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12/24/2020

2

Outline





Section 1Project
OverviewPurpose and
ObjectivesDesign
SolutionCritical
Project
Elements

Purpose and Objectives

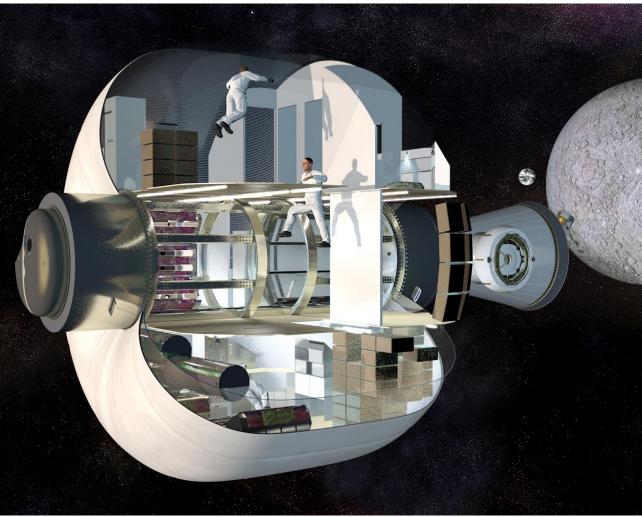


Risk

Mission Context

Purpose

- SNC's inflatable LIFE[™] Habitat is designed for deep space habitation
- Cargo will arrive prior to crew arrival
- Need: Use robotics to unload and transport cargo in the habitat without crew
- Derivative of NASA's need for a remote IVR system

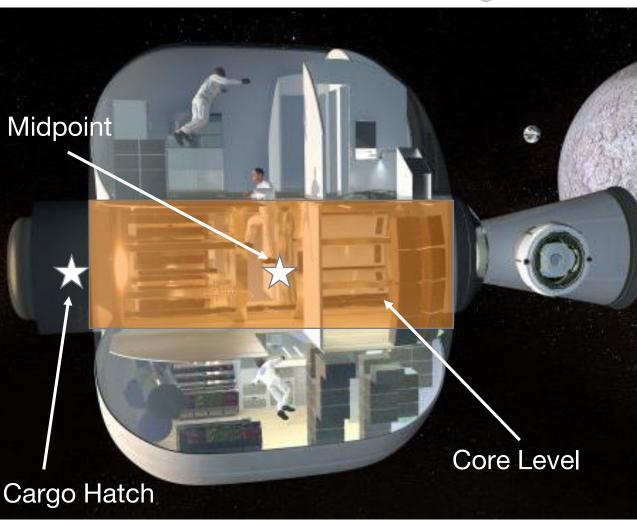




Focus Area

Purpose

- Simplified to one level of the habitat Core
- Demonstrate transport from cargo hatch to midpoint
- Assumptions:
 - Bags are waiting at the opening of the cargo hatch (separate IVR system prior to our process)
 - The environment is pressure and temperature controlled





NASA Applicable Requirements

- Summary of the requirements given by NASA for an IVR system
- Simplified versions of these requirements were adapted for this project

ID	Requirement
L3-HAB-0196	The HAB shall provide the ability to access and service designated internal payloads and logistics without the need for crew intervention.
L3-HAB-0142	The HAB shall provide interfaces to enable internal robotic inspection, mobility, and dexterous manipulation.
L3-HAB-0145	The HAB shall provide a method for determining and communicating internal location information that is common to internal robotics and human operators (crew and ground).
L3-HAB-0312	The HAB shall use robotically compatible interfaces to allow the IVR system to access/retrieve/install internal logistics cargo.

Overview

Risk

Mission Statement

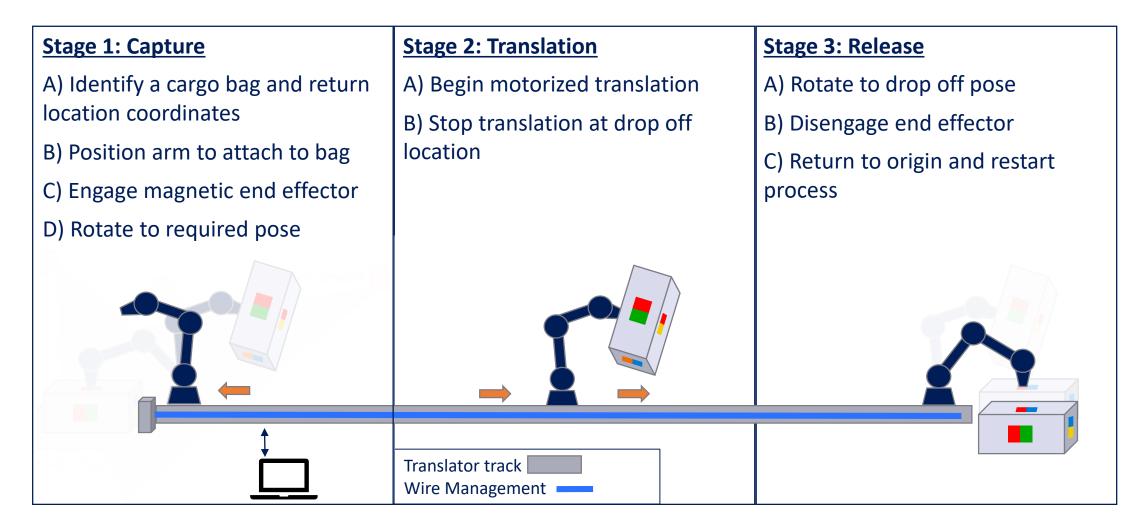
Purpose

RIVeR will prove the feasibility of using Intra-Vehicular Robotics (IVR) to identify and distribute cargo bags within Sierra Nevada's LIFE[™] Habitat to demonstrate task management in an uncrewed environment.

