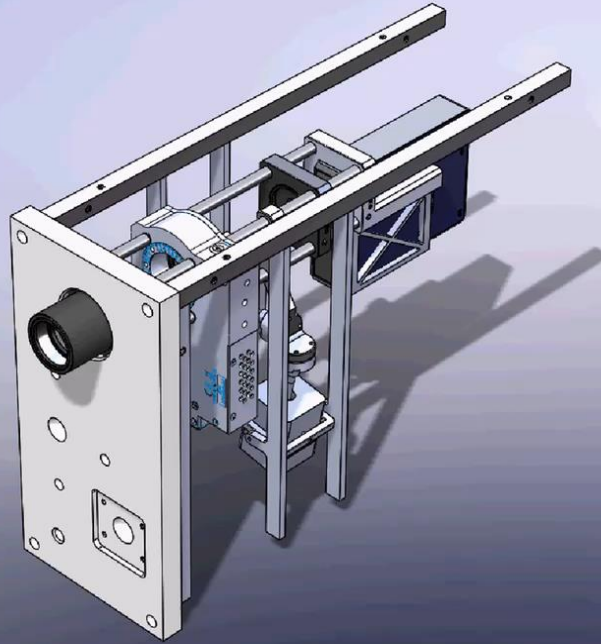
- Thorlabs 30mm Cage System
- Custom Cage System Gimbal Mount
- Haydon Kerk Pittman Hybrid Stepper Linear Actuator with encoder
- Hephaist Spherical Ball Joints
- Custom Gimbal Motor Mounts

## ○ Sources of Error

- Manufacturing error of the alignment of Thorlabs Cage System (  $\pm 180 \mu\text{m}$  )
- Slack in ball joints (  $\pm 2 \mu\text{m}$  )
- Slack in gimbal mounts

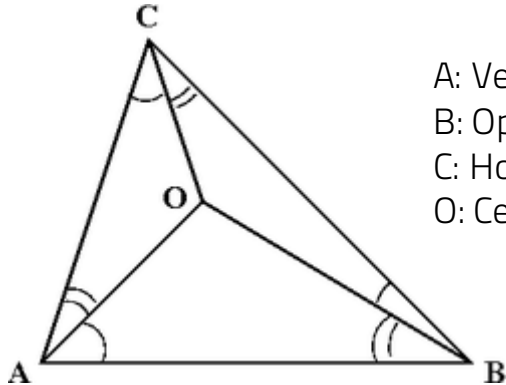


# Pointing Control: Animation

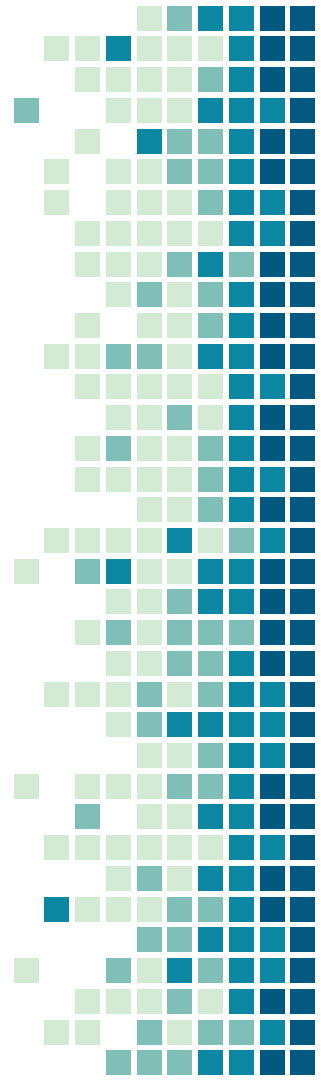


# Pointing Algorithm

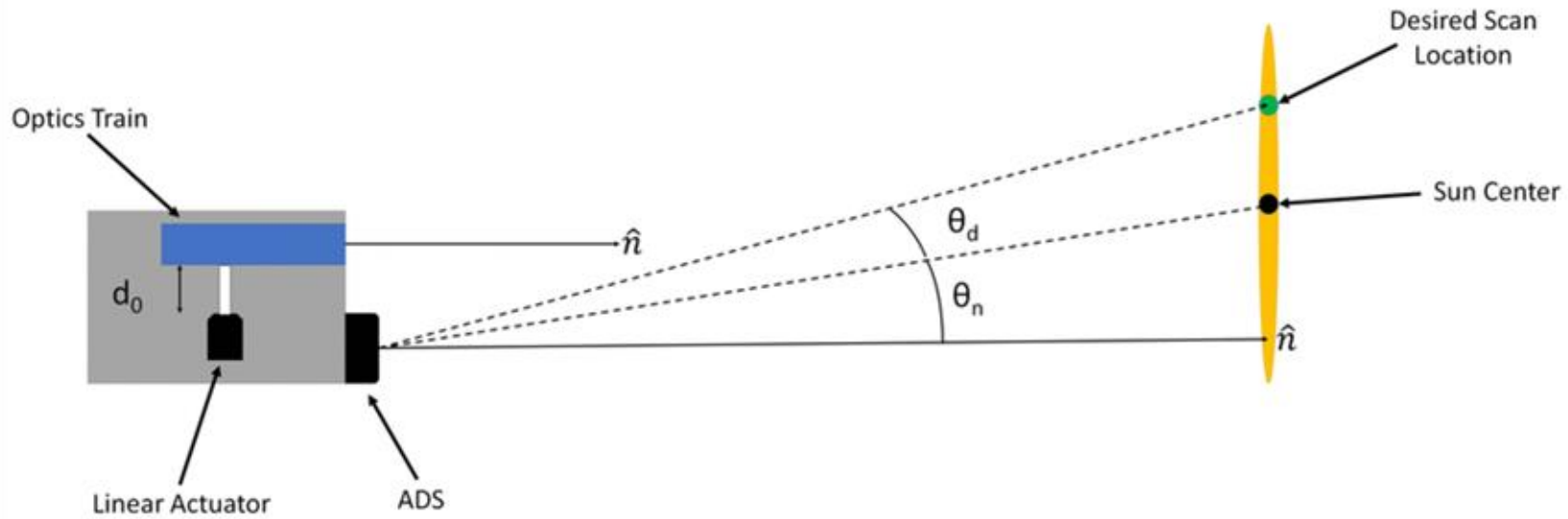
- **Needed Values:** Stepper motor extensions needed for a desired pointing angle
- **Known/Fixed Values**
  - Position of actuators
  - Position of front of optics cage
  - Distance between actuators
  - Distance between actuators and front of optics cage
- **Governing Principles:** Geometry of a tetrahedron
- **Summary**
  - Desired pointing angle can be used to calculate the extension of each motor head
  - Library of 788 different pointing angles needed for a full sun scan will be programmed into the onboard CPU



- A: Vertical actuator center
- B: Optics cage gimbal center
- C: Horizontal actuator center
- O: Center of actuator pushing plane



# Pointing Control: Angle Explanation

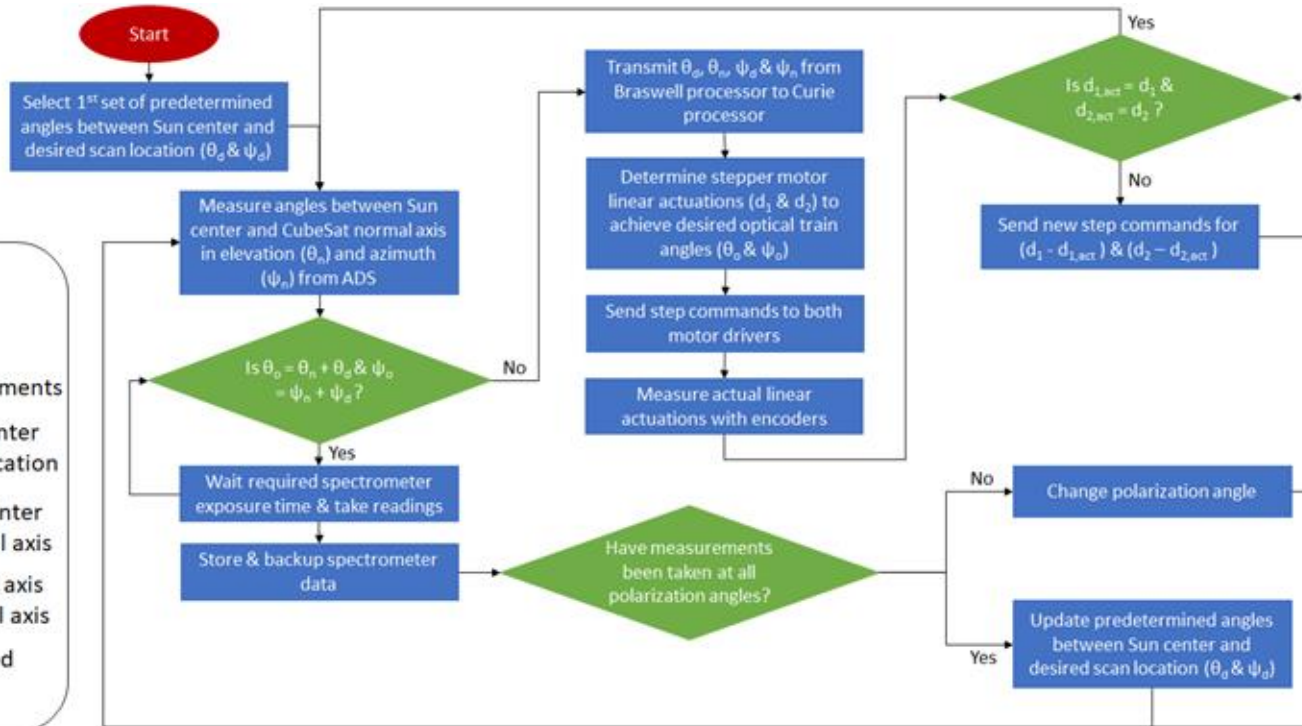
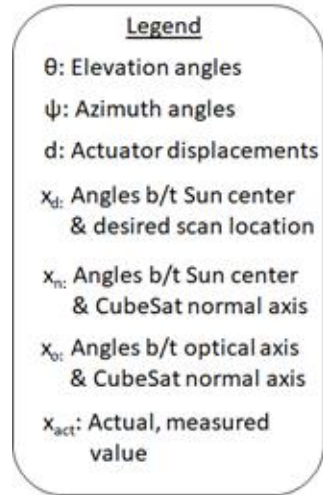


\*Not to Scale\*



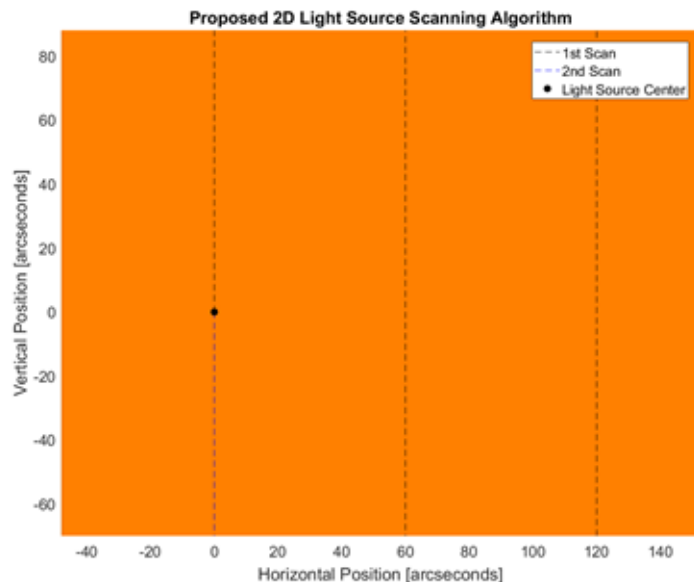
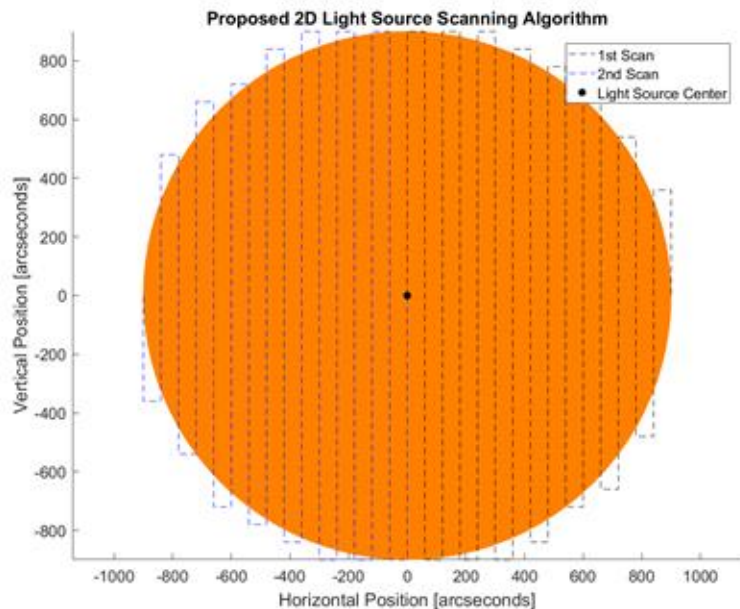


# Pointing Control: Software Flow



# Light Source Scanning Algorithm

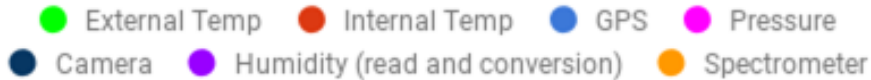
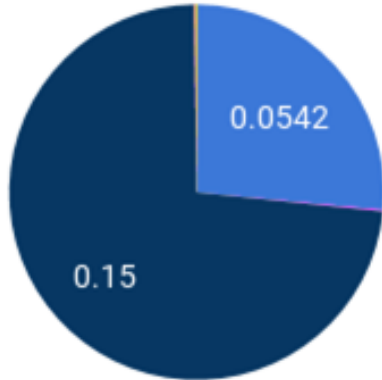
- 1' between scan points
- 788 scan points: 1.1 days to scan entire surface at each needed polarization angle



# Data Acquisition

- Required environmental sensor measurement cadence: 1 Hz

Sensor Read Time [s]



Total Read Time: **0.2068 s**

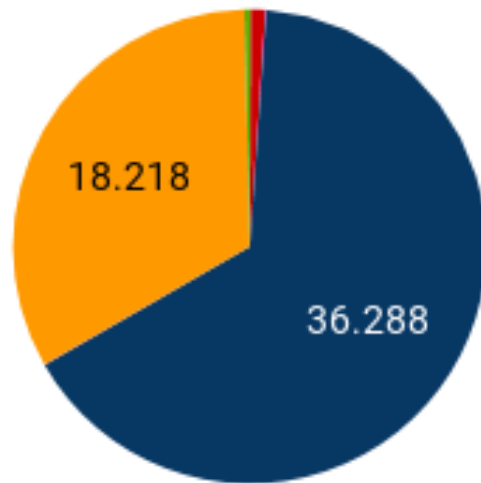
Write Times

| USB Type    | Message Time | Write Rate | Write Sub Total |
|-------------|--------------|------------|-----------------|
| MX-ES Ultra | 620.08 KB    | 26.7 MB/s  | 0.023 s         |
| Samsung Fit | 620.08 KB    | 42.12 MB/s | 0.014 s         |

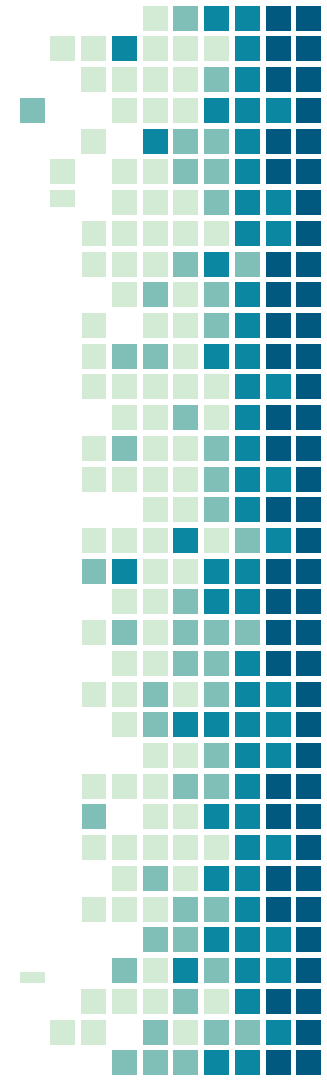
Total Time/Worst Case Write: **0.23 s**

# Data Storage

- Total Storage Required For Entire Flight: 55.34 GB
  - Storage Available: 128 GB
- Sensor Storage [GB]

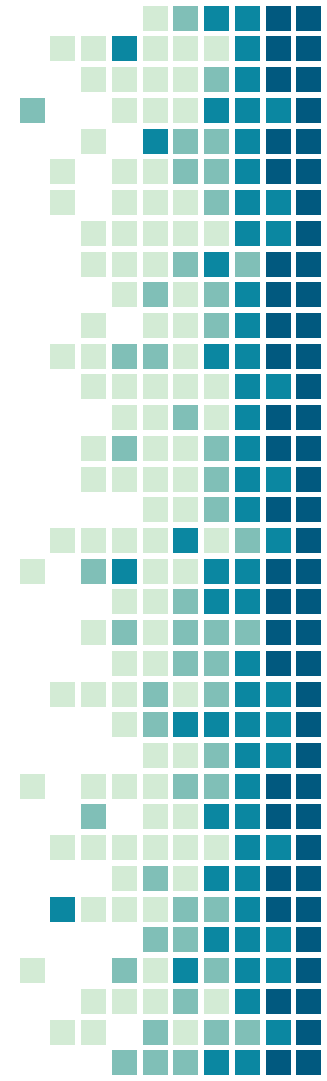


\*Data from both spectrometers and the ADS is saved twice for redundancy

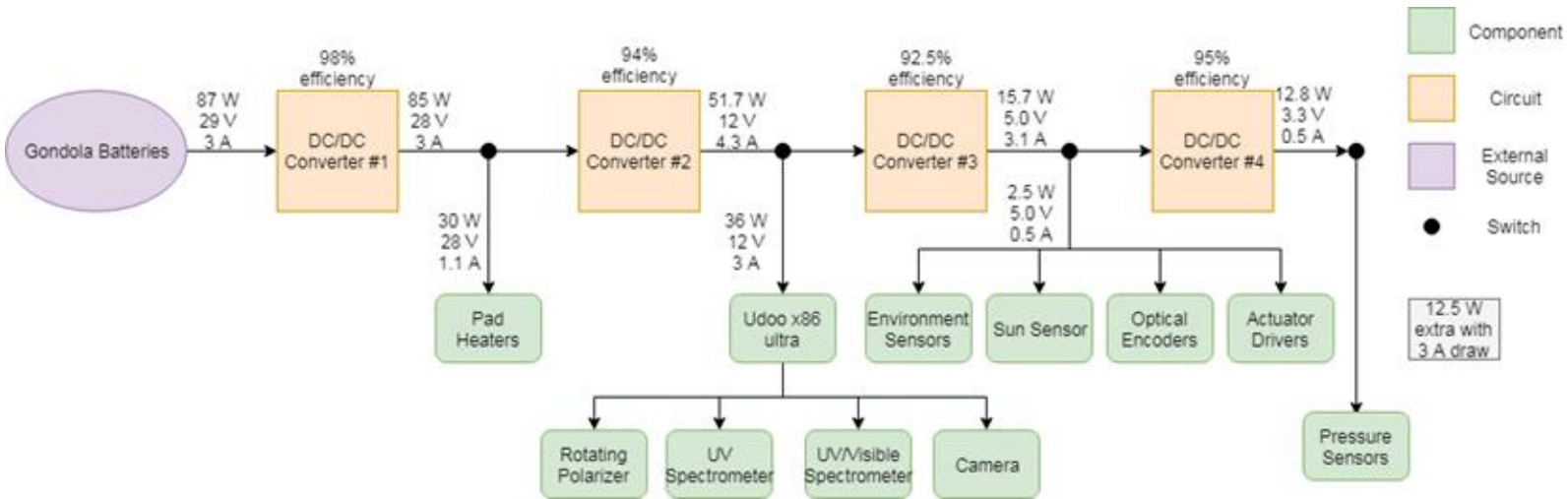


# Power Budget

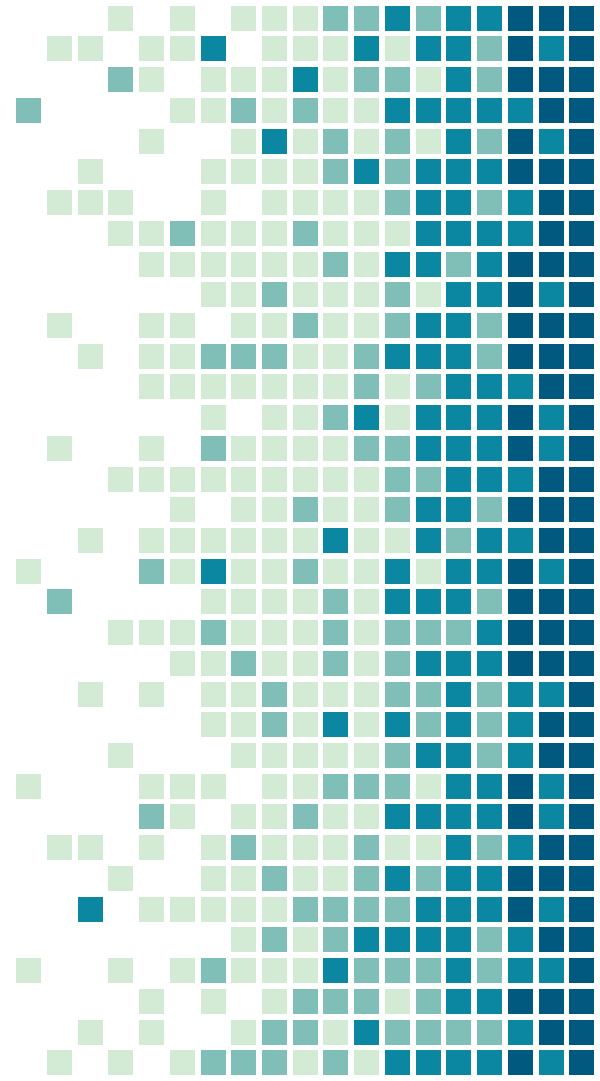
| Component            | Wattage (W)       | Voltage(V) |
|----------------------|-------------------|------------|
| Udoo x86 ultra (DAQ) | 36                | 12.0       |
| Linear Actuators     | 2.45              | 5.0        |
| Pad Heaters          | 40.0              | 28.0       |
| Sun Sensor           | 0.045             | 5.0        |
| Total                | 68.5              | -          |
| Converter Efficiency | 0.8101            | -          |
| Needed Supply        | 74.5              | 28.0       |
| Supply               | 87 W @ 3.0 A draw | 29.0       |
| Margin               | 16.7%             | 3.5%       |



# Power Flow



# Project Risks

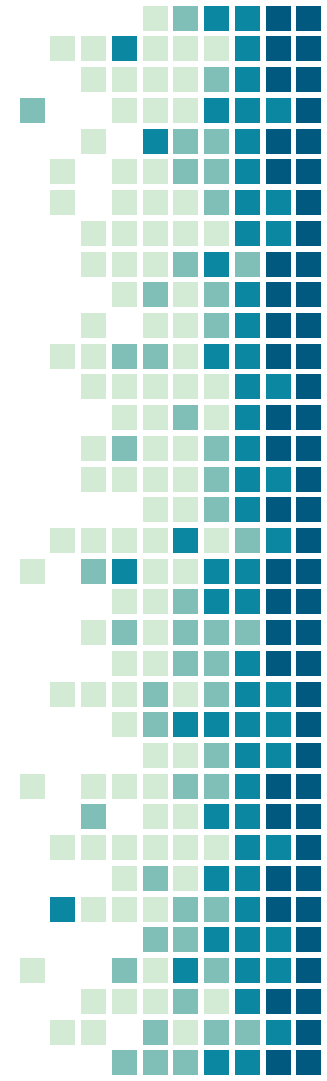


# Risk Summary

| Risk | Risk Description                             | Pertaining Functional Requirement |
|------|--|-----------------------------------|
| R1   | Software Data Write Failure                  | FR 2, FR 3, FR 4, FR5             |
| R2   | Software Bit Flip                            | FR 2, FR 3, FR 4, FR5             |
| R3   | Under-heating of CubeSat Internal Components | FR 1, FR 2, FR 4, FR5             |
| R4   | Over-heating of CubeSat Internal Components  | FR 1, FR 2, FR 4, FR5             |

|            |   | Severity |   |    |       |   |
|------------|---|----------|---|----|-------|---|
|            |   | 1        | 2 | 3  | 4     | 5 |
| Likelihood | 5 |          |   |    | R8    |   |
|            | 4 |          |   |    | R7    |   |
|            | 3 |          |   | R3 | R4    |   |
|            | 2 |          |   | R2 | R1/R6 |   |
|            | 1 |          |   |    | R5    |   |

