



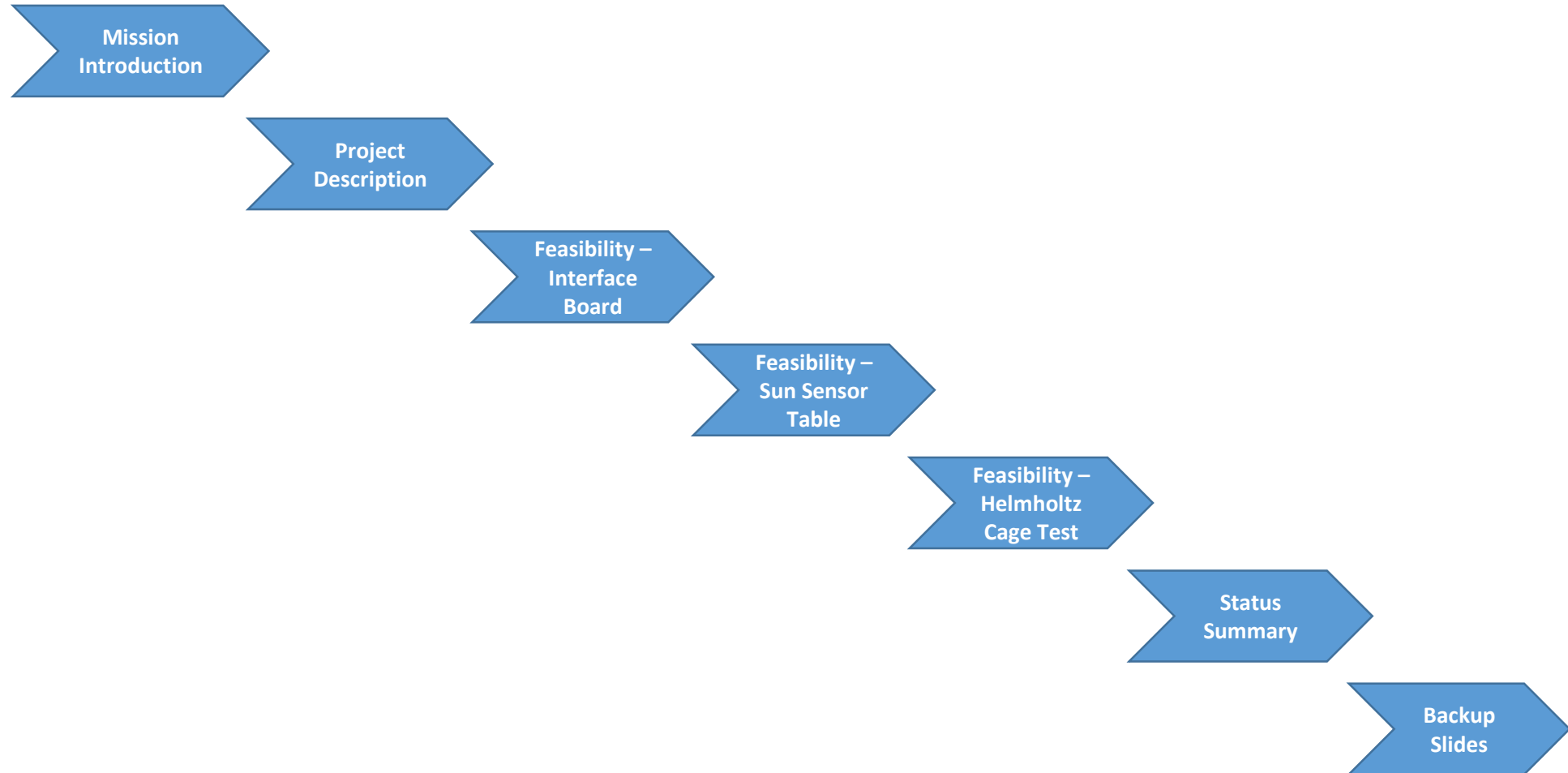
QB50 CubeSat PDR

Team: STAR

Satellite Testbed for Attitude Response

Matt Hong, Nick Andrews, Dylan Cooper, Colin Peterson, Nathan Eckert,
Sasanka Bathula, Cole Glommen

Presentation Outline



Mission Introduction

Mission
Introduction

Project
Description

Feasibility –
Interface
Board

Feasibility –
Sun Sensor
Table

Feasibility –
Helmholtz
Cage Test

Status
Summary

Backup
Slides

QB50 Satellite – Attitude Determination and Control System (ADCS)

ADCS ConOps

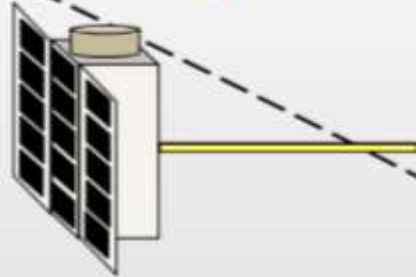


De-tumble

- Orbital Injection
- Recover from initial tip off rate of $10^\circ/\text{sec}$
- B-dot

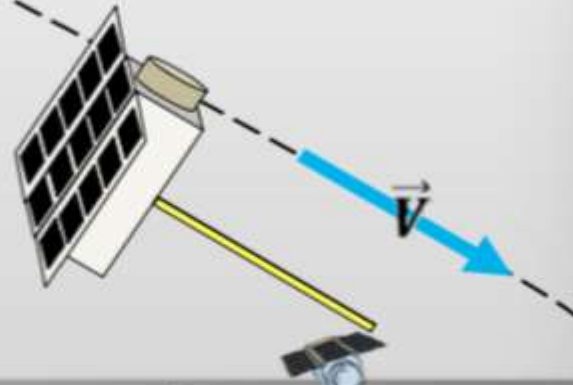
Sun point

- Safe Mode
- Maximize surface area of solar panels in the sun
- PD Control



Ram point

- Science and Normal Mode
- Point INMS in ram direction $\pm 10^\circ$
- Roll spacecraft to optimize comm. link
- Receding Horizon



- One of 50 CubeSats
- 400 km orbit
- ~ 8 month mission
- Provide in situ thermosphere measurements

Requirements:

- Pointing accuracy within $\pm 10^\circ$ of ram direction (Ctrl.)
- Pointing knowledge of within $\pm 2^\circ$ (Est.)
- Recover from tip-off body rates of up to $90^\circ/\text{s}$ within 2 days
- *To be verified with simulation*

Project Description



ADCS Verification ConOps

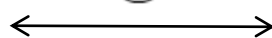
1. Interface Board



①

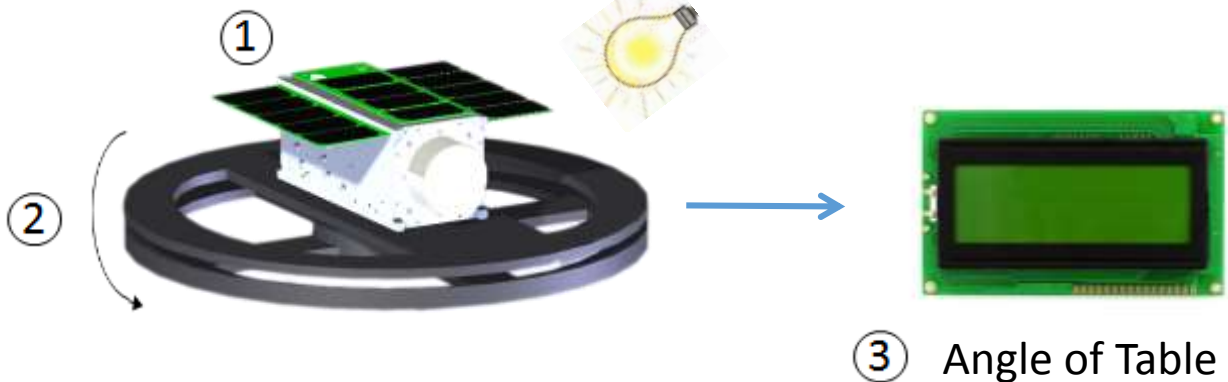


②



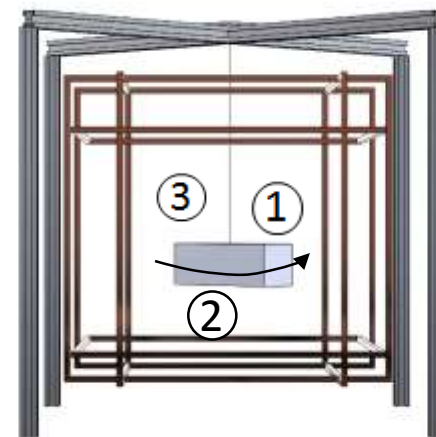
1. USB from simulation to interface board
2. Connect interface to ADCS
3. Run Simulation

2. Sun Sensor Calibration Table



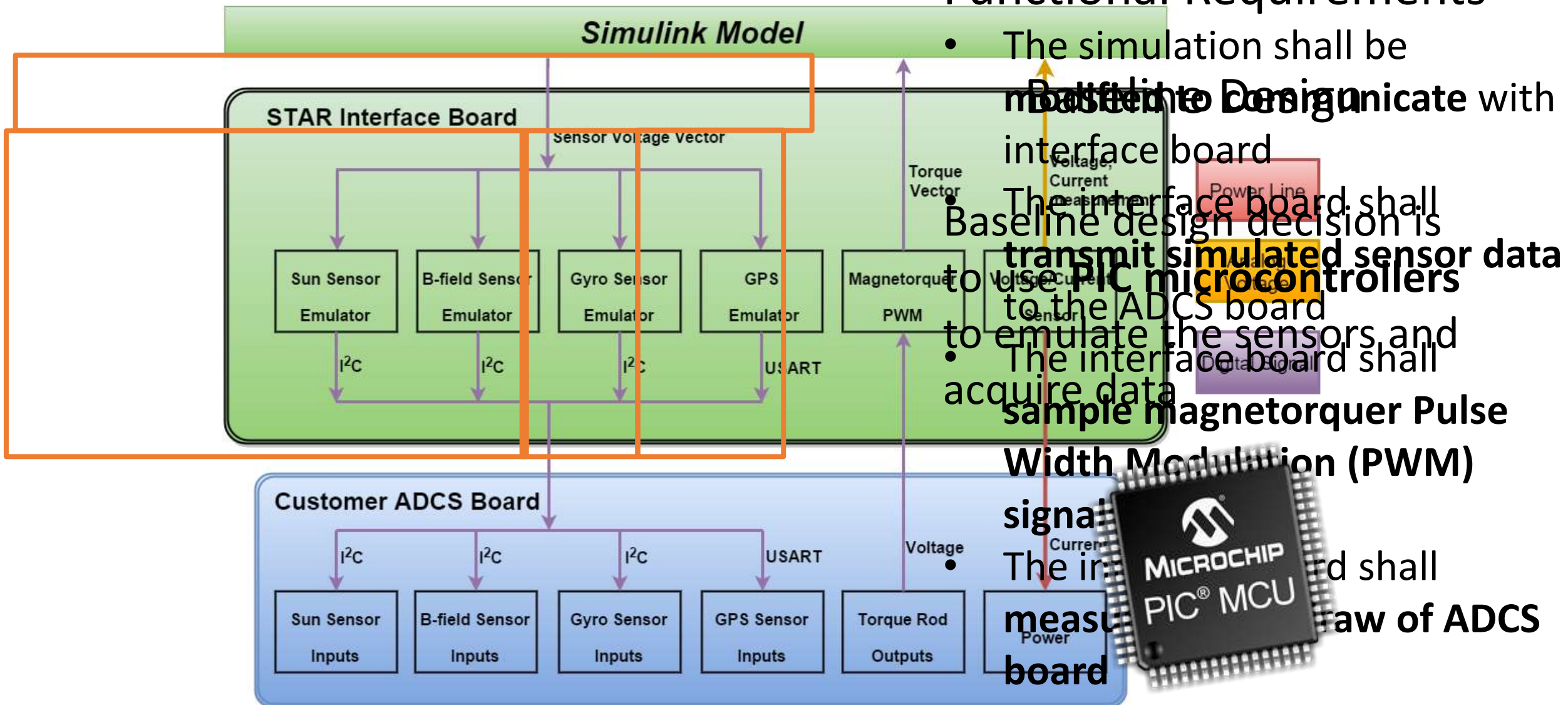
1. Integrate CubeSat
2. Rotate Table to desired angle
3. Compare angle of table to angle reported by satellite

3. Helmholtz Hanging Apparatus



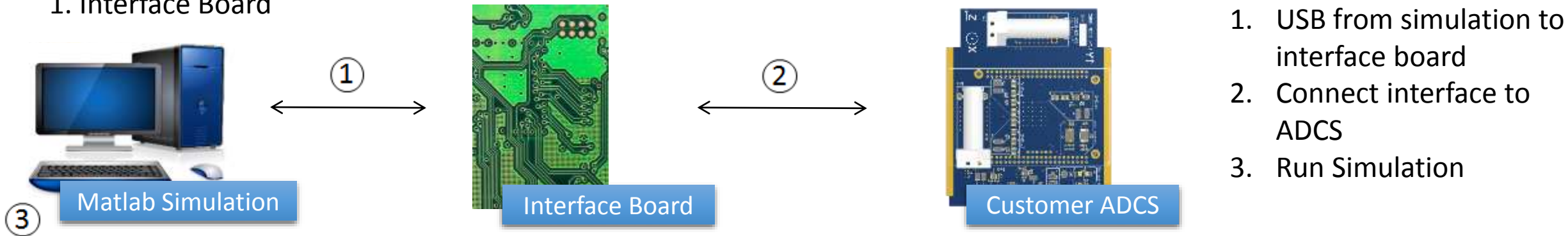
1. Integrate CubeSat
2. Fire Magnetorquer
3. Satellite rotates to verify functionality

Interface Board – Baseline Design

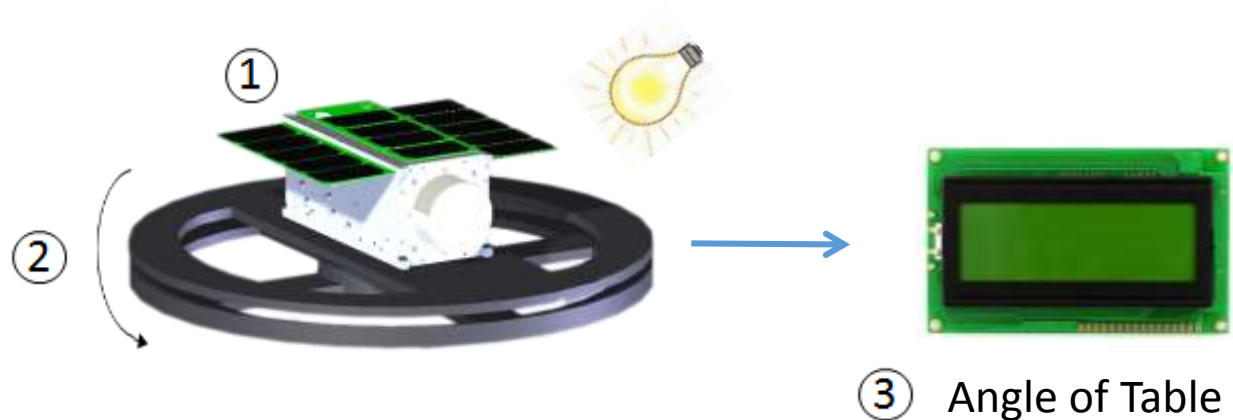


ADCS Verification ConOps

1. Interface Board

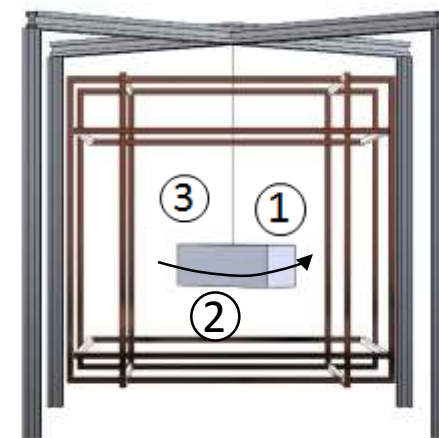


2. Sun Sensor Calibration Table



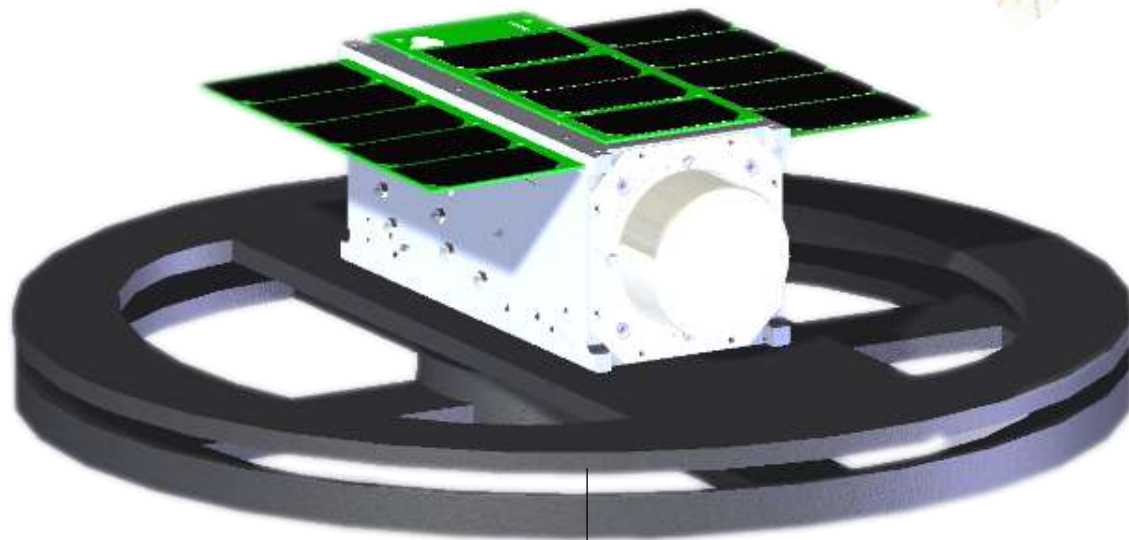
1. Integrate CubeSat
2. Rotate Table to desired angle
3. Compare angle of table to angle reported by satellite

3. Helmholtz Hanging Apparatus



1. Integrate CubeSat
2. Fire Magnetorquer
3. Satellite rotates to verify functionality

Sun Sensor Calibration Table – Baseline Design

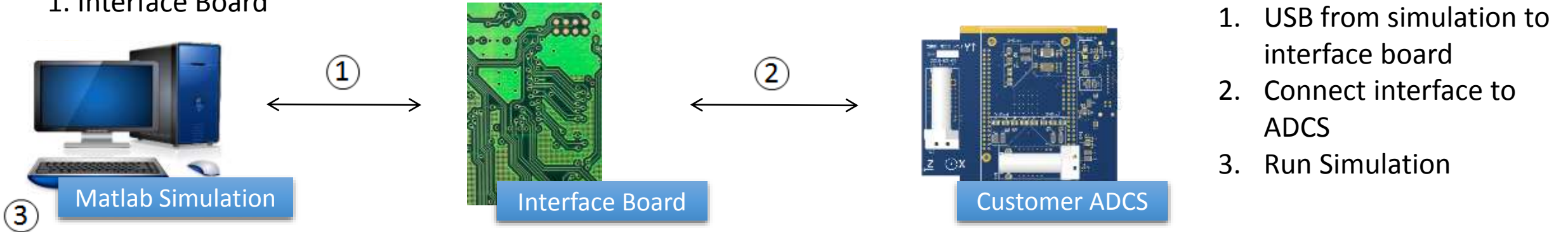


Functional Requirements Baseline Design

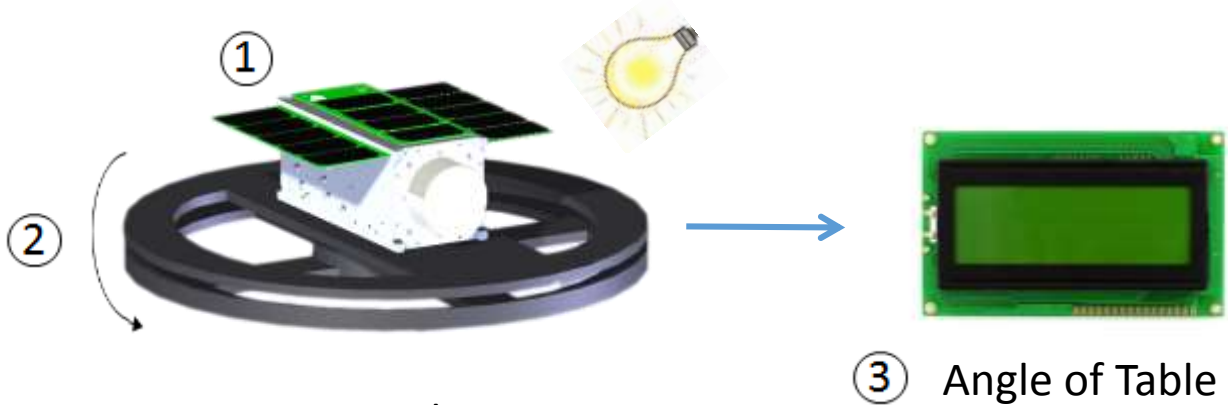
- The turn table shall be **turned to desired angle**
Baseline design decision is to **manually** rotate turn table
- The turn table shall have a **magnetic encoder resolution of 1° with $\pm 0.5^\circ$ accuracy**
to display position on an LED display