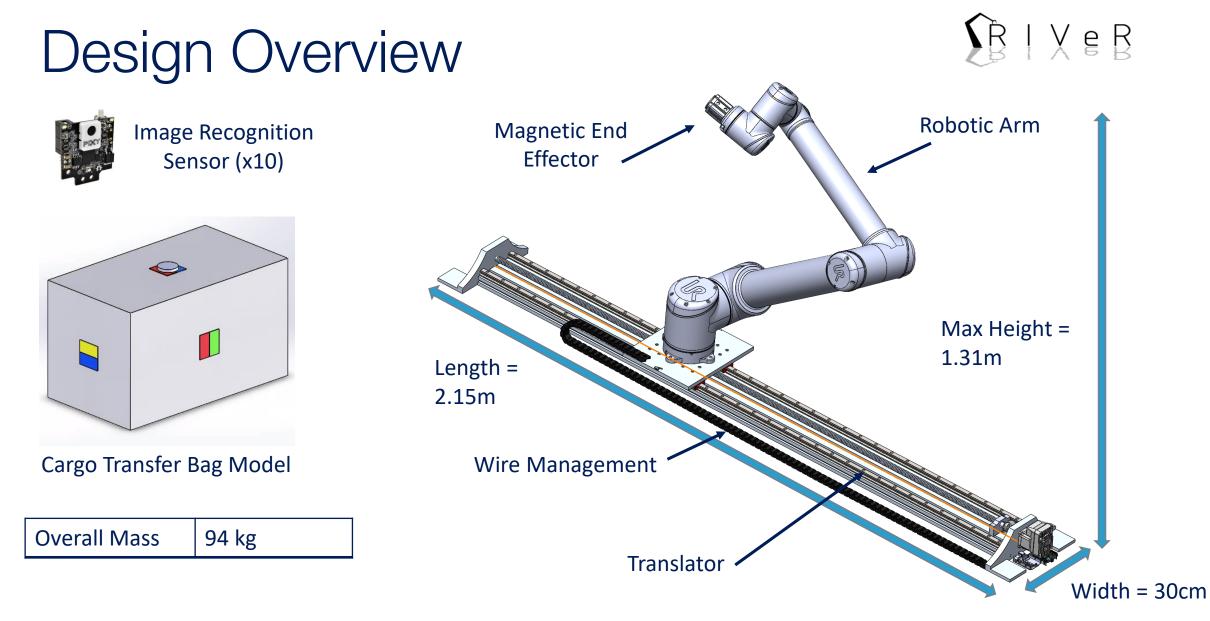


CONOPS

Purpose



Design Solution



Project Management Risk

> Planning

Robotic Arm

- UR10e from Universal Robots and acquired by SNC
- Command Input: Joint trajectory data generated by motion planner in ROS
- Includes force sensor

Purpose

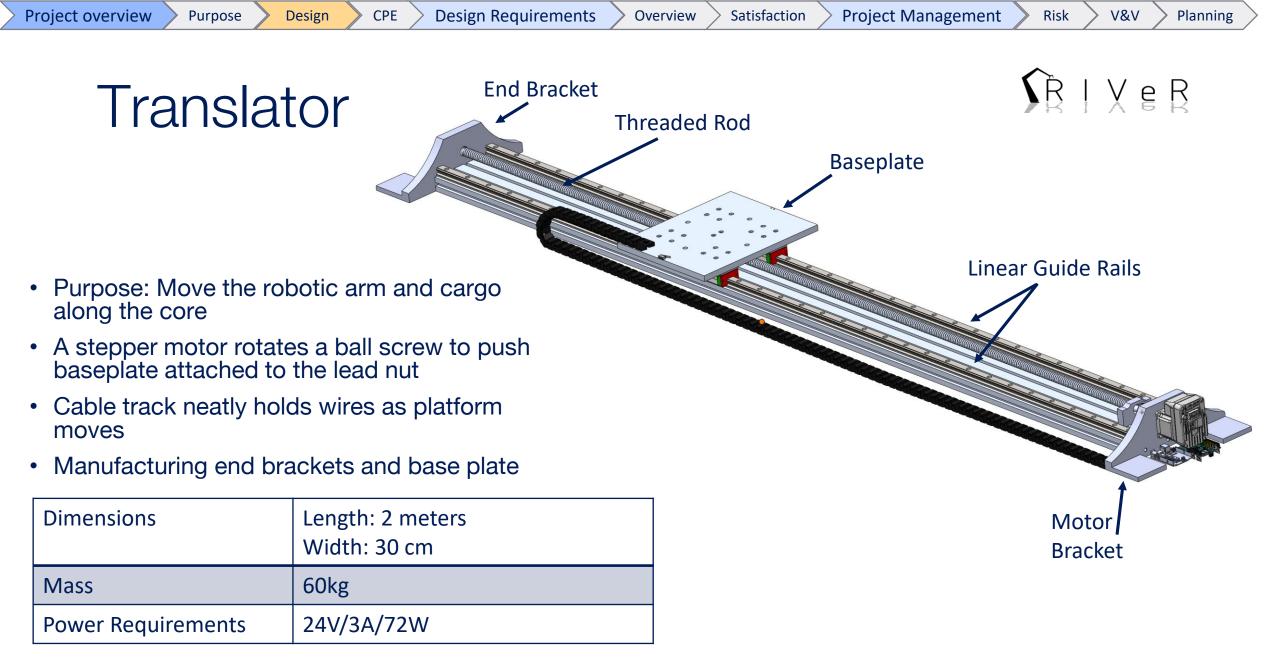
- Force (x,y,z) up to 100N
- Torque (x,y,z) up to 10Nm