Project Risks



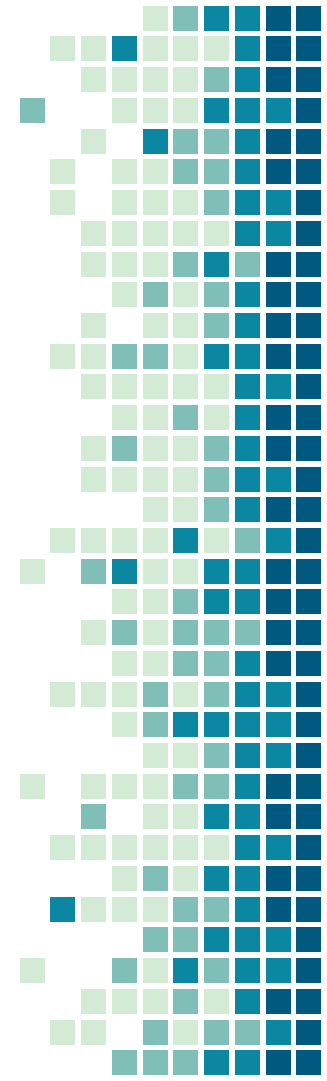


# Risk Summary

| Risk | Risk Description                               | Pertaining Functional Requirement |
|------|--|-----------------------------------|
| R5   | Operation Failure "Freeze" of UDOO X86         | FR 1, FR 2, FR 4, FR5             |
| R6   | Loss of Attitude Determination Calibration     | FR 3, FR 4                        |
| R7   | Manufacturing/Calibration/Test Delays          | FR 1-5                            |
| R8   | Manufacturing creates optical precision errors | FR2, FR4                          |

|            |   | Severity |   |    |       |   |
|------------|---|----------|---|----|-------|---|
|            |   | 1        | 2 | 3  | 4     | 5 |
| Likelihood | 5 |          |   |    | R8    |   |
|            | 4 |          |   |    | R7    |   |
|            | 3 |          |   | R3 | R4    |   |
|            | 2 |          |   | R2 | R1/R6 |   |
|            | 1 |          |   |    | R5    |   |

Project Risks



# High Risk Mitigation

| Risk | Risk Description                                | Risk Mitigation  |
|------|---|--|
| R8   | Manufacturing creates pointing precision errors | <ul style="list-style-type: none"> <li>High precision machined gimbal mounts</li> <li>Calibrate errors out in software &amp; machine shop</li> <li>Contact with AES machining faculty</li> </ul> |
| R7   | Manufacturing/Calibration/Test Delays           | <ul style="list-style-type: none"> <li>Utilize machining, testing and staff resources</li> <li>Finalize test plans early in Spring Semester</li> <li>Follow hard timeline</li> </ul>             |
| R4   | Over-heating of CubeSat Internal Components     | <ul style="list-style-type: none"> <li>Conduct thorough thermodynamic analysis</li> <li>Explore use of peltier devices</li> </ul>  |

## Types of Risks

- Budget
- Technical
- Safety
- Schedule

|            |   | Severity |   |   |    |   |
|------------|---|----------|---|---|----|---|
|            |   | 1        | 2 | 3 | 4  | 5 |
| Likelihood | 5 |          |   |   | R8 |   |
|            | 4 |          |   |   | R7 |   |
|            | 3 |          |   |   | R4 |   |
|            | 2 |          |   |   |    |   |
|            | 1 |          |   |   |    |   |



# Medium Risk Mitigation

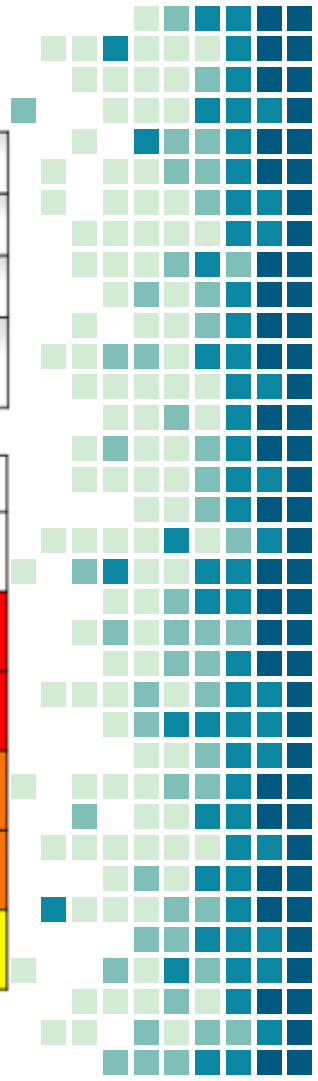
| Risk | Risk Description                             | Risk Mitigation  |
|------|--|--|
| R1   | Software Data Write Failure                  | <ul style="list-style-type: none"> <li>• Watch Dog methodology</li> </ul>  |
| R3   | Under-heating of CubeSat Internal Components | <ul style="list-style-type: none"> <li>• Conduct thorough thermodynamic analysis</li> </ul>                                    |
| R6   | Loss of Attitude Determination Calibration   | <ul style="list-style-type: none"> <li>• Allow larger calibration time in schedule</li> <li>• Transport safety plan</li> </ul> |

## Types of Risks

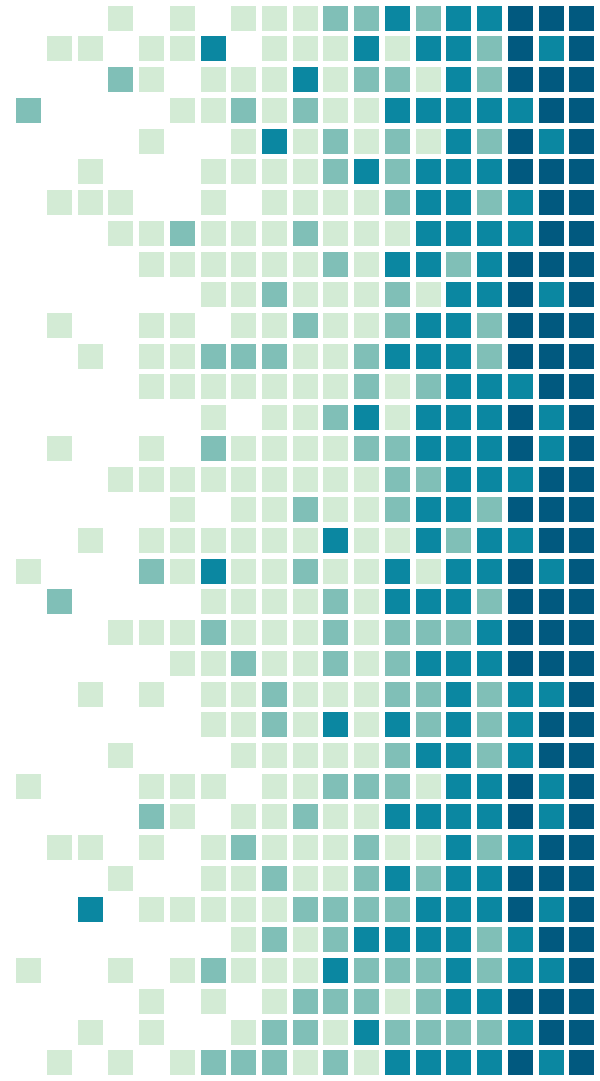
- Budget
- Technical
- Safety
- Schedule

|            |   | Severity |   |    |       |   |
|------------|---|----------|---|----|-------|---|
|            |   | 1        | 2 | 3  | 4     | 5 |
| Likelihood | 5 |          |   |    |       |   |
|            | 4 |          |   |    |       |   |
|            | 3 |          |   | R3 |       |   |
|            | 2 |          |   |    | R1/R6 |   |
|            | 1 |          |   |    |       |   |

Project Risks



# Verification and Validation



# Verification and Test Plan

| Component Selection  | Component Testing   | Subsystem Testing   | Integration Testing   |
|--|---|---|---|
| <ul style="list-style-type: none"> <li>- Operational &amp; Survival Conditions</li> <li>- Resolution</li> <li>- Read/Write Speeds</li> <li>- Control Requirements</li> <li>- Size</li> </ul> | <ul style="list-style-type: none"> <li>- Motors</li> <li>- Polarizer Mount</li> <li>- DAQ/CPU</li> <li>- Powerboard circuit Breadboard</li> <li>- Heaters &amp; Thermocouples</li> <li>- Spectrometers</li> <li>- Sun Sensor</li> </ul> | <ul style="list-style-type: none"> <li>- Optics Train</li> <li>- Udo Board &amp; Storage Devices</li> <li>- Power Board</li> <li>- EMCS</li> <li>- RADIANCE Systems</li> <li>- ADS</li> </ul> | <ul style="list-style-type: none"> <li>- ADS/Pointing Integration and Calibration</li> <li>- FlatSat</li> <li>- TVAC</li> </ul> |
| Completed  | Jan 16 - Jan 26   | Jan 26 - Feb 27   | Feb 27 - Apr 16   |

## Functional Requirements

Take variable polarization angle UV spectrum measurements at various points on the sun

Determine its attitude relative to the Sun

Operate and collect data during the environmental conditions of a 40km high altitude balloon flight

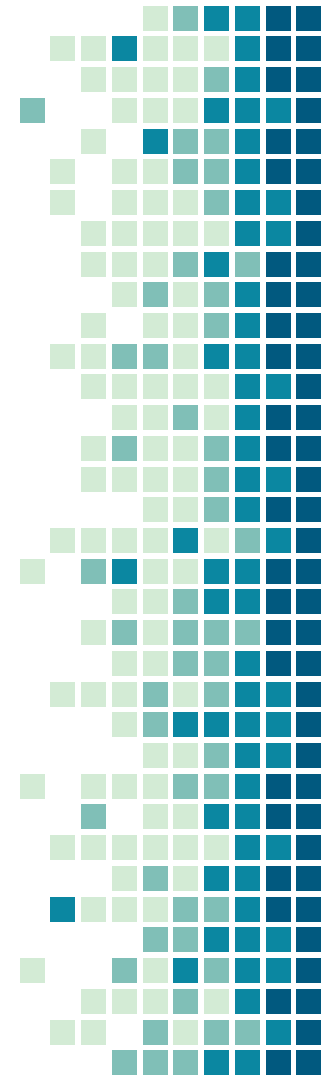
## Requirements Tests

Sommers-Bausch Campaign, Integration Time Test, Focal Length Determination Test

Sommers-Bausch Campaign

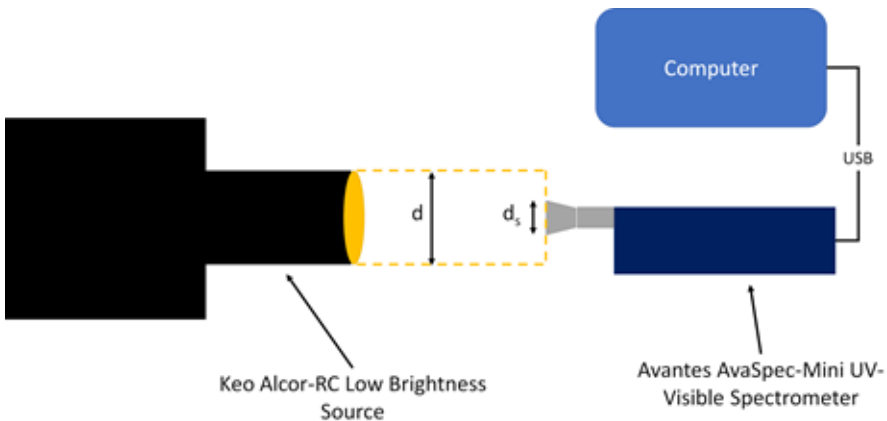
FlatSat, TVAC

Verification and Validation



# Integration Time Test

- **Purpose:** Determine the spectrometer exposure time needed to take high SNR measurements
- **Procedure**
  - Use Keo Alcor Remote Controlled Low Brightness Source (provided by Dr. Marshall) to simulate the expected power input of the spectrometer of  $18.1\mu\text{W}$
  - Use spectrometer software to optimize the exposure time using RADIANCE spectrometer with 200 - 1100 nm grating since the light source produces light in the visible spectrum



$$P_{\text{expected}} = 18.1 \mu\text{W}$$

$$d = 100 \text{ mm}$$

$$d_s = 6 \text{ mm}$$

$$A_{\text{light source}} = \pi * (d_s/2)^2 = 785.4 \text{ mm}^2$$

$$A_{\text{spectrometer}} = \pi * (d/2)^2 = 28.3 \text{ mm}^2$$

$$P_{\text{output,needed}} = P_{\text{expected}} * (A_{\text{light source}} / A_{\text{spectrometer}})$$

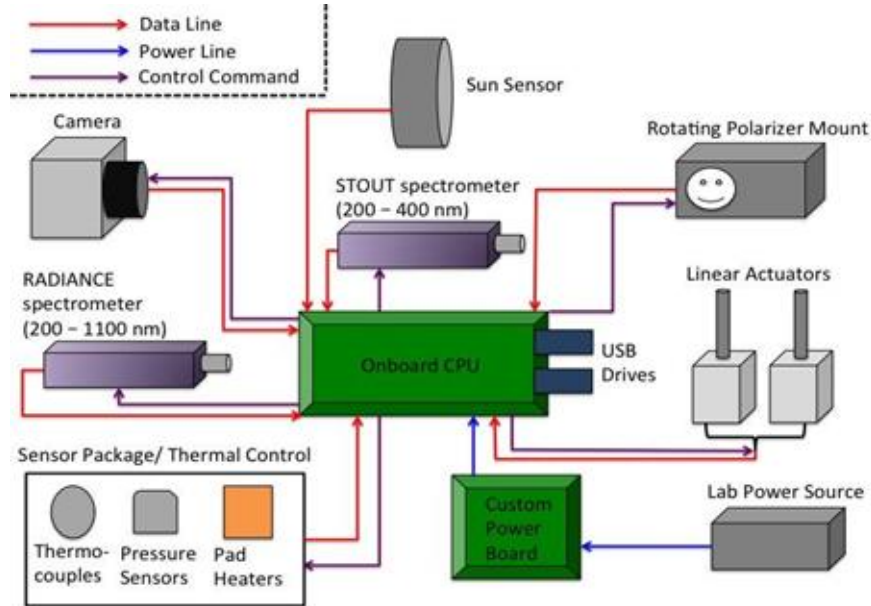
$$= 0.5 \text{ mW}$$

# FlatSat Test

- **Purpose:** Determine that all of the components integrate and operate functionally
- **Procedure**
  - Integrate STOUT and RADIANCE electronics outside of the CubeSat structure
  - Verify expected voltages and currents with a multimeter
  - Calculate and verify expected power draws

## Simplified FlatSat Test Connections

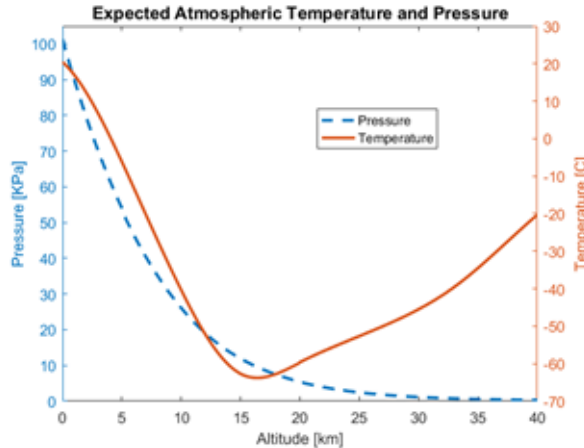
\*Note that the custom power board distributes power to each different component



# Thermal Vacuum Chamber (TVAC) Test

- **Purpose:** Validate EMCS operation and thermal model during the temperature conditions of the high altitude balloon ascent and cruise phases
- **Procedure:** Use TVAC (provided by Phil Oakley at HAO) chamber to put STOUT module through the ascent phase temperature profile and 3 hours of the expected steady state operating temperature
  - Test 1: Structure and EMCS only
    - Post-process data used to verify the module remains at operable temperatures
  - Test 2: Entire module

\*Temperature and pressure profile for proposed flight out of Fort Sumner, NM



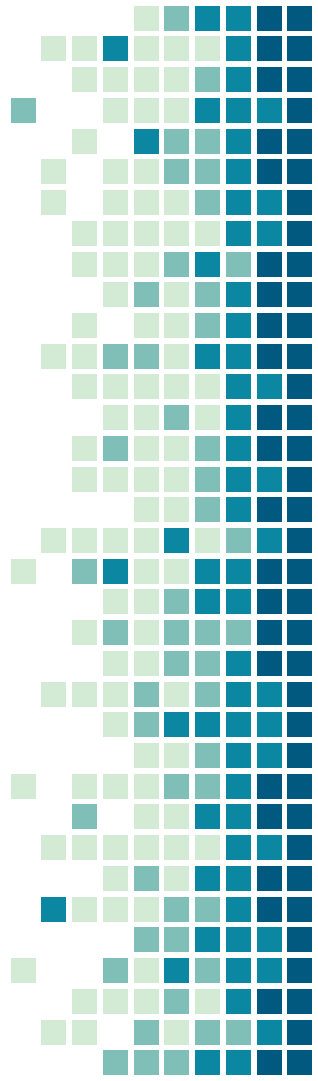
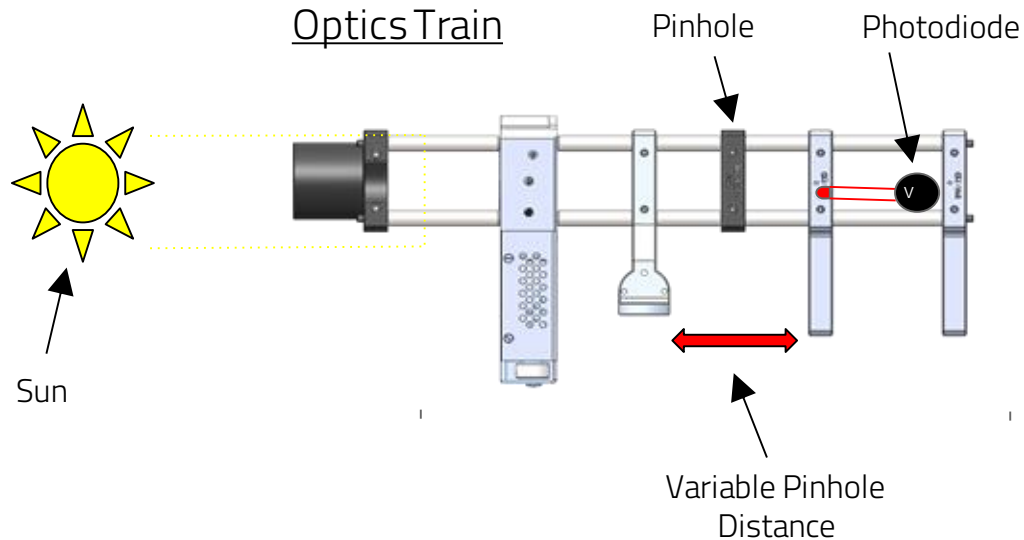
HAO Thermal Vacuum Chamber





# Focal Length Determination Test

- **Purpose:** Experimentally determine the focal point of the main lens
- **Procedure:** Point optics train at Sun and use photodiode to verify pinhole placement within the optics train
  - Maximum voltage potential occurs across the photodiode when pinhole is located in the focal plane and Sun image is focused
  - Move pinhole incrementally until max photodiode voltage occurs



# Sommers-Bausch Testing Campaign

## Problem

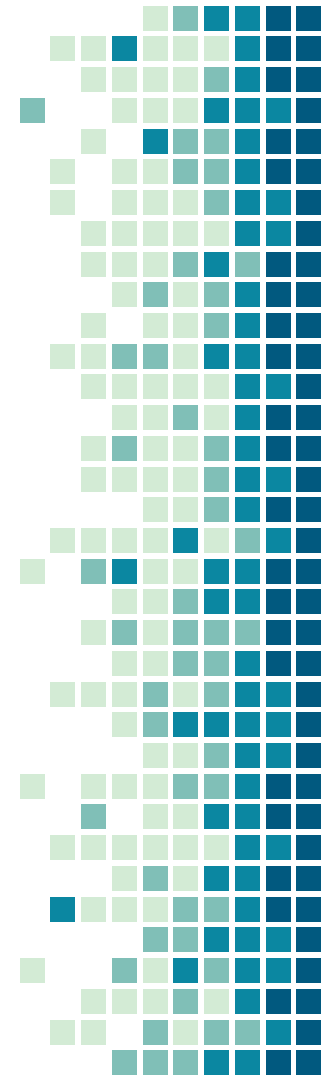
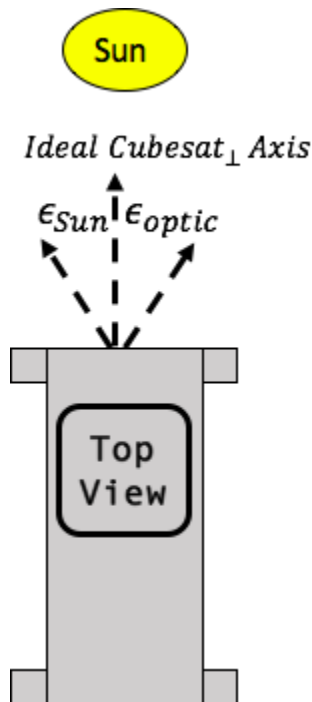
- Manufacturing and mounting errors lead to optical axis and sensor normal axis misalignment

## Sun Sensor Calibration Principles

- Sensor outputs off-sun angles so long as sun is within +/- 5° FOV
- Maximum ADS photocurrent generation occurs when sensor normal axis is aligned with sun center

## Solution

- Use Sommers-Bausch Telescope (provided by Fabio Mezzalira) for alignment to validate outputted off-sun angles, and calibrate angles relative to telescope mount for optics calibration

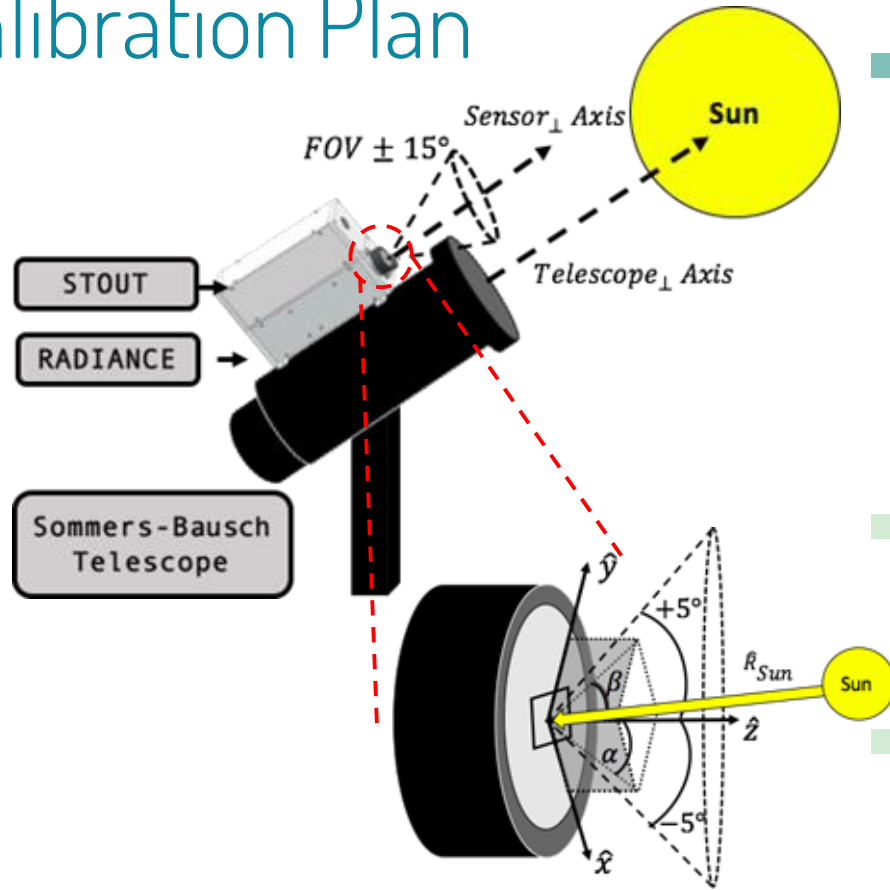


# ADS Verification/Calibration Plan

## Specifications

- Sommers-Bausch telescope has accuracy  $> 20'' \sim 0.0055^\circ$
- Accuracy of Sun sensor:
  - $18'' \sim 0.02^\circ$
  - Total accuracy:  $75.6'' \sim 0.021^\circ$

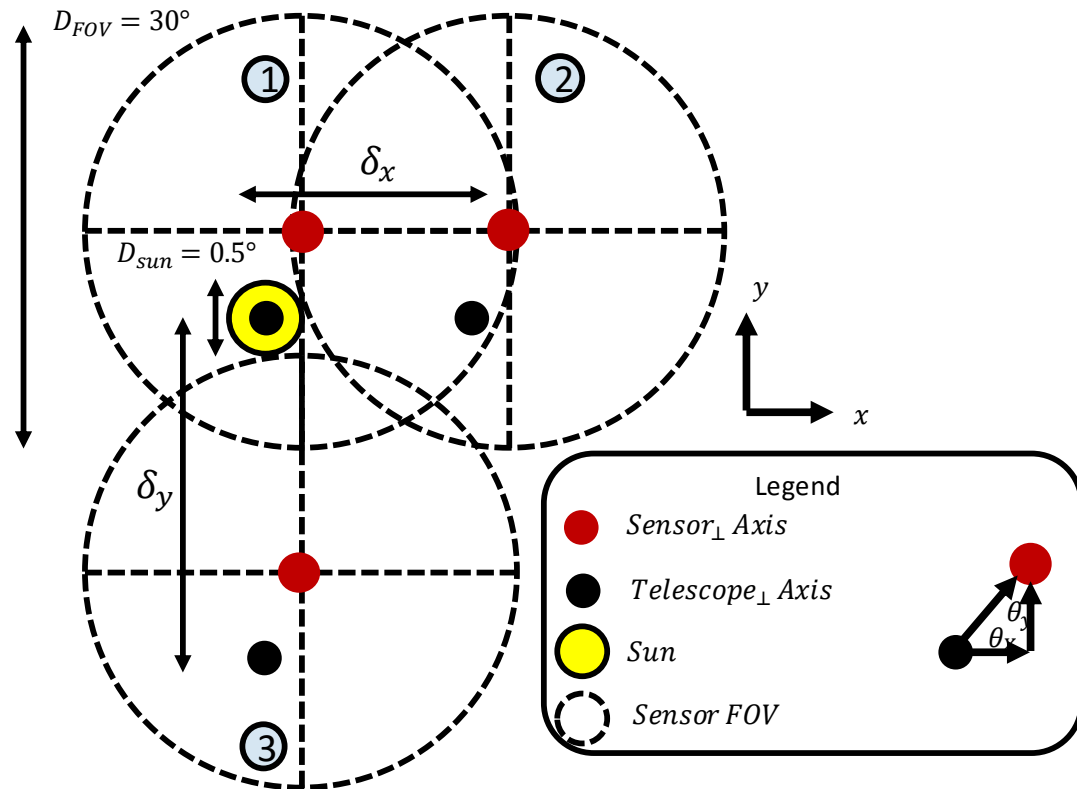
## RADIANCE/Telescope Mount



# ADS Verification Plan

## Verification Procedure

- Point telescope at Sun center
  - Save sensor off-sun angles
- Deviate telescope normal axis and measure deviations between sensor normal axis and sun center using sensor FOV
- Repeat process for multiple nodes to ensure accuracy
- Compare sensor off-sun angles to experimentally determined off-sun angles