ADCS Verification ConOps

1. Interface Board

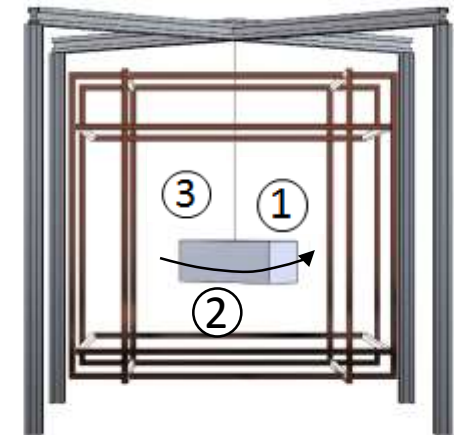


2. Sun Sensor Calibration Table



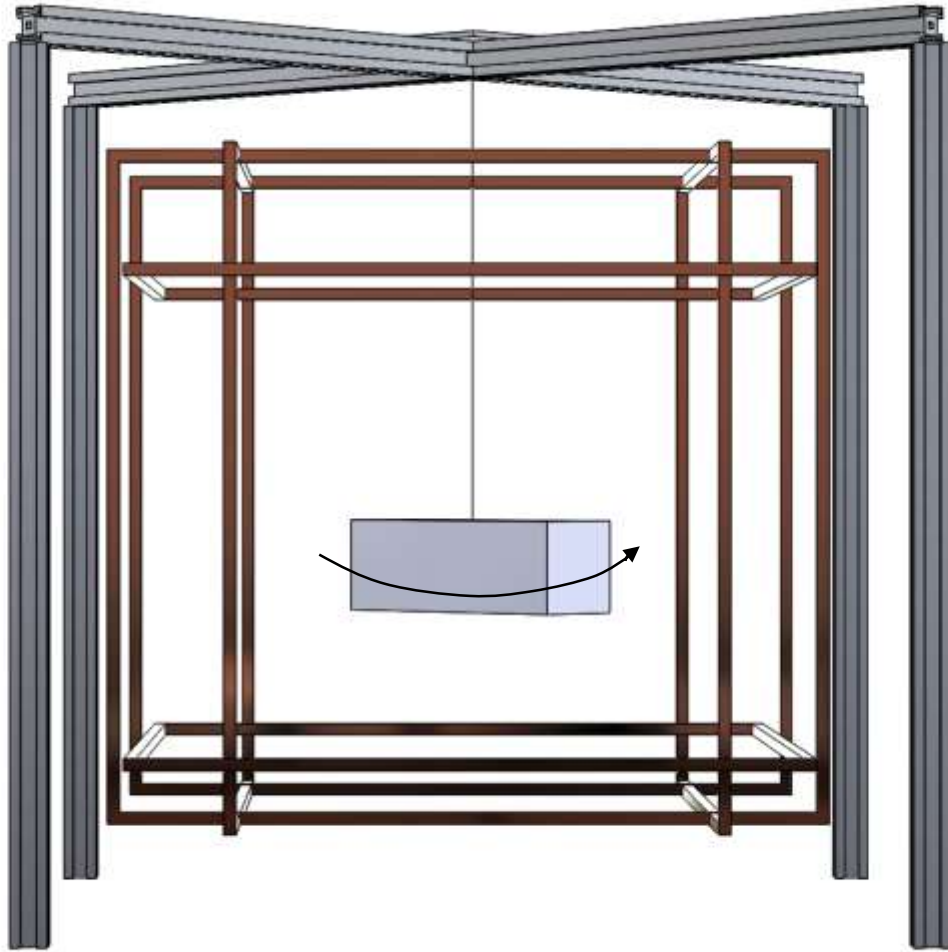
1. Integrate CubeSat
2. Rotate Table to desired angle
3. Compare angle of table to angle reported by satellite

3. Helmholtz Hanging Apparatus



1. Integrate CubeSat
2. Fire Magnetorquer
3. Satellite rotates to verify functionality

Helmholtz Cage – Baseline Design



Functional Requirements Baseline Design

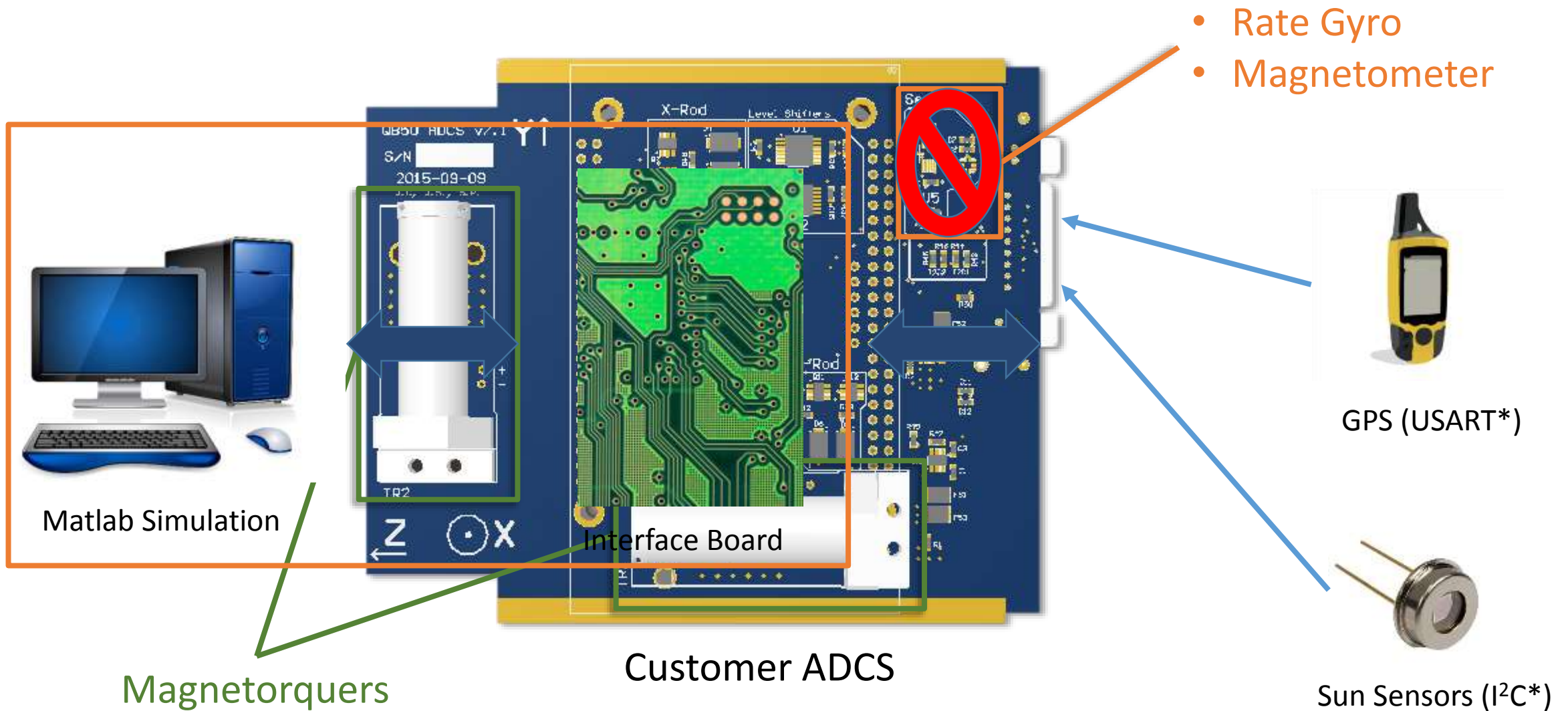
- The CubeSat shall be **suspended in the HelmHoltz Cage**
Baseline design decision is to
- **hang the CubeSat with a line**
The CubeSat shall rotate with 1 degree of freedom(DoF)

Baseline Feasibility

Interface Board



Interface Board - Feasibility



Customer ADCS

*I²C = Inter-Integrated Communication

*USART = Universal Synchronous Asynchronous Receiver/Transmitter

Simulation to Interface Board - Feasibility

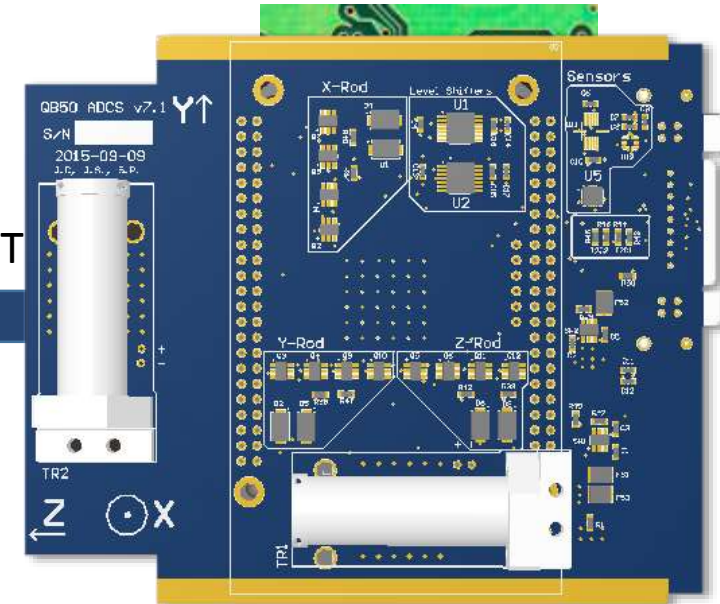
*UART = Universal Synchronous Receiver/Transmitter
 *USB = Universal Serial Bus



Matlab Simulation



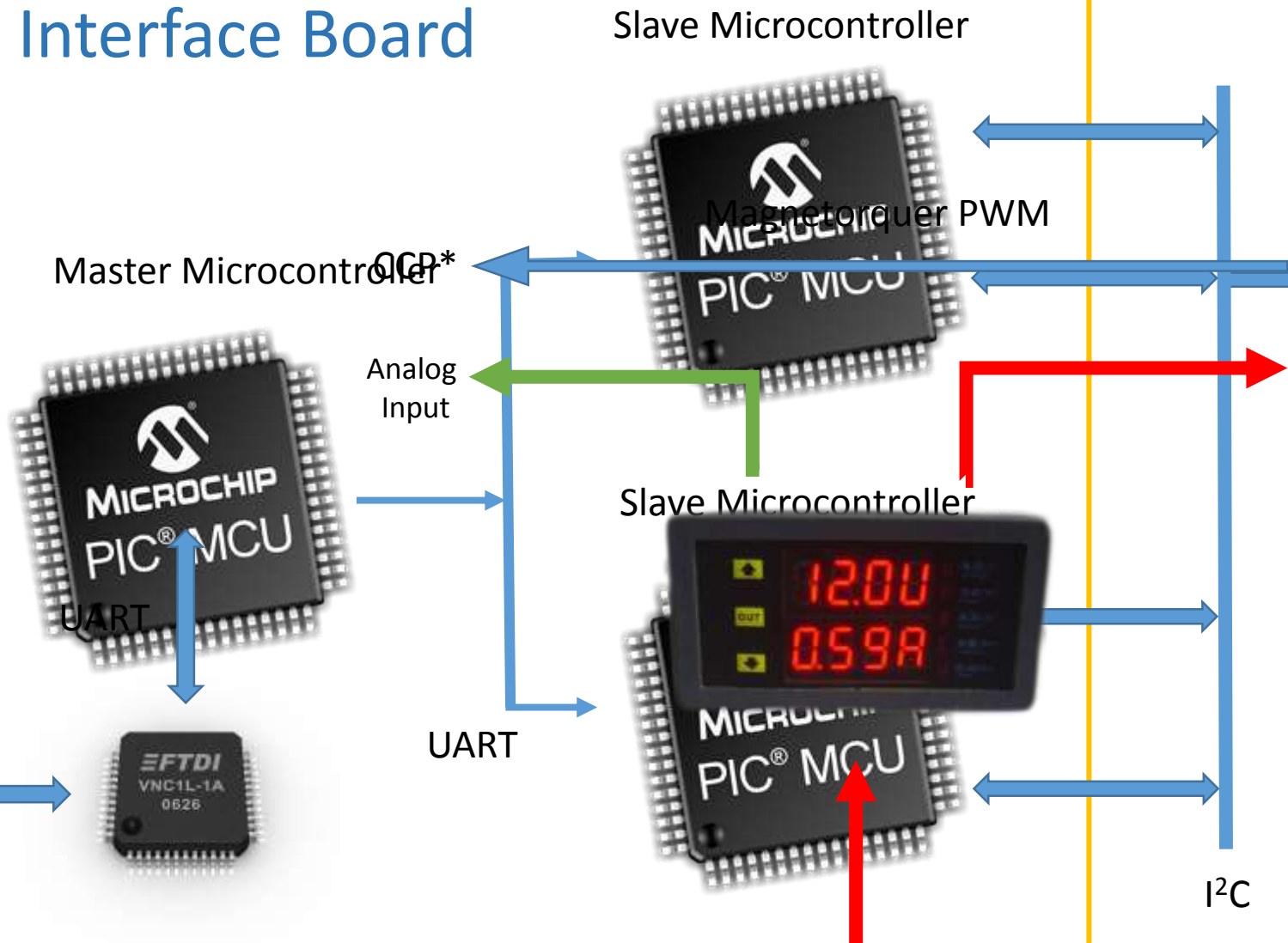
FTDI USB* to UART*



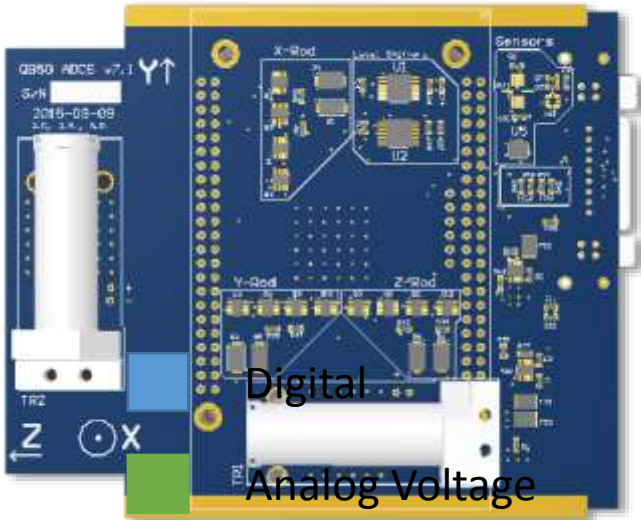
Customer ADCS

- **Compatible with Matlab** using included drivers from FTDI
- Converts USB into a common communication protocol used by microcontrollers

Interface Board



- I²C Bus
- Allows multiple devices to communicate with each other
 - Designated master device with slave devices
 - Slave devices are assigned one address



Customer Power

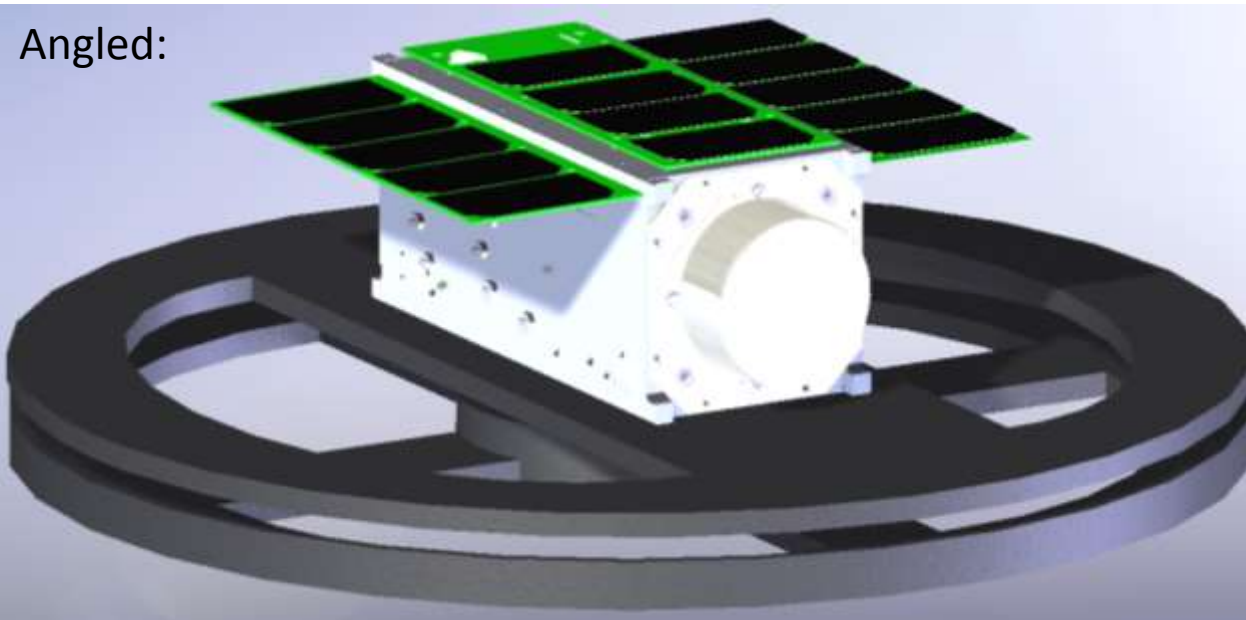
*CCP = Capture/Compare/PWM

Baseline Feasibility

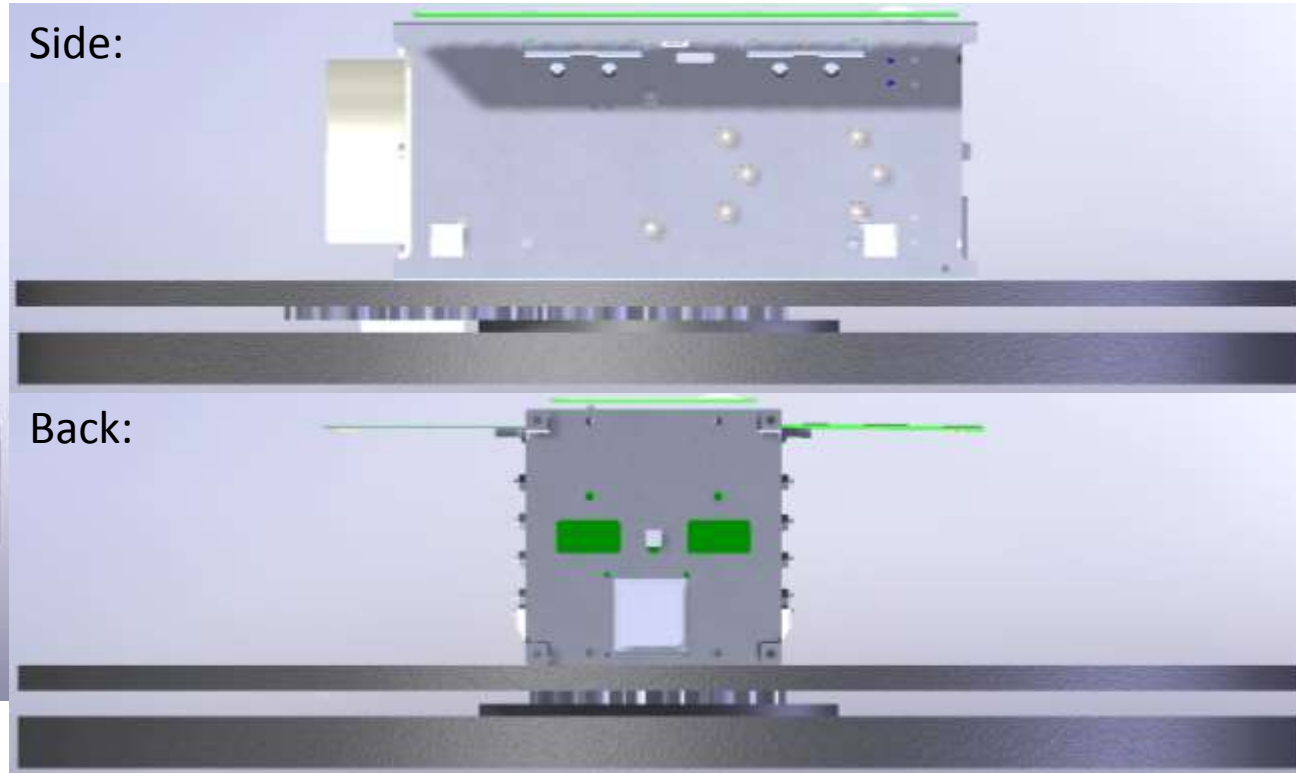
Sun Sensor Calibration Table



Sun Sensor Calibration Table - Feasibility



Diameter = 50 cm
Height = 4 cm

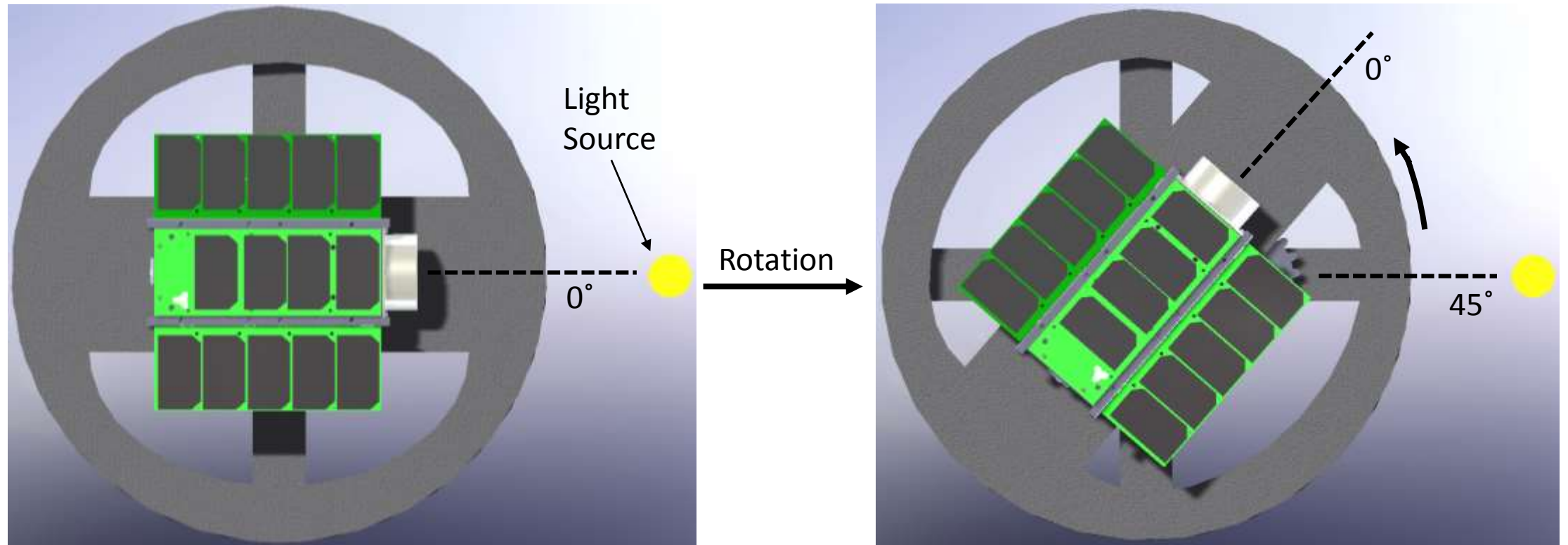


Supports 1U, 2U, and 3U CubeSats in all orientations

Sun Sensor Calibration Table - Usage

Rotation types:

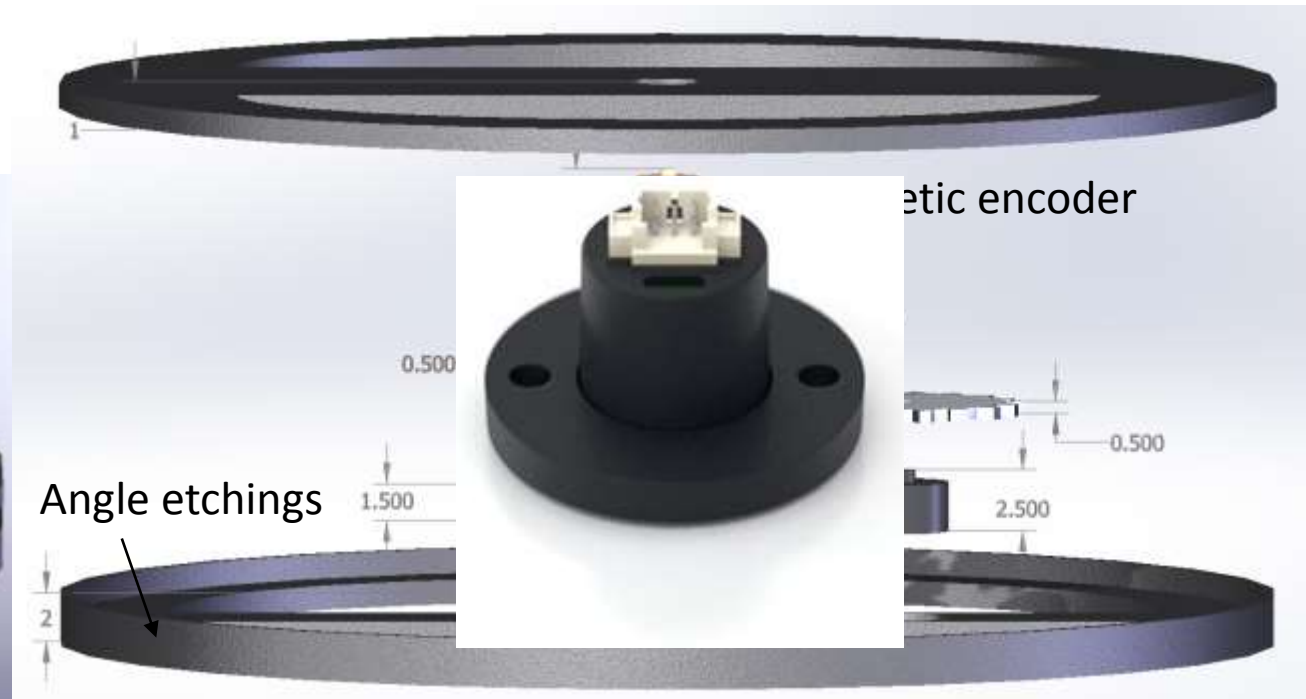
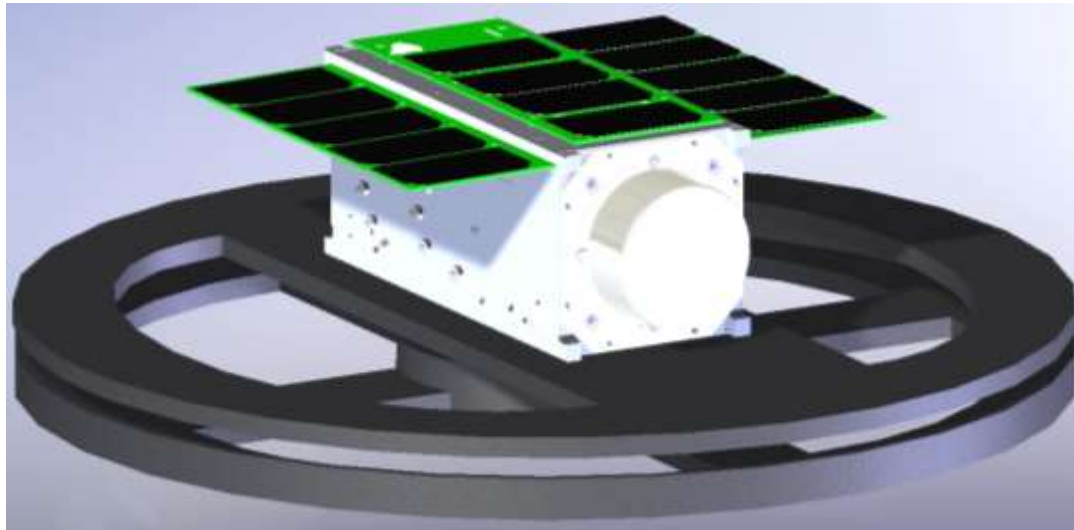
- 1) Manual – rotate to desired angle
- 2) Motor – to be implemented by customer



Sun Sensor Calibration Table - Feasibility

1. Rotate with resolution of 1° with $\pm 0.5^\circ$ accuracy

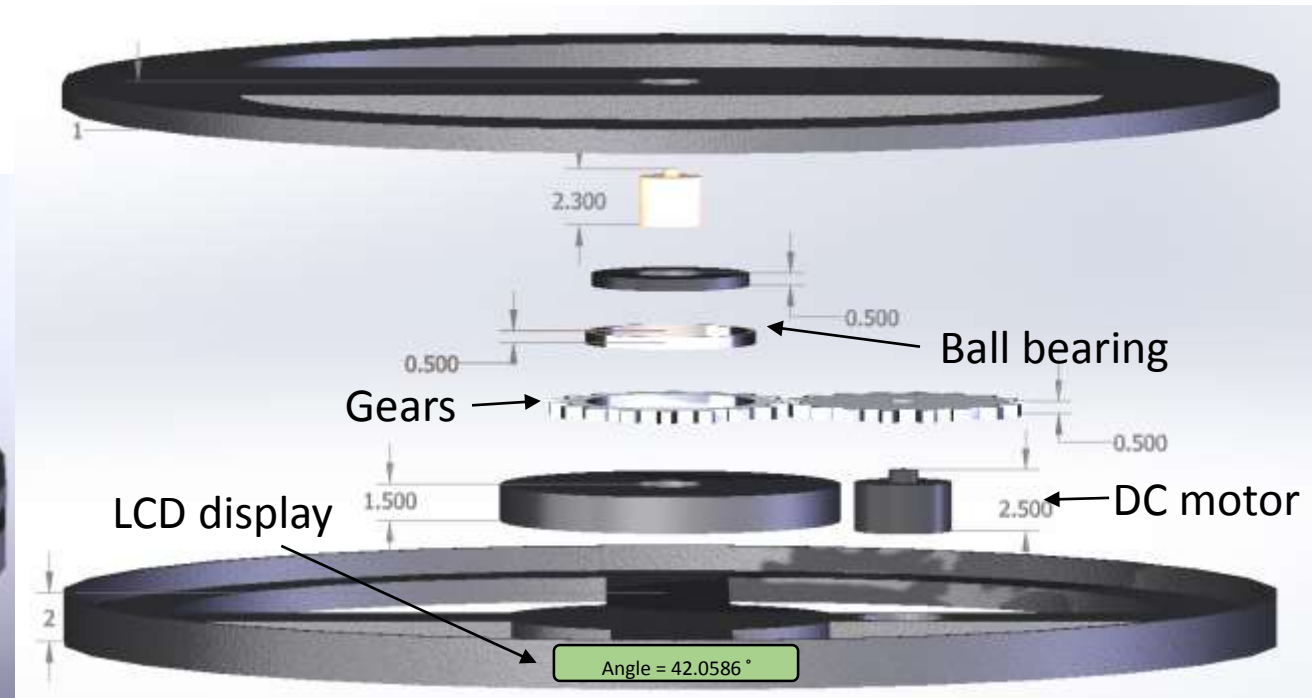
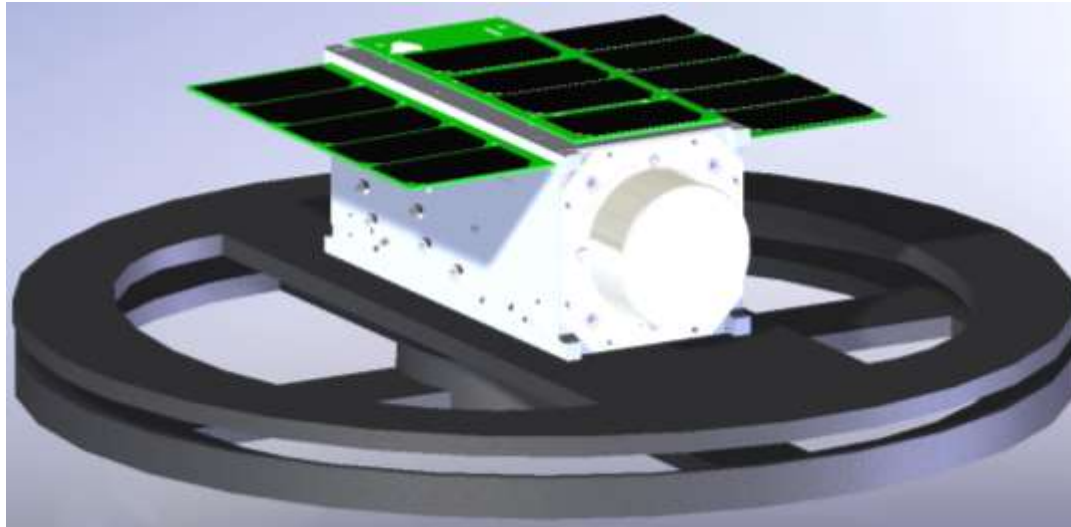
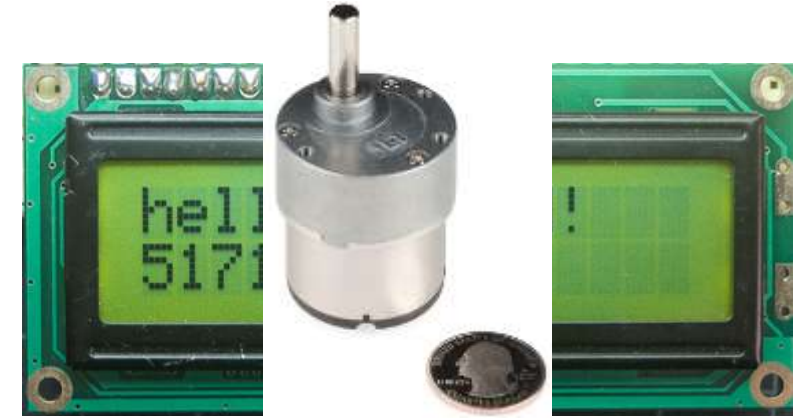
- 10 bit rotary encoder
 - Resolution = $360^\circ / 2^{10} = 0.352^\circ$ per bit $< 1^\circ$
- Angle etchings
 - Physical – electronics redundancy
 - Board diameter = 50 cm = 19.685"
- Arc length spacing = circumference/ $360^\circ = 0.172''$ /degree



All measurements in centimeters

Sun Sensor Calibration Table - Feasibility

2. Display angular position to user
 - LCD display output
3. Manually operated with potential to be automated
 - 10 Hz Sun sensor, RPM of $< 5/3$
 - Torque required = $0.0746 \text{ N}\cdot\text{m}$



Baseline Feasibility

Helmholtz Cage Test



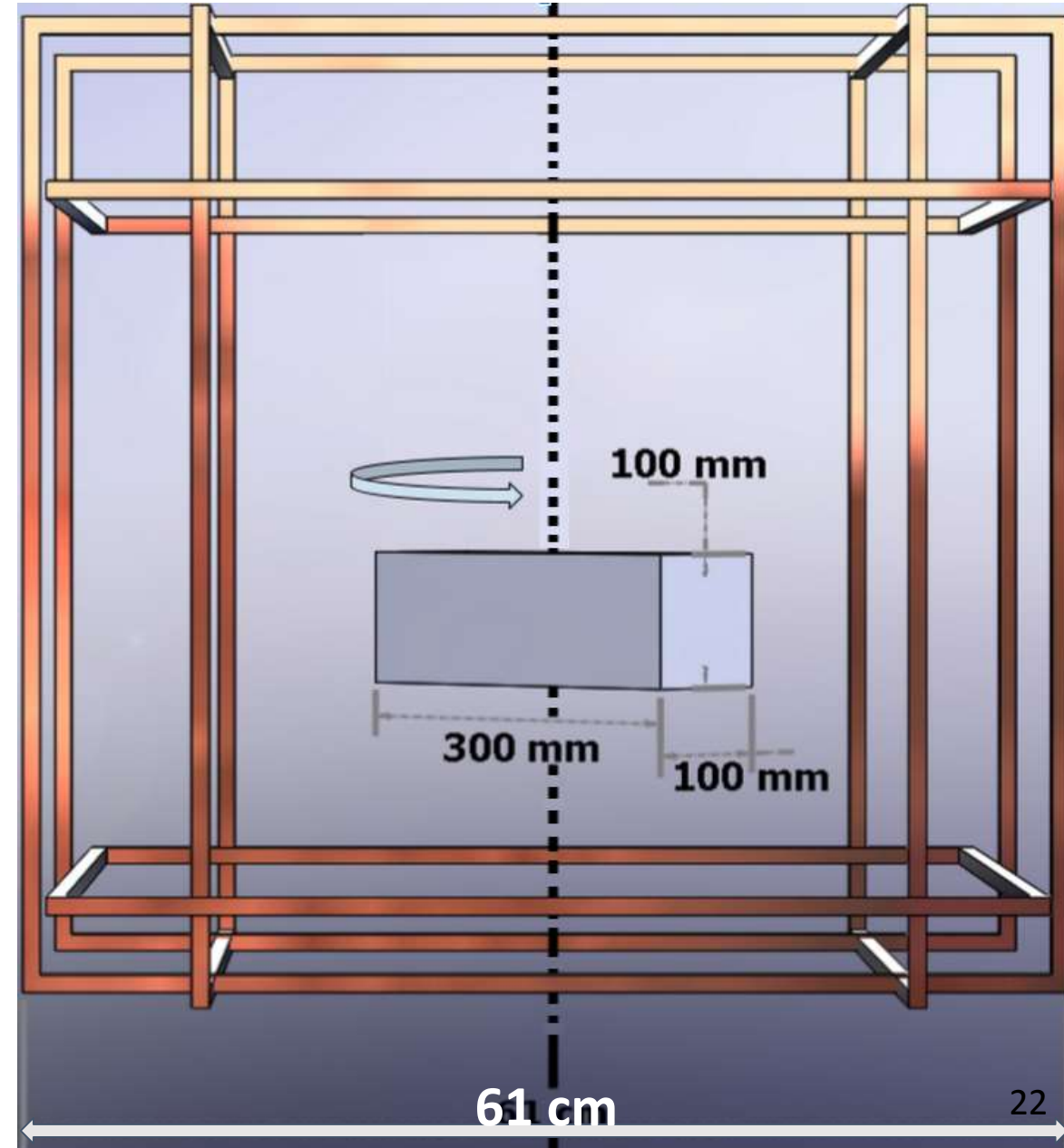
Helmholtz Cage Structure Feasibility

TEST:

- The QB50 will sense attitude and make necessary adjustments using its magnetorquers

Requirements

- Allow for rotation $\pm 360^\circ$ about one axis
- Torquing authority of 0.1 Am^2 equivalent to $5 \times 10^{-6} \text{ Nm}$
- Less than $5 \times 10^{-6} \text{ Nm}$ resistance to rotation
- Do not interfere with the Satellite's magnetometer readings



3D schematic of the experimental setup. The setup consists of a rectangular frame with dimensions 87.6 cm (width), 61 cm (depth), and 91.44 cm (height). A central vertical rod is positioned 52.5 cm from the top. A rectangular block is suspended from the rod, with dimensions 300 mm (width), 100 mm (height), and 100 mm (depth).

Satellite

The image contains two separate 3D coordinate systems, each represented by a light gray rectangular prism. The top prism is oriented horizontally. A dashed line with an arrow at the end points upwards from the top face, labeled with a bold black 'Z'. Another dashed line with an arrow points to the right from the right face, labeled with a bold black 'Y'. A third dashed line with an arrow points diagonally down and to the left from the front face, labeled with a bold black 'X'. The bottom prism is oriented vertically. A dashed line with an arrow points upwards from the top face, labeled with a bold black 'Z'. Another dashed line with an arrow points to the right from the right face, labeled with a bold black 'Y'. A third dashed line with an arrow points diagonally down and to the left from the front face, labeled with a bold black 'X'.

Helmholtz Cage Testing Structure Feasibility

$$M_D = \rho * \alpha^2 * t^2 * h * L^4 * C_D / (64)$$

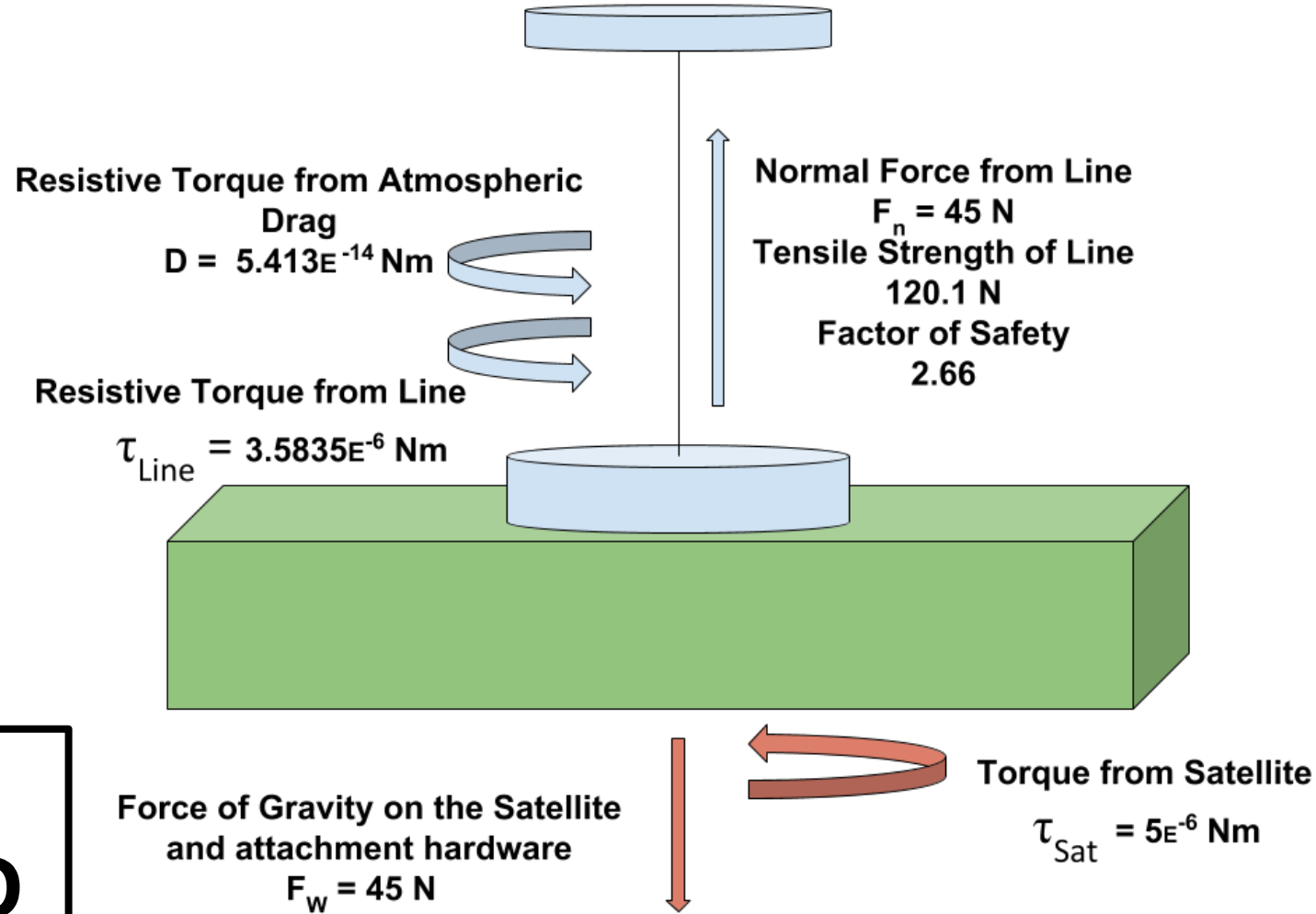
- Assume $C_D = 2.05$
- Assume Moment of Inertia of a hollow rectangular prism