Dimensions	Max Reach: 1.3m Footprint: 19cm
Mass	33.5 kg
Power Requirements	Arm: Max: 615W Avg: 350W Control Box: 24V 2A
Max Load	10 kg
Max Motor Speed	Joint size 2,3: 180 deg/sec Joint size 4: 120 deg/sec



V&V



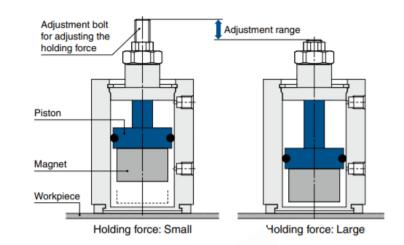


> Planning

XeB

End Effector Assembly

- SMC MHM-32 Magnetic Gripper
- Uses compressed air to actuate a magnetic piston
- All components procured from SMC



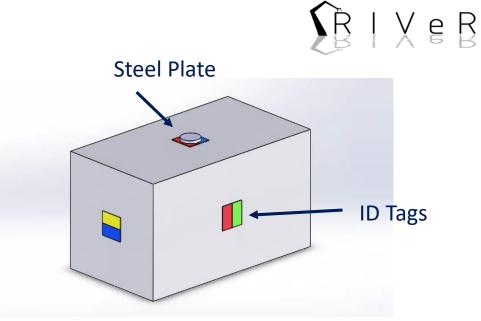
Dimensions	50mm x 50mm x 63mm
Mass	483 g
Power Requirements	1.92 W (for two Programmable Logic Controllers)
Holding Force	500 N
Operating Air Pressure	29-87 psi



Bag Design

- NASA's Cargo Transport Bag
 - In process of acquiring a real bag from NASA Hunch
- Steel plate for magnetic attachment
- Color ID tags for image recognition
- Initial testing with cardboard prototype
 - Gradually increase fidelity of bag model

Bag Dimensions	41 cm x 23 cm x 24 cm
Mass	Max 1 kg
Material	PVC/Vinyl, Polyethylene, Polyurethane
Plate Dimensions	40 [mm] Diameter
Plate Material	409 Steel