Sensor measured off-sun angles

$$\alpha \approx$$

Experimentally determined off-sun angles

$$\theta_{x-Offset} = \tan^{-1} \frac{\delta_y - 5^\circ}{\delta_x - 5^\circ}$$

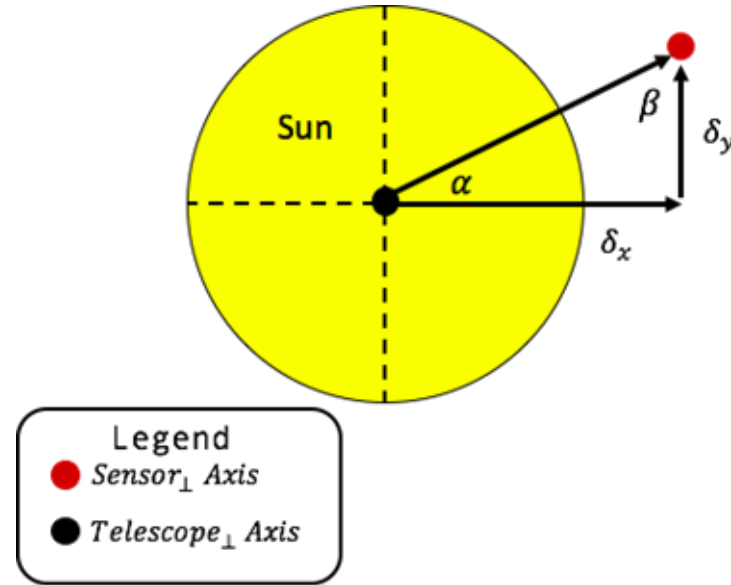
$$\theta_{y-Offset} = \tan^{-1} \frac{\delta_x - 5^\circ}{\delta_y - 5^\circ}$$

Verification and Validation  $\beta \approx$

# ADS Calibration Plan

## Calibration Procedure

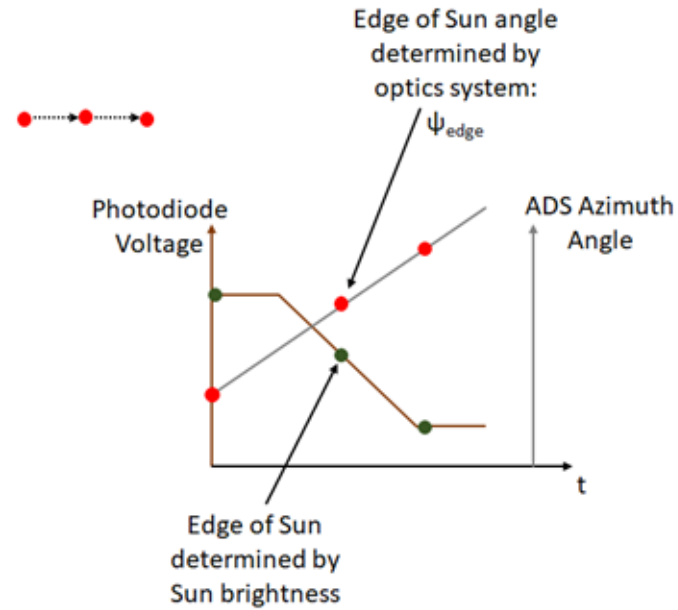
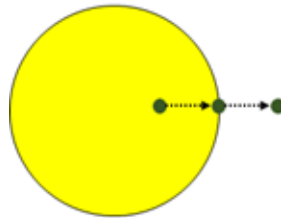
- Point Telescope at Sun center
- Record off sun angles
- Program deviation values in telescope software for optics calibration
- ADS now calibrated to Telescope mount
- Proceed with Optics Calibration



# Optics Calibration Plan

## Calibration Procedure

- Mount photodiode behind pinhole & verify optics train is pointed at the Sun
- Actuate telescope horizontally to move across edge of Sun
- Read photodiode voltage & ADS off-Sun angles as a function of time during movement
- Repeat for vertical actuation
- Post process data to determine offset between optics and ADS axes ( $d\psi$  &  $d\theta$ )

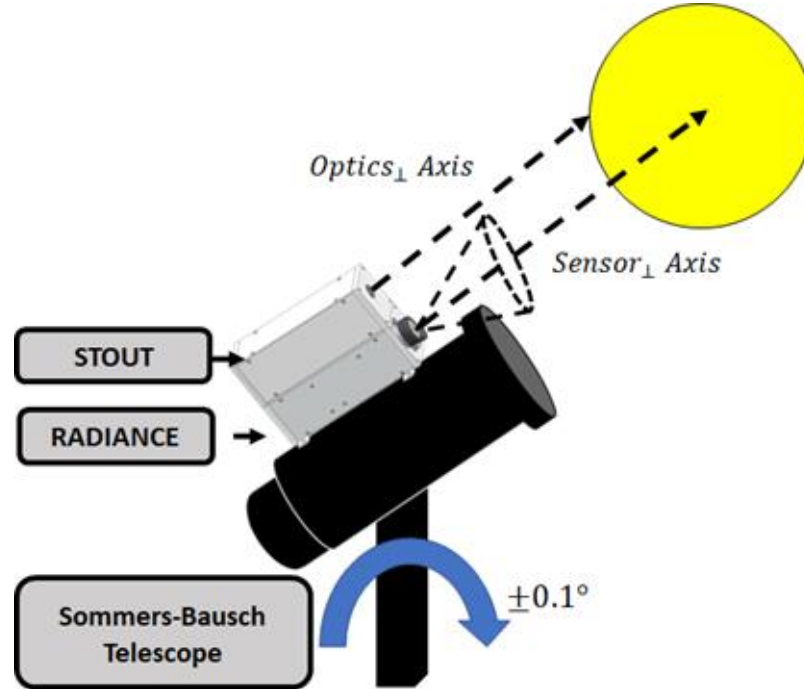


$$\delta\psi = \psi_{edge} - r_{Sun} = \psi_{edge} - 0.5333^\circ$$

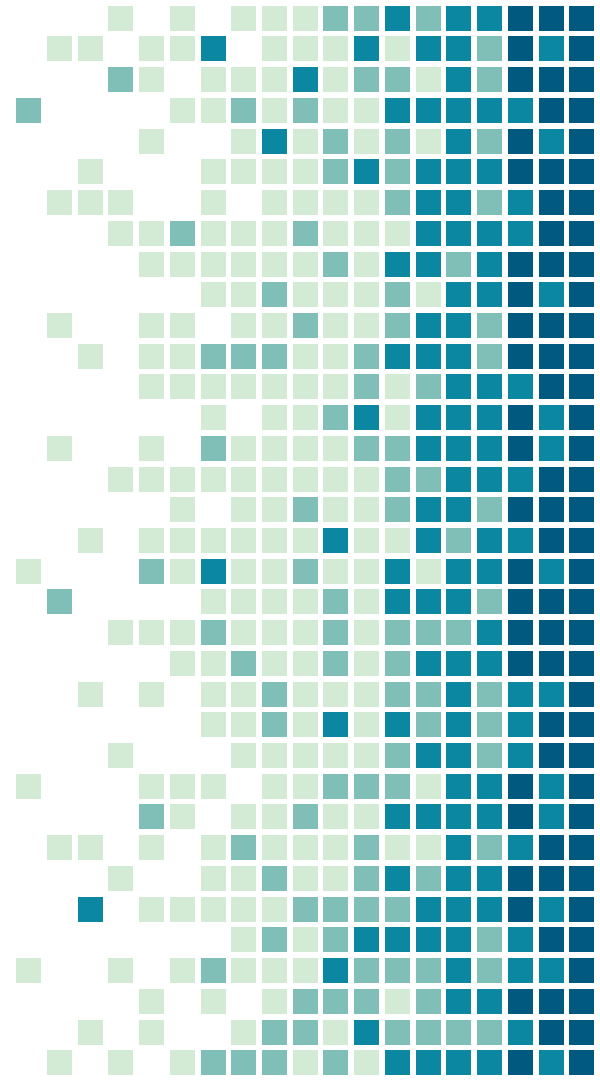
# Pointing Control Verification Plan

## Verification Procedure

- After ADS & Optics calibration are accounted for in software, functionality of pointing control can be verified
- Center Sun in ADS FOV using telescope
- Actuate optics system to the edge of the Sun
- Program telescope to move in pendulum motion to simulate gondola
- Control system will maintain constant photodiode voltage if the pointing system accurately accounts for movement

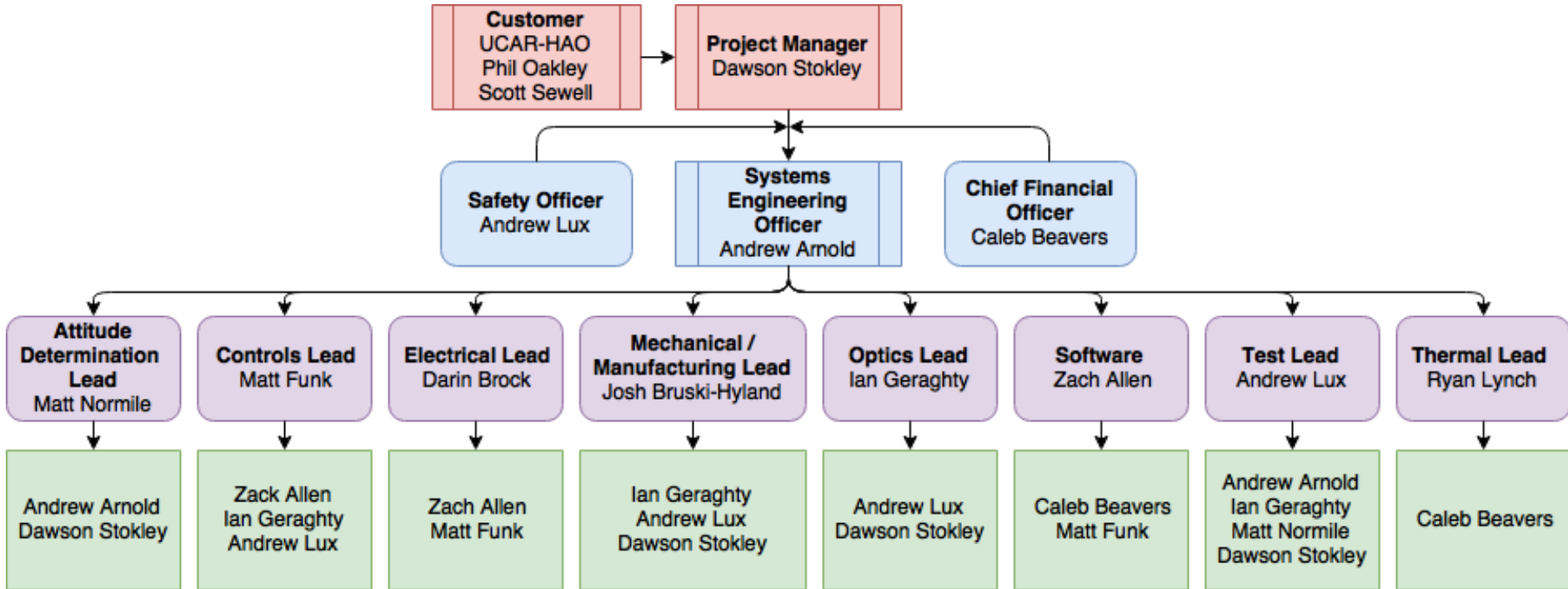


# Project Planning

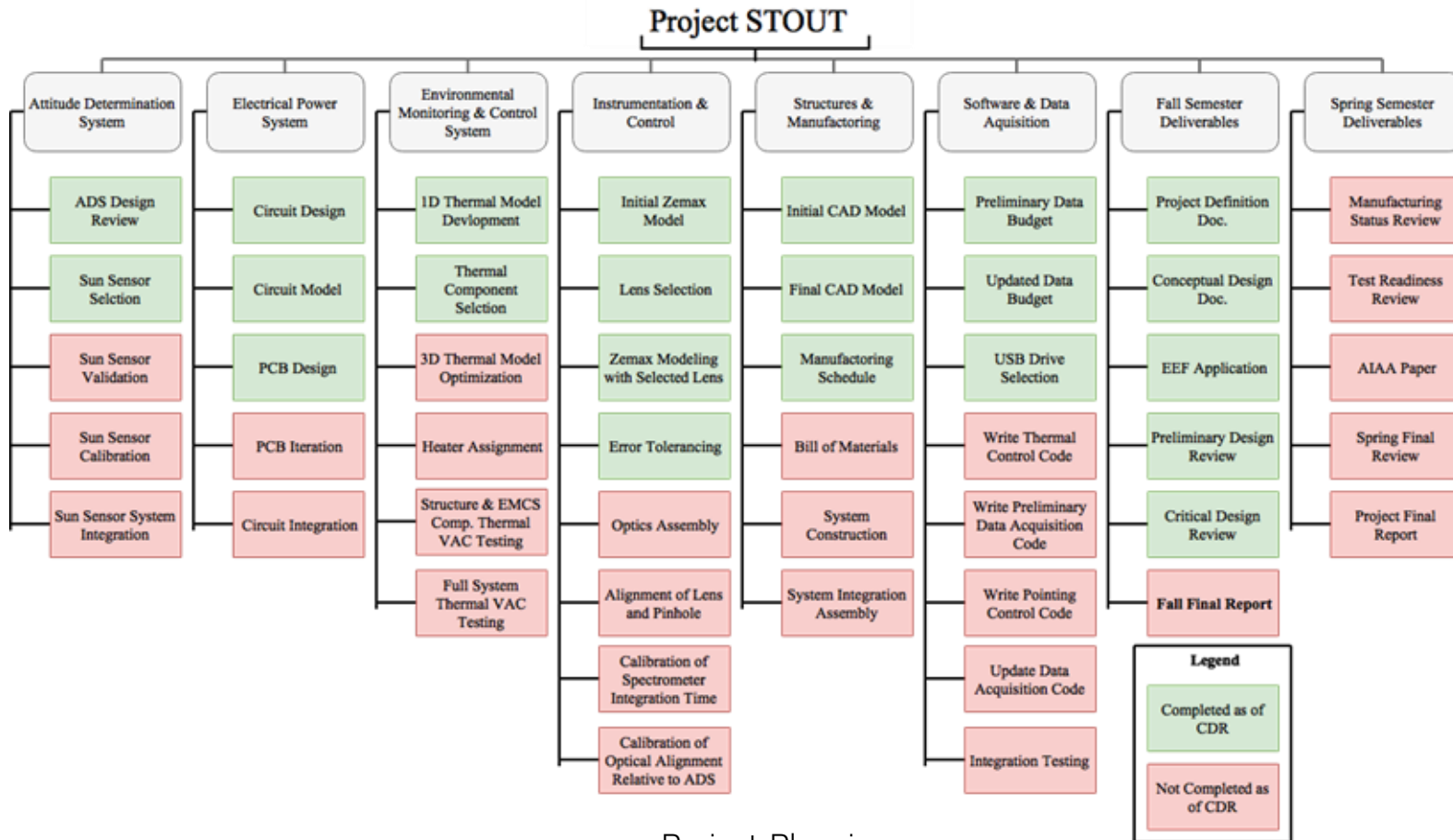




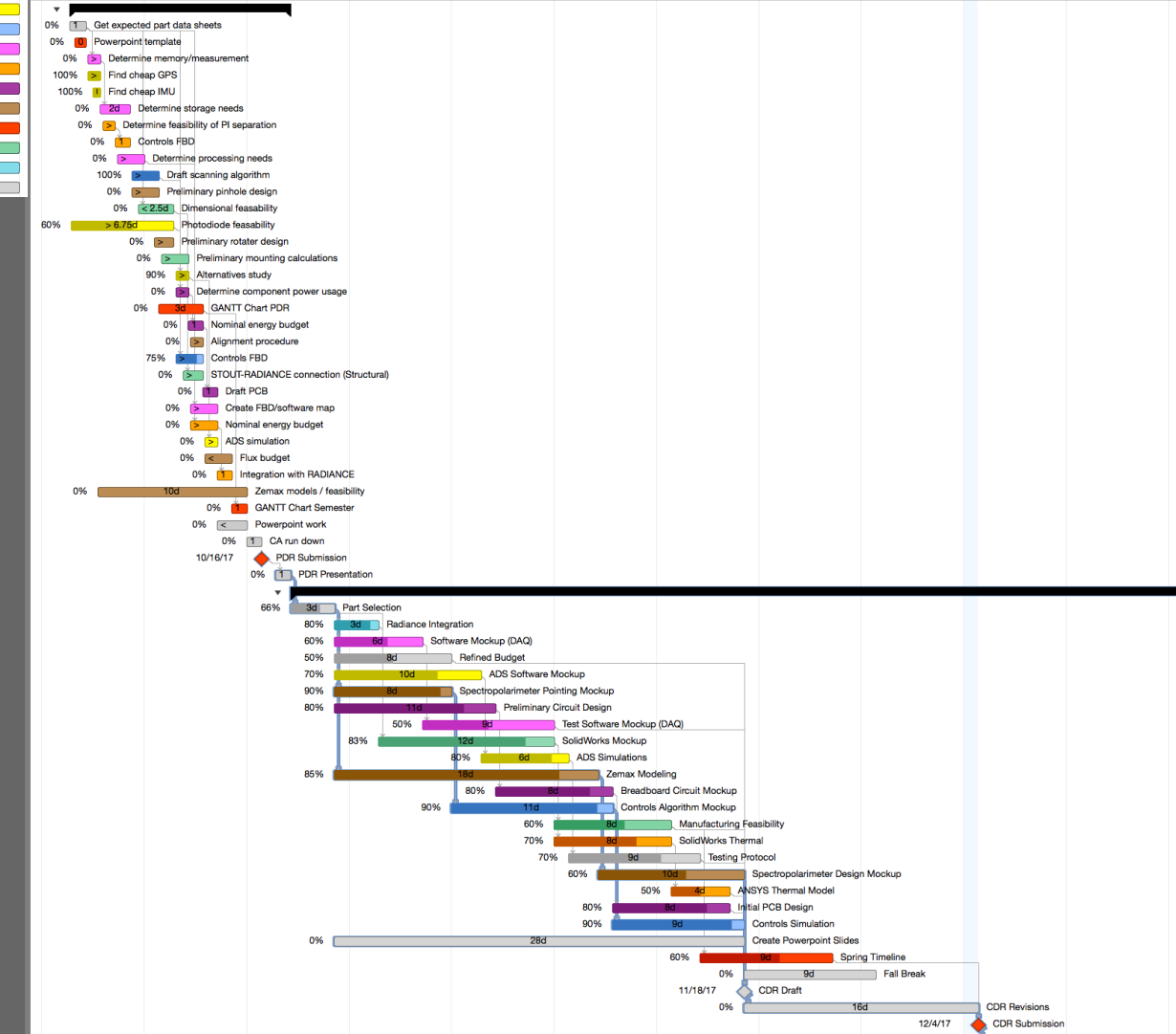
# Organizational Chart



# Work Breakdown Structure



| Title                                    | Planned Start | Planned End |
|--|---------------|-------------|
| PDR                                      | 10/2/17       | 10/17/17    |
| • Get expected part data sheets          | 10/2/17       | 10/3/17     |
| • Powerpoint template                    | 10/3/17       | 10/3/17     |
| • Determine memory/measurement           | 10/4/17       | 10/4/17     |
| • Find cheap GPS                         | 10/4/17       | 10/4/17     |
| • Find cheap IMU                         | 10/4/17       | 10/4/17     |
| • Determine storage needs                | 10/5/17       | 10/6/17     |
| • Determine feasibility of PI separation | 10/5/17       | 10/5/17     |
| • Controls FBD                           | 10/6/17       | 10/6/17     |
| • Determine processing needs             | 10/6/17       | 10/7/17     |
| • Draft scanning algorithm               | 10/7/17       | 10/8/17     |
| • Preliminary pinhole design             | 10/7/17       | 10/8/17     |
| • Dimensional feasibility                | 10/7/17       | 10/9/17     |
| • Protodiode feasibility                 | 10/3/17       | 10/9/17     |
| • Preliminary rotator design             | 10/6/17       | 10/9/17     |
| • Preliminary mounting calculations      | 10/9/17       | 10/10/17    |
| • Alternatives study                     | 10/10/17      | 10/10/17    |
| • Determine component power usage        | 10/10/17      | 10/10/17    |
| • GANTT Chart PDR                        | 10/9/17       | 10/11/17    |
| • Nominal energy budget                  | 10/11/17      | 10/11/17    |
| • Alignment procedure                    | 10/11/17      | 10/11/17    |
| • Controls FBD                           | 10/10/17      | 10/11/17    |
| • STOUT-RADIANCE connection (Structural) | 10/10/17      | 10/11/17    |
| • Draft PCB                              | 10/12/17      | 10/12/17    |
| • Create FBD/software map                | 10/11/17      | 10/12/17    |
| • Nominal energy budget                  | 10/11/17      | 10/12/17    |
| • ADS simulation                         | 10/12/17      | 10/12/17    |
| • Flux budget                            | 10/12/17      | 10/13/17    |
| • Integration with RADIANCE              | 10/13/17      | 10/13/17    |
| • Zemax models / feasibility             | 10/4/17       | 10/14/17    |
| • GANTT Chart Semester                   | 10/14/17      | 10/14/17    |
| • Powerpoint work                        | 10/13/17      | 10/14/17    |
| • CA run down                            | 10/15/17      | 10/15/17    |
| • PDR Submission                         | 10/16/17      | 10/16/17    |
| • PDR Presentation                       | 10/17/17      | 10/17/17    |
| CDR/FFR                                  | 10/18/17      | 12/18/17    |
| • Part Selection                         | 10/18/17      | 10/20/17    |
| • Radiance Integration                   | 10/21/17      | 10/23/17    |
| • Software Mockup (DAQ)                  | 10/21/17      | 10/26/17    |
| • Refined Budget                         | 10/21/17      | 10/28/17    |
| • ADS Software Mockup                    | 10/21/17      | 10/30/17    |
| • Spectropolarimeter Pointing Mockup     | 10/21/17      | 10/28/17    |
| • Preliminary Circuit Design             | 10/21/17      | 10/31/17    |
| • Test Software Mockup (DAQ)             | 10/27/17      | 11/4/17     |
| • SolidWorks Mockup                      | 10/24/17      | 11/4/17     |
| • ADS Simulations                        | 10/31/17      | 11/5/17     |
| • Zemax Modeling                         | 10/21/17      | 11/7/17     |
| • Breadboard Circuit Mockup              | 11/1/17       | 11/8/17     |
| • Controls Algorithm Mockup              | 10/29/17      | 11/8/17     |
| • Manufacturing Feasibility              | 11/5/17       | 11/12/17    |
| • SolidWorks Thermal                     | 11/5/17       | 11/12/17    |
| • Testing Protocol                       | 11/6/17       | 11/14/17    |
| • Spectropolarimeter Design Mockup       | 11/8/17       | 11/17/17    |
| • ANSYS Thermal Model                    | 11/13/17      | 11/16/17    |
| • Initial PCB Design                     | 11/9/17       | 11/16/17    |
| • Controls Simulation                    | 11/9/17       | 11/17/17    |
| • Create Powerpoint Slides               | 10/21/17      | 11/17/17    |
| • Spring Timeline                        | 11/15/17      | 11/23/17    |
| • Fall Break                             | 11/18/17      | 11/26/17    |
| • CDR Draft                              | 11/18/17      | 11/18/17    |
| • CDR Revisions                          | 11/18/17      | 12/3/17     |
| • CDR Submission                         | 12/4/17       | 12/4/17     |



# Cost Plan

| System    | Part                                | Price (\$) | Shipping | Quantity | Total      |
|-----------|-------------------------------------|------------|----------|----------|------------|
| ADS       | Solar Mems Sun Sensor               | \$900.00   | \$0.00   | 1        | \$900.00   |
|           | UDDO RS-485 Shield                  | \$9.95     | \$0.00   | 1        | \$9.95     |
| Optics    | Main Lens                           | \$969.00   | \$10.00  | 1        | \$979.00   |
|           | Polarizer Mount                     | \$1,289.00 | \$0.00   | 1        | \$1,289.00 |
|           | 40 um Pinhole                       | \$67.50    | \$0.00   | 1        | \$67.50    |
|           | Lens/Pinhole Mounts                 | \$23.20    | \$0.00   | 2        | \$46.40    |
|           | Cage Rods 2 inch                    | \$23.18    | \$0.00   | 1        | \$23.18    |
|           | Cage Rods 6 inch                    | \$32.21    | \$0.00   | 1        | \$32.21    |
|           | Lens tubes                          | \$14.10    | \$0.00   | 2        | \$28.20    |
|           | Avantes COL-UV/VIS Collimating lens | \$140.00   | \$10.00  | 1        | \$150.00   |
| TCS       | Photodiode for Testing              | \$100.00   | \$0.00   | 1        | \$100      |
|           | Internal Temp Sensor                | \$3.95     | \$0.00   | 4        | \$15.80    |
|           | External Temp Sensor                | \$10.00    | \$0.00   | 2        | \$20.00    |
|           | Pressure Sensor                     | \$59.95    | \$0.00   | 1        | \$59.95    |
|           | Resistive pad heaters               | \$130.00   | \$0.00   | 1        | \$130.00   |
|           | Humidity sensor                     | \$16.95    | \$0.00   | 1        | \$16.95    |
| System    | Amplifier board                     | \$14.95    | \$0.00   | 2        | \$29.90    |
|           | GPS                                 | \$45.00    | \$11.00  | 1        | \$56.00    |
| Structure | Aluminum                            | \$118.27   | \$20.00  | 1        | \$138.27   |
|           | Spherical roller bearings           | \$400.00   | \$20.00  | 2        | \$820.00   |
|           | Test Mounting Structure             | \$75.00    | \$0.00   | 1        | \$75.00    |
| EPS       | Converters                          | \$2.50     | \$0.00   | 1        | \$2.50     |
|           | PCB                                 | \$80.00    | \$0.00   | 2        | \$160.00   |
| Various   | Printing                            | \$100.00   | \$0.00   | 1        | \$100.00   |
| Controls  | Stepper Motor                       | \$237.35   | \$20.00  | 2        | \$494.70   |
|           | Motor controllers                   | \$14.95    | \$0.00   | 2        | \$29.90    |
| DAQ       | Camera                              | \$45.99    | \$0.00   | 1        | \$45.99    |
|           | USB Hub                             | \$16.99    | \$0.00   | 1        | \$16.99    |
|           | USB Drives                          | \$50.00    | \$0.00   | 1        | \$50.00    |
|           | Logic level converters              | \$2.95     | \$0.00   | 10       | \$29.50    |
|           | UDDO x86 Ultra                      | \$267.00   | \$20.00  | 1        | \$287.00   |

| System       | Cost             | Cost w/15% Margin |
|--------------|------------------|-------------------|
| ADS          | \$909.95         | \$1046.44         |
| Optics       | \$2715.49        | \$3122.81         |
| TCS          | \$272.60         | \$313.49          |
| Systems      | \$56.00          | \$64.40           |
| Structure    | \$1033.27        | \$1188.26         |
| EPS          | \$162.50         | \$186.88          |
| Various      | \$100.00         | \$115.00          |
| Controls     | \$524.60         | \$603.29          |
| DAQ          | \$429.48         | \$493.90          |
| <b>Total</b> | <b>\$6203.89</b> | <b>\$7134.44</b>  |



Budget  
Increased to  
\$737



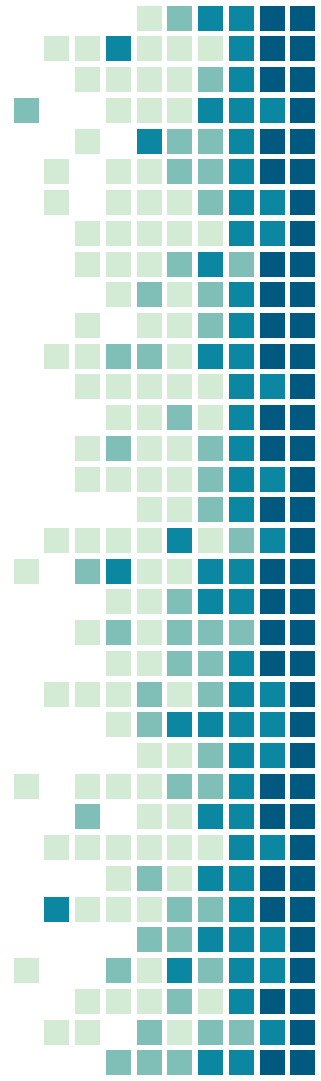
# STOUT

Thank you for listening! We appreciate your feedback.