$$\tau_{\text{Line}} = 0.5 * \pi * r^4 * G * \theta * L^{-1}$$

- Assume line can be modeled as a Rod

$$\tau_{\text{Sat}} = \mu \times B$$

$$\Rightarrow \tau_{\text{Sat}} > \tau_{\text{Line}} + \mathbf{M_D}$$



Helmholtz Cage Testing Structure – Feasibility

Line Resistive Torque

$$\tau_{\text{Line}} = I * \alpha$$

τ_{Line} = Resistive Torque from the line

I = mass moment of inertia of the rod

α = angular acceleration of the rod

r = cross-sectional radius of the line

θ = angular deflection = 360°

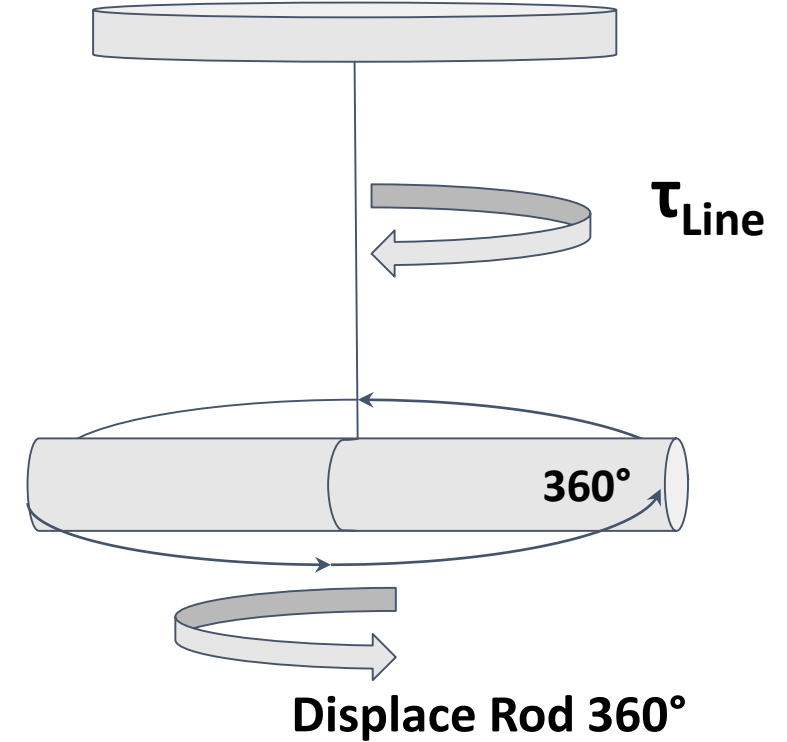
t = time for the rod to rotate θ°

- found experimentally

$$I = m * (2 * r^2 + h^2) / 12$$

$$\alpha = 2 * \theta * t^{-2}$$

$$\tau_{\text{Line}} = 3.5835\text{E}^{-6} \text{ Nm}$$



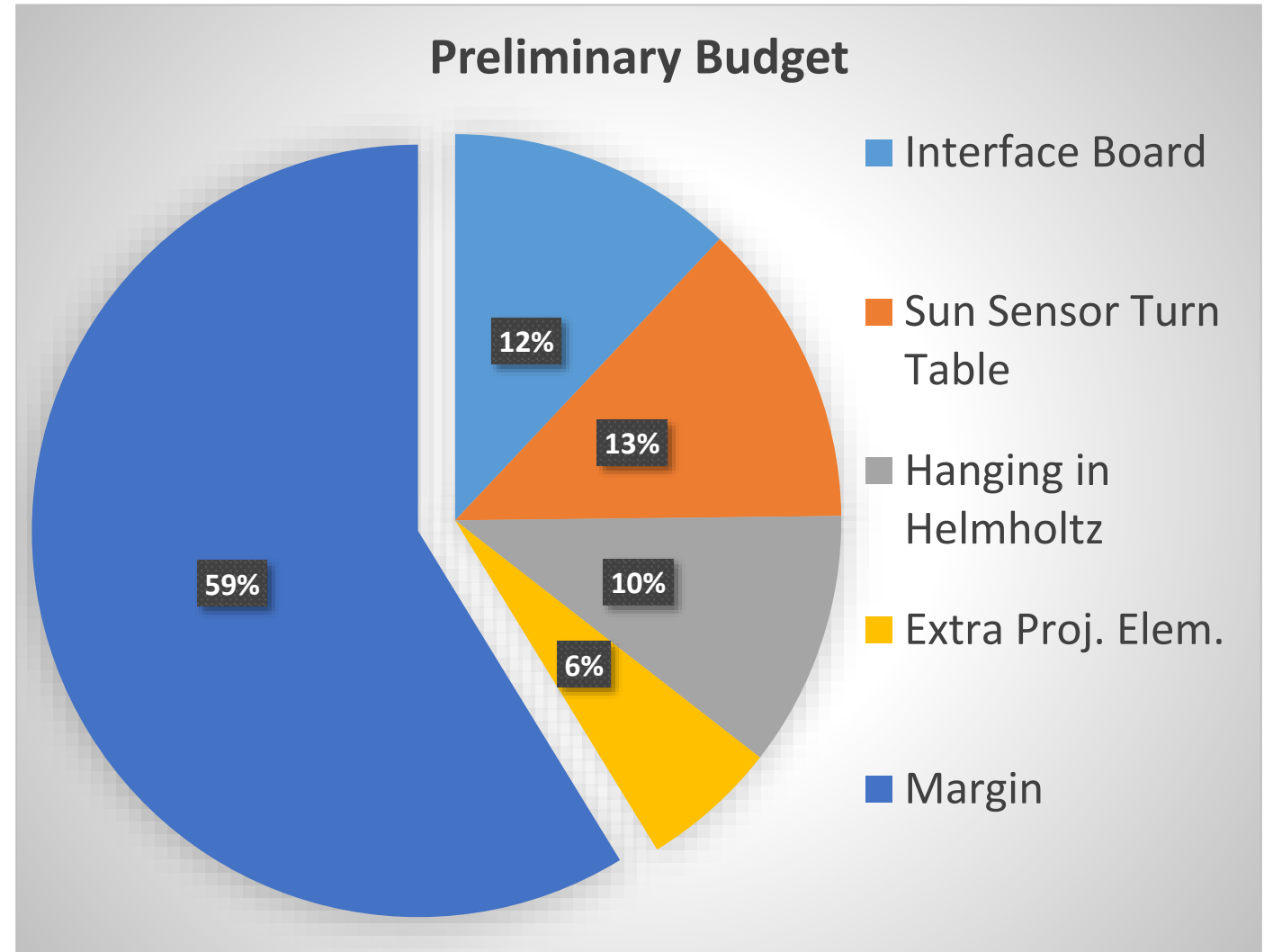
measure time (t) until rod
returns to initial

Status Summary

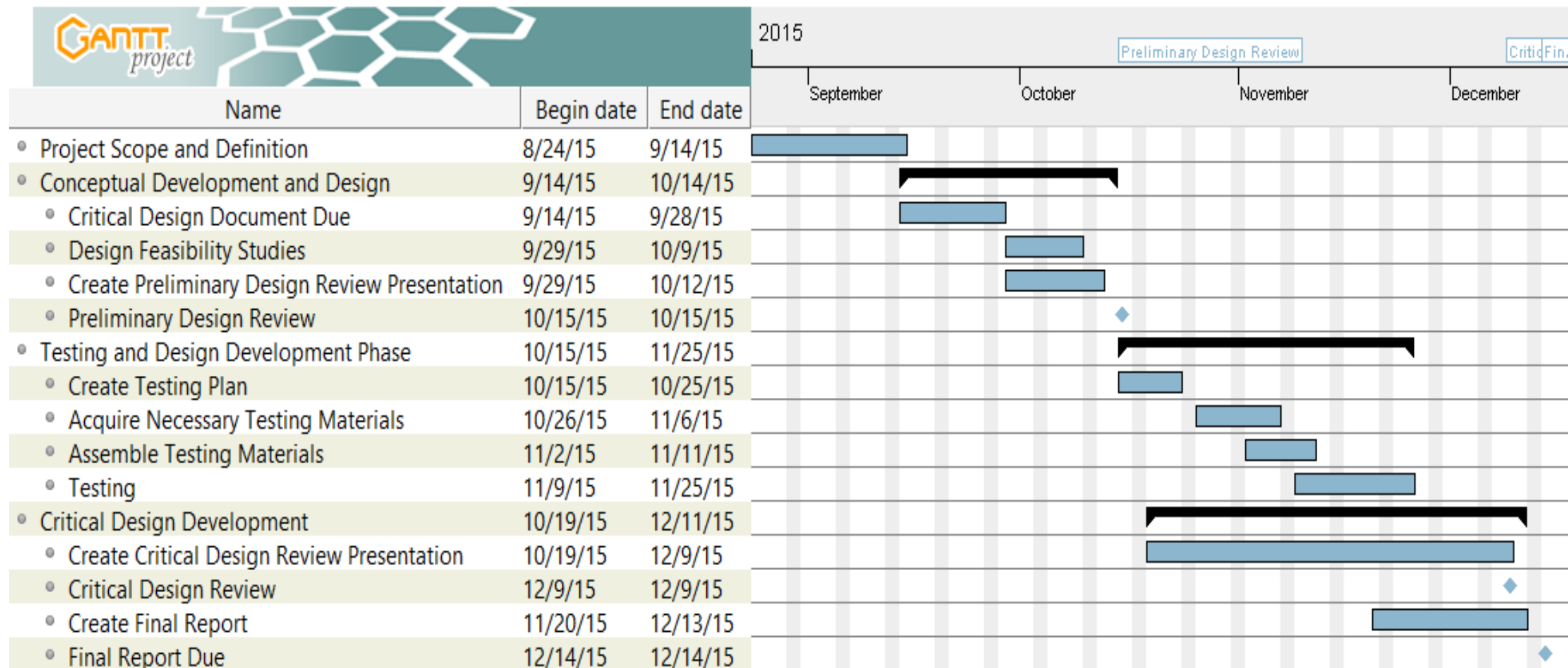


Budget Feasibility

- Funding:
 - \$5,000.00 CU ASEN
 - Total Project Cost:
 - ~\$2,000
 - 5 revisions for electronics
 - Project Margin:
 - ~\$3,000
- *certain project elements costs are estimates/TBD



Project Schedule



Future Studies

- Interface Board
 - Design layout of interface board
 - Selection of precise PIC microcontrollers
- Sun Sensor Calibration Table
 - Design encoder-LCD circuit
 - Selection of gears and gear ratio
- Helmholtz Cage Test
 - Further testing of hanging lines for margin
- Software
 - Increase of simulation accuracy

Questions?



Backup Slides

- [Interface Board](#)
- [Simulation](#)
- [Sun Sensor Calibration Table](#)
- [Helmholtz Cage Test](#)
- [Logistics](#)



Interface Board



Interface Board: Requirements

- Interface board shall output digital sun sensor, rate gyro, magnetometer, and GPS data at 10Hz or greater.
- Interface board shall sample the 3 magnetorquer PWM outputs
- Interface board shall measure power draw of ADCS board
 - Shall measure voltage and current for 3.3V and 5V lines
 - Shall have a minimum accuracy of 5% with a desired accuracy of 1%
 - Shall sample at a rate of 20Hz or greater

Functional Requirement 1

- An interface board shall provide the means for the Matlab/Simulink simulation to communicate with the QB50 ADCS board
 - DR.1 The interface board shall transmit simulated sun sensor data, via I2C, to the ADCS board at a rate of 10Hz or greater
 - DR.2 The interface board shall transmit simulated rate gyro data, via I2C, to the ADCS board at a rate of 10Hz or greater
 - DR.3 The interface board shall transmit simulated magnetometer data, via I2C, to the ADCS board at a rate of 10Hz or greater
 - DR.4 The interface board shall transmit simulated GPS data, via USART to the ADCS board at a rate of 10Hz or greater
 - DR.5 The interface board shall sample the 3 magnetorquer PWM outputs

Cont.

- DR.5.1 The PWM outputs will be sampled such that the spacecraft torque generated by the magnetorquers can be calculated to an accuracy of 10% or greater
- DR.5.2 A compare, capture, and PWM (CCP) module capable of 1kHz operation shall be used to capture the PWM signals
- DR.6 The interface board shall measure the power draw of the ADCS board
 - DR.6.1 The interface board shall measure the voltage and current of the individual 5V and 3.3V lines at a rate of 1kHz or greater
 - DR.6.2 The interface board shall measure the voltage and current of the individual 5V and 3.3V lines with a desired accuracy of 1% and minimum accuracy of 5%
 - DR.6.3 The voltage and current measurements shall be sent to the computer to be logged
- DR.7 The interface and ADCS board shall operate via USB power

Functional Requirement 2

- The existing Matlab/Simulink simulation shall be modified to communicate with ADCS interface board
 - DR.1 The simulation shall communicate with the interface board via USB
 - DR.2 The supporting simulation shall convert the magnetorquer signal to a torque value and maintain an accuracy of 10% or greater
 - DR.2.1 The magnetorquer torque value shall be recorded to a file at a rate of 1kHz for the entire duration of the simulation
 - DR.3 The measured voltage and current to the ADCS board shall be recorded to a file
 - DR.4 A GUI shall be added to the simulation
 - DR.4.1 The GUI shall allow the user to override sensor output to simulate sensor failure
 - DR.5 The supporting software shall feed the magnetorquer output back into the simulation to allow for closed loop testing
 - DR.6 The supporting software shall log the simulated satellite motion computed by the customer simulation

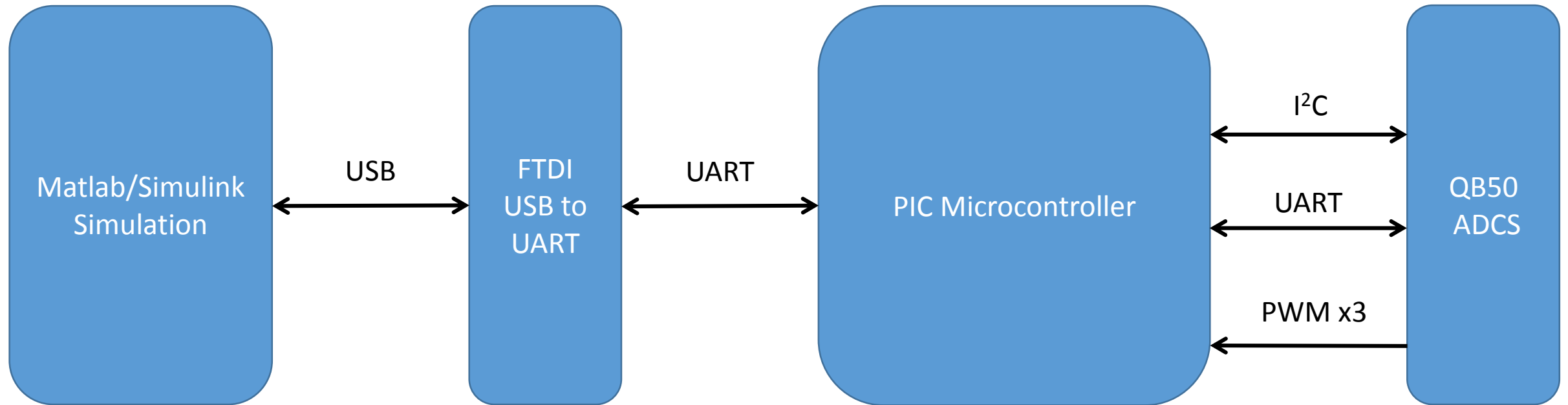
Input to ADCS

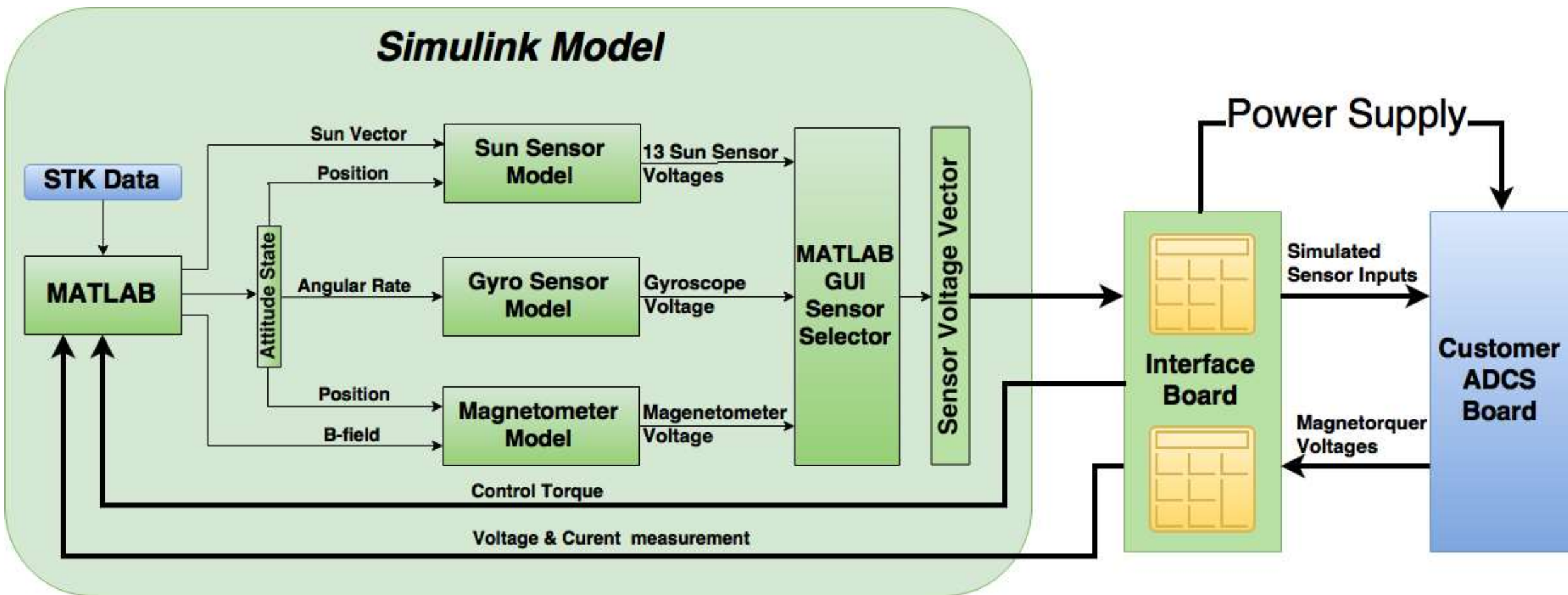
- 15 Analog Sun Sensors
 - Analog to Digital conversion takes place at the sensors
 - Communicate to the ADCS over I2C
- 3 Rate Gyros
 - Communicate over I2C
- 3 Magnetometers
 - Communicate over I2C
- 1 GPS
 - Communicates over UART

Output from ADCS

- 3 magnetorquer PWM signals
 - Operates at 1kHz
- Voltage and current measurement of 5V line to ADCS
 - Max expected current of 600mA
- Voltage and current measurement of 3.3V line to ADCS
 - Less than 20mA

Interface Board





Interface Board - Components

Component	Manufacturer	Part Number	Price
Master Microcontroller	Microchip	PIC18F65J94	\$3.94
Slave Microcontroller	Microchip	PIC16F18325	\$1.18
USB to UART	FTDI	FT232RL	\$4.50
Current Sensor	Allegro	ACS712	\$4.82
Linear Voltage Regulator	STMicroelectronics	LD1117S33CTR	\$0.51
Printed Circuit Board	Advanced Circuits	N/A	\$33.00

Interface Board – Microcontrollers

PIC18F65J94

- 4 - UART
- 2 - I2C
- 16 10/12-Bit A/D Channels
 - 500ksps @ 10-Bits
 - 200ksps @ 12-Bits
- 7 - CCP modules
 - Run at a scaled rate to oscillator

PIC16F18325

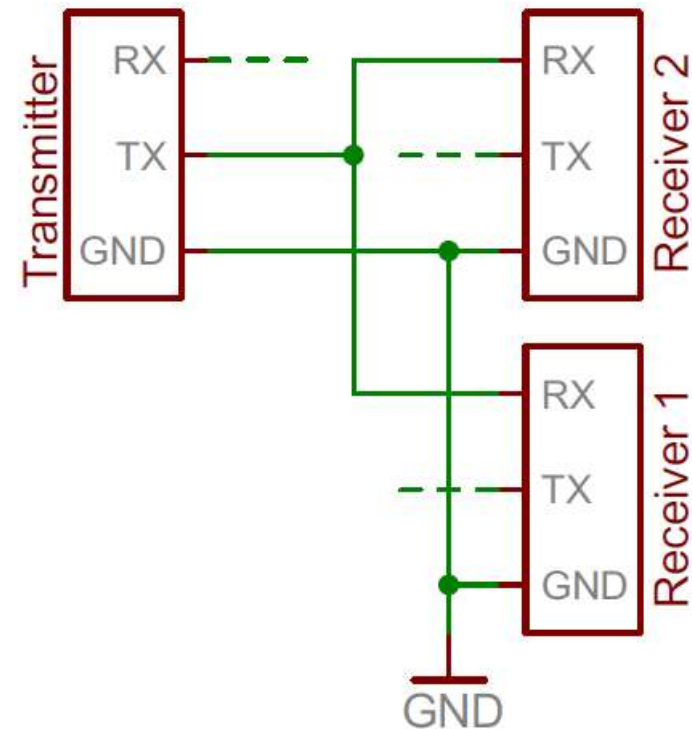
- 1 – UART
 - Allows communication to master microcontroller
- 2 - I2C
 - Allows each microprocessor to emulate 2 sensors

UART – 1 transmitter, multiple receivers

“It can be safe to connect multiple receiving devices to a single transmitting device. Not really up to spec and probably frowned upon by a hardened engineer, but it’ll work. For example, if you’re connecting a serial LCD up to an Arduino, the easiest approach may be to connect the LCD module’s RX line to the Arduino’s TX line. The Arduino’s TX is already connected to the USB programmer’s RX line, but that still leaves just one device in control of the transmission line.”

“Distributing a TX line like this can still be dangerous from a firmware perspective, because you can’t pick and choose which device hears what transmission. The LCD will end up receiving data not meant for it, which could command it to go into an unknown state.”

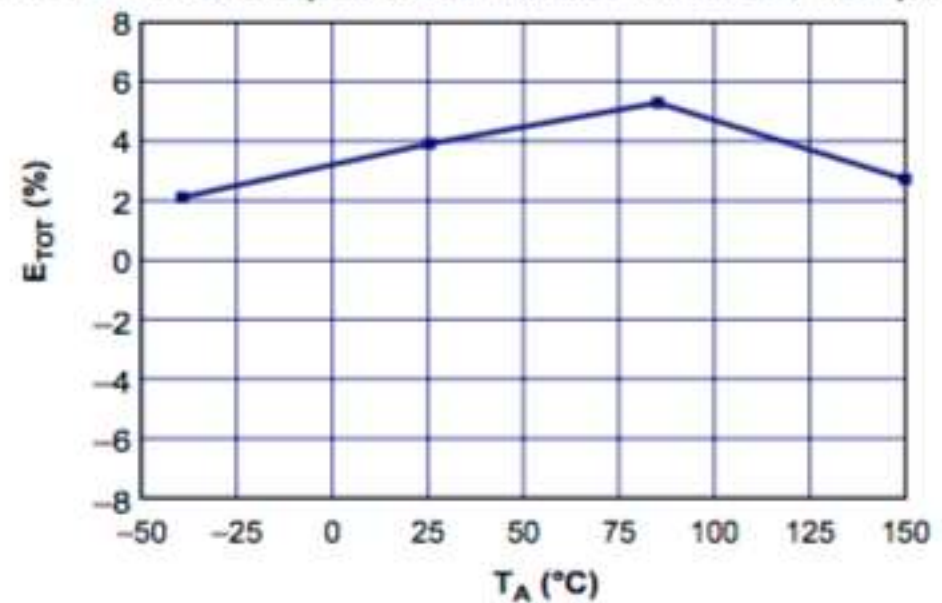
<https://learn.sparkfun.com/tutorials/serial-communication>



Interface Board - Current Sensor

- 1.5% Typical total output error
- PIC 12-Bit ADC between 0 and 5 Volts
 - $5/(2^{12}) = 1.2\text{mV}$ resolution
- Current sensor sensitivity
 - 185mV/A base
 - 610mV/A with op-amp
- Current resolution
 - 6.5mA
 - 2.0mA

Mean Total Output Error versus Ambient Temperature



(tested using the ACS712ELC-05A).

Interface Board – Power Budget

Interface Board

- Microchip eXtreme Low Power
 - As low as 35uA/Mhz for 8-Bit MCU
 - 0.35mA at 10Mhz
 - <10mA for 23 MCUs
- FTDI < 25mA
- Current Sensor < 13mA

Total: ~48mA

Customer ADCS

- Beaglebone < 500mA
 - Observed ~250mA in normal operation
- Magnetorquers
 - 90 Ohms @ 5V is 56mA max
 - <167mA for 3 magnetorquers
- Sensors < 20mA

Total: ~ 437mA

Current Sensor – ACS712

Selection Guide

Part Number	Packing*	T _A (°C)	Optimized Range, I _P (A)	Sensitivity, Sens (Typ) (mV/A)
ACS712ELCTR-05B-T	Tape and reel, 3000 pieces/reel	–40 to 85	±5	185
ACS712ELCTR-20A-T	Tape and reel, 3000 pieces/reel	–40 to 85	±20	100
ACS712ELCTR-30A-T	Tape and reel, 3000 pieces/reel	–40 to 85	±30	66

*Contact Allegro for additional packing options.