CTB Stored on the ISS

Project overview Purpose

Overview

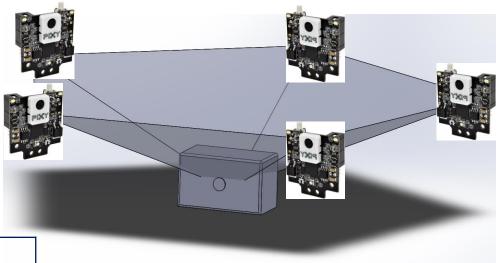
Risk V&V Planning

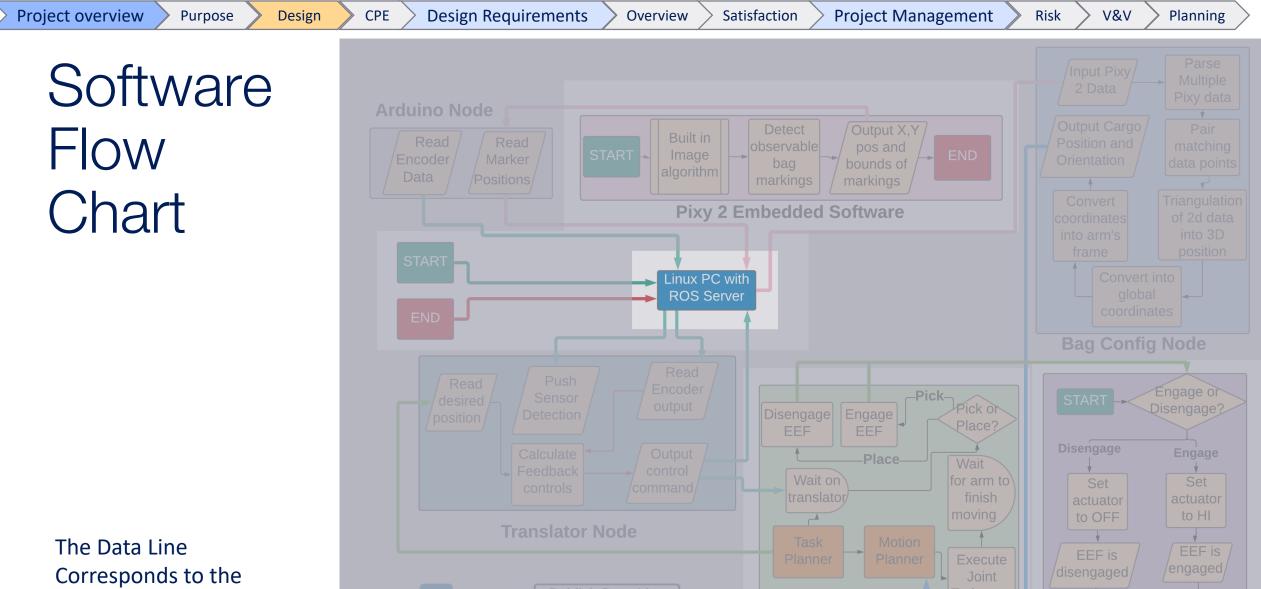
XeR

Sensing and Identification

- Object Recognizing Pixy2 Cameras
- Orientation Determination
 - 3+ bag faces & 2+ images of each face
 - 4+ cameras to determine all possible orientations
- Pentagonal-Pyramidal configuration
 - 4 for capture location
 - 5 for release location
- 1 Camera Facing Translator

Dimensions	43mm x 39mm x 16mm
Mass	10g
Power Requirements	5V / 140mA / 3.5W
Quantity	10
Sample Rate	100 detections per frame at 60fps
Accuracy	≈ 3 − 10%





Corresponds to the Color of the Node

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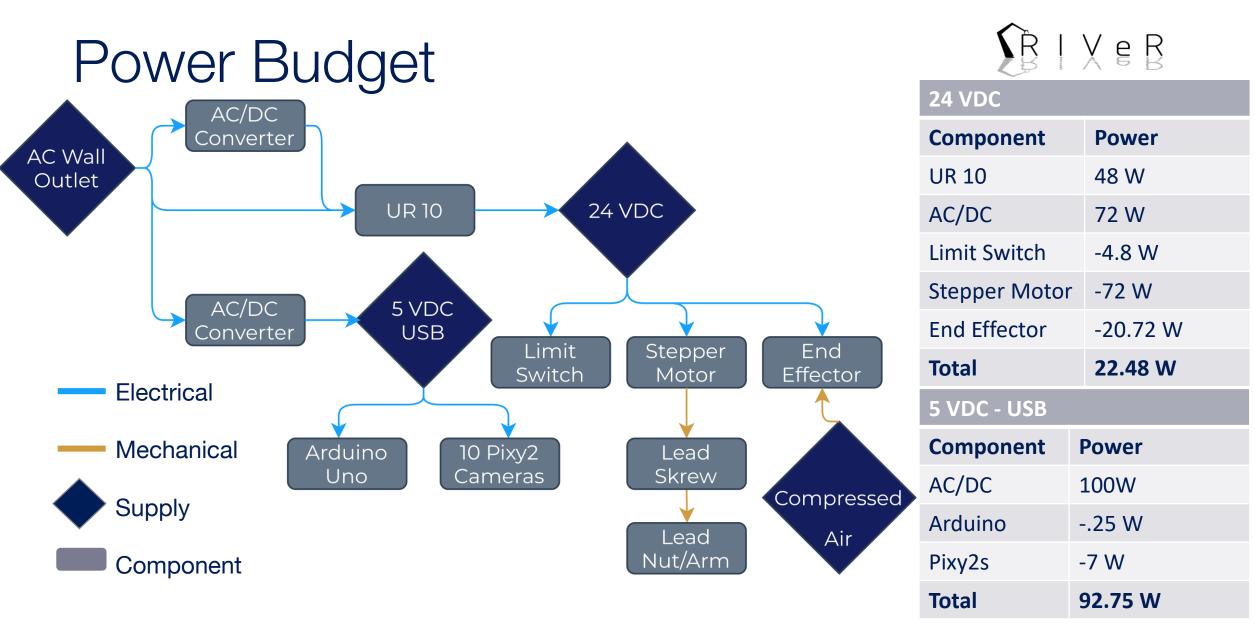
Robotic Arm Node

End Effector Node





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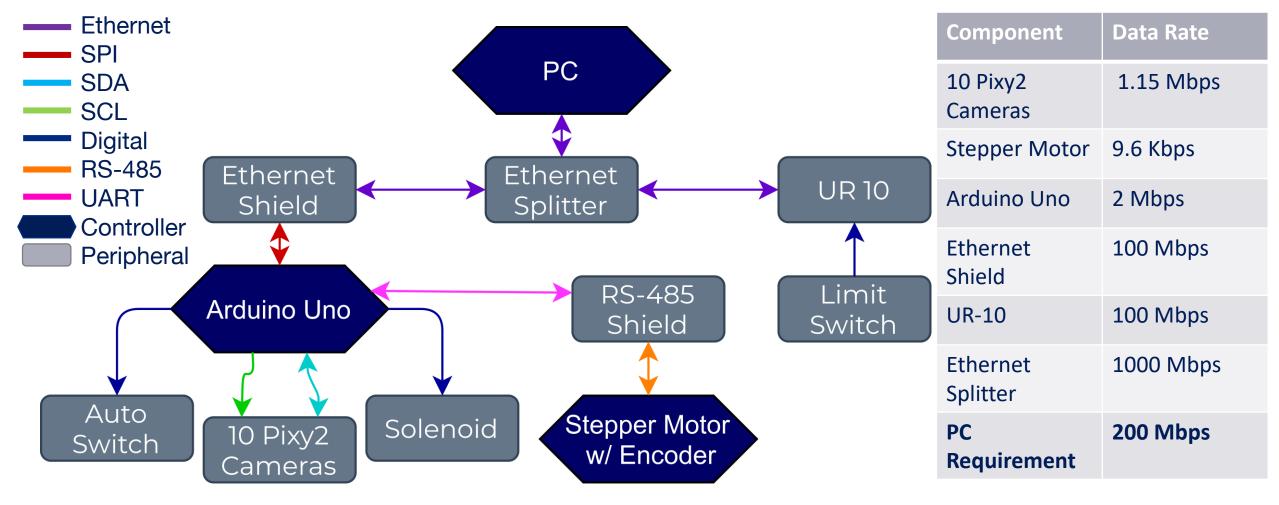