Are there any questions?

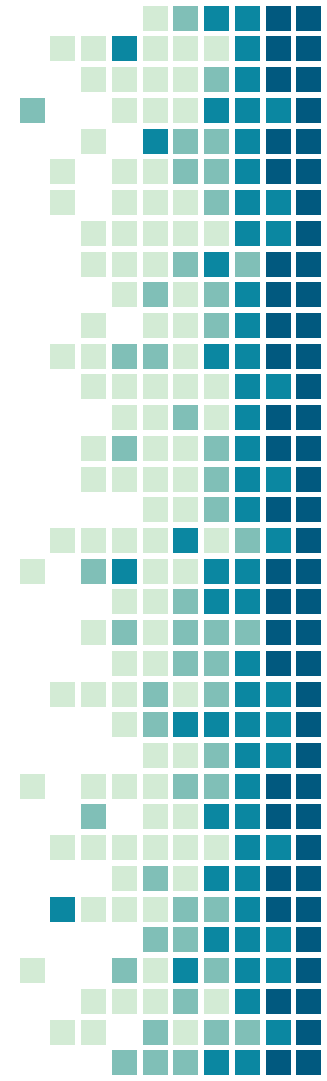
# References

- SolidWorks Thermal Analysis - [http://help.solidworks.com/2014/english/solidworks/cosmosxpresshelp/c\\_Thermal\\_Analysis.htm](http://help.solidworks.com/2014/english/solidworks/cosmosxpresshelp/c_Thermal_Analysis.htm)
- Measuring Humidity on a High Altitude Balloon - [http://www.societyofrobots.com/space\\_balloon\\_humidity\\_test.shtml](http://www.societyofrobots.com/space_balloon_humidity_test.shtml)
- Pad Heaters - [https://www.omega.com/pptst/KHR\\_KHLV\\_KH.html](https://www.omega.com/pptst/KHR_KHLV_KH.html)
- Peltier Device - <https://www.digikey.com/product-detail/en/cui-inc/CP60240/102-1676-ND/1747368>
- Spectrometer Datasheet - <https://www.avantes.com/products/spectrometers/compactline/item/723-avaspec-mini>
- Robert Salter. Typical Lithium Sulphur Dioxide batteries supplied to Scientific Groups. PDF. Columbia Scientific Balloon Facility, Jan. 2013. <https://www.nsbf.nasa.gov/documents/conventional/EC-500-20-D.C.pdf>
- Reflectance and Albedo of Surfaces - [http://curry.eas.gatech.edu/Courses/6140/ency/Chapter9/Ency\\_Atmos/Reflectance\\_Albedo\\_Surface.pdf](http://curry.eas.gatech.edu/Courses/6140/ency/Chapter9/Ency_Atmos/Reflectance_Albedo_Surface.pdf)
- The Sun's Energy - <https://ag.tennessee.edu/solar/Pages/What%20is%20Solar%20Energy/Sun's%20Energy.aspx>
- ADS Sun Sensor - <http://www.solar-mems.com/>
- Polarizer Mount - [https://www.thorlabs.com/newgrouppage9.cfm?objectgroup\\_id=8750](https://www.thorlabs.com/newgrouppage9.cfm?objectgroup_id=8750)
- MATLAB and Aerospace Toolbox Release 2016b, The MathWorks, Inc., Natick, Massachusetts, United States.



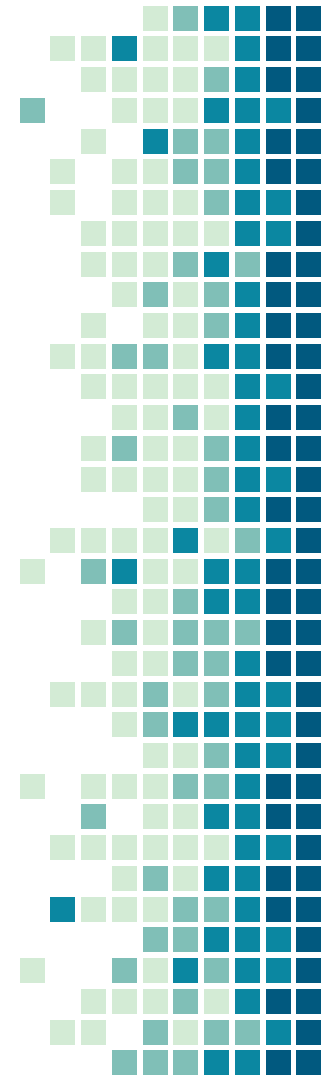
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- MATLAB and Aerospace Toolbox Release 2016b, The MathWorks, Inc., Natick, Massachusetts, United States.
- Antoniak, Brandon (2016). One Dimensional Thermal Sims, MATLAB code. Retrieved Sept 25, 2017.
- Çiğengel, Yunus A., et al. *Fundamentals of Thermal-Fluid Sciences*. McGraw-Hill Higher Education, 2012.
- Structural Requirements and Recommendations for Balloon Gondola Design - Columbia Scientific Balloon Facility/NASA
- Zemax User Manual - <https://neurophysics.ucsd.edu/Manuals/Zemax/ZemaxManual.pdf>
- Battery Configuration Characteristics - [ftp://apollo.ssl.berkeley.edu/pub/jolson/COSI\\_final\\_report/Final\\_report/CSBFGondolaDesignRecommendations%20newer%20version.pdf](ftp://apollo.ssl.berkeley.edu/pub/jolson/COSI_final_report/Final_report/CSBFGondolaDesignRecommendations%20newer%20version.pdf)
- Ext Temp Sensor - <https://www.adafruit.com/product/1727>, <https://www.adafruit.com/product/270>
- Int Temp Sensor - <https://www.sparkfun.com/products/245>
- Actuator Supplier - <http://www.haydonkerkittman.com>
- Pressure Sensor - <https://www.sparkfun.com/products/9569>
- Testing Photodiode - <https://sglux.de/en/product/sg01s-18-en/>



# Table of Contents

| Sections  | Backups                                       |
|---|---|
| <a href="#">Project Purpose/<br/>Objectives</a> | <a href="#">EMCS</a>                          |
| <a href="#">Design Solutions</a>                | <a href="#">ADS</a>                           |
| <a href="#">Critical Project Elements</a>       | <a href="#">Optical Components</a>            |
| <a href="#">EMCS Design</a>                     | <a href="#">Instrument Control Components</a> |
| <a href="#">ADS Design</a>                      | <a href="#">EPS</a>                           |
| <a href="#">Optics Design</a>                   | <a href="#">DAQ</a>                           |
| <a href="#">Pointing Control Design</a>         | <a href="#">Photodiode for Testing</a>        |
| <a href="#">Other Subsystem Design</a>          | <a href="#">Pointing Angle Algorithm</a>      |
| <a href="#">Risk Analysis</a>                   | <a href="#">Parts to Manufacture</a>          |
| <a href="#">Test</a>                            |   |
| <a href="#">Project Planning</a>                |   |





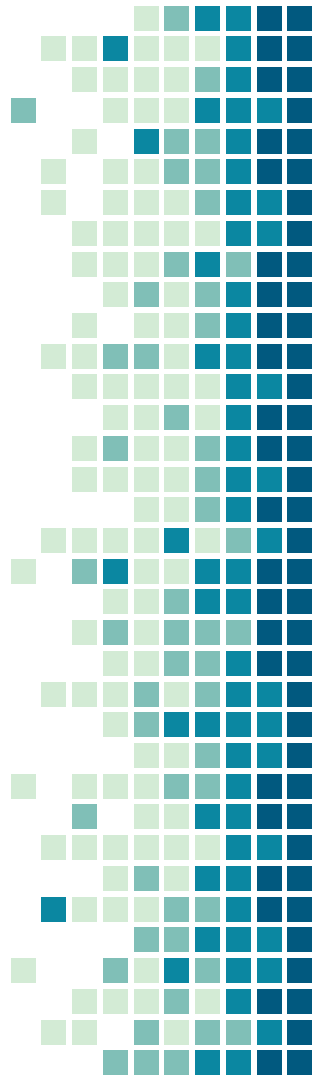
# Backups



Customer

**HAO**

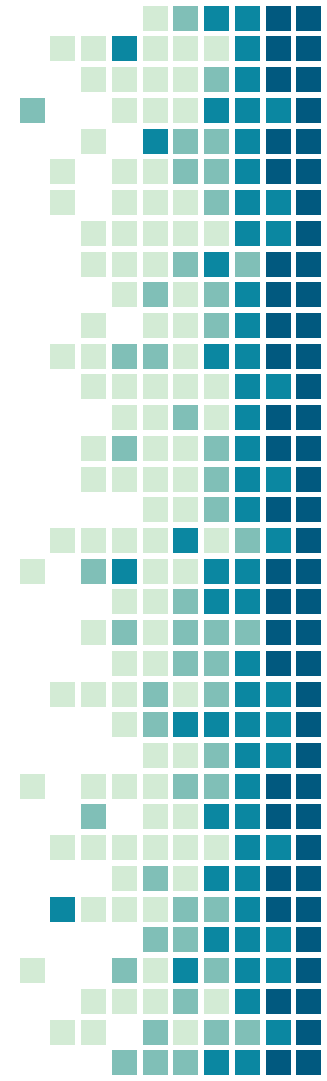
High Altitude Observatory



# Design Requirements: EMCS

## Solidworks 3D thermal modeling

- Purpose
  - Verify validity of baseline EMCS design through more robust model, alleviating bulk temperature assumptions of matlab model
  - Allows for further development and optimization of design
- Reasoning
  - Accessible program
  - Baseline knowledge within team and implementation of existing CAD model
- Methodology
  - Create highly simplified CAD model consisting of main instruments
  - Conduct partial transient thermal model at harshest environmental conditions

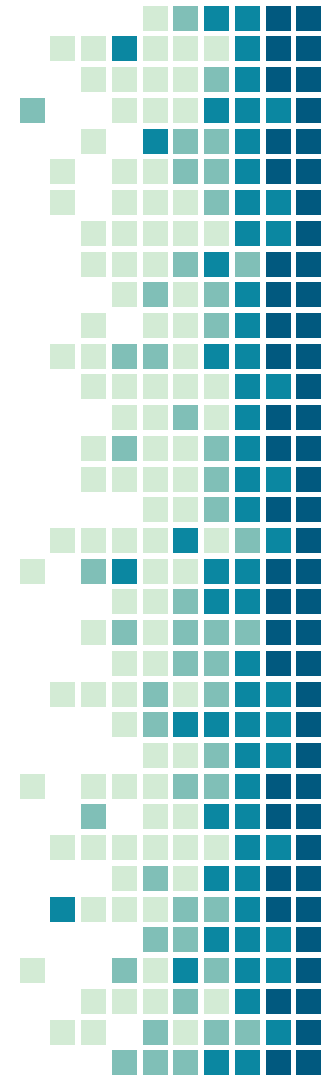
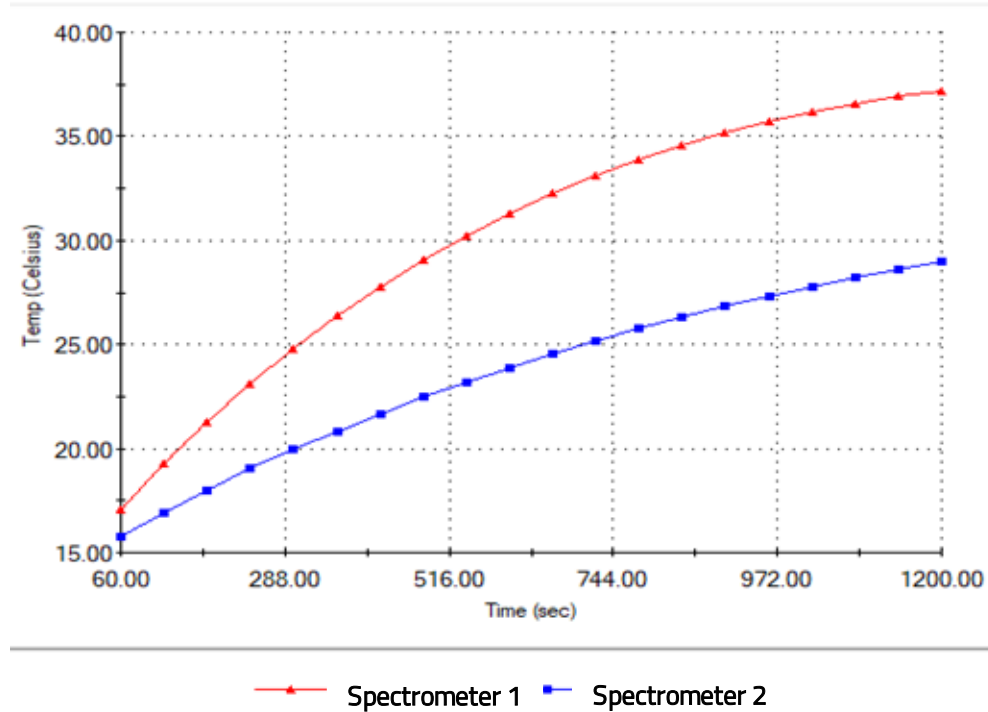


# Solidworks Result

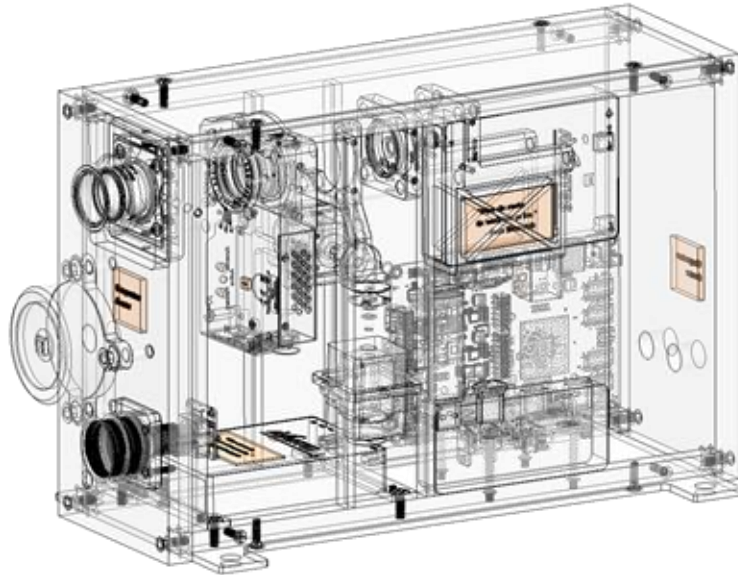
## Partial Transient Time Profile

- 30 minute stimulation
- 60 second time interval

### Spectrometer Temperature VS Time



# Environmental Monitoring & Control System



## Instrumentation

- 7 DS18B20 Temperature Sensors to measure the module's internal temperature
- 2 K-Type Thermocouples w/ Amplifier Boards to measure external environmental temperature
- MS5803-14BA Pressure Sensor to measure external environmental pressure
- HIH-4030 Humidity Sensor to measure environmental humidity
- 2-3 Kapton Resistive Pad Heaters to keep the interior of the module at an operable temperature

# Relevant Thermal Equations

## Radiated Heat

$$\sigma = 5.67 \times 10^{-8} \frac{W}{m^2 \cdot K^4}$$

$$\dot{Q} = \sigma AT^4 \epsilon$$

## Convection

$$Nu(Ra, Pr) = \frac{g C_p \rho (T_s - T_\infty) L_c^3}{k \nu}$$

$$h = \frac{k}{L_c} Nu$$

## Absorbed Heat

$$\dot{Q}_{in} = \dot{Q}_{Source} A \alpha$$

$$\dot{Q}_{Ground} \approx 1050 [W/m^2]$$

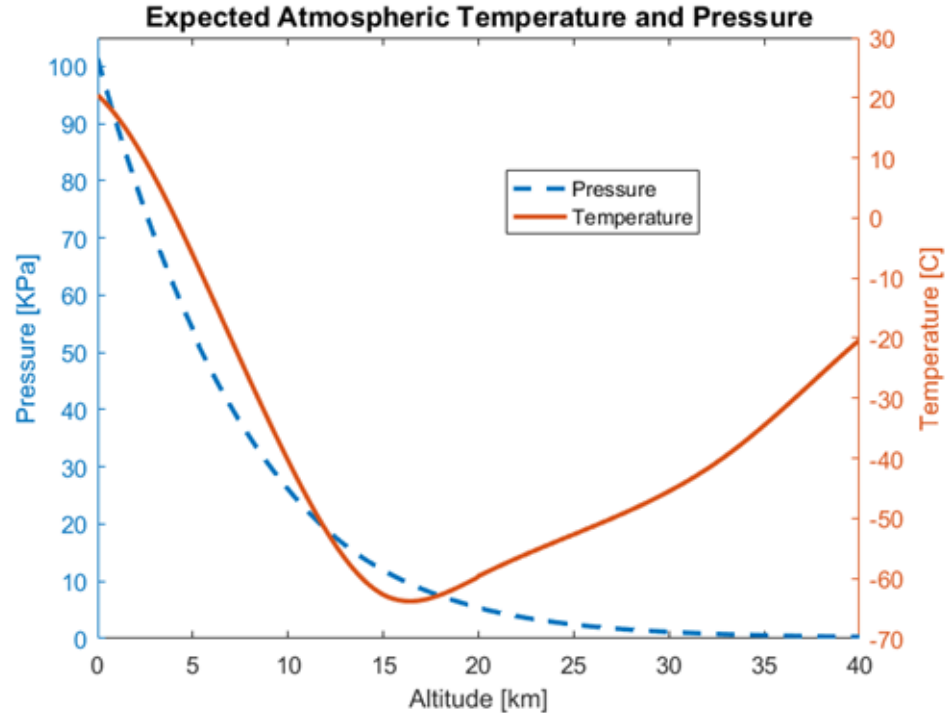
$$\dot{Q}_{Ground+Albedo} \approx 1120 [W/m^2]$$

$$\dot{Q}_{Vacuum} \approx 1367 [W/m^2]$$



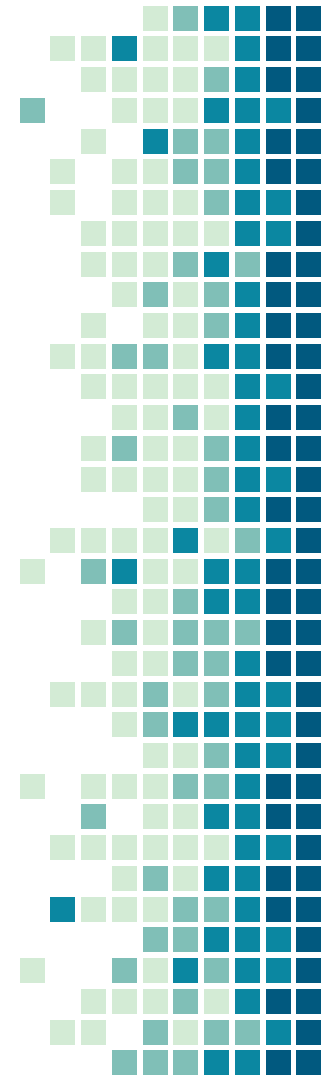
# Atmospheric Model

- Flight conditions for Fort Sumner, NM launch
- Based on 2001 US Navy Model (temperature) & COESA Model (Pressure)



# EMCS Feasibility: Pressure

| Component       | Minimum Pressure Rating (Pa) |
|-----------------|------------------------------|
| Actuators       | 0.1                          |
| Polarizer Mount | 0.133                        |
| ADS Sensor      | 5                            |
| Pressure Sensor | 0                            |





# EMCS Feasibility: Pad Heaters

## ➤ Omega Polyimide Film Insulated Flexible Heaters

- 28 V supply voltage, 0.357 A max supply current
- 10 x 2.5 x 0.025 cm dimensions
- 0-10 W evenly distributed heat output each



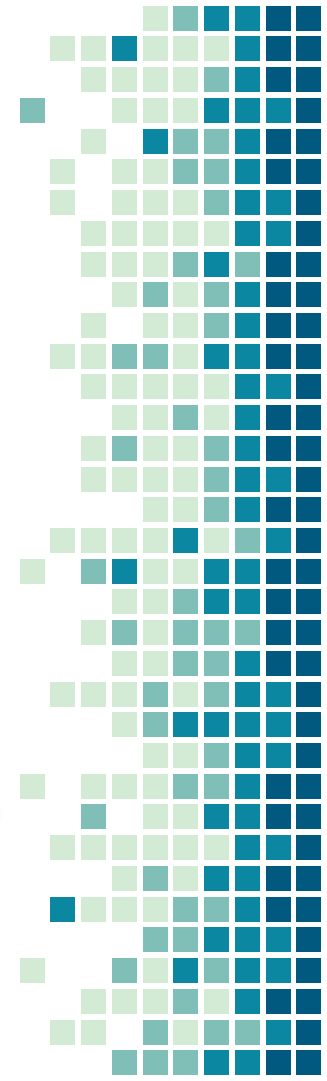
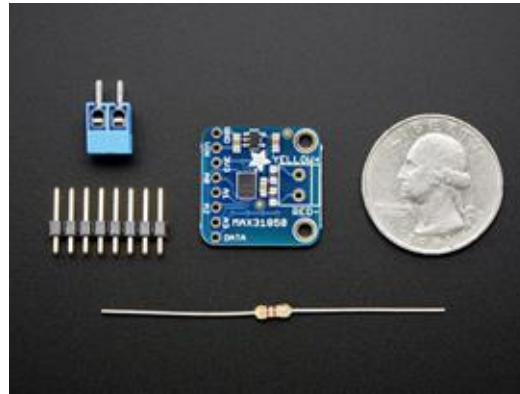
# EMCS Feasibility: Temperature Sensors

- External Temperature:  
K-type thermocouples  
w/ amplifier boards



- Internal Temperature:

7x DS18B20 One Wire Digital  
Temperature Sensors (Same as  
RADIANCE)



# EMCS Feasibility: Pressure Sensor

- **Sparkfun MS5803-14BA**
  - 0 to 1400 kPa operating pressure
  - 1.8 to 3.6 V operating voltage
  - I2C interface