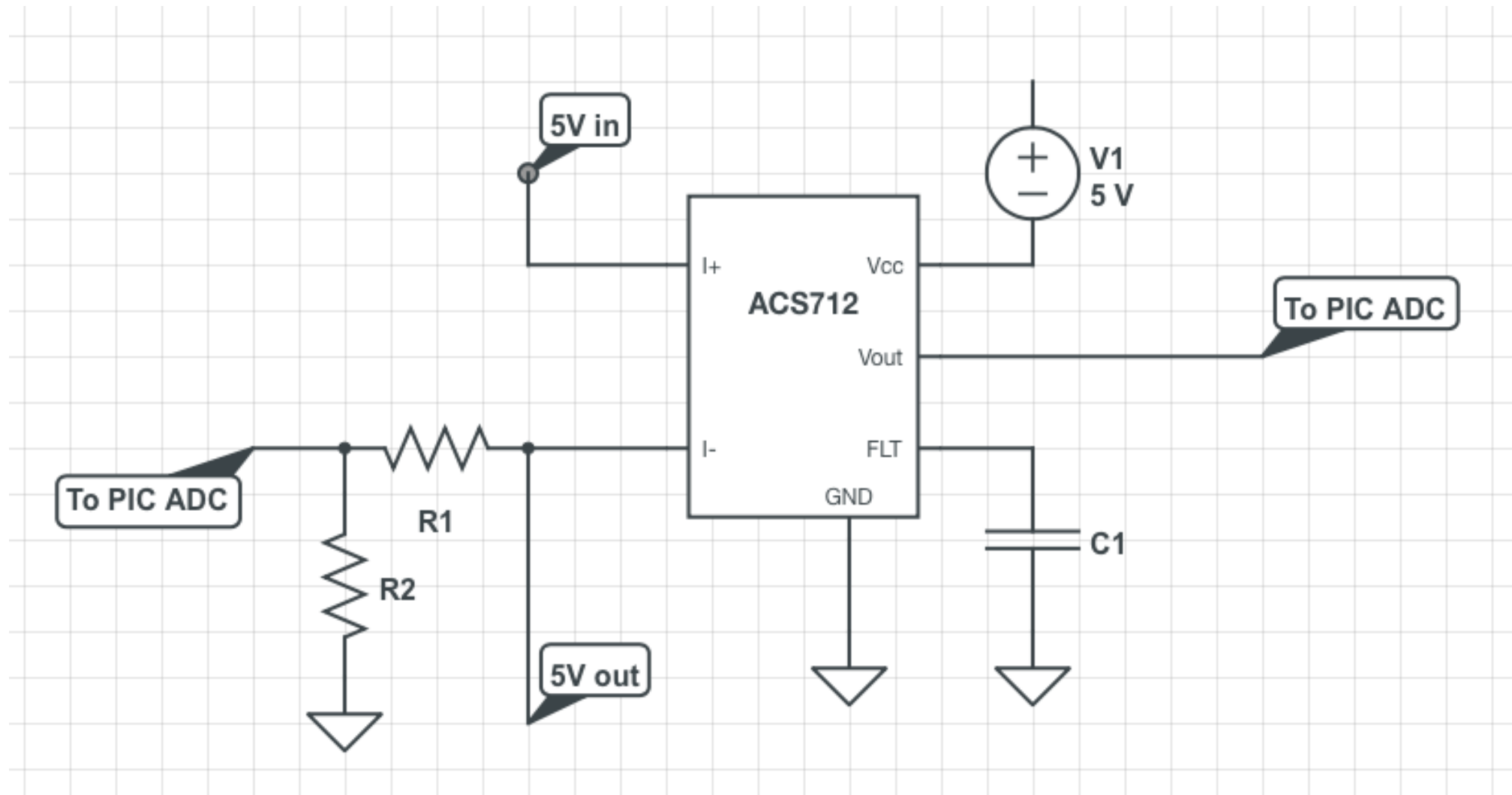
Absolute Maximum Ratings

Characteristic	Symbol	Notes	Rating	Units
Supply Voltage	V _{CC}		8	V
Reverse Supply Voltage	V _{RCC}		–0.1	V
Output Voltage	V _{IOUT}		8	V
Reverse Output Voltage	V _{RIOUT}		–0.1	V
Reinforced Isolation Voltage	V _{ISO}	Pins 1-4 and 5-8; 60 Hz, 1 minute, T _A =25°C	2100	V
		Voltage applied to leadframe (Ip+ pins), based on IEC 60950	184	V _{peak}
Basic Isolation Voltage	V _{ISO(bsc)}	Pins 1-4 and 5-8; 60 Hz, 1 minute, T _A =25°C	1500	V
		Voltage applied to leadframe (Ip+ pins), based on IEC 60950	354	V _{peak}
Output Current Source	I _{IOUT(Source)}		3	mA
Output Current Sink	I _{IOUT(Sink)}		10	mA
Overcurrent Transient Tolerance	I _P	1 pulse, 100 ms	100	A
Nominal Operating Ambient Temperature	T _A	Range E	–40 to 85	°C
Maximum Junction Temperature	T _J (max)		165	°C
Storage Temperature	T _{stg}		–65 to 170	°C

Features and Benefits

- Low-noise analog signal path
- Device bandwidth is set via the new FILTER pin
- 5 μs output rise time in response to step input current
- 80 kHz bandwidth
- Total output error 1.5% at T_A = 25°C
- Small footprint, low-profile SOIC8 package
- 1.2 mΩ internal conductor resistance
- 2.1 kV_{RMS} minimum isolation voltage from pins 1-4 to pins 5-8
- 5.0 V, single supply operation
- 66 to 185 mV/A output sensitivity
- Output voltage proportional to AC or DC currents
- Factory-trimmed for accuracy
- Extremely stable output offset voltage
- Nearly zero magnetic hysteresis
- Ratiometric output from supply voltage

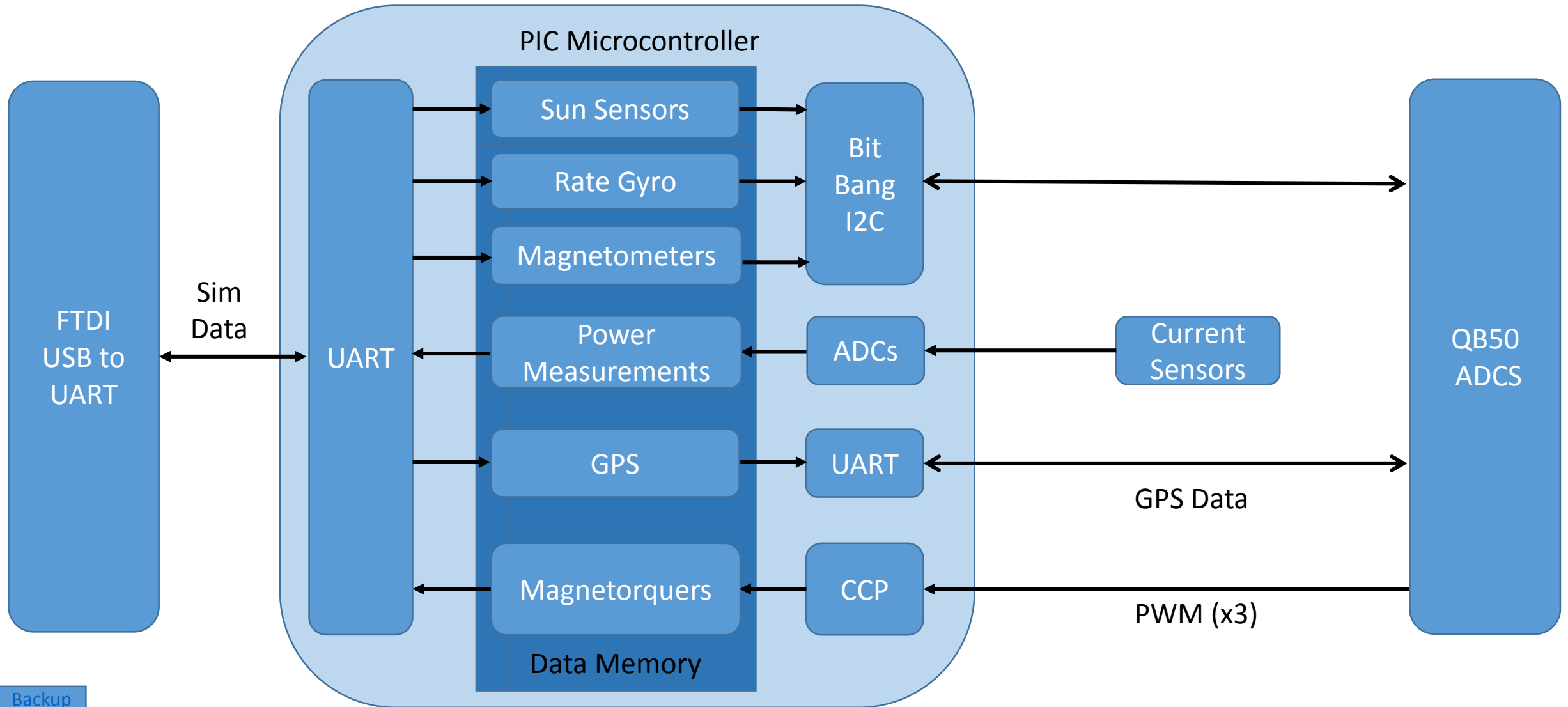
Current and Voltage Measurement



Voltage Regulator – LD1117

Symbol	Parameter	Test condition	Min.	Typ.	Max.	Unit
V_O	Output voltage	$V_{in} = 5.3 \text{ V}$, $I_O = 10 \text{ mA}$, $T_J = 25 \text{ }^\circ\text{C}$	3.267	3.3	3.333	V
V_O	Output voltage	$I_O = 0$ to 800 mA , $V_{in} = 4.75$ to 10 V	3.235		3.365	V
ΔV_O	Line regulation	$V_{in} = 4.75$ to 15 V , $I_O = 0 \text{ mA}$		1	6	mV
ΔV_O	Load regulation	$V_{in} = 4.75 \text{ V}$, $I_O = 0$ to 800 mA		1	10	mV
ΔV_O	Temperature stability			0.5		%
ΔV_O	Long term stability	1000 hrs, $T_J = 125 \text{ }^\circ\text{C}$		0.3		%
V_{in}	Operating input voltage	$I_O = 100 \text{ mA}$			15	V
I_d	Quiescent current	$V_{in} \leq 15 \text{ V}$		5	10	mA
I_O	Output current	$V_{in} = 8.3 \text{ V}$, $T_J = 25 \text{ }^\circ\text{C}$	800	950	1300	mA
eN	Output noise voltage	$B = 10 \text{ Hz}$ to 10 kHz , $T_J = 25 \text{ }^\circ\text{C}$		100		μV
SVR	Supply voltage rejection	$I_O = 40 \text{ mA}$, $f = 120 \text{ Hz}$, $T_J = 25 \text{ }^\circ\text{C}$ $V_{in} = 6.3 \text{ V}$, $V_{ripple} = 1 \text{ V}_{PP}$	60	75		dB
V_d	Dropout voltage	$I_O = 100 \text{ mA}$		1	1.1	V
		$I_O = 500 \text{ mA}$		1.05	1.15	
		$I_O = 800 \text{ mA}$		1.10	1.2	
	Thermal regulation	$T_a = 25 \text{ }^\circ\text{C}$, 30 ms Pulse		0.01	0.1	%/W

Interface Board – Bit Bang Method



Simulation

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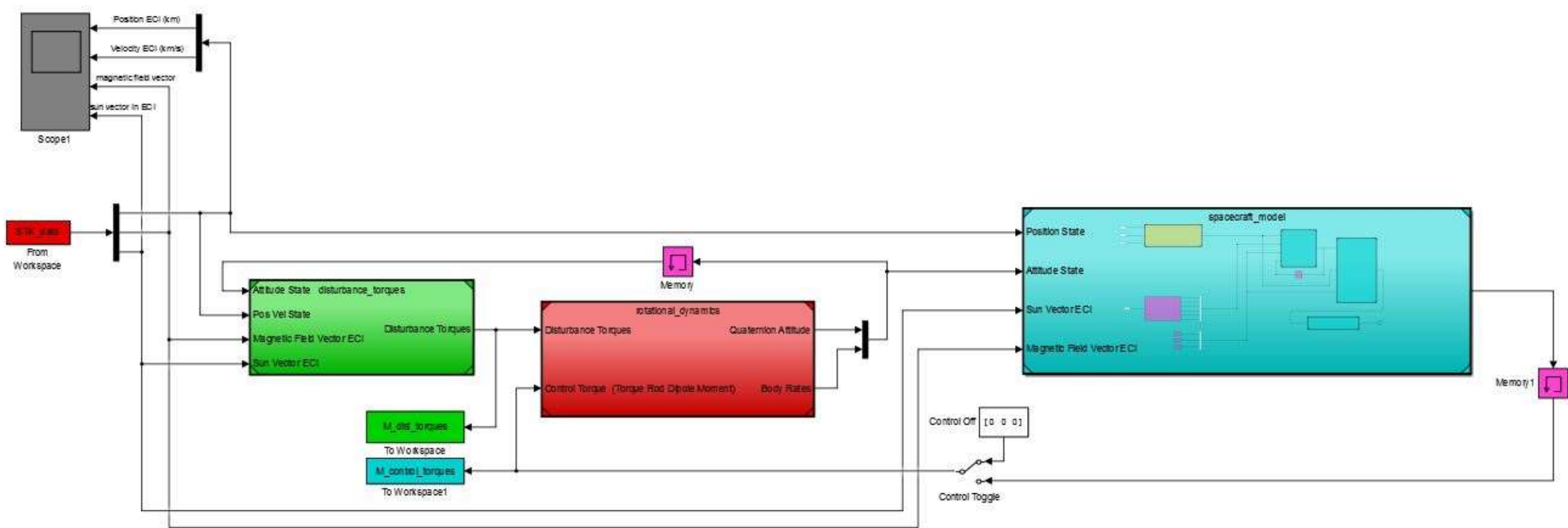
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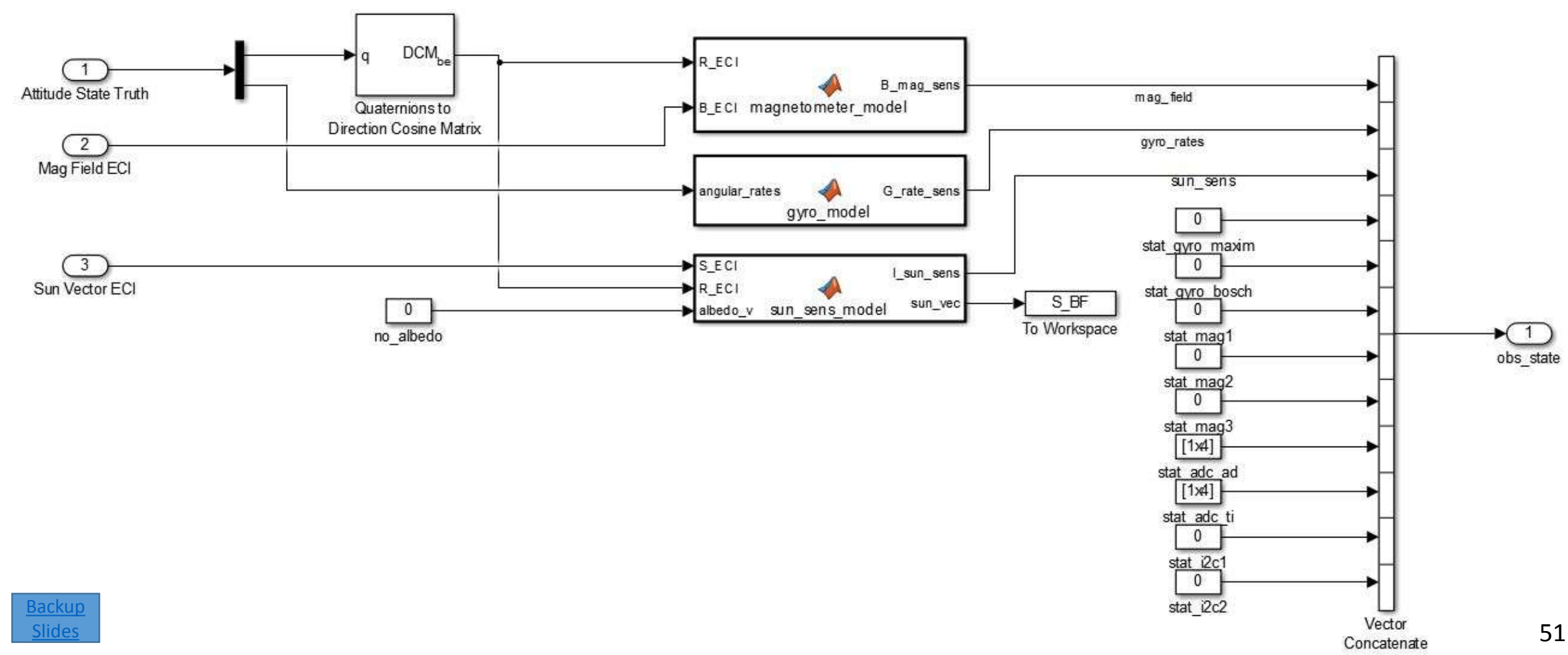
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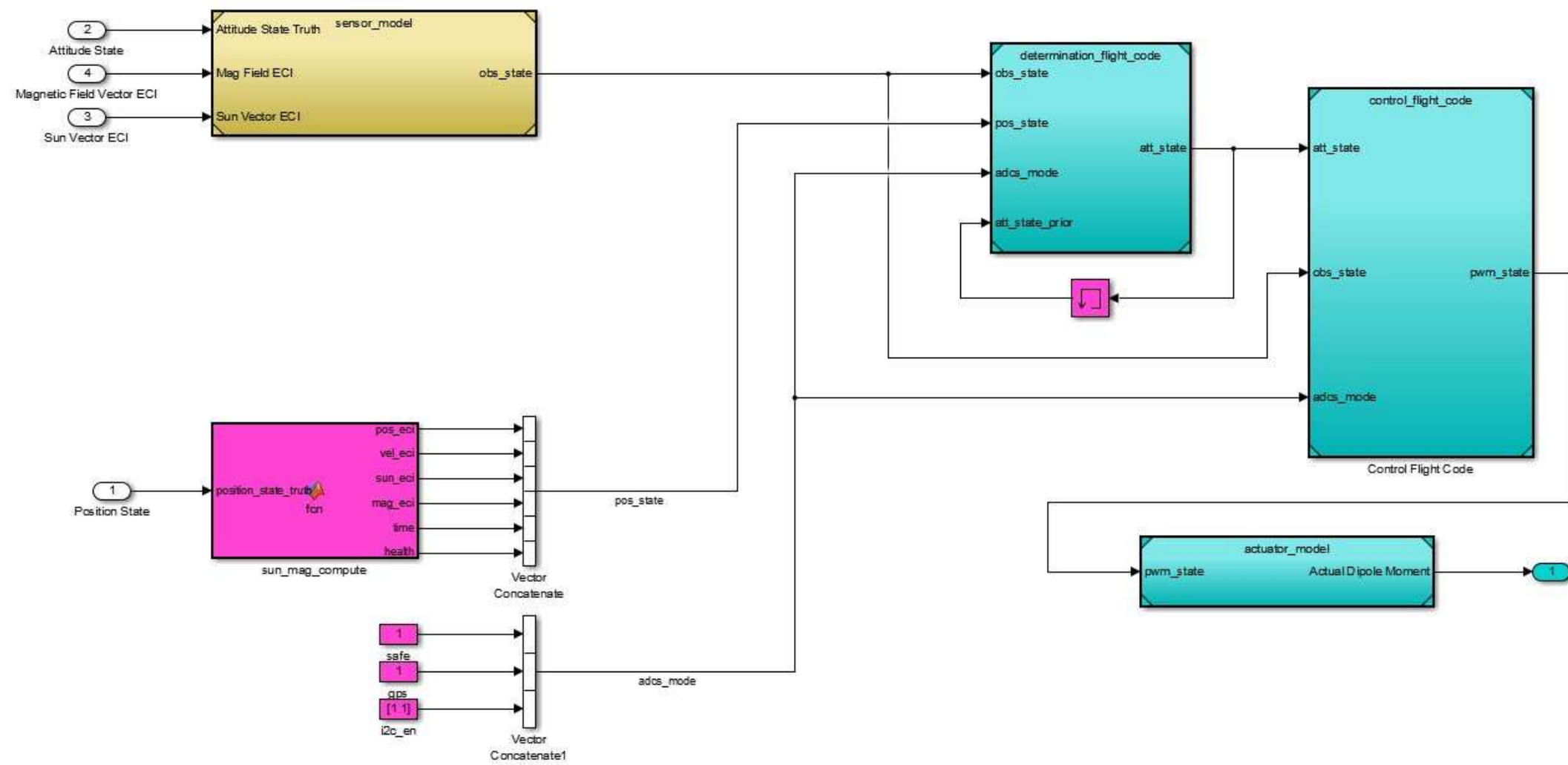
CUBESAT SIMULATION MODEL



CUBESAT SIMULATION MODEL



CUBESAT SIMULATION MODEL



Sensor Override

The image shows a 'Sensor Override' interface with three main sections: 'Coarse Sun Sensor', 'GPS Sensor', and 'Magnetometers'. Each section contains various controls for overriding sensor data.