V&V Planning

Data Budget

Purpose





Critical Project Elements

> Planning

Project Elements

Purpose



Structural	Robotics	Actuators	Electronics	Software
Translator Track	Robotic Arm	Solenoid Valve (End effector)	Arduino	Image Processing
Base Plate (Arm)	End Effector	Motor (Translator)	Wire Management	Control System
			Imaging sensors	

Overview

Critical Element

Critical Element & CDR Focus

Critical Project Elements



СРЕ	Function	Analysis
Base Plate (Arm)	Integrates the robotic arm base with the translator	Base plate deformation/deflection
Motor (Translator)	Moves the robotic arm and base plate	Motor torque analysis
Image Processing (Software)	Manage data from each sensor and determine the orientation and position of cargo bags	Object position and orientation determination
Imaging Sensors	10 cameras to identify and locate the ID tags on cargo bags	Camera positioning, visual feasibility



Satisfaction

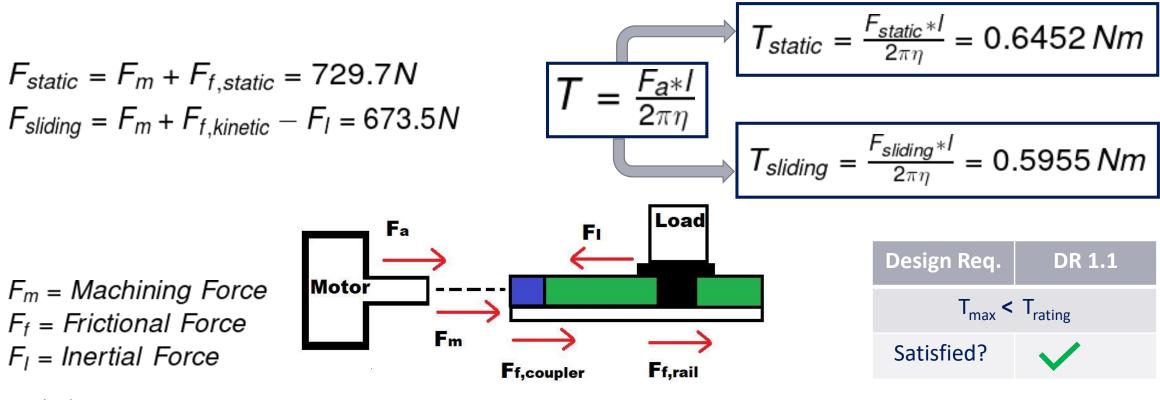


Motor Torque Analysis

DR 1.1: The translation system shall be capable of translating the robotic arm, end effector, and cargo bag's combined mass.

Overview

• Criteria: T_s and $T_m < T_{rating} = 1.22 \text{ N*m}$ (given by motor datasheet)



Project overview > Purpose

IVeR

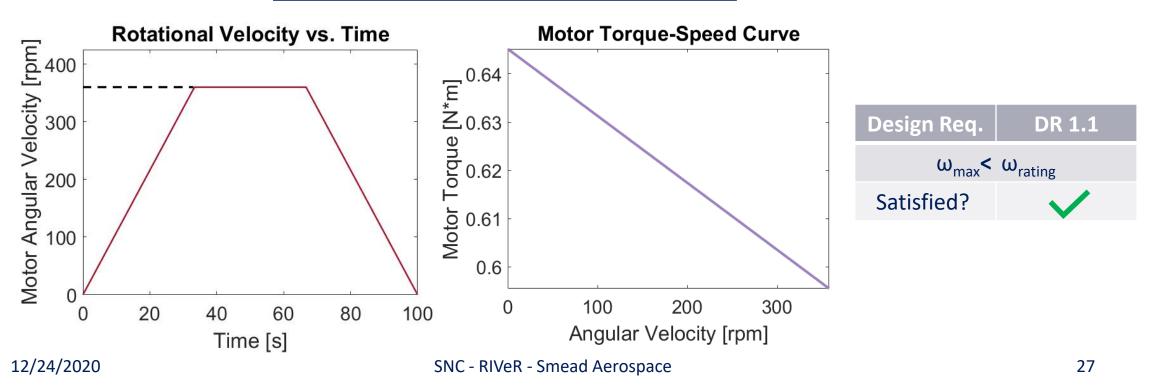
R

Motor Torque – Rotation Velocity

- **DR 1.1:** The translation system shall be capable of translating the robotic arm, end effector, and cargo bag's combined mass.
 - Criteria: $\omega_{max} < \omega_{rating} = 2160 \text{ rpm}$ at 24 V (given by motor data sheet)