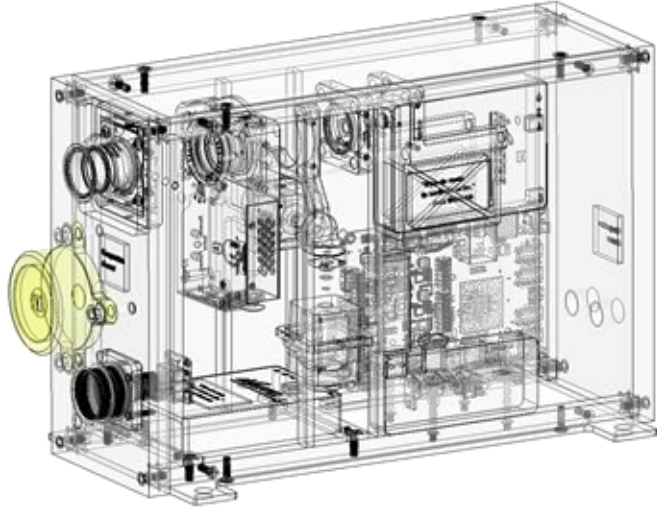
# EMCS Feasibility: Humidity Sensor

## ➤ **Sparkfun HIH-4030**

- 0 to 100% relative humidity measurement
- 4 - 5.8 V supply voltage
- Analog output



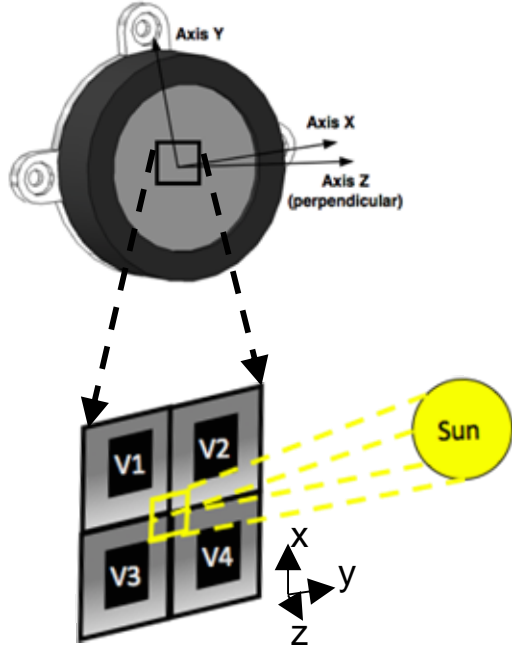
# System Overview



## Sun Sensor

- Determines Sun's position in the system FOV for optics control
- Photocurrent generation to determine off-sun angles
- Field of View: dual axes  $\pm 5^\circ$
- Accuracy:  $\pm 0.005^\circ$
- Serial RS 485 Communication
- Bit Rate: 19200 bps
- 0.05 mbar certified
- $-40$  to  $85^\circ\text{C}$  operating temperature

# Attitude Determination Feasibility



## Solar Mems Sun Sensor

- Measures Incident Angle
- Uses Quadrant photodetector
- Photocurrents generated
- Field of View: Dual Axes  $\pm 15^\circ$
- Accuracy:  $\pm 0.02^\circ$

## Calibration

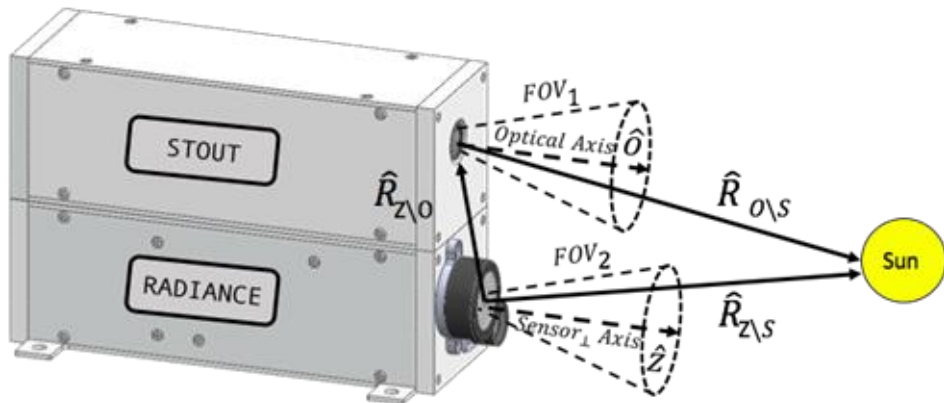
- Telescope w/ high-precision sidereal tracking
- Control telescope to get max power generation
- Determine off sun angle, program as zero degree position



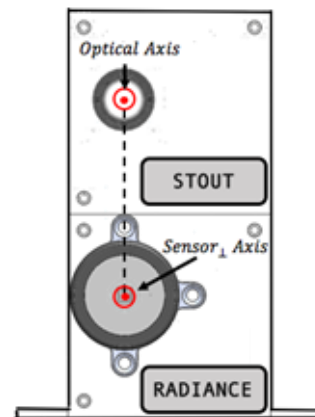
# Attitude Determination Thermal Expansion

Purpose: Solve Off-Sun Angles

Side View



Front View



## Assumptions

Sun within  $\pm 15^\circ$  of optical axis  
(given by customer)

## Given

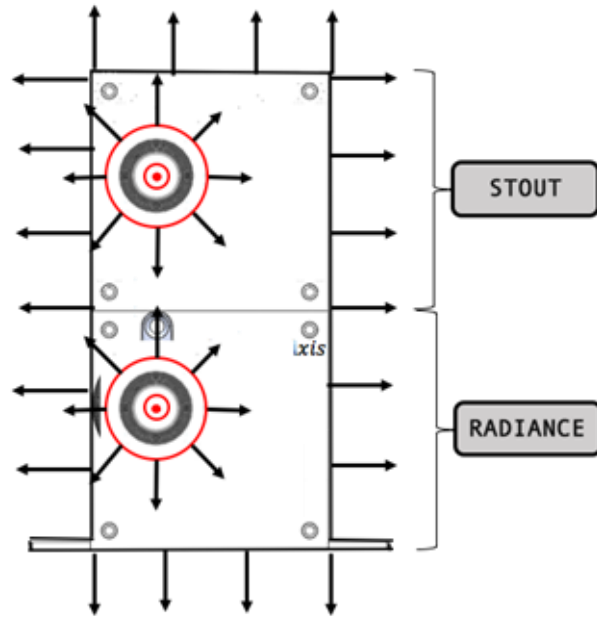
$$\hat{o} = \hat{z}, \hat{R}_{o\setminus s}, \hat{R}_{z\setminus s} \gg \hat{R}_{s\setminus o}$$

- $\hat{R}_{o\setminus s} = \hat{R}_{z\setminus s}$

## Conclusion

Sun off-angles relative to Sun  
Sensor axis is equal to that of  
the optical axis

# Attitude Determination Thermal Expansion

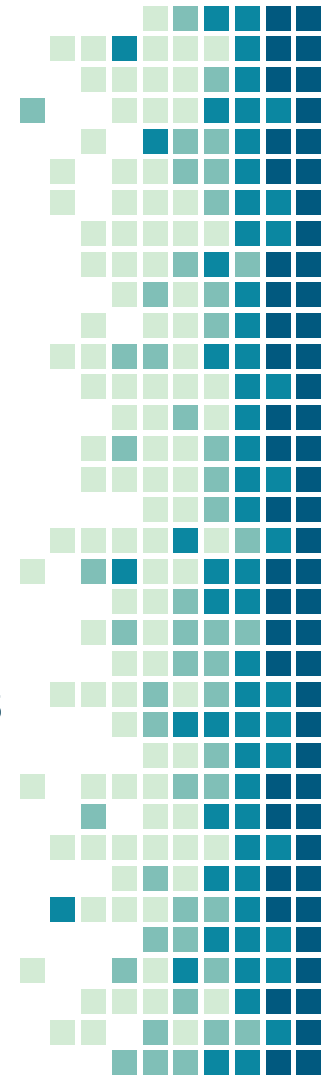


## Thermal Expansion

- Expanding material assumed uniform
- Sun Face is assumed as flat plate
- Every linear dimension increases by the same percentage with a change in temperature, including holes.

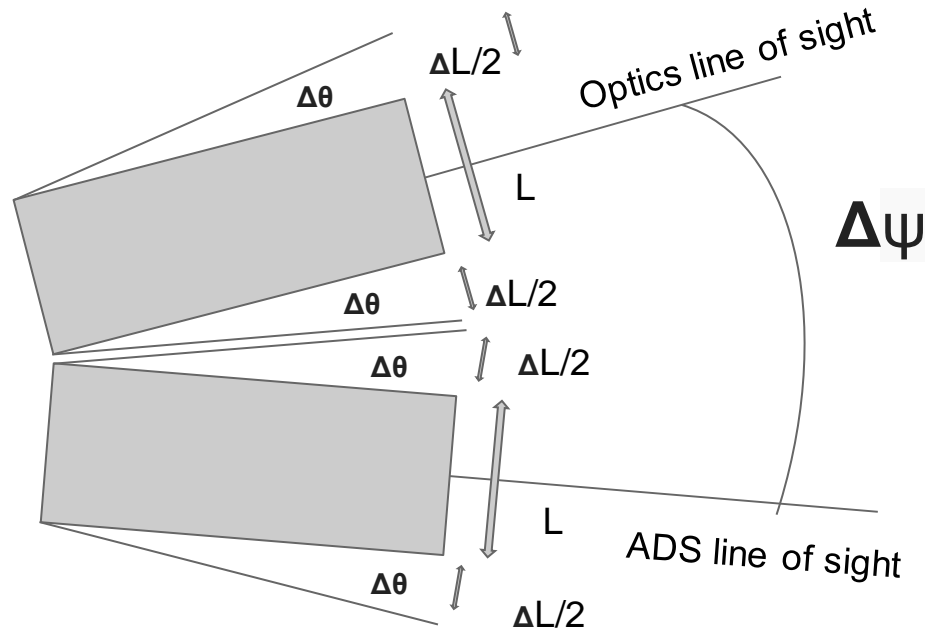
## Conclusion

- Expansions assumed negligible so long as linear expansion and no bending (Explained on next slide)

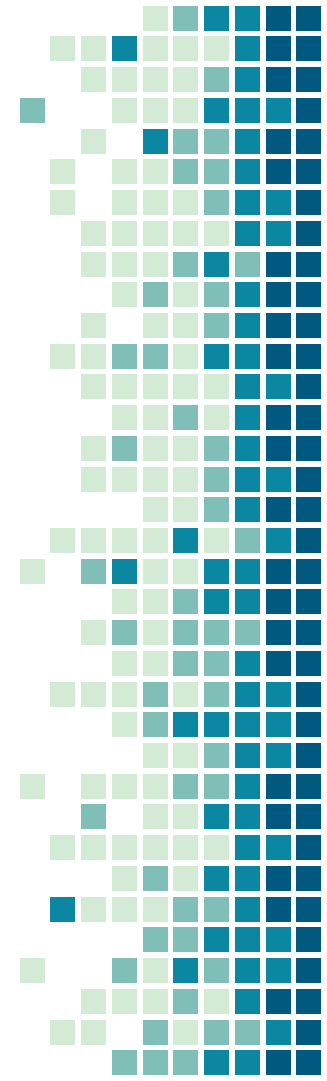




# Attitude Determination Thermal Expansion

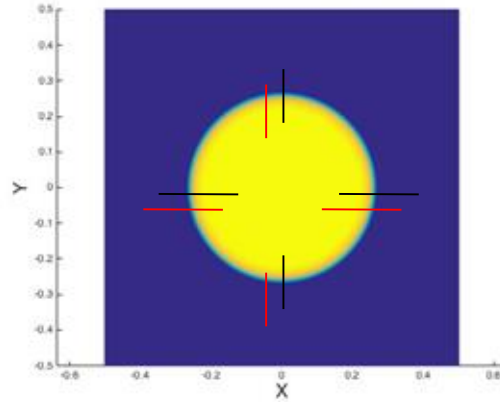
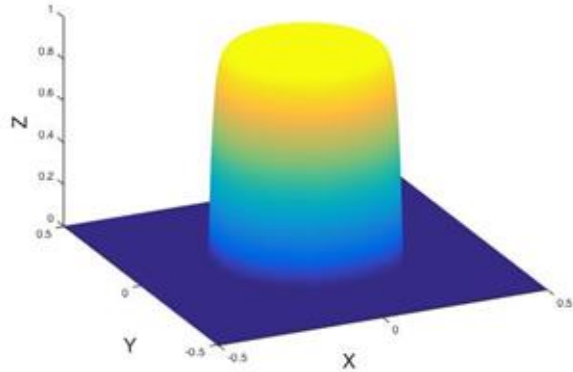


At an extreme variation in temperature where the front sun facing side is  $20^\circ\text{K}$  warmer than back side, the difference in optics and ADS line of sight will only be  $\Delta\psi = 0.00886^\circ$

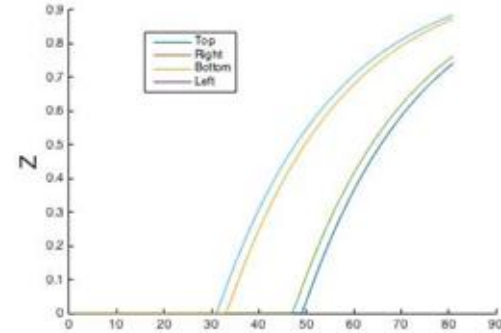


# ADS Calibration Plan Model

Brightness Map of Sun

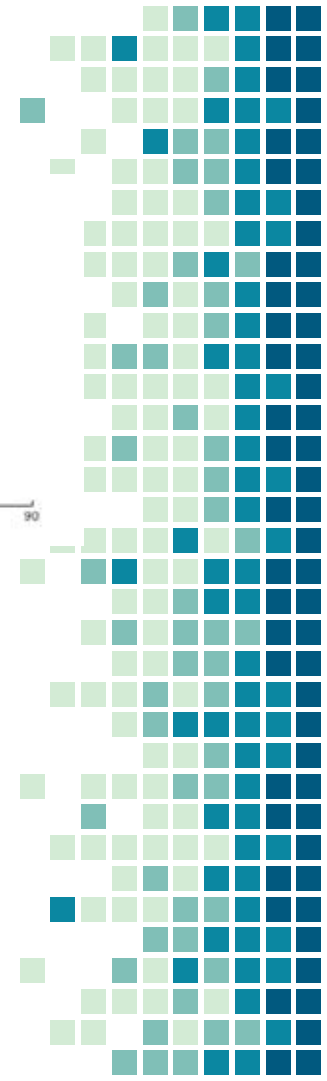


Photodiode measurements along **red lines**



## Model Process

- Build mock brightness map of the Sun in MATLAB, value of 1 at center and drop sharply to zero at edges
- Sample line of data at top, bottom, left, and right edges of Sun (black lines) with offset in X and Y coordinates (red lines, represent what optical axis "sees")
- View functions from sample lines and find offset from these functions
- Vary model to account for various decreases in brightness and add more outward radial sample lines



# Should Sun's Ellipticity be Accounted for?

Diameter of Sun from viewing point in degrees [Data from SunPy]

$D = 149,559,787$  km (distance from Sun to Earth)

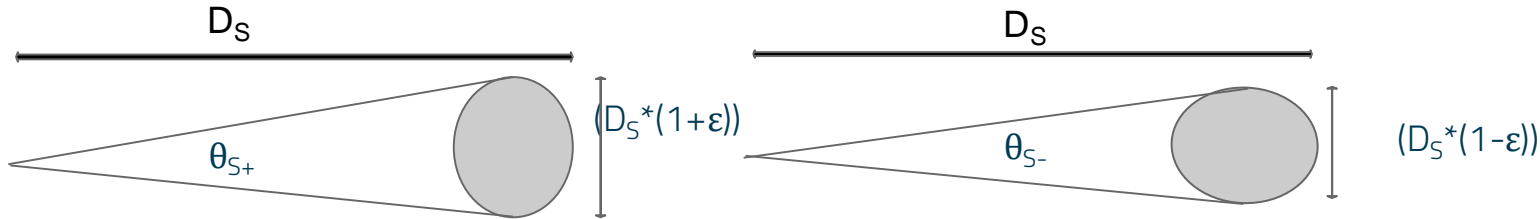
$D_S = 1,391,016$  km (Diameter of Sun)

$\epsilon = 5e-05$  (ellipticity of Sun)

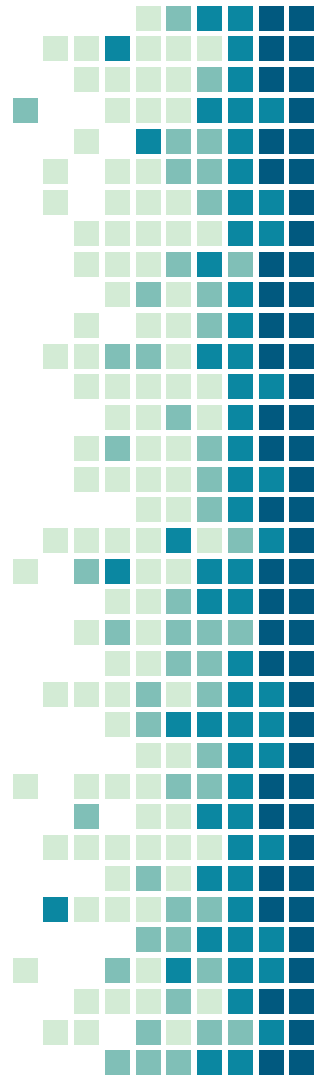
$\theta_{S+} = \tan^{-1}((D_S*(1+\epsilon))/D) = 0.532904^\circ$

$\theta_{S-} = \tan^{-1}((D_S*(1-\epsilon))/D) = 0.532851^\circ$

$\Delta\theta = |\theta_{S+} - \theta_{S-}| = 5.3e-05^\circ = \underline{0.00318}$  arc minutes



No, we can assume a perfect circle



# Lens Baseline Design

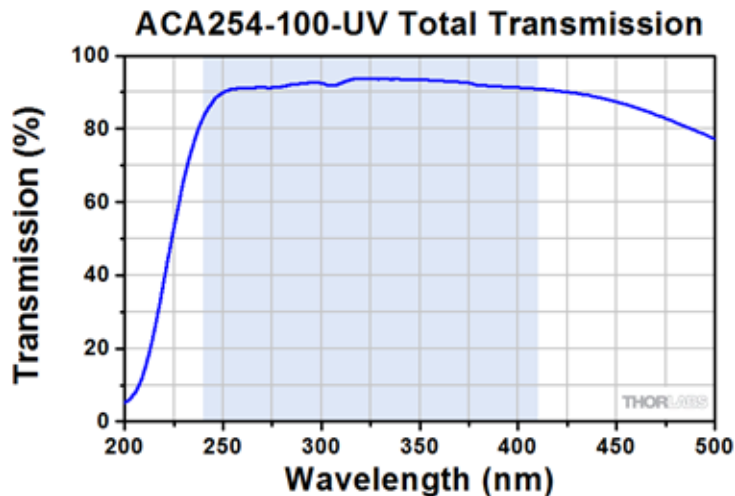
## Thorlabs ACA254-UV-150

- Air-Spaced Doublet to correct for chromatic aberrations



ACA254-100-UV

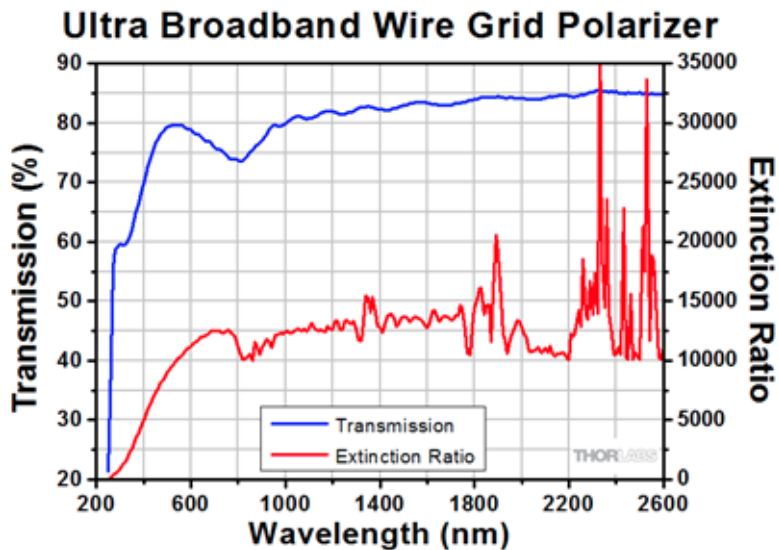
|                |       |
|----------------|-------|
| Price          | \$969 |
| Focal Length   | 150mm |
| Clear Aperture | 18mm  |



# Polarizer Baseline Design

## Thorlabs 25 mm Diameter Mounted Wire Grid Polarizer

➤ Provided by Customer

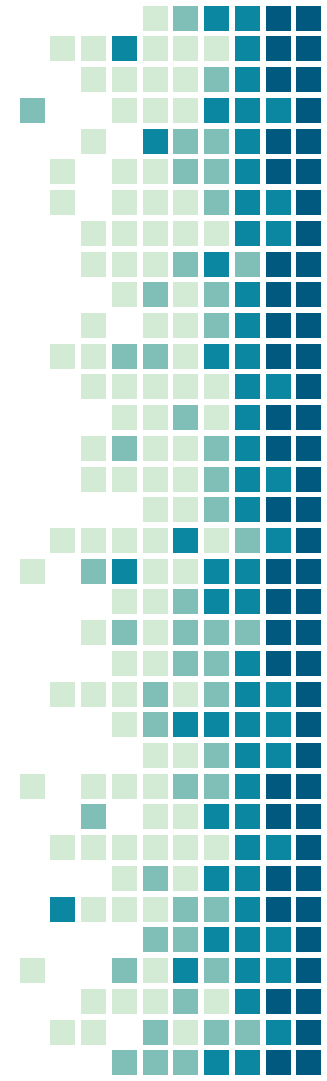


# Spectrometer Baseline Design

## Avantes Mini 2048

➤ Inherited From RADIANCE

| Avantes AvaSpec-Mini 2048L-UVI25 |                               |
|----------------------------------|-------------------------------|
| Optics                           | 200-1100nm, 1.4 nm resolution |
| Grating                          | 300 lines/mm                  |
| Slit Size                        | 25µm                          |
| Price                            | \$2946.25                     |



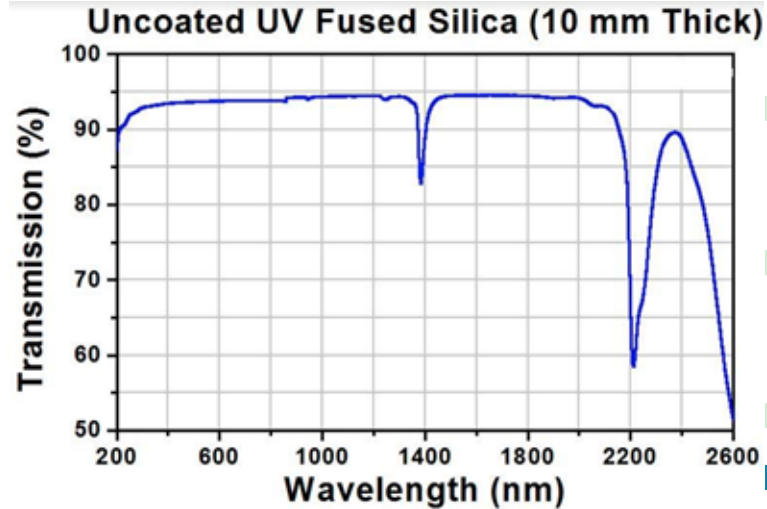
# Spectrometer Coupling Design



## Avantes COL-UV/VIS-25

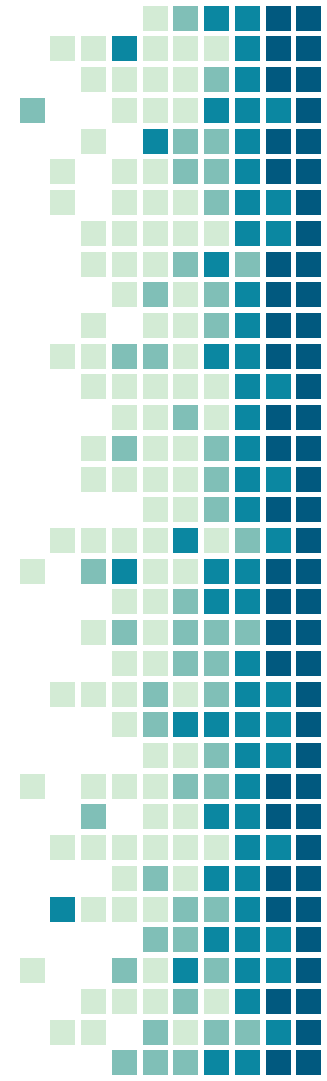
- Collimating lens attached to spectrometer delivers light from image plane to the spectrometer aperture

|          |       |
|----------|-------|
| Price    | \$600 |
| Diameter | 25 mm |
| FOV      | ~25°  |



# Polarizer Mount

| Key Specifications              |               |
|---------------------------------|---------------|
| Maximum Speed                   | 10 deg/sec    |
| Minimum Speed                   | 0.005 deg/sec |
| Repeatable Incremental Movement | 0.03 deg      |
| Absolute Accuracy               | +/- 0.14 deg  |