Coarse Sun Sensor

- ☒ Simulation Data
- ☐ Kill Sensor
- ☐ Increase Noise 10%
- ☐ Offset/Drift -13mV

GPS Sensor

- ☐ Kill X
- ☐ Kill Y
- ☐ Kill Z
- ☒ Kill Time

Magnetometers

☐ Kill X	☐ Kill Y	☐ Kill Z	☐ Offset/Drift X Gauss	☒ Offset/Drift Y Gauss	☐ Offset/Drift Z Gauss
☐ Increase Noise X %	☐ Increase Noise Y %	☐ Increase Noise Z %			

USB Power Supply

- Use External USB Battery
- Royal PB10000
- 2 USB Lines
 - 5V, 2.1 A
 - 5A, 1 A
- 10,000 mAh



Image from <http://newgizmoblog.com/wp-content/uploads/2014/10/Royal-Power-1.jpg>

Trade Studies

Processor Weight Table

Criteria	Sub-Criteria	Percentages		Weights	
Performance	-	30%	-	0.30	-
-	Speed/Freq.	-	20%	-	0.20
-	Power	-	10%	-	0.10
Reliability	-	10%	-	0.10	-
-	Long Term	-	5%	-	0.05
-	Consistency	-	5%	-	0.15
Language	-	40%	-	0.40	-
-	Learning Curve	-	20%	-	0.20
-	Ease of Use	-	20%	-	0.20
Cost	-	10%	-	0.10	-
Support	-	10%	-	0.10	-
		100%		1.00	

Software/GUI Weight Table

Criteria	Sub-Criteria	Percentages		Weights	
License	-	5%	-	0.05	-
Learning Curve	-	35%	-	0.35	-
Ease of Use	-	25%	-	0.25	-
Compatibility	-	35%	-	0.35	-
-	Software	-	15%	-	0.15
-	Hardware	-	20%	-	0.20
		100%		1.00	

Trade Study Results

Summary Matrix			PIC		Arduino		FPGA		Ras Pi	
Criteria	Sub-Criteria	Weight	Raw Score	Weighted Score	Raw Score	Weighted Score	Raw Score	Weighted Score	Raw Score	Weighted Score
Performance	-	30%	-	-	-	-	-	-	-	-
	Speed/Frequency	20%	3	0.60	3	0.60	5	1.00	4	0.80
	Power Use	10%	3	0.30	4	0.40	5	0.50	2	0.20
Reliability	-	10%	-	-	-	-	-	-	-	-
	Long Term Use	5%	5	0.25	5	0.25	5	0.25	5	0.25
	Consistency	5%	4	0.20	4	0.20	5	0.25	4	0.20
Language	-	40%	-	-	-	-	-	-	-	-
	Learning Curve	20%	4	0.80	4	0.80	1	0.20	3	0.60
	Ease of Use	20%	4	0.80	5	1.00	1	0.20	3	0.60
Cost	-	10%	5	0.50	4	0.40	5	0.50	4	0.40
Support	-	10%	5	0.50	4	0.40	2	0.20	3	0.30
TOTAL			-	3.95	-	4.05	-	3.10	-	3.35

Summary Matrix			Matlab		LabView		C	
Criteria	Sub-Criteria	Weight	Weighted Score	Raw Score	Weighted Score	Raw Score	Weighted Score	Weighted Score
License	-	5%	5	0.25	2	0.10	4	0.20
Learning Curve	-	35%	5	1.75	4	1.40	3	1.05
Compatibility	-	35%	-	-	-	-	-	-
-	Software	15%	5	0.75	4	0.60	3	0.45
-	Hardware	20%	4	0.80	5	1.00	3	0.60
Ease of Use	-	25%	4	1.00	4	1.00	2	0.50
TOTAL			-	4.55	-	4.10	-	2.80

Sun Sensor Calibration Table

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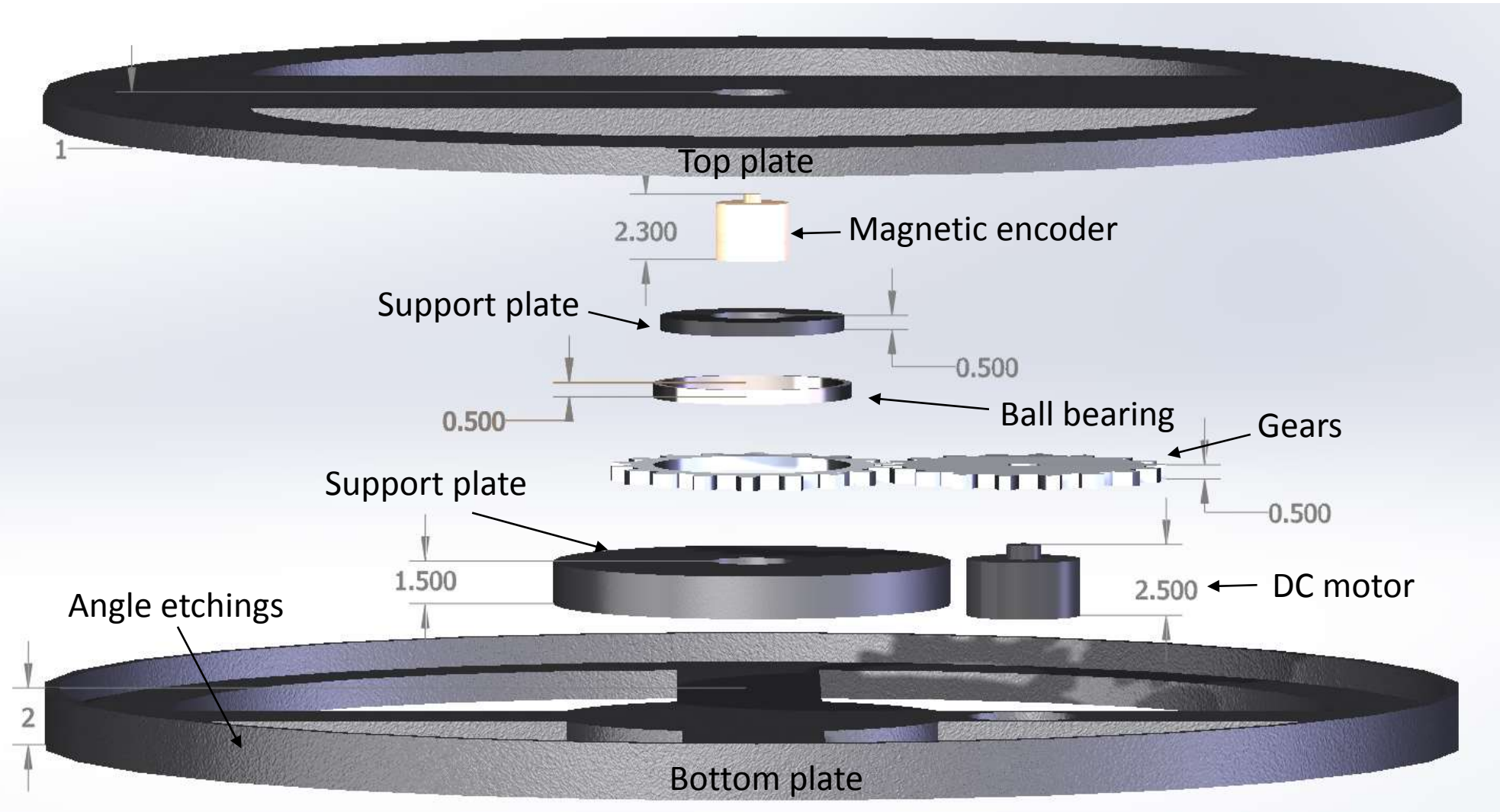
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Sun Sensor Calibration Table – Full Model



All measurements in centimeters

Sun Sensor Calibration Table – Torque Calculation

τ_R = max motor torque required (N*m) g = gravity = 9.81 m/s²

ρ = max density of Aluminum = 2830 kg/m³

r = radius of board = 0.25 m t = max thickness of board = 0.03 m

m_c = max mass of CubeSat (3U) = 3.6 kg m_t = max total mass (kg)

C_f = max bearing coefficient of friction = 0.0015

$$m_t = \rho * \pi * r^2 * t + m_c = 20.270 \text{ kg}$$

$$\tau_R = C_f * m_t * g * r \approx 0.0746 \text{ N * m}$$

*Assumes 1:1 gear ratio

Sun Sensor Calibration Table – RPM Calculation

f = sampling frequency of Sun sensors = 10 Hz

n_m = number of teeth on motor gear

n_b = number of teeth on board/shaft gear

Need at least one sample per degree:

$$\text{Max board RPM} = 1^\circ * f = 10^\circ/\text{second} = 5/3 \text{ RPM}$$

$$\text{Gear Ratio} = \frac{n_m}{n_b}$$

$$\text{RPM}_{\text{board}} = \frac{5}{3} \geq \frac{\text{RPM}_{\text{motor}}}{\text{Gear Ratio}}$$

Sun Sensor Calibration Table – Bit Calculation

Rotate with resolution of 1° with $\pm 0.5^\circ$ accuracy

- US Digital - MAE3 Absolute Magnetic Kit Encoder
- 10-bit analog output

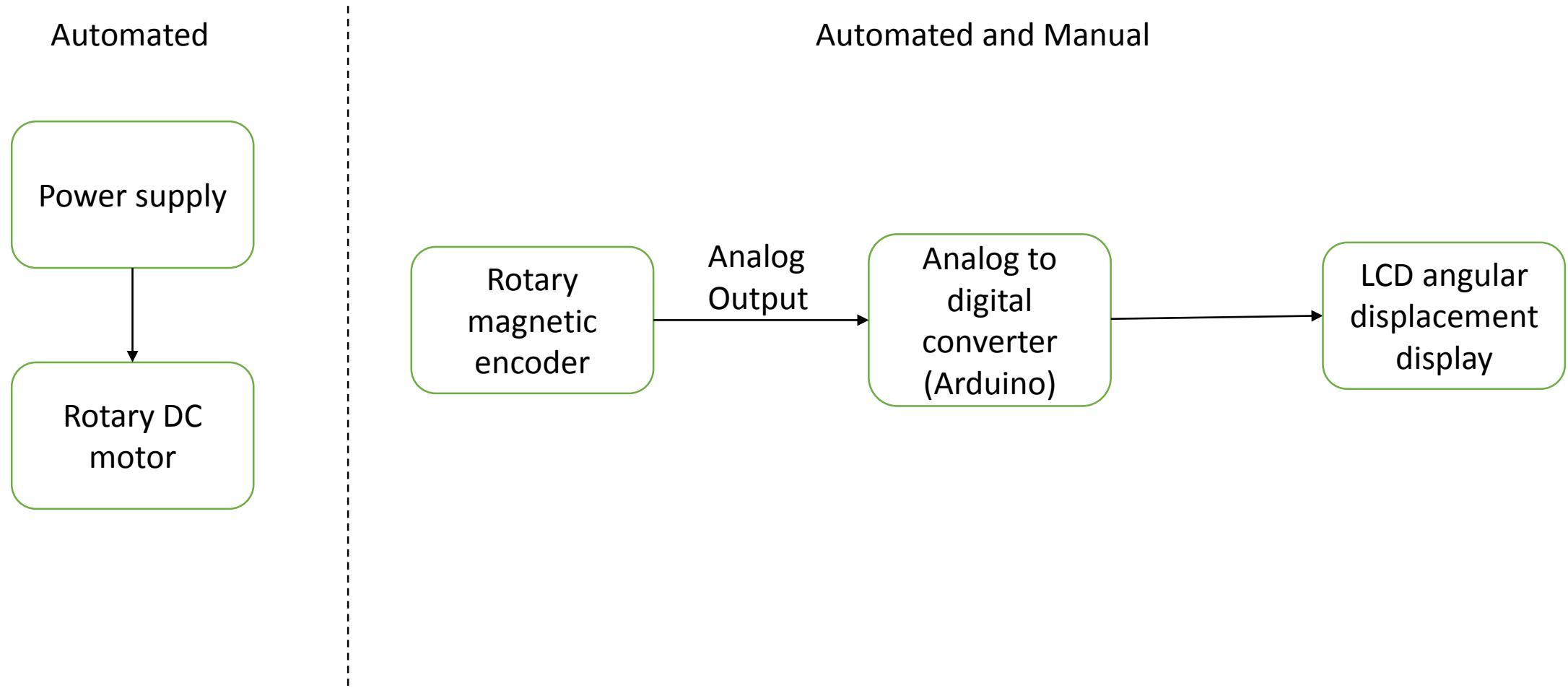
$$\text{Resolution} = 360^\circ / 2^{10} = 0.352^\circ \text{ per bit}$$

Sun Sensor Calibration Table – Reflectivity

Reflectivity less than or equal to 5% for visible wavelengths (400-700 nm)

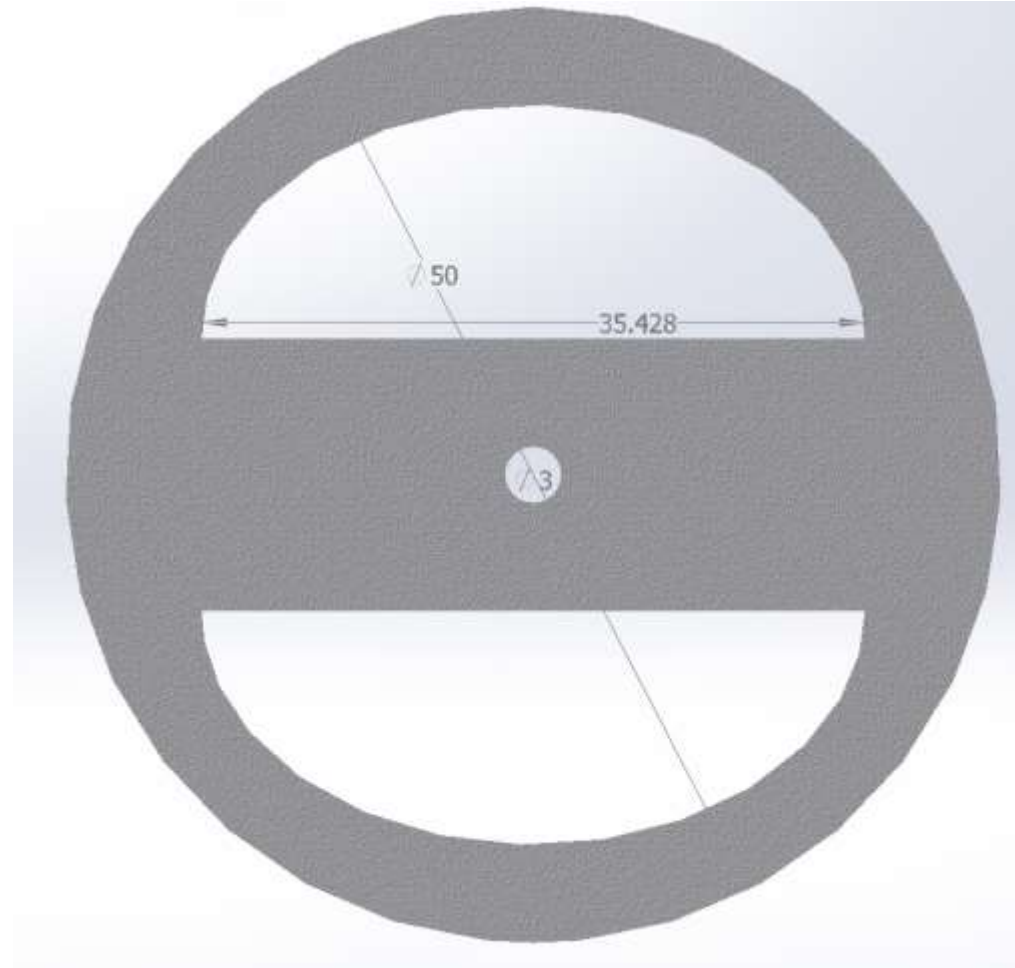
- Avian Technologies LLC
- Avian Black-S coating has reflectance of 3.1% in visible wavelengths

Sun Sensor Calibration Table - Flow Chart



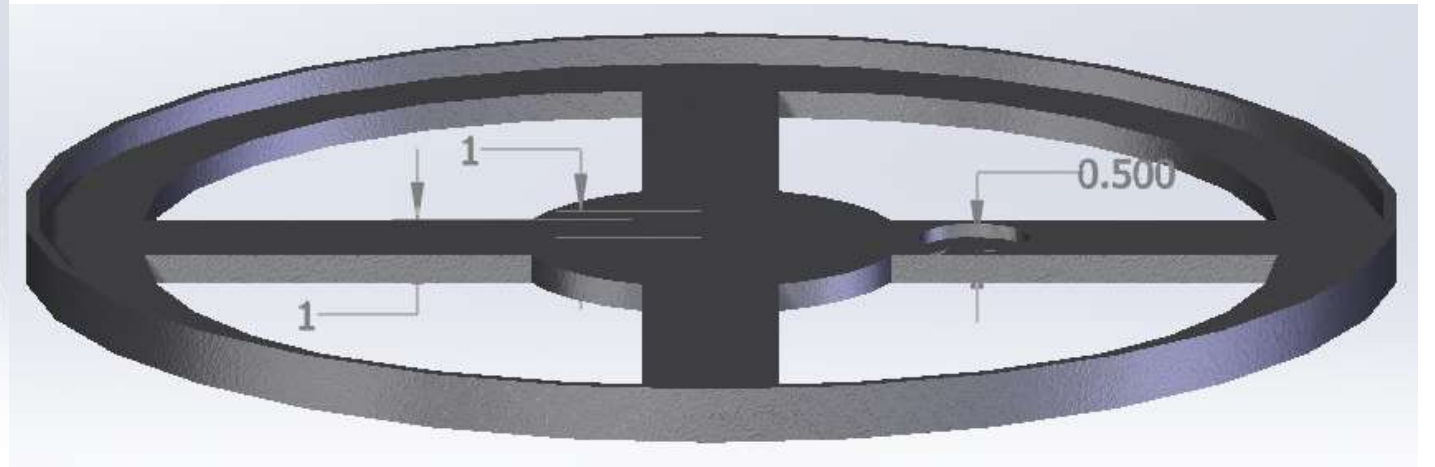
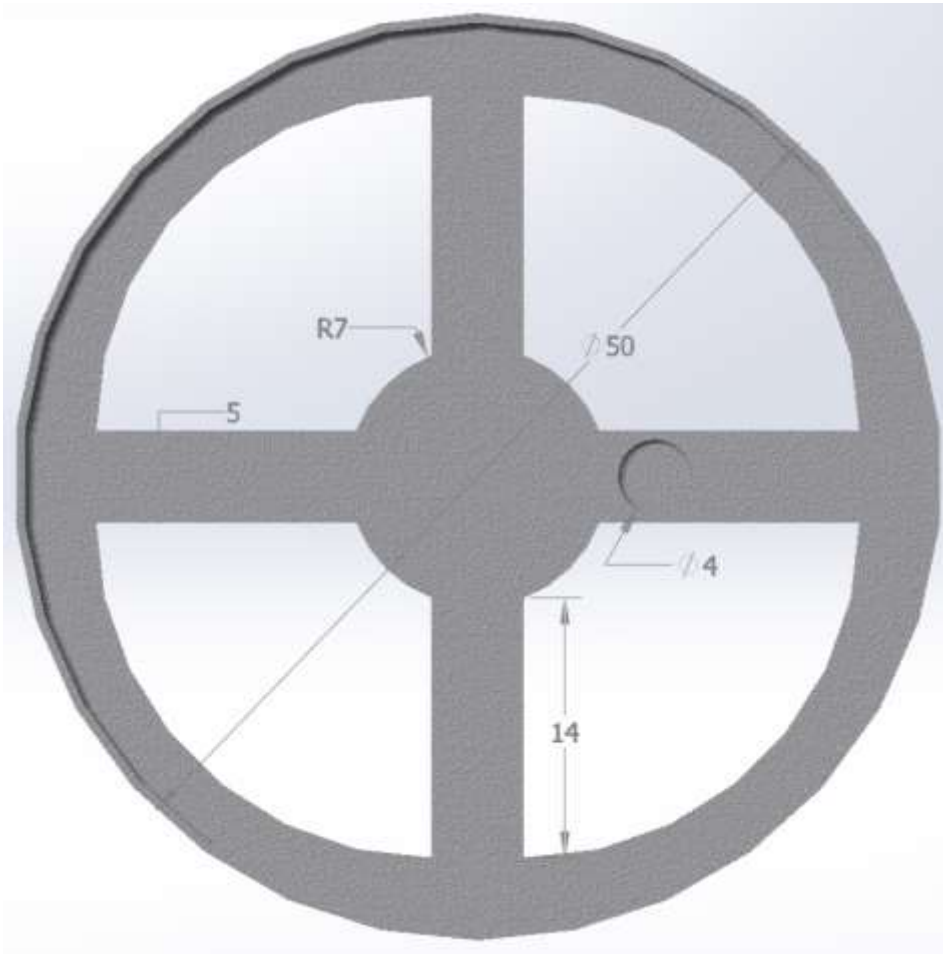
Sun Sensor Calibration Table – Part Model

Top Platform – all measurements in centimeters



Sun Sensor Calibration Table – Part Model

Bottom Platform – all measurements in centimeters



Sun Sensor Calibration Table - Components

- 2x Aluminum disk, made from 50x50x3cm block
- 2x Aluminum gear, made from same Aluminum block
- Mechanical ball bearing
- Rotary magnetic encoder
- DC motor
- Analog to digital converter
- Digital LCD display

Functional Requirement 3

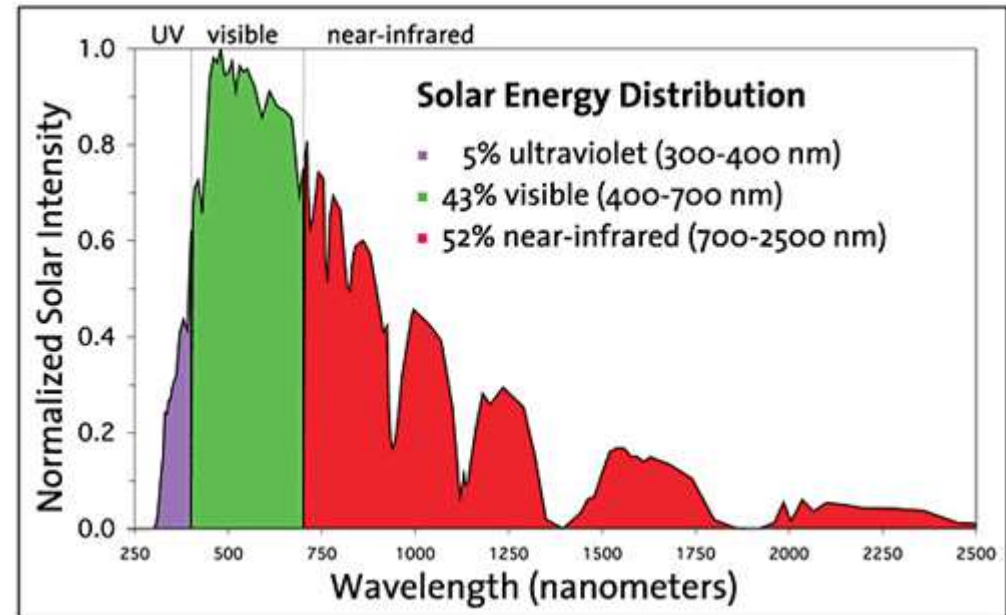
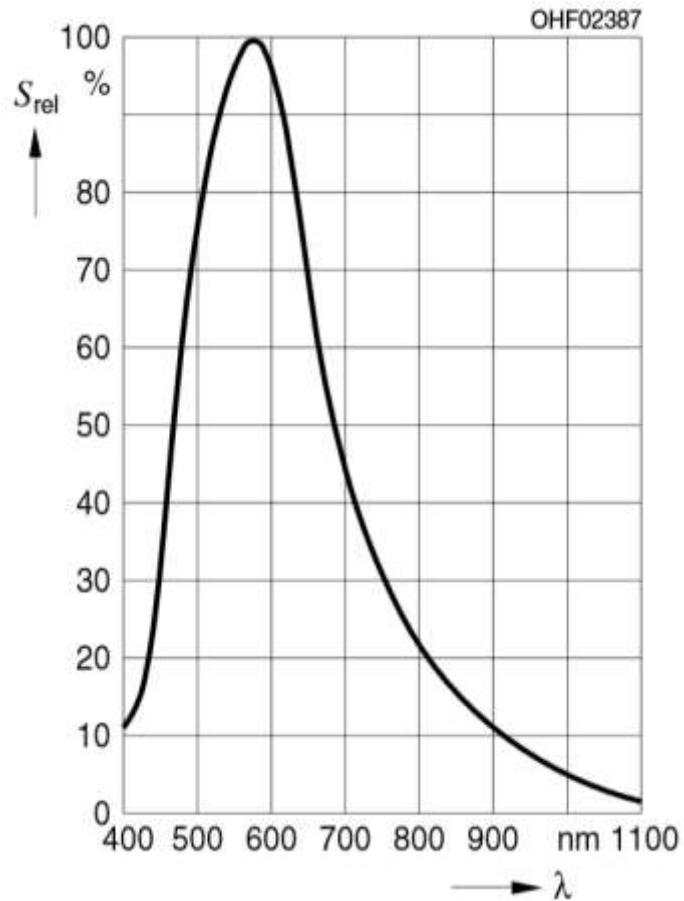
- A turn table shall be delivered to the QB50 team that has resolution of 1 degree with accuracy of $\pm 0.5^\circ$
 - DR.1 The turn table should have low reflectivity
 - DR.1.1 The table will not have an albedo exceeding 5% in the visible light spectrum
 - DR.2 The table shall sense angular position and display it to the user
 - DR.3 A stepper motor shall be used to rotate the table