Overview

$$\omega_{max} = PPS(\frac{60s}{1min})/n = 357.6rpm$$



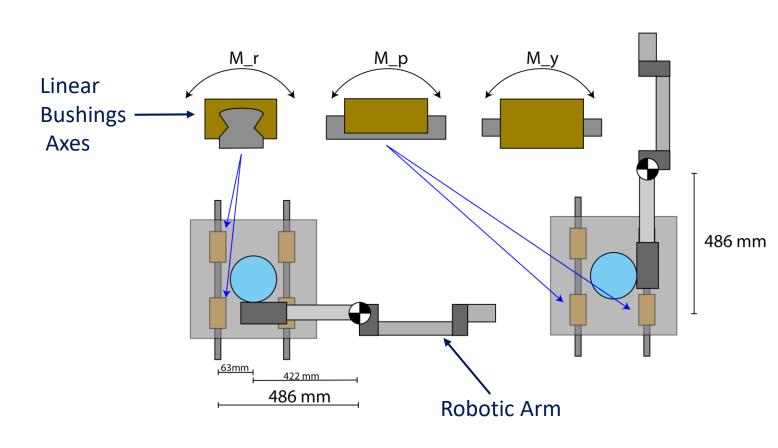
Overview

Satisfaction Pr

Project Management

V&V > Planning

Linear Bushing Compatibility



Variable	Linear Bushing Rating	Maximum Value per Bushing
M_r	270 Nm	163.6 Nm
M_p	200 Nm	162.4 Nm
M_y	200 Nm	82.5 Nm
Dynamic Load	17.75 KN	140 N
Static Load	27.76 KN	167.75 N

Risk

<u>Ř</u> I X e R

Max Arm Motor Torque = 330 Nm Per Bushing = 82.5 Nm Total Moment = Motor Torque + Gravity *Stepper Motor Torque included on M_r 1.23 FOS for Linear Stage

DR.8.1 The system shall not deflect from any torques caused by motors.



Project overview > Purpose

Design CPE

Design Requirements

Overview

Von Mises Designed Baseplate

Von Mises Original Baseplate

Calculated Beam Deflection



Risk

Maximum Deflection

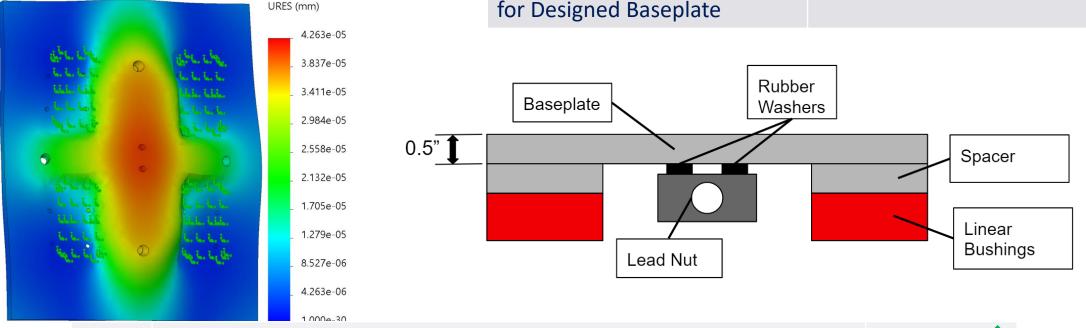
4.236×10^-5 mm

2.944×10^-5 mm

1.89×10^-8 mm

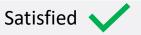
Baseplate Deflection

- Baseplate Material: Aluminum 6061
 - Youngs Modulus: 69 GPa
 - Yield Strength: 55.1 GPa
- Expected stress .165 MPa < 55.1 GPa
 - Von Mises Model holds for elastic material



Model

DR.8.2 The rail system shall not experience any deflection that misaligns the threads.



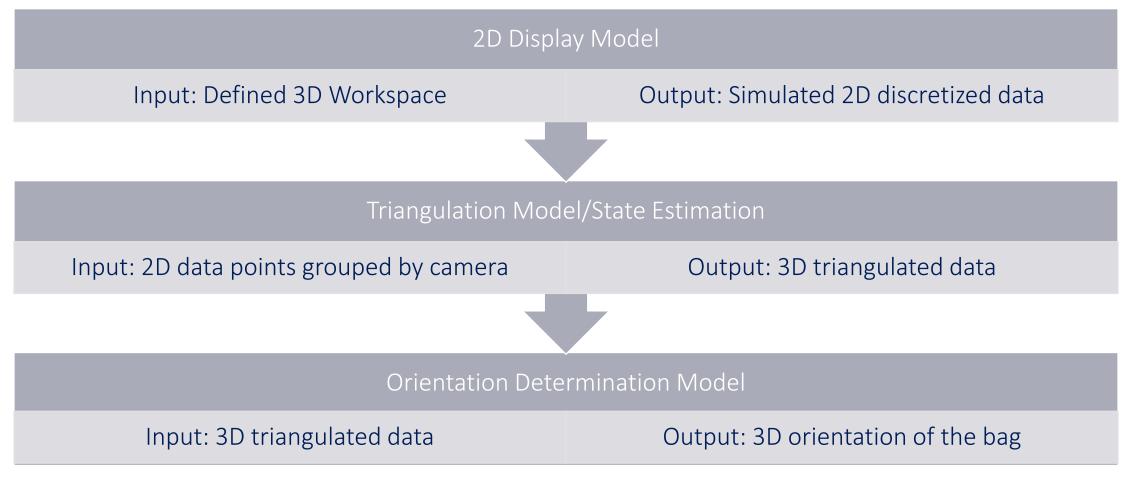
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Overview