# Instrument Actuators

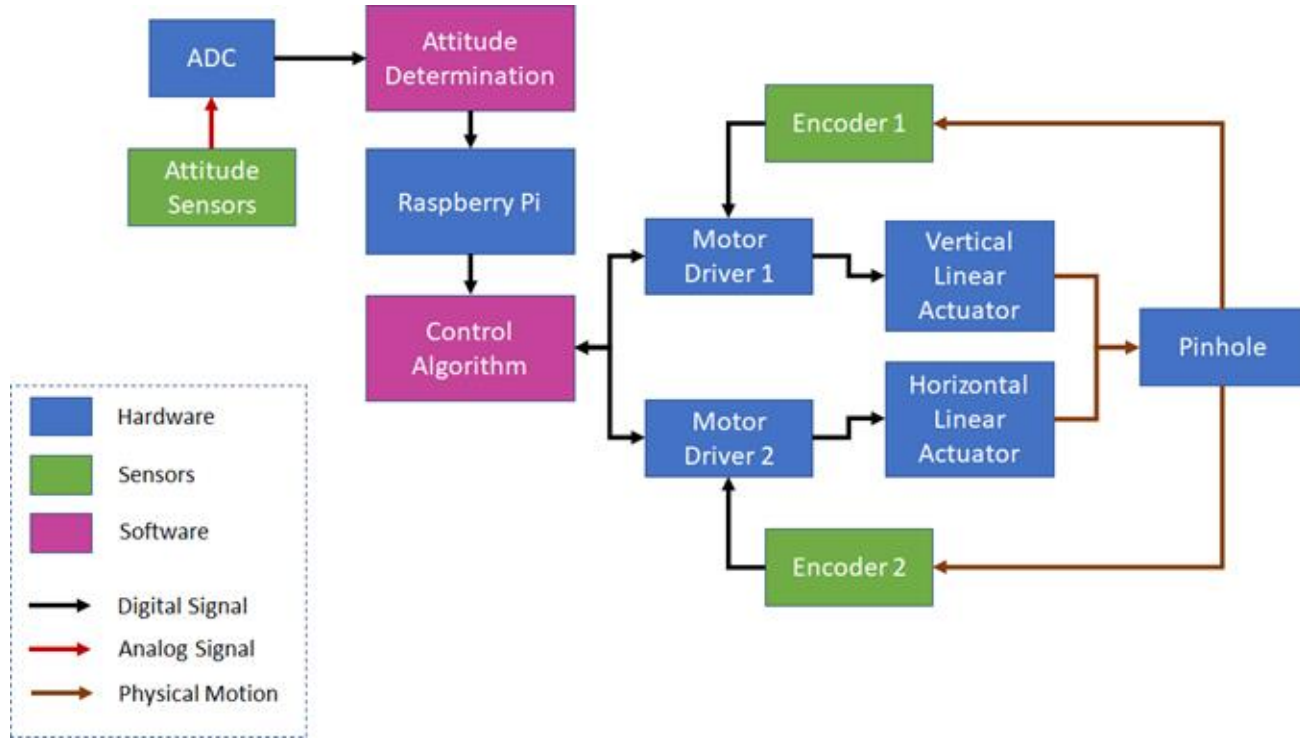
## Haydon Kerk Size 8 Type U Linear Actuators

- Non-captive for horizontal movement

| Key Specifications |                 |
|--------------------|-----------------|
| Step Size          | .0015 mm        |
| Dimensions         | 28.8 mm x 20 mm |
| Max Displacement   | 101.6 mm        |



# Functional Block Diagram - Controls



# Battery Baseline Design

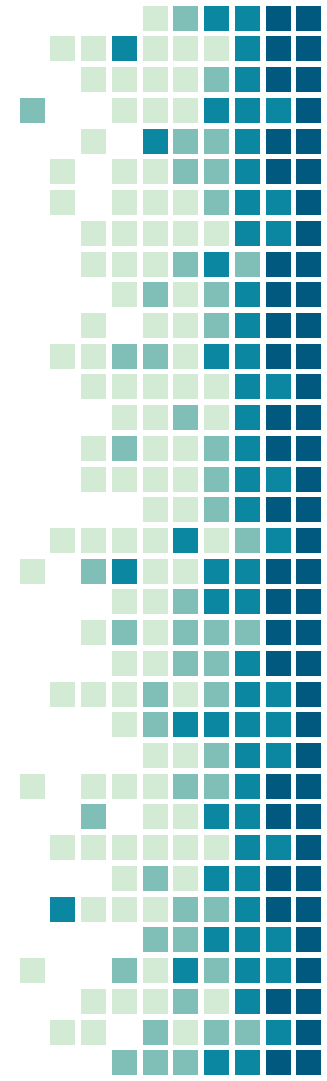
Table 3 Battery Types

| Battery  | Cells per Pack | Loaded Voltage | Ampere Hour* |
|----------|----------------|----------------|--------------|
| B7901-10 | 10             | 26             | 30           |
| B7901-11 | 11             | 29             | 30           |
| B7901-12 | 12             | 32             | 30           |
| B9660    | 10             | 26             | 7            |
| B9525    | 5              | 14             | 7            |
| B9808    | 4              | 11.2           | 1            |
| G20-12   | 1              | 2.6            | 7            |
| G62-12   | 1              | 2.6            | 30           |

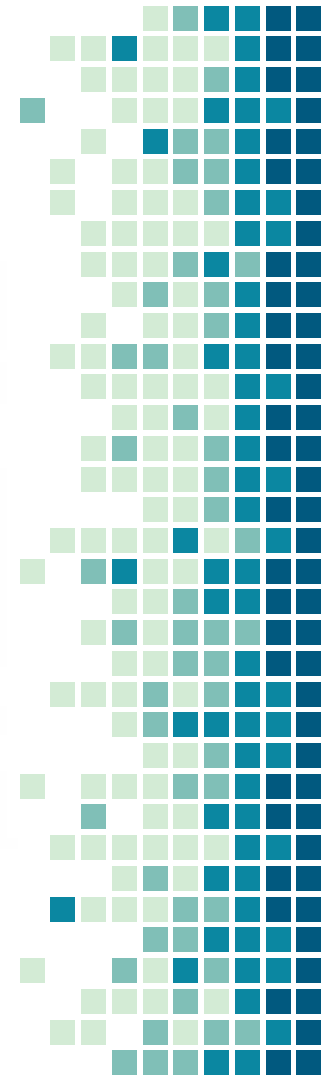
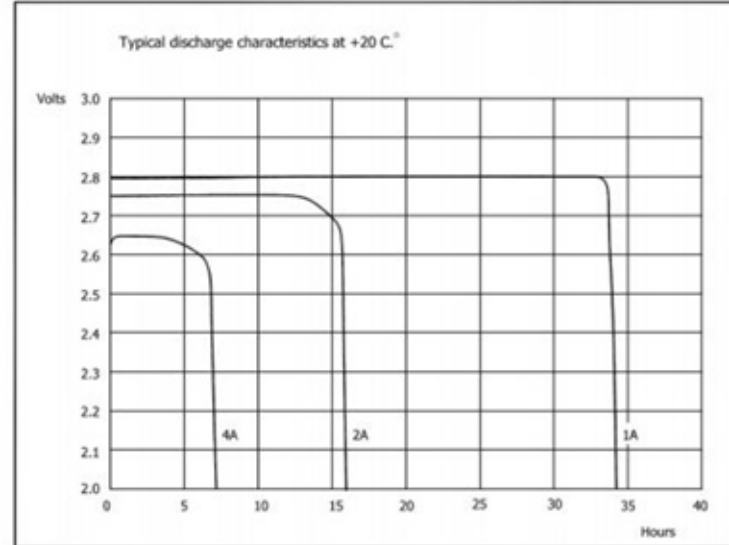
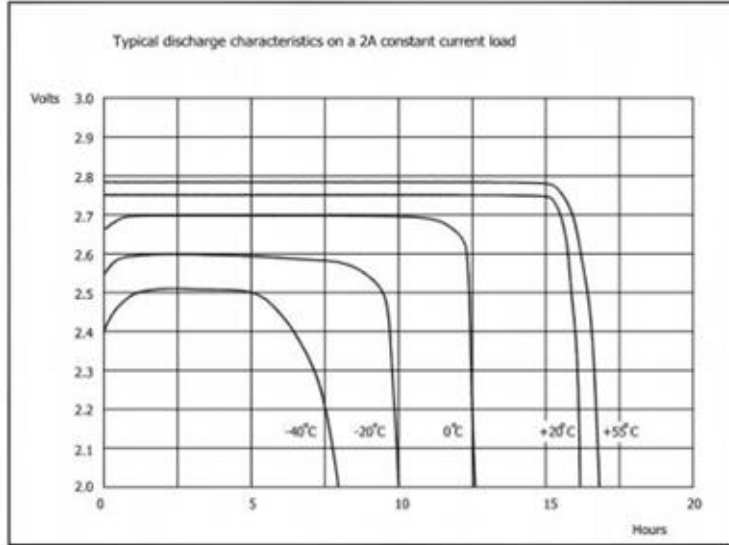
\* De-rate ampere hour ratings for temperatures below -20°C.

Size (ASA Designation) .. N/A  
Length ..... 141.0mm  
Diameter ..... 41.7mm  
Weight ..... 300g  
Construction ..... Hermetically sealed, all welded steel casing, incorporating a safety vent and a glass to metal seal

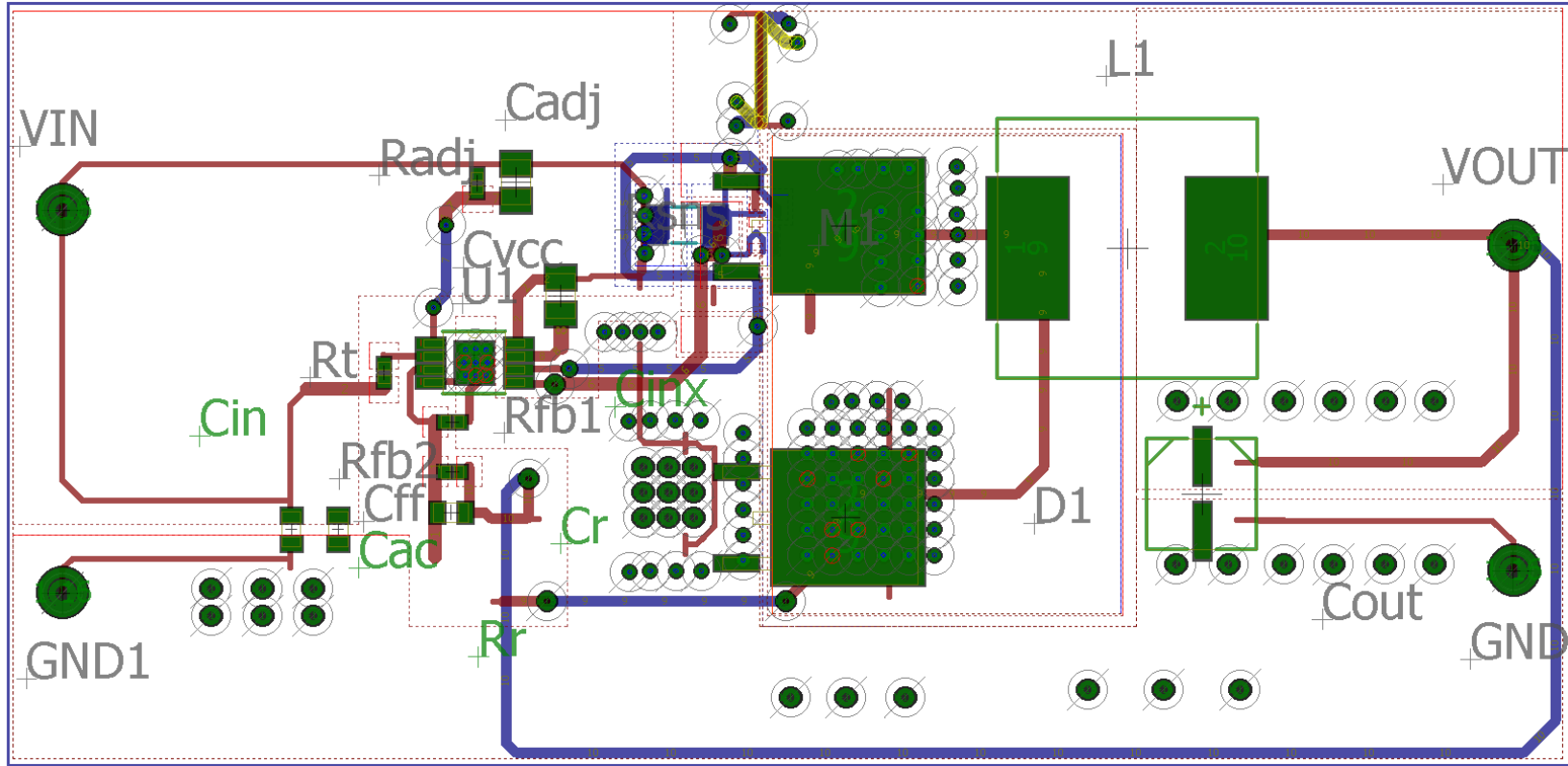
Voltage ..... Nominal 3.0 volts  
Typical operating  
Voltage ..... 2.65 - 2.80 volts  
Capacity (1000mA - 2.0v) ..... 34Ah  
50% capacity achieved at ..... 8000mA  
Temperature range ..... -50°C + 70 °C  
Shelf life at ambient temperature ... 10 years  
Self discharge ..... Typical 2% p.a.



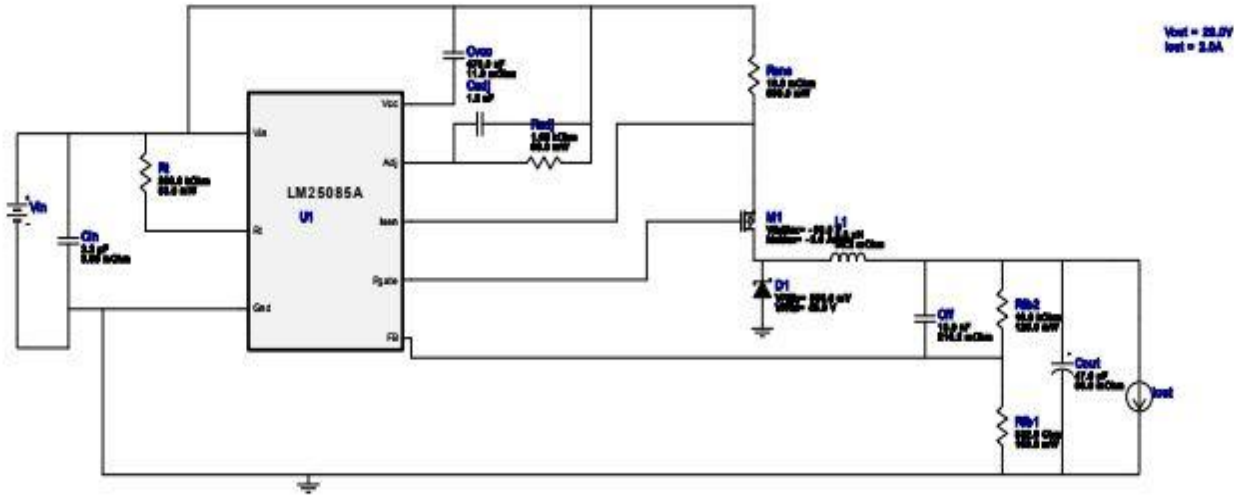
# Power Feasibility: Batteries



# Power PCB Design



# Converter Specifications: 29 V to 28 V

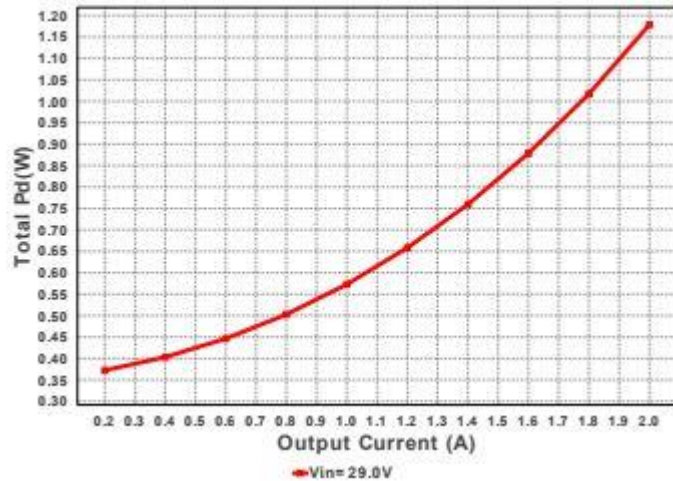


VinMin = 29.0V  
VinMax = 29.0V  
Vout = 28.0V  
Iout = 2.0A

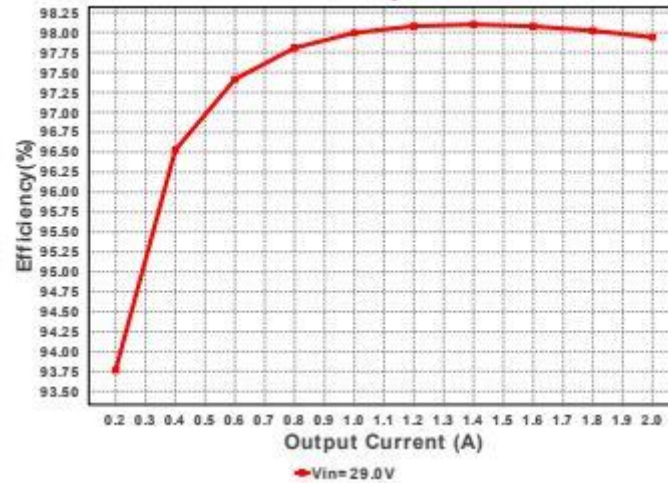
Device = LM25085AMY/NOPB  
Topology = Buck  
Created = 2017-11-29 16:04:52.713  
BOM Cost = \$2.18  
BOM Count = 14  
Total Pd = 1.17W

# Converter Specifications: 29 V to 28 V

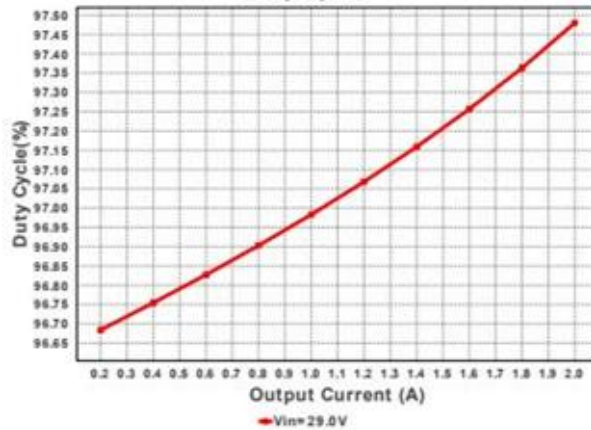
Total Pd



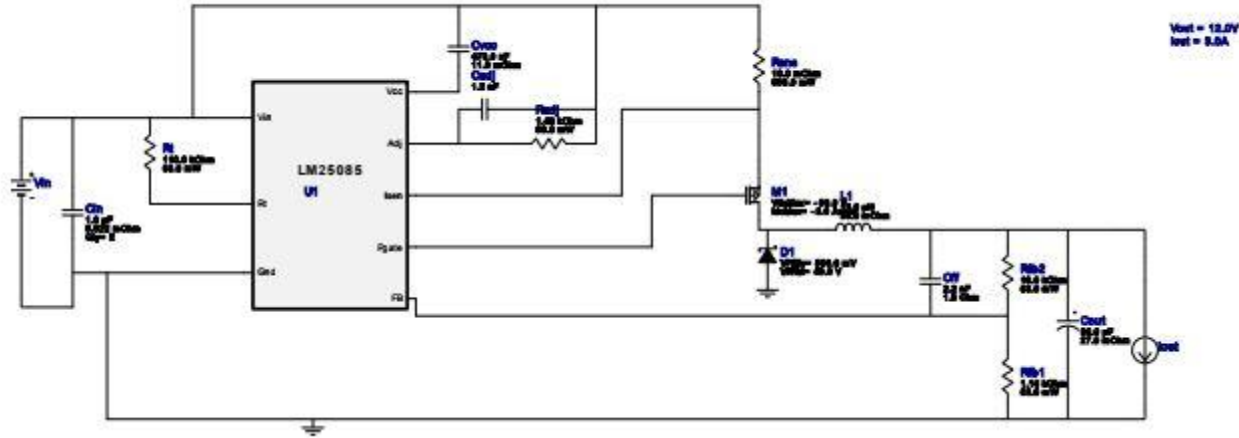
Efficiency



Duty Cycle



# Converter Specifications: 28 V to 12 V

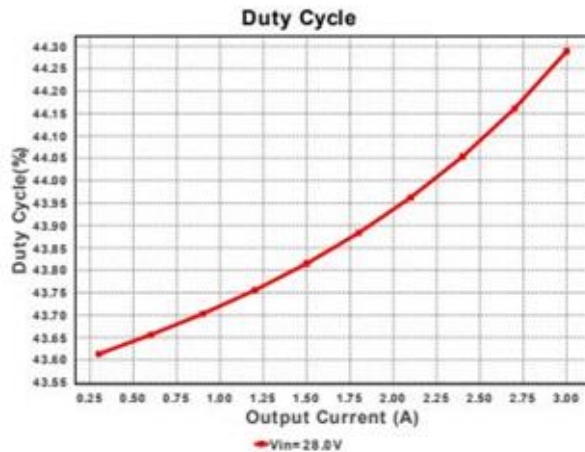
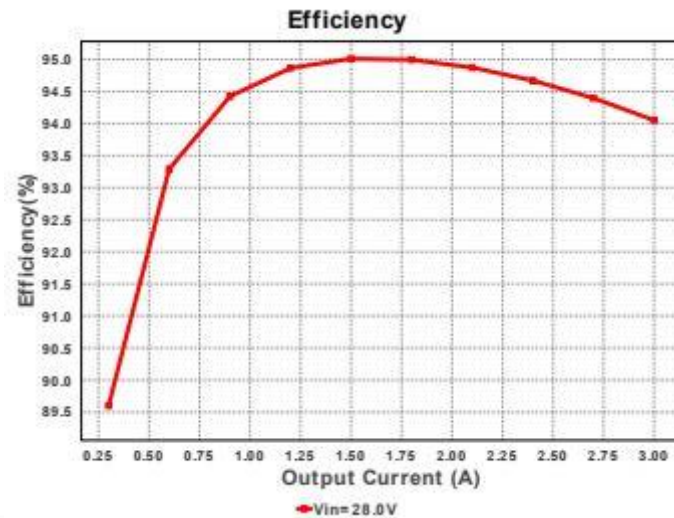
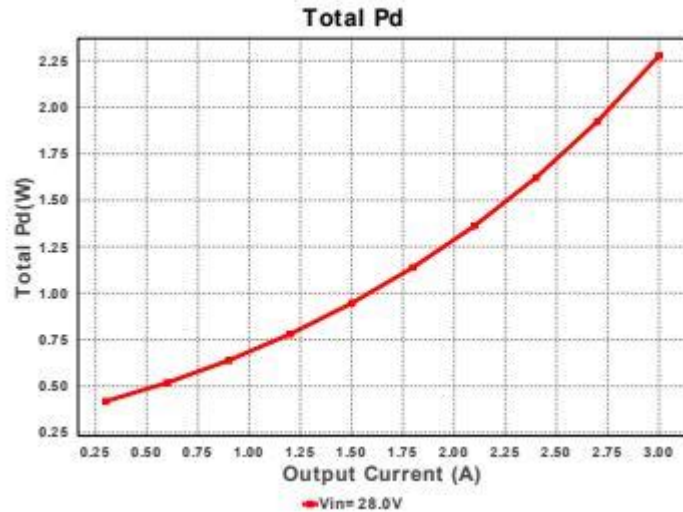


VinMin = 28.0V  
VinMax = 28.0V  
Vout = 12.0V  
Iout = 3.0A

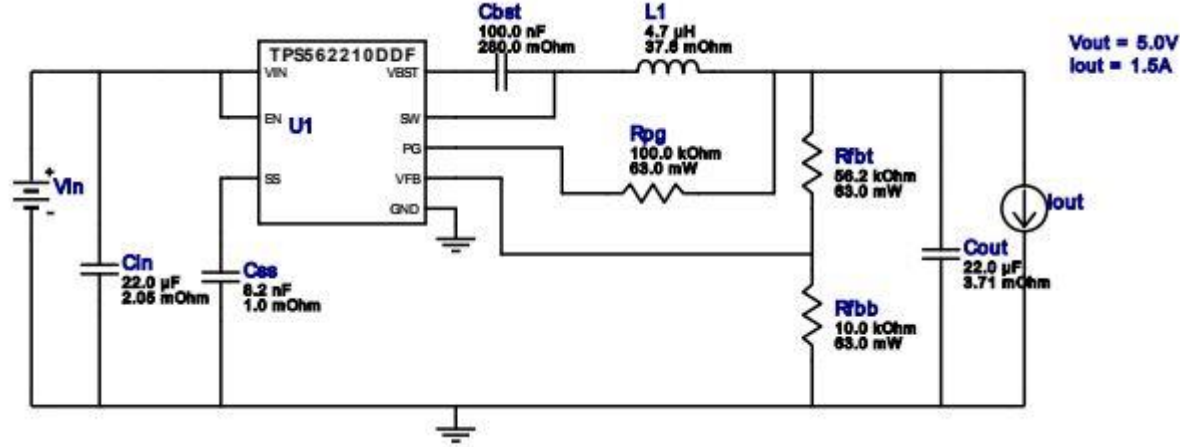
Device = LM25085MY/NOPB  
Topology = Buck  
Created = 2017-11-29 16:06:10.910  
BOM Cost = \$2.01  
BOM Count = 15  
Total Pd = 2.27W