OSRAM SFH 2430 Sun Sensor

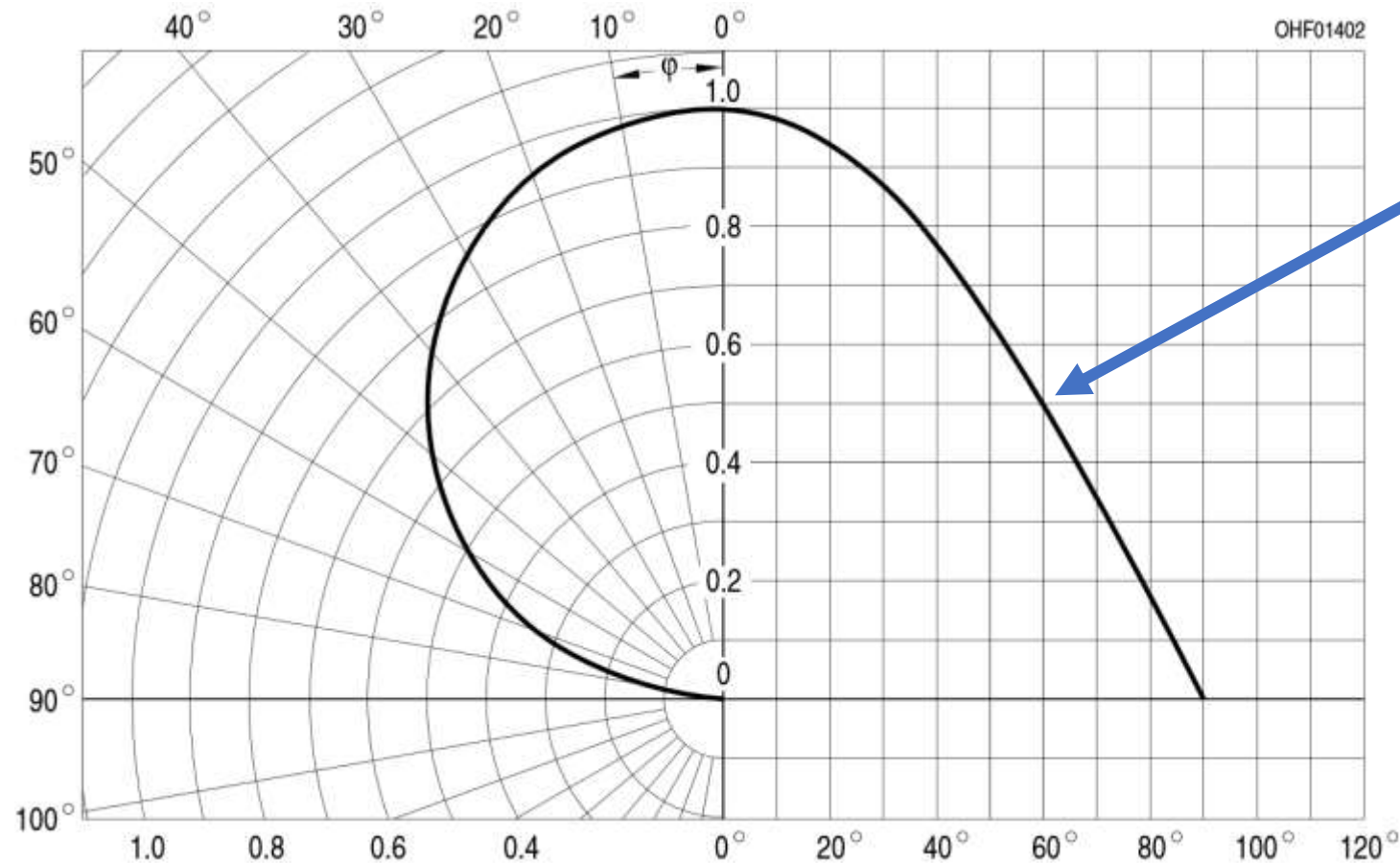
- Peak Wavelength: 570 nm
- Rise Time: 200 μ s
- Fall Time: 200 μ s
- Forward Current: 100 mA
- Power Dissipation: 150 mW



Sensor EM Spectrum vs. Solar EM Spectrum



Directional Characteristics



- $\frac{1}{2}$ angle $\sim 60^\circ$
- Generally follows a cosine function until 60° angle

Trade Studies

• Sun Sensor Table Weights

Criteria	Sub-Criteria	Percentages	Weights
Time to Design	-	25%	0.25
Time to Make	-	25%	0.25
Reliability	-	20%	0.20
Ease of Use	-	20%	0.20
Cost	-	10%	0.10
		100%	1.00

• Angular Position Sensor Weights

Criteria	Sub-Criteria	Percentages	Weights
Accuracy	-	40%	0.40
Integration	-	25%	0.25
Life Cycle	-	5%	0.05
Ease of Use	-	10%	0.10
Cost	-	20%	0.20
		100%	1.00

Trade Study Results

Summary Matrix		Manual		Semi-Manual		PC	
Criteria	Weight	Raw Score	Weighted Score	Raw Score	Weighted Score	Raw Score	Weighted Score
Time to Design	25%	5	1.25	3	0.75	2	0.50
Time to Make	25%	4	1.00	3	0.75	1	0.25
Reliability	20%	5	1.00	4	0.80	2	0.40
Ease of Use	20%	2	0.40	4	0.80	5	1.00
Cost	10%	5	0.50	3	0.30	2	0.20
TOTAL		-	4.15	-	3.40	-	2.35

Summary Matrix		Potentiometer		Optical Encoder	
Criteria	Weight	Raw Score	Weighted Score	Raw Score	Weighted Score
Accuracy	40%	4	1.60	4	1.60
Integration	25%	3	0.75	5	1.25
Life Cycle	5%	3	0.15	5	0.25
Ease of Use	10%	3	0.30	5	0.50
Cost	20%	5	1.00	3	0.60
TOTAL		-	3.80	-	4.20

Helmholtz Cage Test

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Helmholtz Cage Testing Structure: Backup Calculations - Torque from Satellite

Turning Authority (T_a) = $0.1 \text{ Am}^2 = 0.1 \text{ J/T}$

Magnetic Field Strength (B) = $0.5 \text{ Gs} = 5 \times 10^{-5} \text{ T}$

Maximum Torque = $B * T_a = 5 \times 10^{-6} \text{ Nm}$

Helmholtz Cage Testing Structure:

Backup Calculations - Modulus of Rigidity Test

L_0 = initial length of line

d = diameter of line

G = modulus of rigidity

E = modulus of elasticity

ν = Poisson's Ratio

σ = Normal Stress

ϵ = Strain

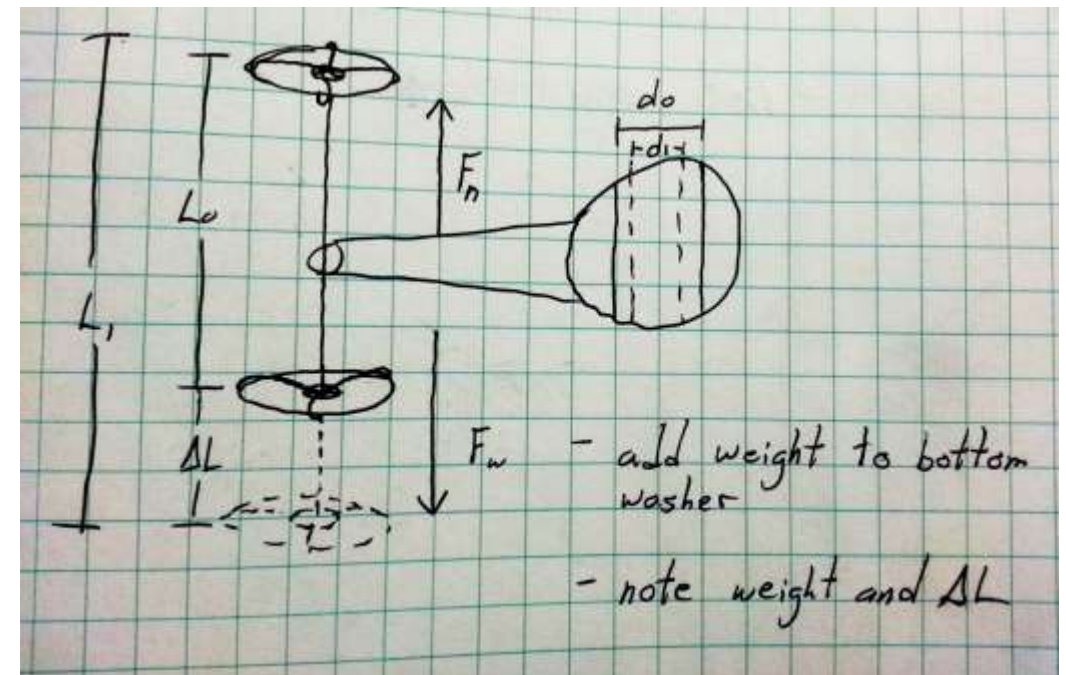
F = load on line

A_{CS} = cross-sectional area of line

$$E = \sigma / \epsilon_y \quad \sigma = F / A_{CS} \quad \epsilon_y = (L_1 - L_0) / L_0$$

$$\nu = \epsilon_x / \epsilon_y \quad \epsilon_x = (D_1 - D_0) / D_0$$

$$G = \frac{1}{2} * E * (1 - \nu)^{-1}$$



Helmholtz Cage Testing Structure:

Backup Calculations - Modulus of Rigidity Test

		E test [mm]				E test [N]				V test [mm]			
Line Type	Line Capacity	L ₀	L ₁	L ₂	L ₃	F ₀	F ₁	F ₂	F ₃	d ₀	d ₁	d ₂	d ₃
Braided	50 lbs	257	7.25 4	15.03	21.7 5	0	42	67	92	0.81	.608	.58	.569
Braided	27 lbs	225	47.5 2	15.28	21.2 8	0	30	42	57	.57	.46	.42	.41
Steelon	45 lbs	346	35.0	35.5	36.0	0	90	290	362	.682	.682	.673	.673
Steelon	20 lbs	253	5.00	9.76	12.0 2	0	15	76	126	.66	.51	.5	.5
Nanofil	17 lbs	316	32.2	32.6	33.2	0	14	43	76	.282	.29	.268	.263

Helmholtz Cage Testing Structure:

Backup Calculations - Line Resistive Torque

τ_{Line} = Resistive Torque from the line

τ_{Sat} = Torque from satellite = 5×10^{-6} Nm

L = length of line = 30 cm (half of the cage height)

J = polar moment of inertia

G = modulus of rigidity

θ = angular deflection = 360°
(requirement from customer)

r = cross-sectional radius of the line

Alternative Calculation

$$G_{\text{max}} = 2 * L * \tau_{\text{Sat}} * r^{-4} * \theta^{-1} * \pi^{-1}$$
$$= 0.5 \text{ GPa}$$

Compare to other materials

$$G_{\text{Aluminum}} = 27 \text{ GPa}$$

$$G_{\text{Polycarbonate}} = 2.3 \text{ GPa}$$

$$G_{\text{Polyethylene}} = 0.12 \text{ GPa}$$

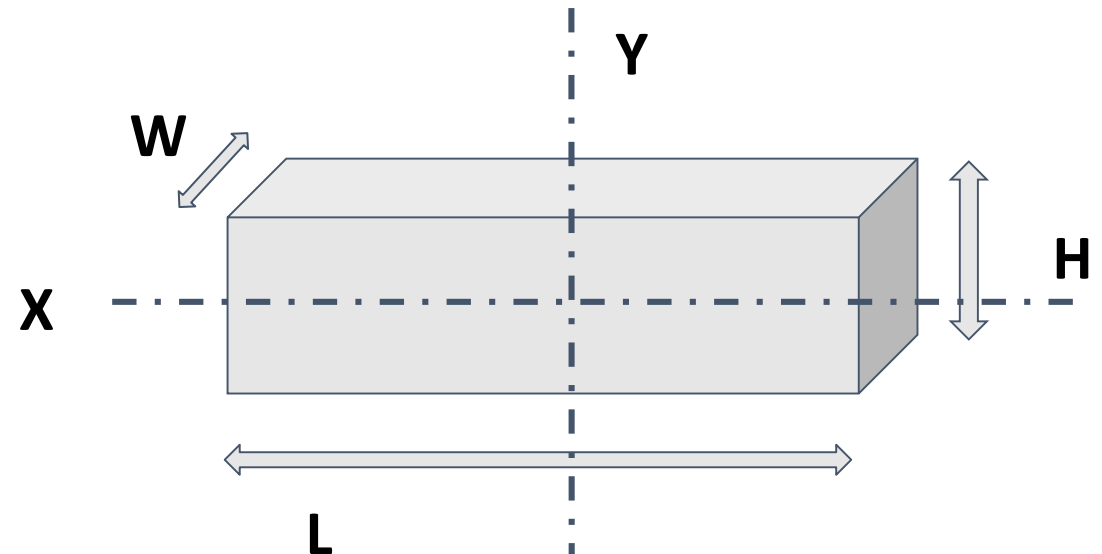
Assume line has smaller G than polyethylene

Helmholtz Cage Testing Structure:

Backup Calculations - Satellite Acceleration

τ_{Sat} = Torque from satellite = $5\text{E-}6$ Nm
 I = mass moment of inertia about y axis
 α = angular acceleration of satellite
 ω = angular velocity of satellite
 t = time satellite is accelerating
 L = length of satellite = 30 cm
 W = width of satellite = 10 cm
 H = Height of satellite = 10 cm
 m = mass of satellite = 3.6 kg
 V = velocity of satellite edge

$$\tau_{\text{Sat}} = I * \alpha \longrightarrow \alpha = \tau_{\text{Sat}} / I$$
$$I = (m/12 * W^2_{\text{outer}} + m/3 * L^2_{\text{outer}}) - (m/12 * W^2_{\text{inner}} + m/3 * L^2_{\text{inner}})$$
$$V = \alpha * t * L * \frac{1}{2}$$



Helmholtz Cage Testing Structure:

Backup Calculations - Moment From Drag

D = Drag Force

C_D = Drag Coefficient of flat plate = 1.05 to 2.05

- assumed to be 2.05 to be conservative

ρ = density = 1.05 kg/m³

- assumed to be standard atmosphere at 1500 m (5000 ft)

V = velocity of outermost satellite edge

A = Area of satellite side

M_D = Moment caused by Drag

$$D = \frac{1}{2} * \rho * V^2 * C_D * A$$

- V and A vary from the center to the edge of the satellite

$$M_D = \rho * \alpha^2 * t^2 * h * L^4 * C_D / (64)$$

- Drag was integrated over half of the satellite length

Helmholtz Cage Testing Structure:

Backup Calculations - Moment From Drag

D = Drag Force

C_D = Drag Coefficient of flat plate = 1.05 to 2.05

- assumed to be 2.05 to be conservative

ρ = density = 1.05 kg/m³

- assumed to be standard atmosphere at 1500 m (5000 ft)

V = velocity of outermost satellite edge

A = Area of satellite side

M_D = Moment caused by Drag

$$D = \frac{1}{2} * \rho * V^2 * C_D * A$$

- V and A vary from the center to the edge of the satellite

$$F_{\text{equivalent}} = D * L / 4$$

- Drag approximated by distributed load

$$d = \frac{2}{3} * r$$

$$M_D = 2 * F_{\text{equivalent}} * d$$

Helmholtz Cage Testing Structure: Backup Calculations - Moment From Drag

$$D = \frac{1}{2} * \rho * V^2 * C_D * A$$

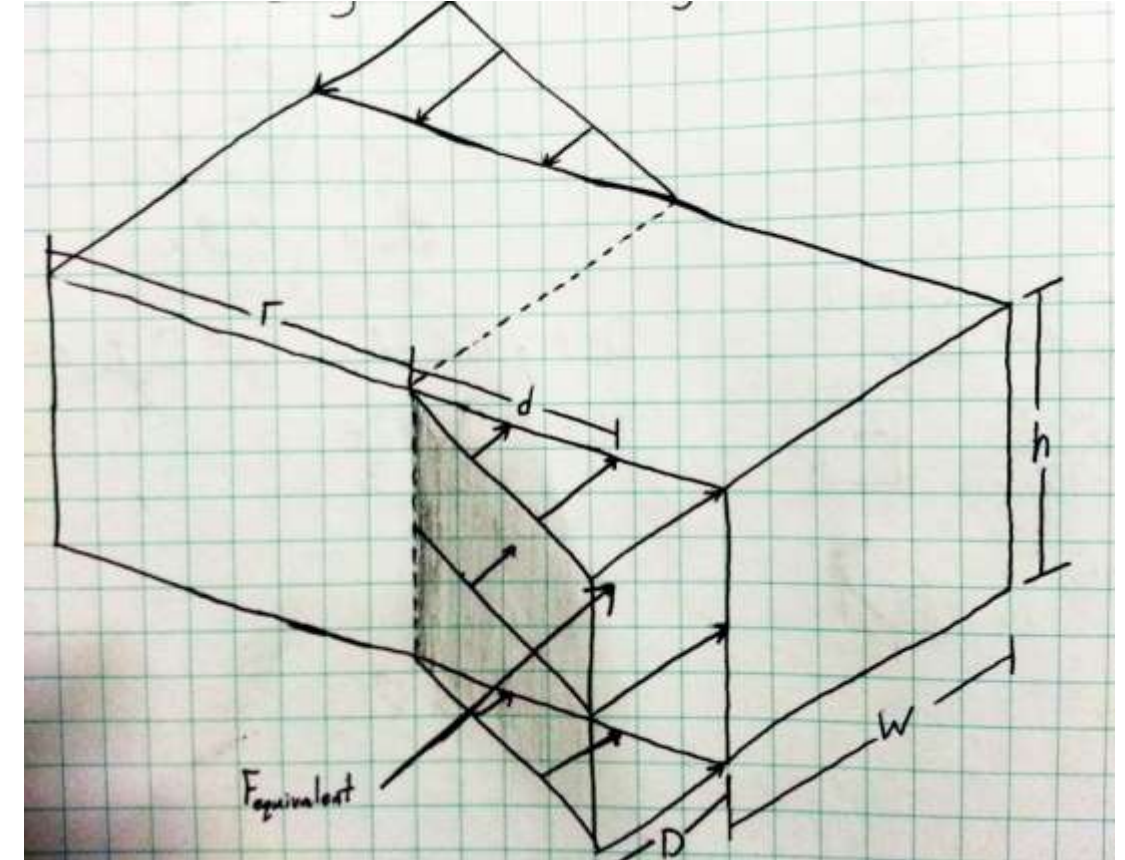
- V and A vary from the center to the edge of the satellite