Sensory Modeling

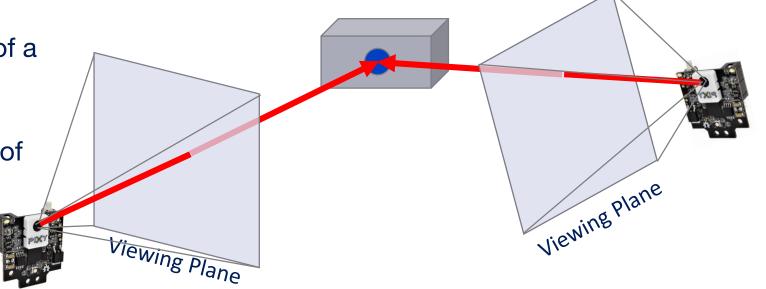


Overview

Risk V&V Planning



- **Object Position Determination**
- Must determine the bag position to pick it up with the robotic arm
- Sensors return (x, y) coordinate of a detected object
 - In the Sensor Frame
- Can reconstruct the 3D position of an object, based on:
 - Measurements
 - Sensor Positions
 - Sensor Orientations



DR.3.1	The system shall identify a cargo bag with its orientation and position.
DR.3.2	The system shall be able to determine if the cargo has reached the target location
DR.3.3	The operating system shall be able to determine if the cargo is irretrievable.
DR.3.4	The system shall give feedback if the transportation has failed and cease operations.

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Design Requirements

Overview



- Define the Estimation Cost Function
 - Nonlinear Least Squares of the Measurement Residuals

Object Position Determination

$$\begin{split} J(T) &= \sum_{k=1}^{T} (y(k) - \hat{y}(k))^{T} (y(k) - \hat{y}(k)) \\ y(k) &= \begin{bmatrix} x_{S1} \\ y_{S1} \\ x_{S2} \\ y_{S2} \\ \vdots \end{bmatrix} = & \text{True Sensor Measurements} \\ \hat{y}(k) &= \mathcal{H}_{i}(\mathbf{x}) = & \text{Non-Linear Measurement Function (Based on the geometry)} \end{split}$$

- Our goal is to find the ${\bf x}$ that minimizes J(T) using gradient descent

Overview

Satisfaction Project Management

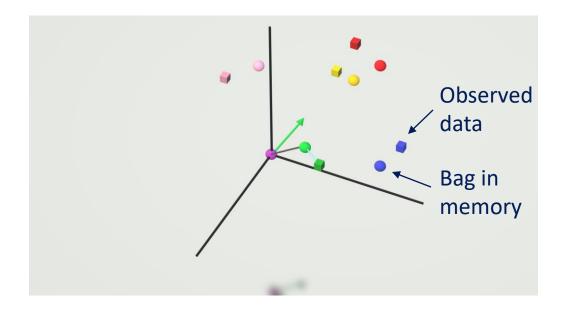
Risk V&V Planning

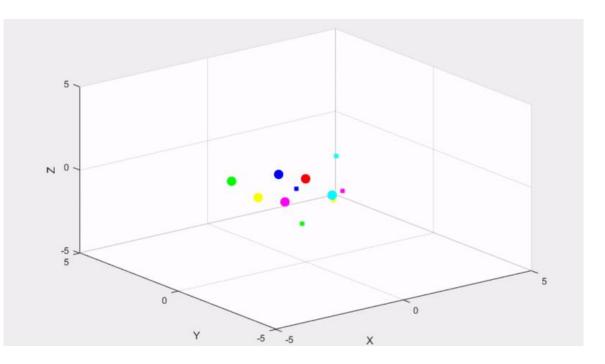


Object Orientation Determination

Goal: Determine the orientation of the bag based on observed markers.