# Converter Specifications: 28V to 12 V

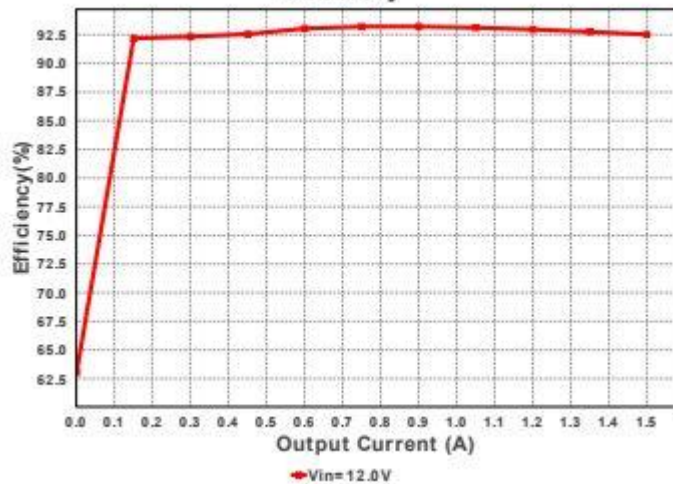


# Converter Specifications: 12 V to 5 V

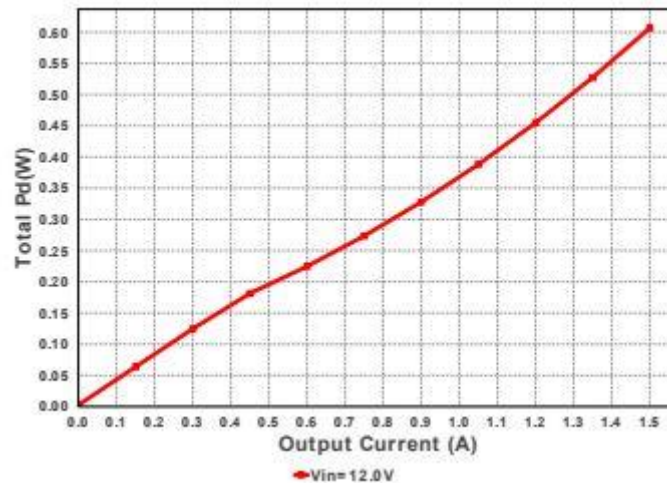


# Converter Specifications: 12 V to 5 V

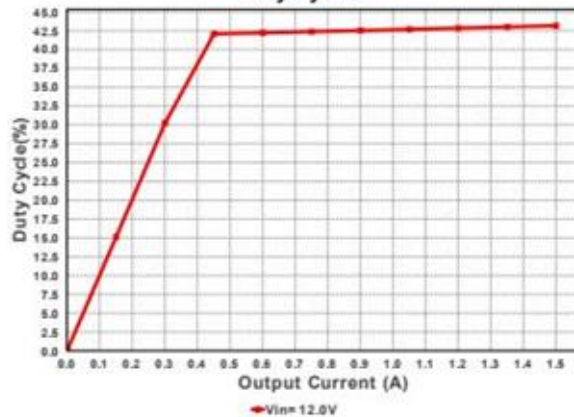
Efficiency



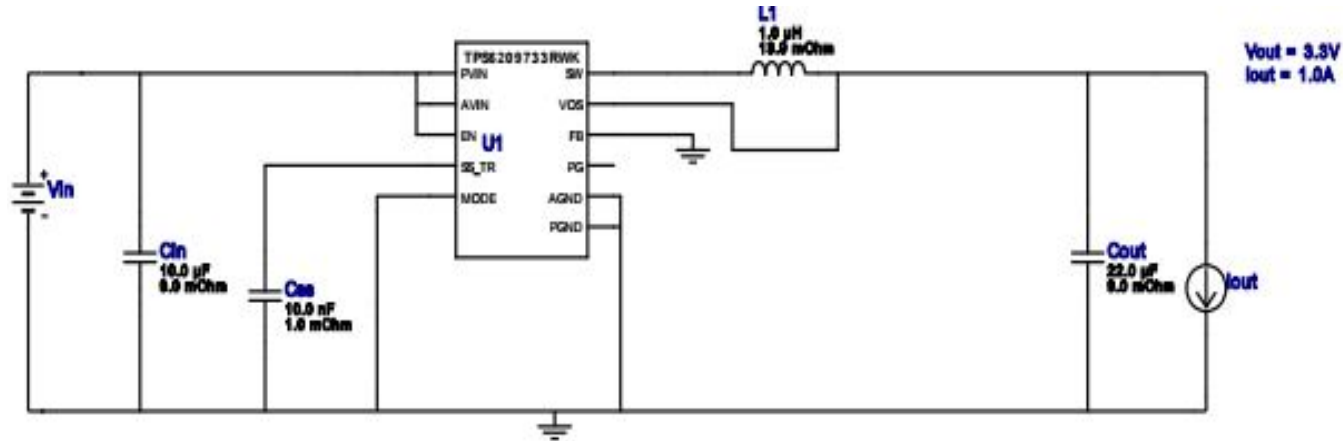
Total Pd



Duty Cycle



# Converter Specifications: 5 V to 3.3 V

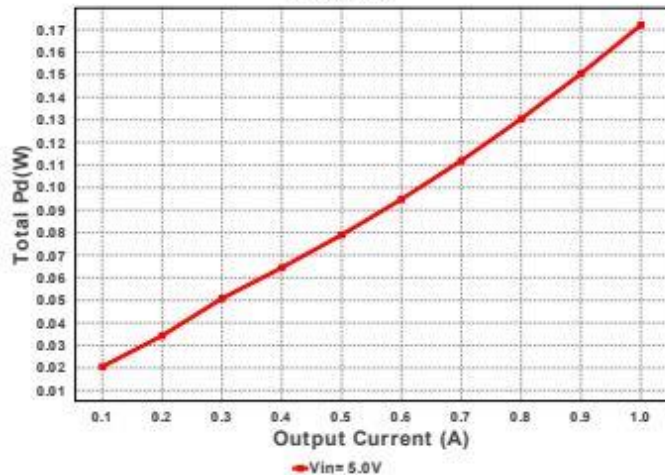


$V_{inMin} = 5.0\text{V}$   
 $V_{inMax} = 5.0\text{V}$   
 $V_{out} = 3.3\text{V}$   
 $I_{out} = 1.0\text{A}$

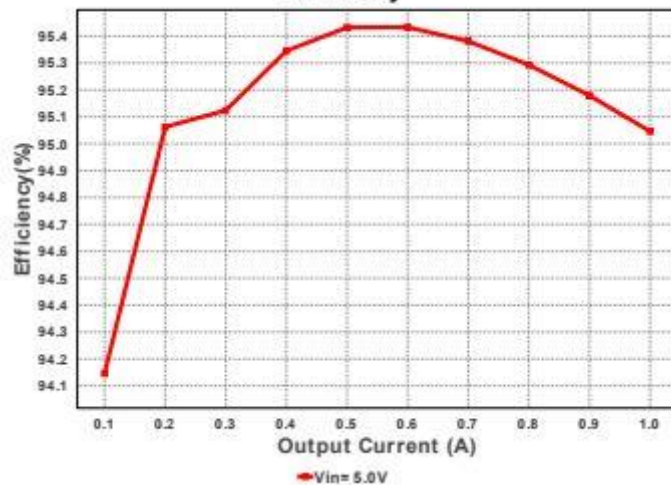
Device = TPS6209733RWKR  
Topology = Buck  
Created = 2017-11-29 16:07:26.646  
BOM Cost = \$0.99  
BOM Count = 5  
Total Pd = 0.17W

# Converter Specifications: 5 V to 3.3 V

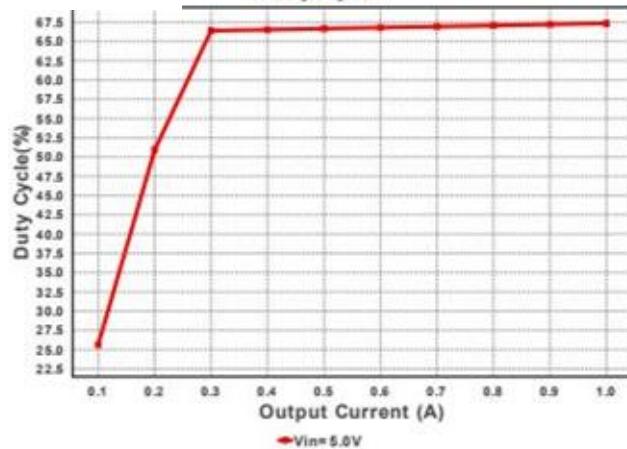
Total Pd



Efficiency



Duty Cycle

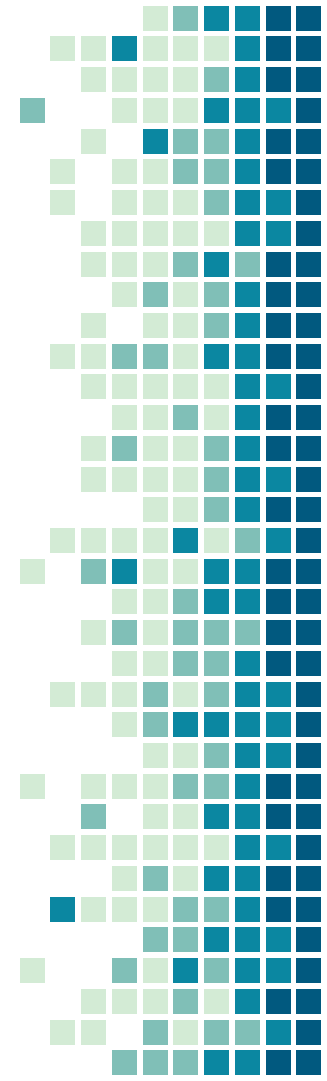


# Storage Calculations for Storage Medium

| Component     | Number of Sensors | Size of Meas. [bits] | Times Recorded | Total Data Over Flight [GB] |
|---------------|-------------------|----------------------|----------------|-----------------------------|
| External Temp | 2                 | 16                   | 1209600        | 0.0387072                   |
| Internal Temp | 7                 | 64                   | 1209600        | 0.5419008                   |
| GPS           | 1                 | 520                  | 10             | 0.0000052                   |
| Pressure      | 1                 | 24                   | 1209600        | 0.0290304                   |
| Camera        | 1                 | 600000               | 60480          | 36.288                      |
| Humidity      | 1                 | 8                    | 1209600        | 0.0096768                   |
| Spectrometer  | 2                 | 10000                | 248220         | 9.9288                      |
| ADS           | 2                 | 17                   | 6048000        | 0.205632                    |
|               |                   |                      | Total:         | 47.0417524                  |

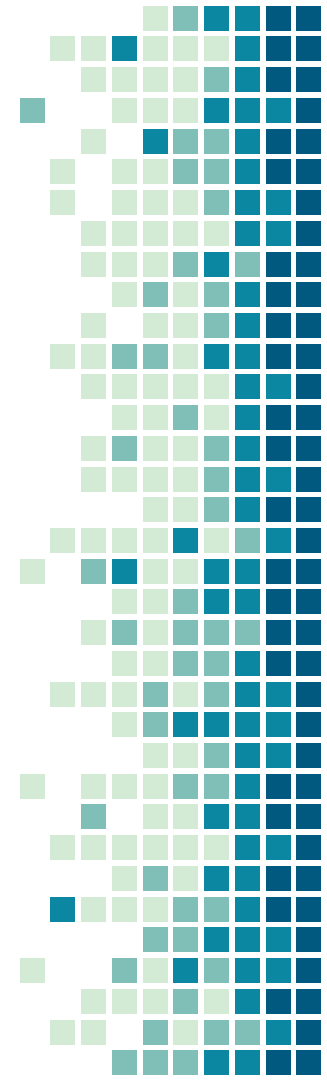
## Assumptions:

- Time of flight is two weeks=1,209,600s
- Pictures will only be taken during daytime
- Each single number measurement will be stored as a C++ double; 8 bytes



# Read Rates Calculations

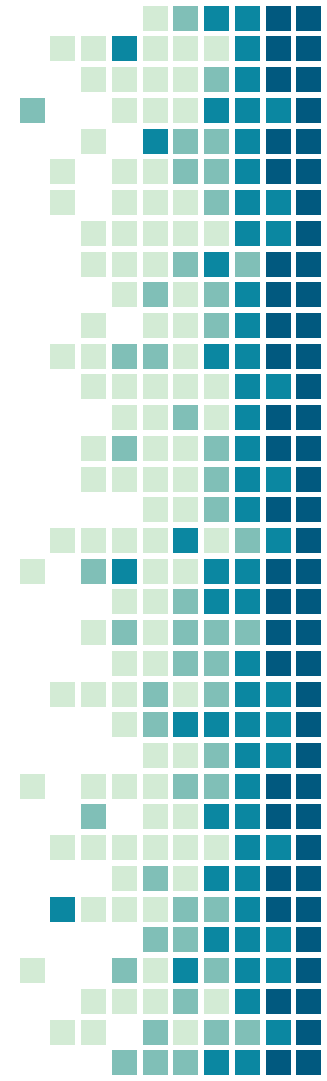
| Component     | Number of Sensors | Size of Meas. [bits] | Read Rate   | Sub Total [s] |
|---------------|-------------------|----------------------|-------------|---------------|
| External Temp | 2                 | 16                   | 100 kbit/s  | .00016        |
| Internal Temp | 7                 | 64                   | 83 ns/port  | .00000581     |
| GPS           | 1                 | 520                  | 9600 bit/s  | .0542         |
| Pressure      | 1                 | 24                   | 100 kbits/s | .00024        |
| Camera        | 1                 | 600000               | 40 MB/s     | 0.15          |
| Humidity      | 1                 | 8                    | 10 KB/s     | 0.0001        |
| Spectrometer  | 2                 | 10000                | 30 MB/s     | 0.00034       |
| ADS           | 2                 | 17                   | 9600 bits/s | 0.001770      |
|               |                   |                      | Total:      | 0.2069766433  |



# Data Storage Feasibility

## Spectrometer Data Approximation:

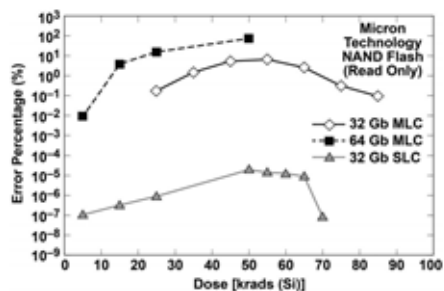
- 788 scan points on sun \* 8 polarization angles per scan
  - 6304 measurements
- 10 kB per measurement
- 63.4 MB required for full sun scan
- MX-ES 64GB SLC Flash Drive
  - Has radiative protection
- Assume 3 second integration time: 1.0945 days for full sun scan
- 12 full scans possible





# Data Storage Radiation Effect Research

- Radiation events are common at altitude
  - Graph shows that number of detected radiation events grows with altitude
  - STOUT will fly at 40km
  - Hundreds of events detected at 35 km
- Radiation Events can affect flash memory
  - Single event upsets can cause bit flips in flash memory
  - Single layer cell flash memory has less chance of having a bit flip due to a Single event upset



Source: "Single Event Effect and Total Ionizing Dose Results of Highly Scaled Flash Memories"  
<http://ieeexplore.ieee.org/stamp/stamp.jsp?arnumber=6658209>

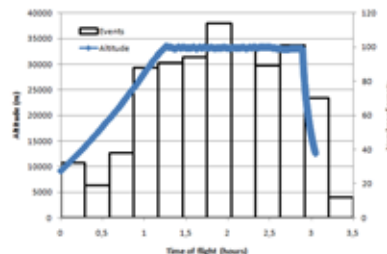


Figure 9 : Comparison between the evolution of the number of detected events as a function of time of flight and altitude profile.

Source: "Radiation Measurements in the Stratosphere" [http://spaceflight.esa.int/pac-symposium\\_archives/files/papers/s7\\_10pantel.pdf](http://spaceflight.esa.int/pac-symposium_archives/files/papers/s7_10pantel.pdf)

# Photodiode for Testing

## ➤ **SG01S-18**

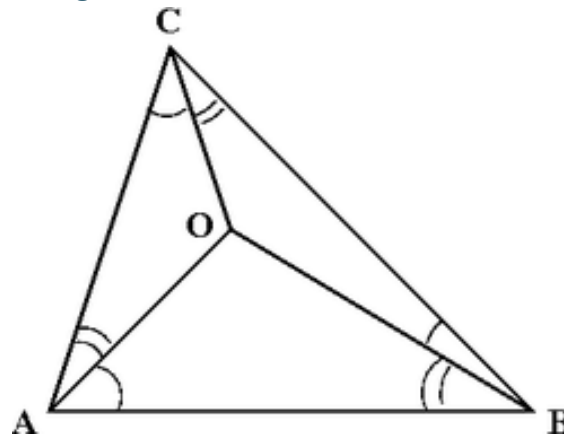
- UV broadband spectrum
- 0.06 mm<sup>2</sup> detector area
- 10 mW/cm<sup>2</sup> irradiation at 280 nm (peak responsivity)



# Pointing Angle Determination

1. Positions of A (vertical gimbal), B (front gimbal), C(horizontal gimbal) always known
2. Lengths of AB, BC, AC,BO always known
3. Knowing desired azimuth and altitude of pointing, can find vector of BO -  
[Sin(azimuth)\*Cos(altitude), -Sin(altitude), Cos(azimuth)\*Cos(altitude)] \* |BO|
1. Position and direction of actuator connections to optical cage relative to O are constant in the frame of the optical cage
1. Once O coordinates are found, can find coordinates of ball joint centers, which connect linear actuators to the optical cage. This is accomplished by rotating their vectors relative to O by the azimuth and altitude.
1. The normal of the vector between the ball joint center, and motor gimbal center is taken. This is considered to be the extension length of the two actuators. To find the actual actuator extension the actuators need to measured inside their mounting cases on their gimbals, in order to find the extension of the center of the gimbal to the edge of the motor

- A: Vertical actuator center
- B: Optics cage gimbal center
- C: Horizontal actuator center
- O: Center of actuator pushing plane

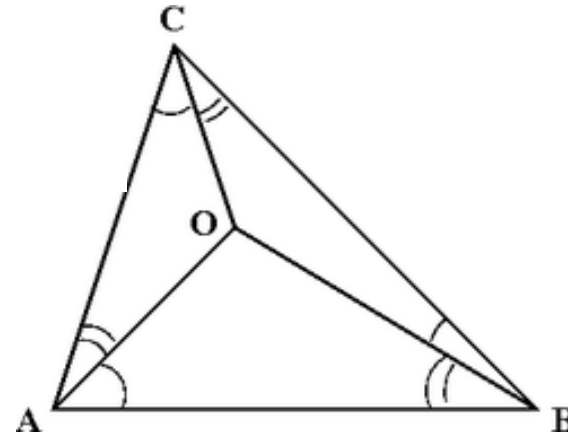


# Pointing Angle Determination

```
(*Declare positions of gimbal and ball joint centers*)
(*Offset from CAD origin*)(**)
FrontGiml = {33.7, 330.74, 381.61};
(*Center of optics cage gimbal*)
FrontGim = {0, 0, 0};
(*Center of vertical actuator gimbal*)
VertGim = {59.2, 232.47, 280.25} - FrontGiml;
(*Center of horizontal actuator gimbal*)
HorGim = {15.60, 287.47, 280.32} - FrontGiml;
(*Center of vertical actuator spherical rolling joint*)
VertBall = {66.85, 274.42, 281.73} - FrontGiml;
(*Center of horizontal actuator spherical rolling joint*)
HorBall = {54.34, 286.93, 281.75} - FrontGiml;

(*Determine lengths between nodes*)
(*Length between vertical actuator spherical rolling joint and optics gimbal*)
FVlength =  $\sqrt{\text{FrontGim.VertGim}}$ ;
(*Length between horizontal actuator spherical rolling joint and optics gimbal*)
FHlength =  $\sqrt{\text{FrontGim.HorGim}}$ ;
(*Length between vertical actuator spherical
rolling joint horizontal actuator spherical rolling joint*)
VHlength =  $\sqrt{\text{VertGim.HorGim}}$ ;
(*Distance from pointing apex to front gimbal mount*)
FApexlength = 99.86;
```

A: Vertical actuator center  
B: Optics cage gimbal center  
C: Horizontal actuator center  
O: Center of actuator pushing plane



# Pointing Angle Determination

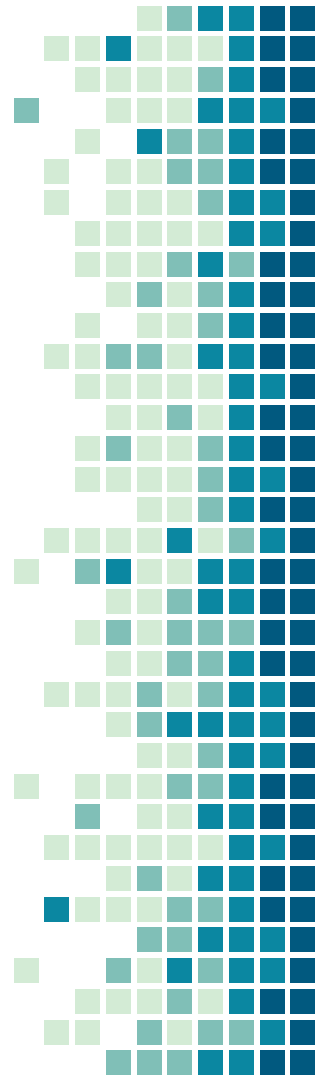
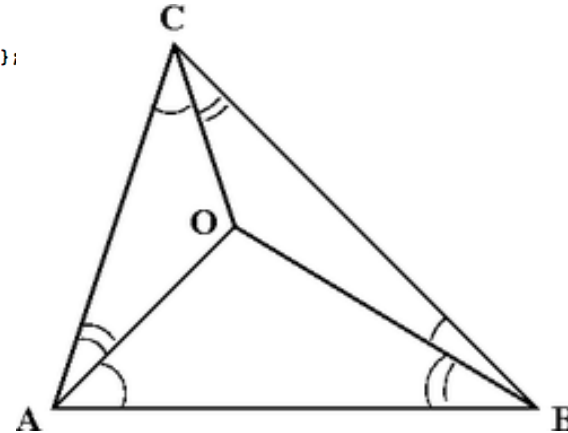
```
(*Find apex cartesian coordinates for zero degree actuation*)
ApexZero = FrontGim - {0, 0, FApexlength};
(*Vector between apex center and spherical rolling joints*)
ApexHorVec = ApexZero - HorBall;
ApexVertVec = ApexZero - VertBall;

(*Input desired deflections*)
azimuth = -1 *  $\frac{\pi}{180}$ ;
altitude = -1 *  $\frac{\pi}{180}$ ;

(*Find optical axes vector at desired pointing angles*)
normalVecUnit = {Sin[azi] * Cos[alt], -Sin[alt], Cos[azi] * Cos[alt]};
normalVec = normalVecUnit * FApexlength;

(*Find cartesian coordinates of pointing apex at desired pointing angle*)
Apex = FrontGim - normalVec;
(*Rotation matrix for vectors between apex center and spherical rolling joints*)
ConvertMat = {{Cos[azimuth], Sin[azimuth] * Sin[altitude],
  Sin[azimuth] * Cos[altitude]}, {0, Cos[altitude], -Sin[altitude]},
  {-Sin[azimuth], Cos[azimuth] * Sin[altitude], Cos[azimuth] * Cos[altitude]}};
(*Find cartesian coordinates of spherical rolling joints*)
ApexHorVecNew = ConvertMat.ApexHorVec;
ApexVertVecNew = ConvertMat.ApexVertVec;
VertBallNew = Apex - ApexVertVecNew;
HorBallNew = Apex - ApexHorVecNew;
VertBallFinal = Transpose[ConvertMat].VertBallNew;
```

- A: Vertical actuator center
- B: Optics cage gimbal center
- C: Horizontal actuator center
- O: Center of actuator pushing plane



# Pointing Angle Determination

```
HorBallFinal = Transpose[ConvertMat].HorBallNew;  
(*Find vectors between spherical rolling joints and motor gimbals*)  
HorBallGimVec = HorBallFinal - HorGim;  
VerBallGimVec = VertBallFinal - VertGim;  
(*Determine length between spherical rollings joints and motor gimbals*)  
"Vertical Length"  
VertActLength = Norm[VerBallGimVec]  
"Horizontal Length"  
HorActLength = Norm[HorBallGimVec]
```