$$F_{\text{equivalent}} = D * L / 4$$

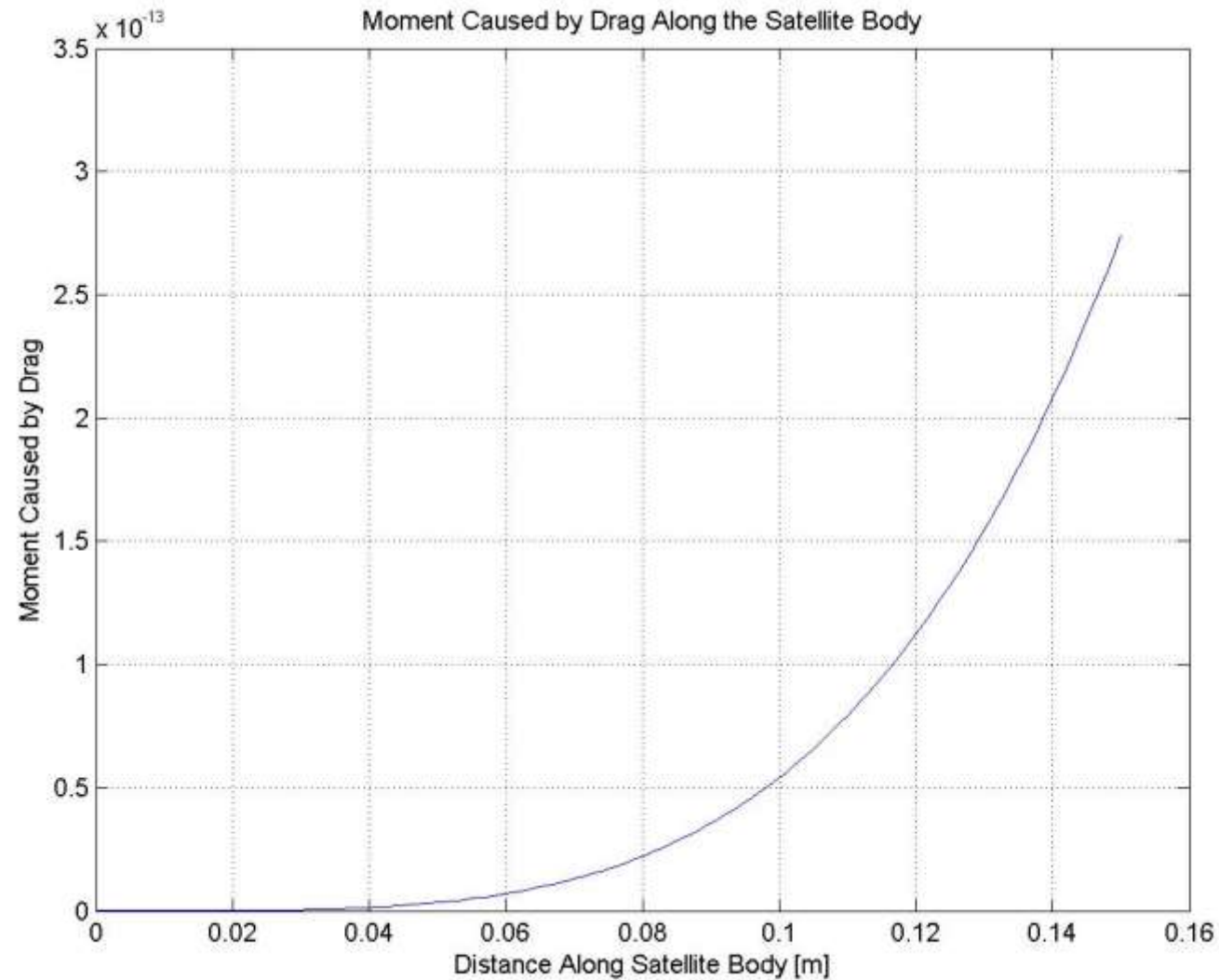
- Drag approximated by distributed load

$$d = \frac{2}{3} * r$$

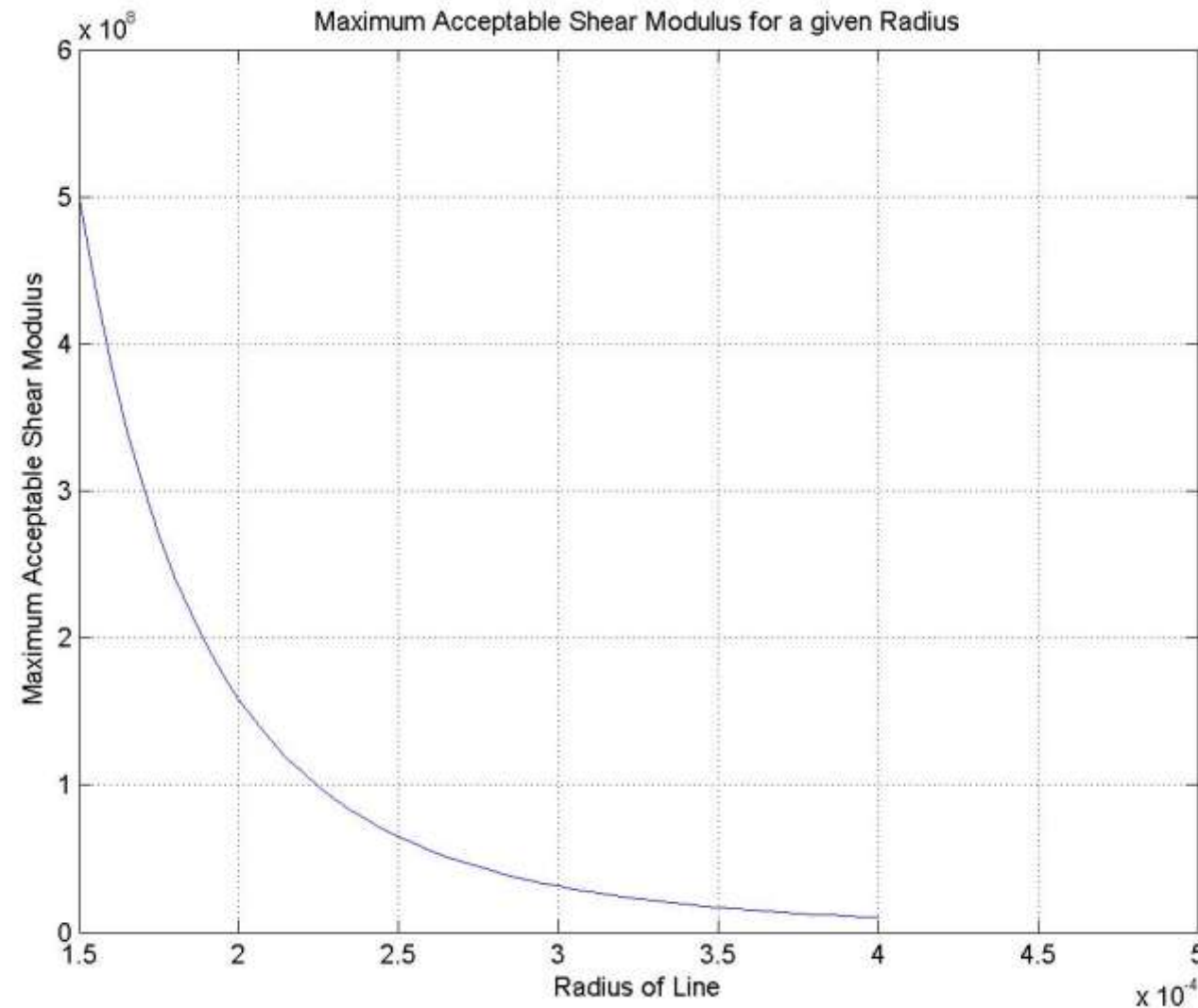
$$M_D = 2 * F_{\text{equivalent}} * d$$



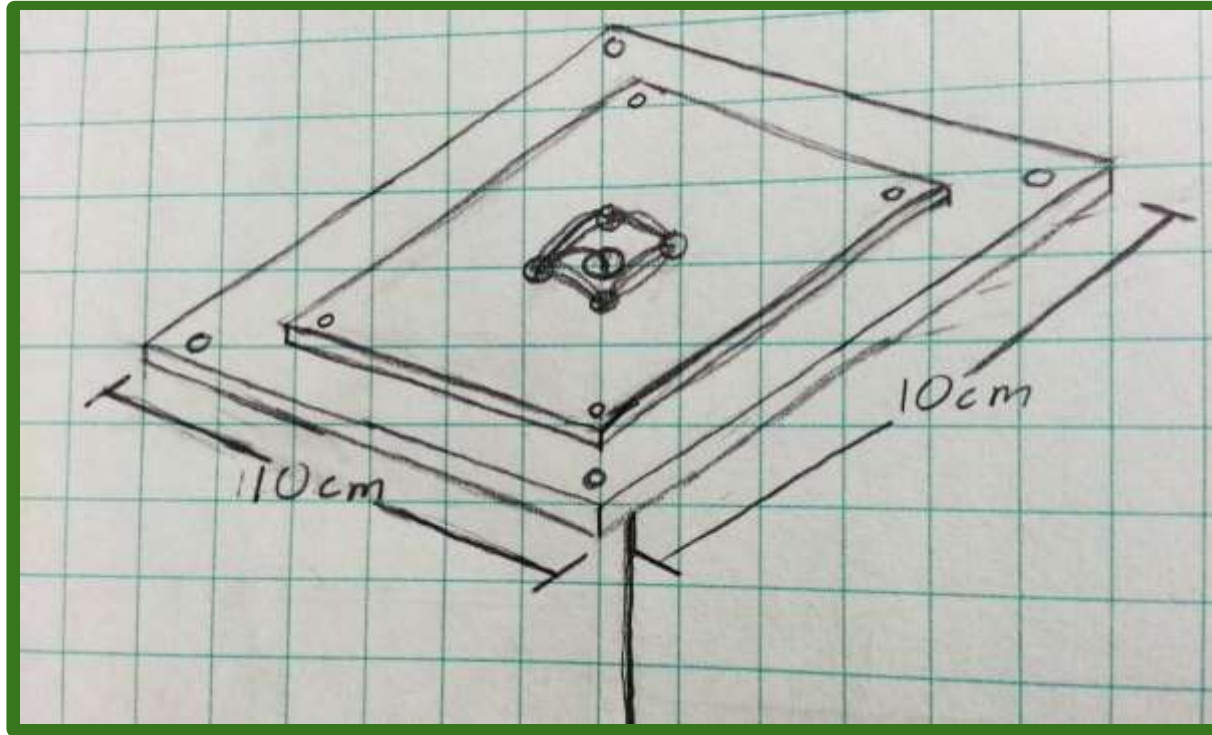
Helmholtz Cage Testing Structure: Backup Calculations - Moment From Drag



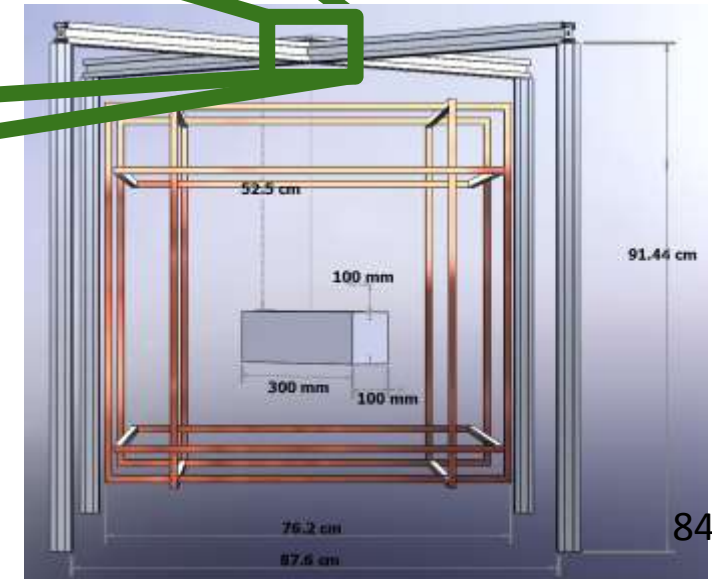
Helmholtz Cage Testing Structure: Backup Calculations - Allowable Shear Modulus



Helmholtz Cage Testing Structure: Backup - Attachment

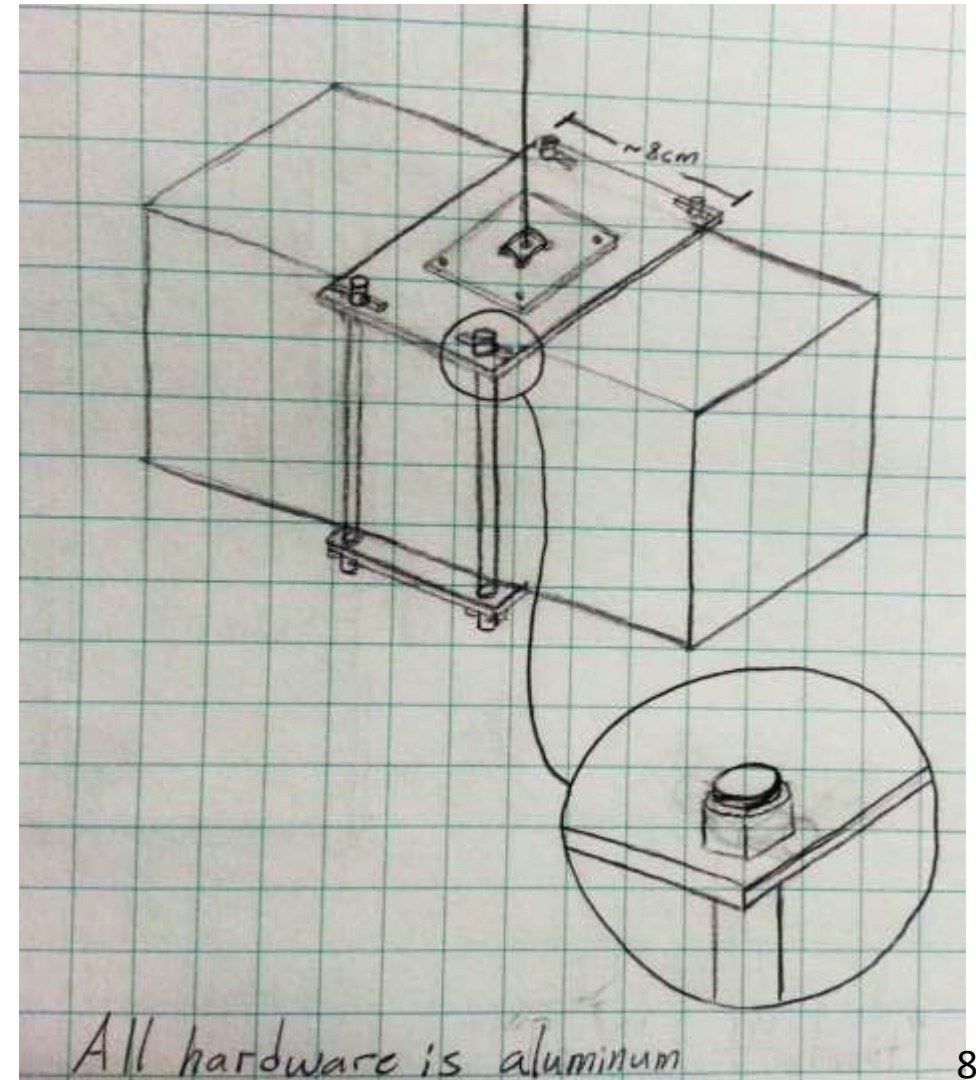
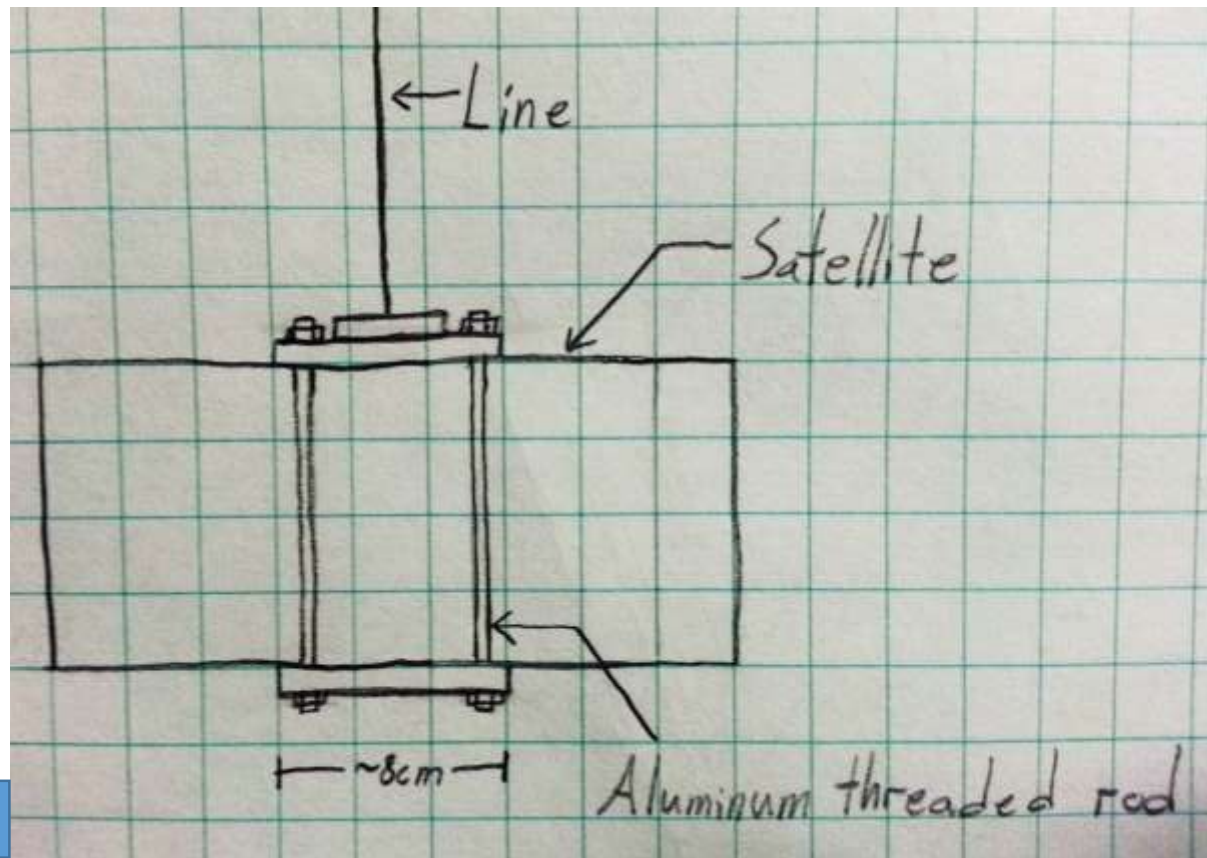


Top Attachment
Mechanism

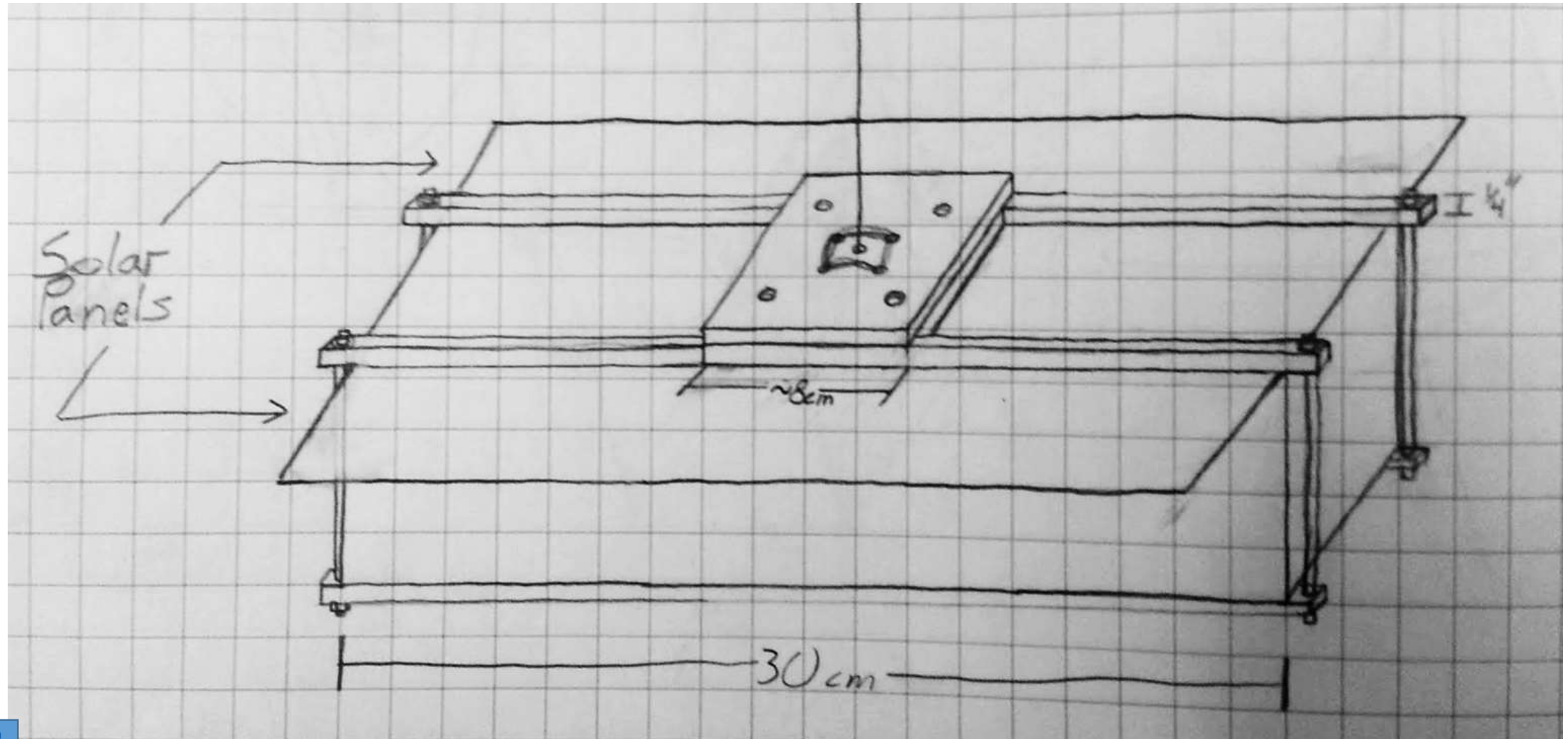


Helmholtz Cage Testing Structure: Backup - Attachment

Satellite Attachment Mechanism 1



Helmholtz Cage Testing Structure: Backup - Attachment



Trade Study Weights and Results

Criteria	Sub-Criteria	Percentages	Ratios
Resistance	-	30%	0.30
Time to Design	-	10%	0.10
Time to Make	-	20%	0.20
Additional Components	-	15%	0.15
Ease of Use	-	15%	0.15
Cost	-	10%	0.10
		100%	1.00

Summary Matrix		Magnetic Levitation		Mechanical Bearing		Hanging		Air Bearing	
Criteria	Weight	Raw Score	Weighted Score	Raw Score	Weighted Score	Raw Score	Weighted Score	Raw Score	Weighted Score
Resistance	30%	5	1.50	3	0.90	4	1.20	3	0.90
Time to Design	10%	2	0.20	4	0.40	3	0.30	2	0.20
Time to Make	20%	3	0.60	4	0.80	4	0.80	2	0.40
Additional Components	15%	3	0.45	5	0.75	4	0.60	2	0.30
Ease of Use	15%	4	0.60	5	0.75	2	0.30	3	0.45
Cost	10%	3	0.30	3	0.30	5	0.50	2	0.20
TOTAL		-	3.65	-	3.90	-	3.70	-	2.45

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Detailed Preliminary Budget

System	Item	Quantity	Item Cost	Total
Interface Board	Master Microcontroller	1x5	\$3.94	\$19.70
	Slave Microcontroller	22x5	\$1.18	\$129.80
	USB to UART	1x5	\$4.50	\$22.50
	Current Sensor	2x5	\$4.82	\$48.20
	Linear Voltage Regulator	2x5	\$0.51	\$5.10
	PCB (2-layer)	2x5	\$33.00	\$330.00
			TOTAL:	\$555.30
Helmholtz Cage Hang	Extruded Aluminum	22ft.	\$12.00/ft.	\$264.00
	¼" Aluminum Plate	4sq.ft.	\$37.80/sq.ft.	\$151.20
	Line	20in.	\$0.0023/ft.	\$20.00
	Fasteners			\$100.00
			TOTAL:	\$535.20

System	Item	Quantity	Item Cost	Total
Sun Sensor Calibration	Aluminum	1	\$100.00	\$100.00
	Ball Bearing	1	\$30.00	\$30.00
	Rotary Magnetic Encoder	1	\$80.00	\$80.00
	DC Motor	1	\$70.00	\$70.00
	Analog to Digital Converter	1	\$30.00	\$30.00
	LCD Display	1	\$30.00	\$30.00
	Anodized Coating	1	\$300.00	\$300.00
			TOTAL:	\$640.00
Extra Elements	Project Poster	2	\$43.00	\$86.00
	Miscellaneous		\$200.00	\$200.00
			TOTAL:	\$286.00