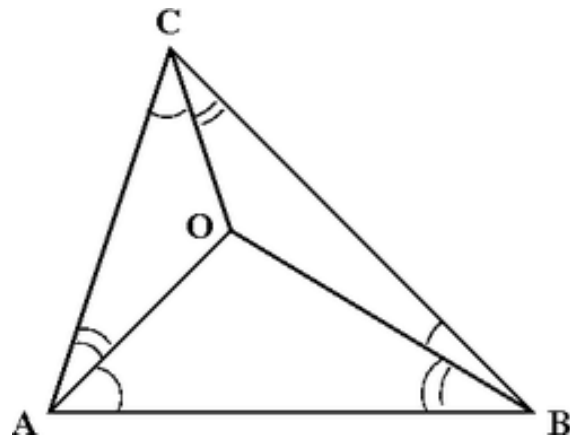
Out[156]= Vertical Length

Out[157]= 42.6675

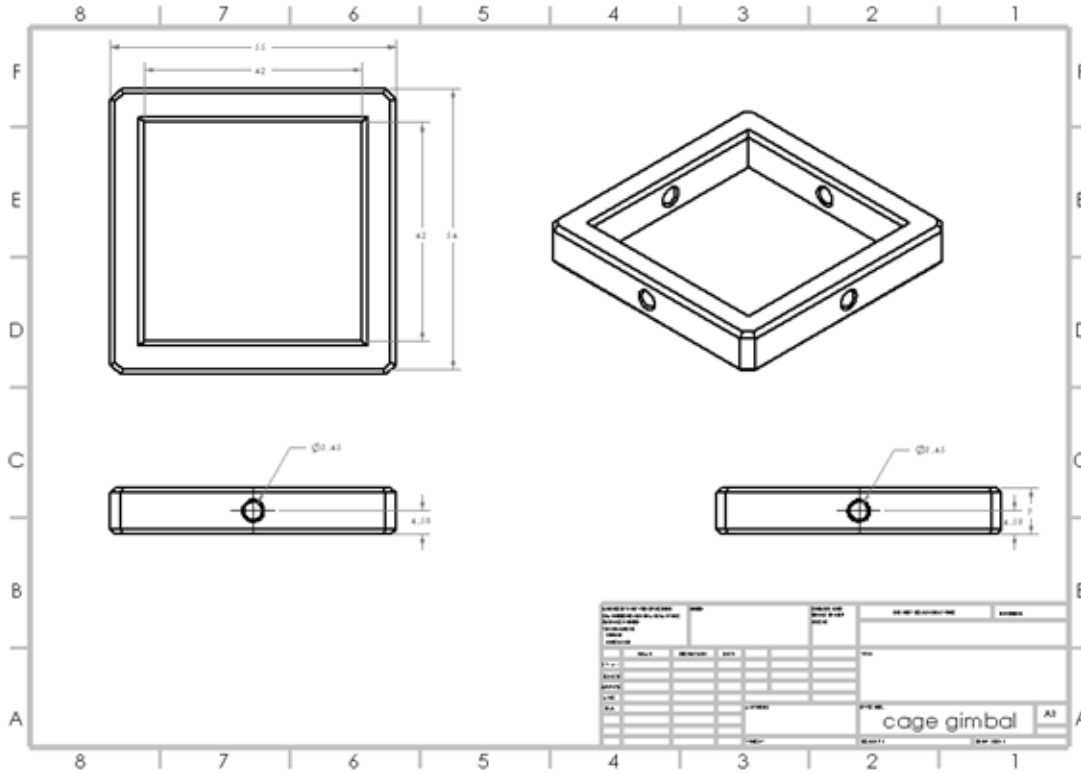
Out[158]= Horizontal Length

Out[159]= 38.7701

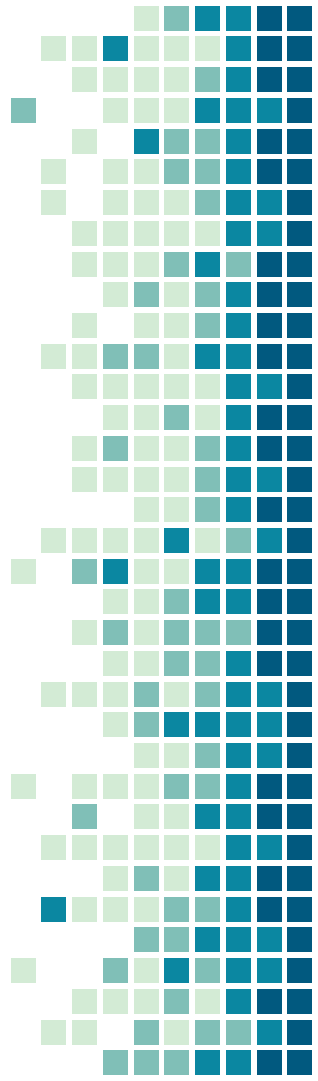
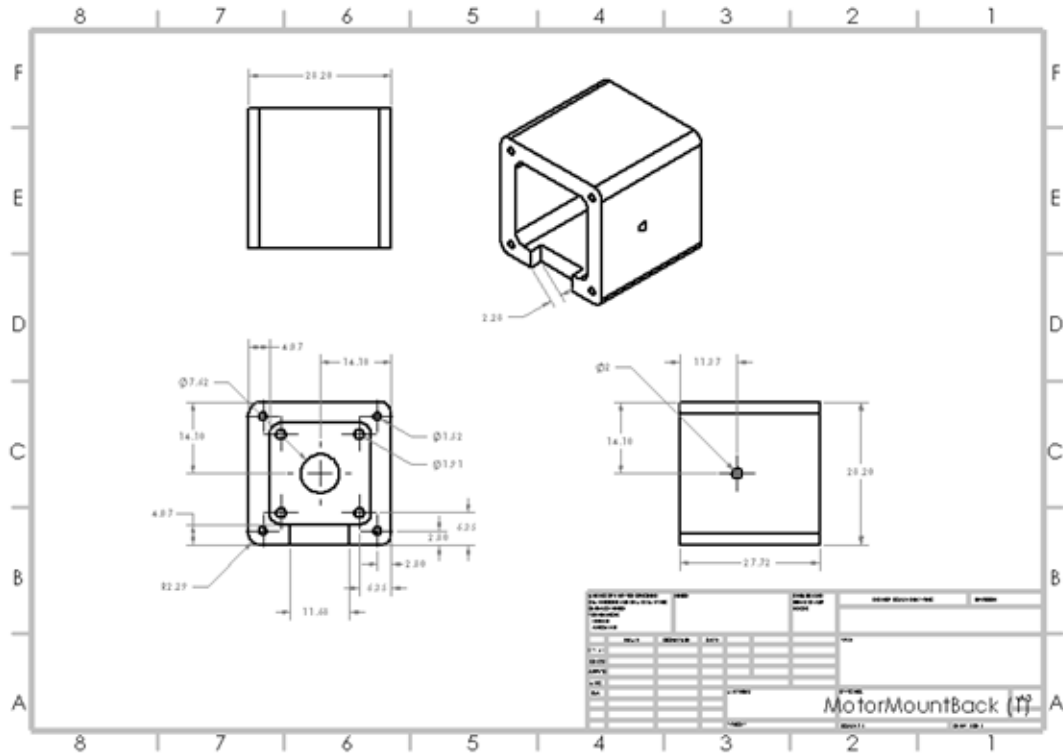
A: Vertical actuator center  
B: Optics cage gimbal center  
C: Horizontal actuator center  
O: Center of actuator pushing plane



# Cage Gimbal Drawing

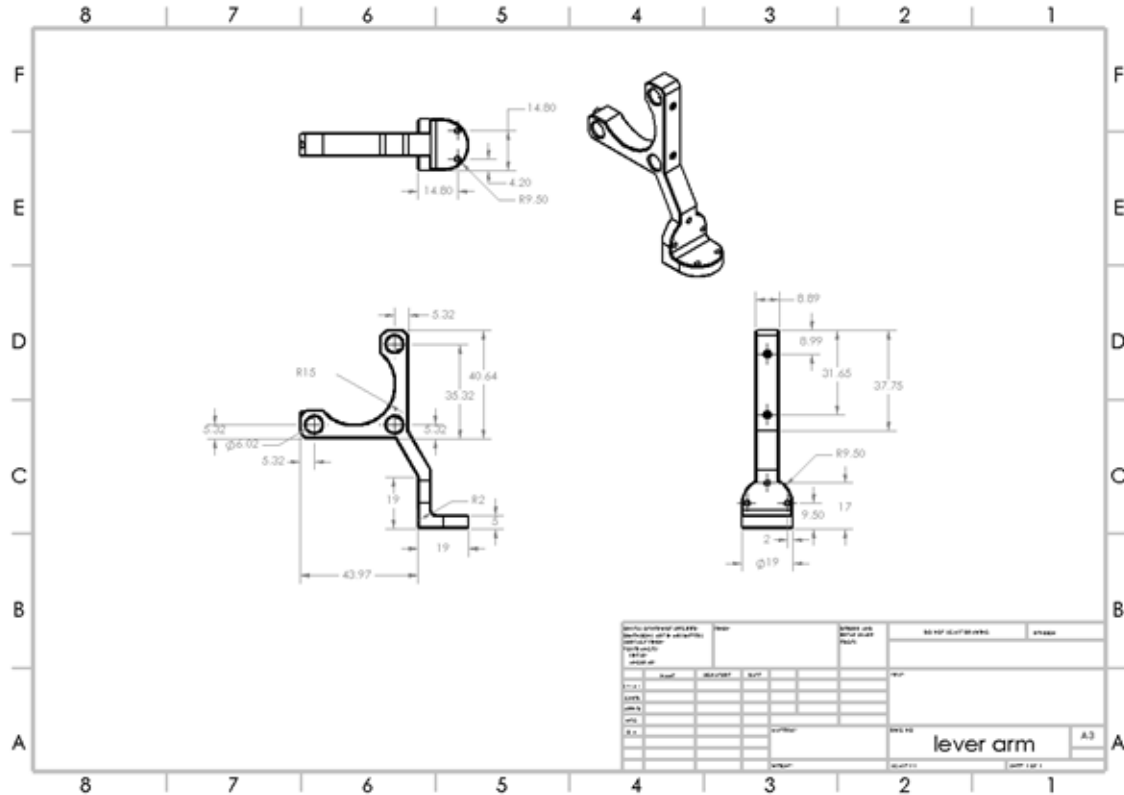


# Motor Case Gimbal - Back Drawing

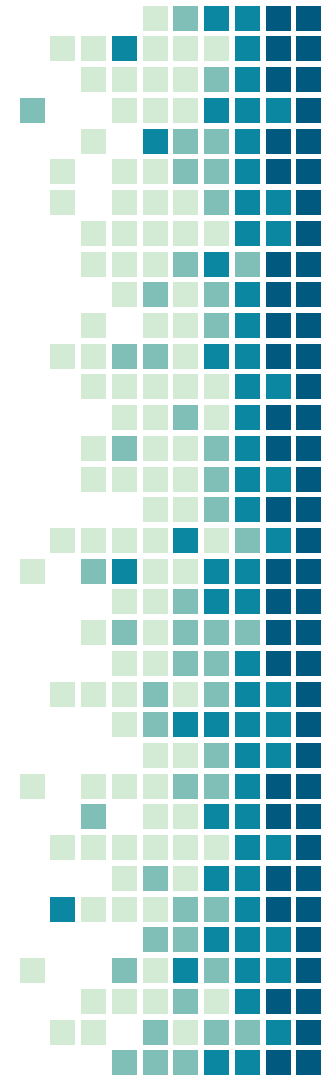
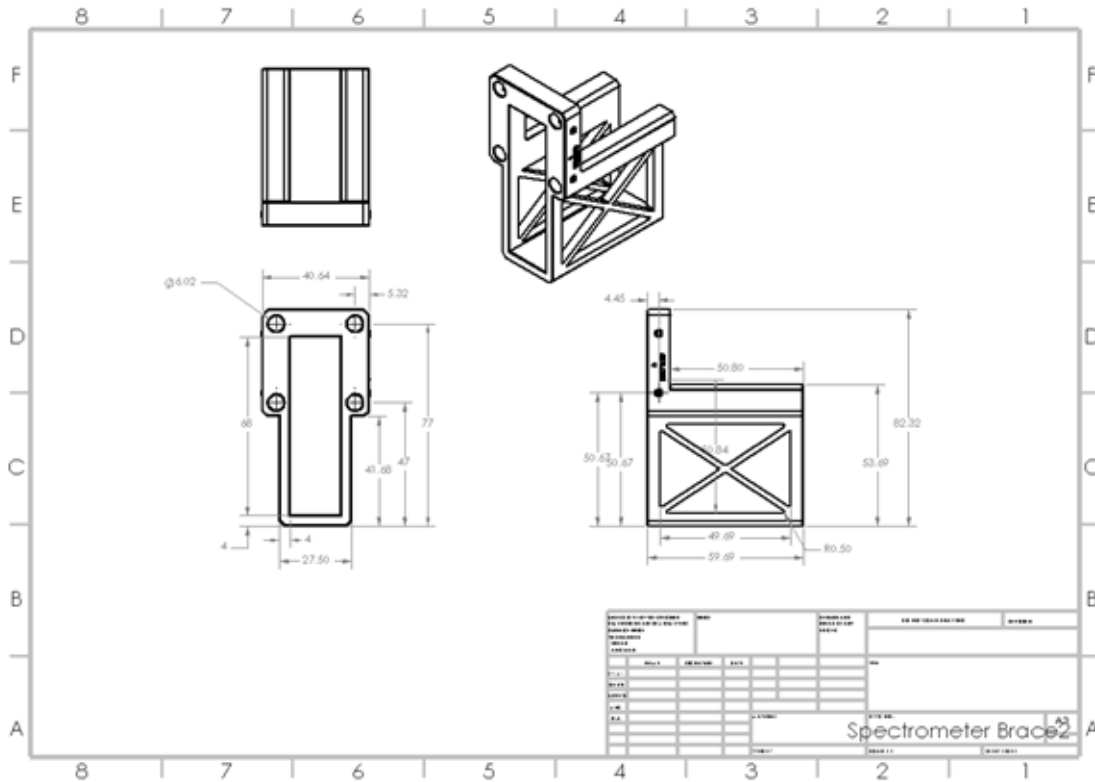




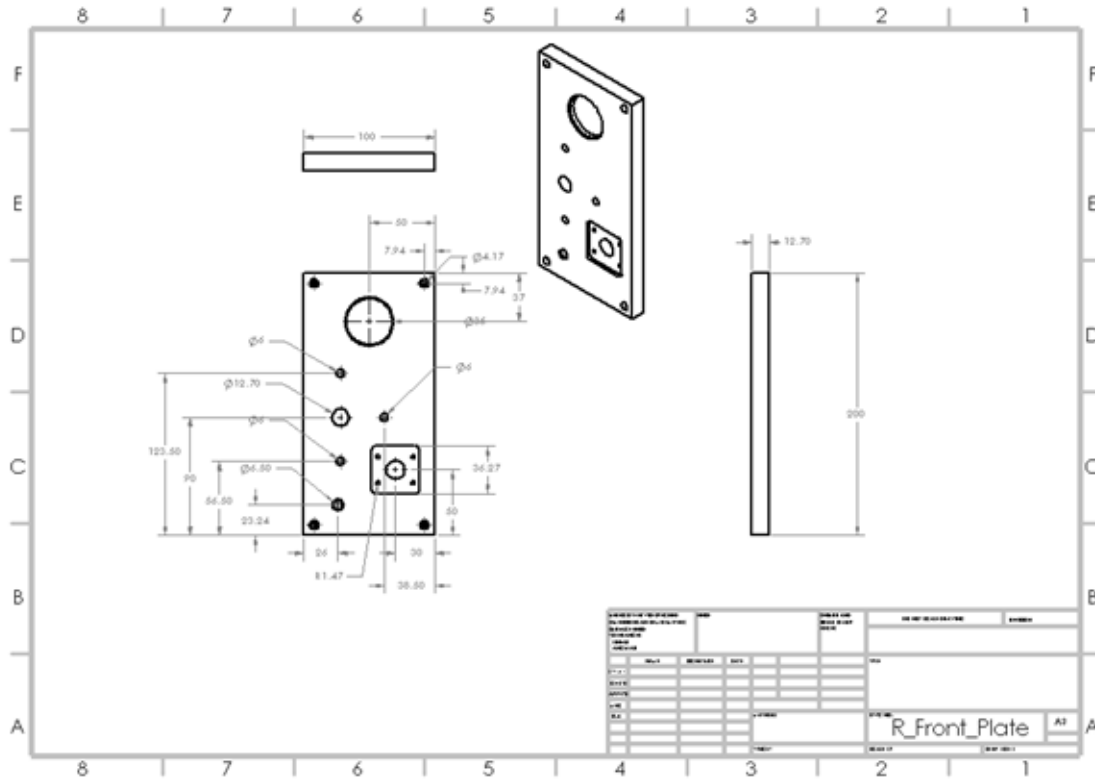
# Actuation Arm Drawing



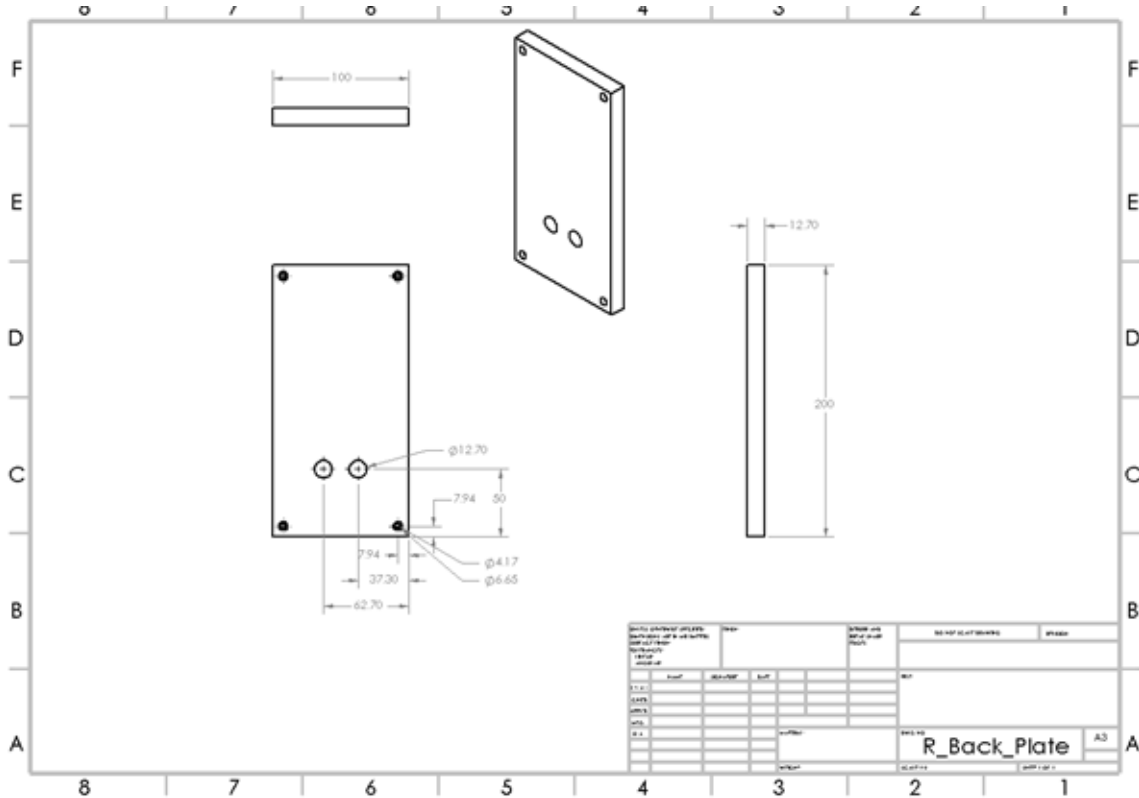
# Spectrometer Brace Drawing



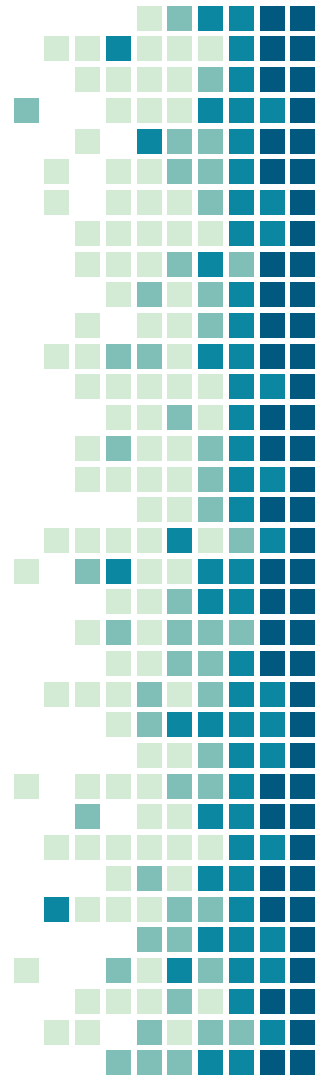
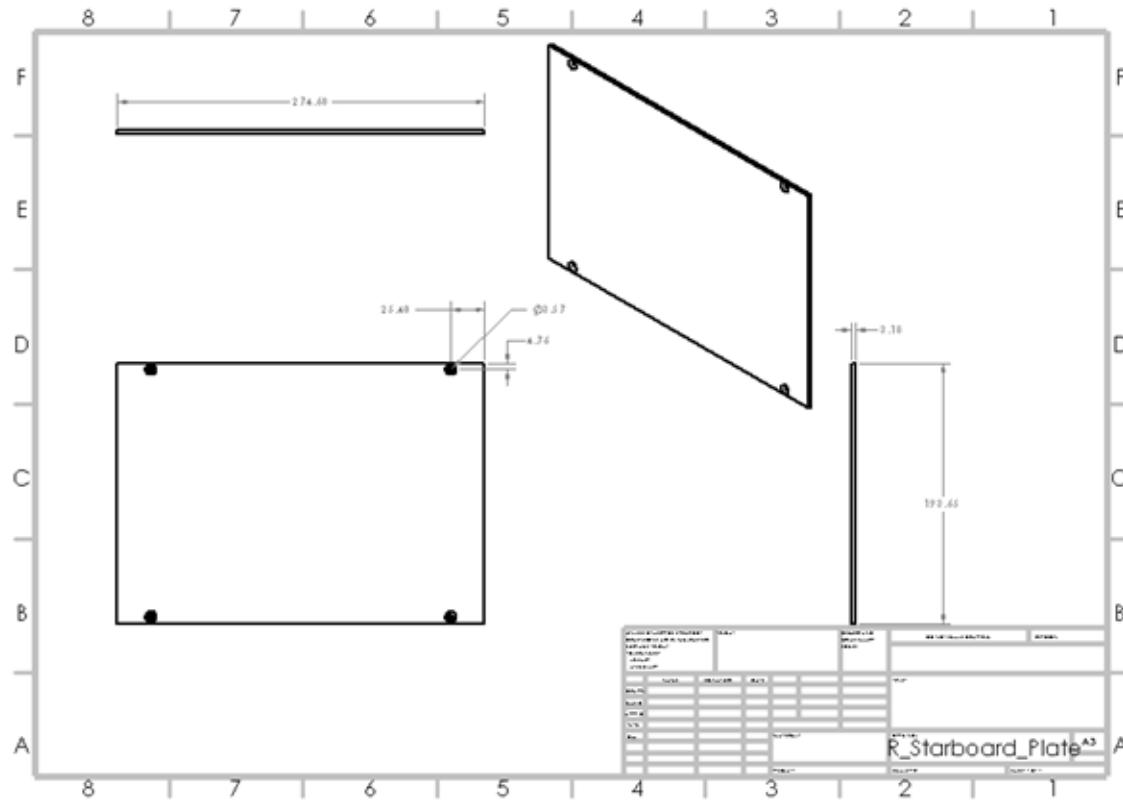
# Front Plate Drawing



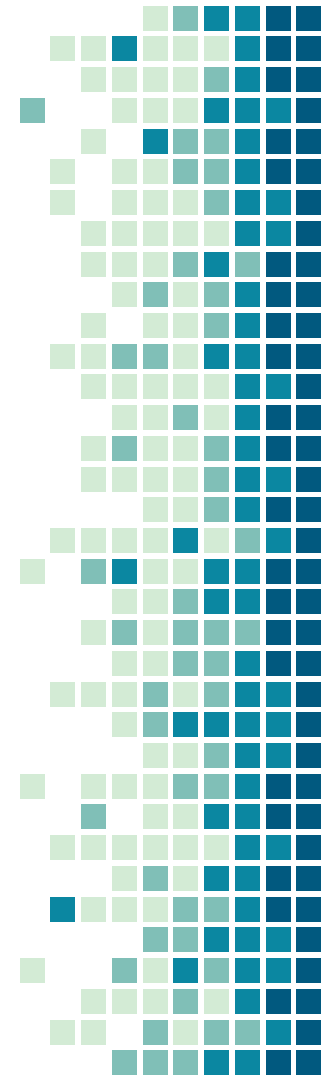
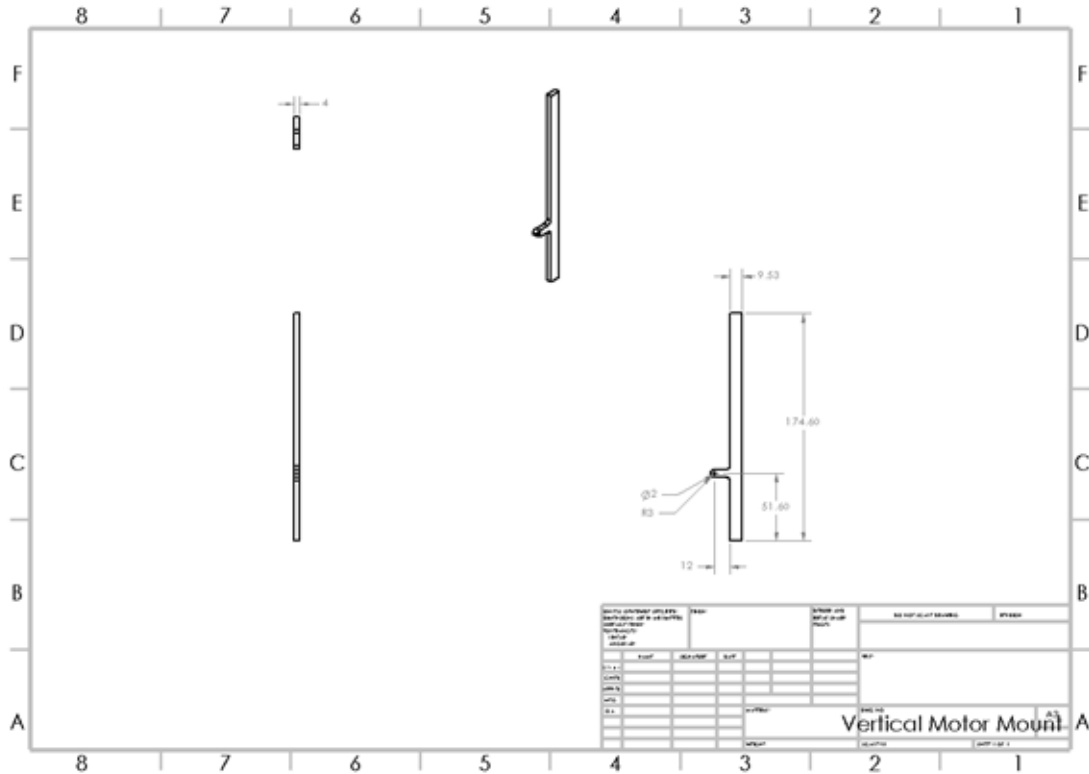
# Back Plate Drawing



# Side Panel Drawing



# Vertical Motor Brace Drawing



# Horizontal Motor Brace Drawing