Rotates a predefined set of markers to best represent the input data





Overview

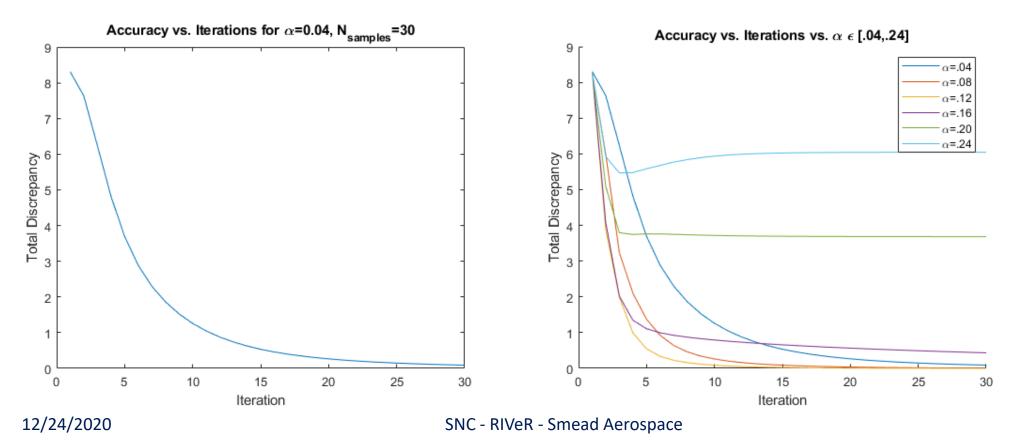
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Risk > V&V > Planning



Object Orientation Determination

- Performs gradient descent to minimize the summed cartesian distance discrepancy
- "α" (gradient gain) affects rate of convergence and stability
- Converges to non-zero minimum value



34

Sensor Suite



V&V

Position Determination Algorithm

Design

Orientation Determination Algorithm

DR.3.1	The system shall identify a cargo bag with its orientation and position.	
DR.3.2	The system shall be able to determine if the cargo has reached the target location	\checkmark
DR.3.3	The operating system shall be able to determine if the cargo is irretrievable.	\checkmark
DR.3.4	The system shall give feedback if the transportation has failed and cease operations.	\checkmark





Risk Matrix

Purpose



Risks

ARM-1	Arm is commanded to a position that damages it
ARM-2	Arm cannot make contact with bag
TR-1	Stripping of lead screw
TR-2	Linear stage tipping over
SOFT-1	Cargo bag cannot be identified
END-1	Pressure actuator failure
END-2	Improper alignment/bag dropping

	5					
	4		SOFT-1			TR-2
Likelihood	3			END-2	ARM-2	
Like	2					TR-1
	1					ARM-1, END-1
		1	2	3	4	5
			S	everity		

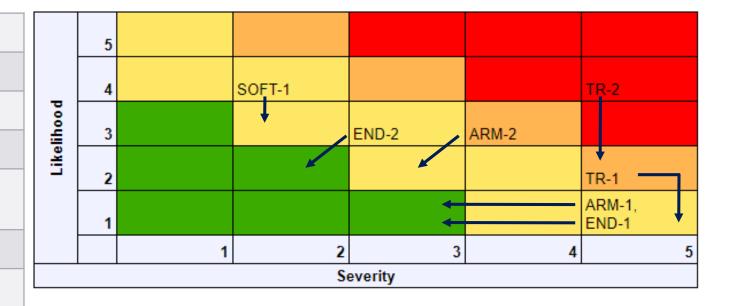
Mitigation

Purpose



Risks

ARM-1	Arm has built in safety features
ARM-2	Manual control directs arm
TR-1	Alleviate force with linear bushings
TR-2	Weighted end brackets
SOFT-1	Arm can be controlled manually to find the cargo bag
END-1	Replacement Parts
END-2	Arm can be manually driven



Verification and Validation





Test Name	Definition/ Purpose	Driving Requirements	Completion Date	Location and Equipment
Robotic Arm: Functionality Test	Test UR10e Motion Planning and Pose Determination.	FR.1 FR.2 FR.4	February 5 th	Senior Projects Room Wall Power Supply
End-Effector: Static Load Test	Test Capture Mechanism and End-Effector Controls with Bags.	FR.1 FR.2 FR.5 FR.6	February 5 th	Senior Projects Room Air Supply Wall Power Supply
Translator: Calibration and Arduino Test	Test Motor Accuracy, Sensor Functionality, and Translator Controls.	FR.1 FR.7 FR.8	February 19 th	Senior Projects Room Wall Power Supply
Pixy Camera: Bag Identification Test	Test Camera Triangulation Method and Accuracy for Bag Retrieval.	FR.1 FR.3 FR.4	March 12 th	Senior Projects Room Wall Power Supply
Robotic Arm: ROS Test	Utilize ROS to Integrate the Translator and Arm for Dynamics Test and Failure Detection.	FR.3	March 19 th	Senior Projects Room Wall Power Supply

Overview



Testing Plan II

Purpose

Test Name	Definition/ Purpose	Driving Requirements	Completion Date	Location and Equipment
Cargo Bag: Varied Bag Fidelity for Capture	Test Capture/Identification of Cargo Bags of Varied Fidelity	FR.1 FR.2 FR.3	April 9 th	Senior Projects Room Air Supply Wall Power Supply
Full System Software Test	Test Control Software of the UR10, Translator, and Camera System with Single PC Control.	FR.1 FR.2 FR.3 FR.4 FR.5 FR.6 FR.7 FR.8	April 9 th	Senior Projects Room Air Supply Wall Power Supply
Full System Functionality Test	Test UR10, End- Effector, Translator, and Camera System for a Full Cycle of Operations.	FR.1 FR.2 FR.3 FR.4 FR.5 FR.6 FR.7 FR.8	April 9 th	Senior Project Room Air Supply Wall Power Supply
Full Systems Test	Test Software and Hardware of the Assembled System for a Full Cycle of Operations.	FR.1 FR.2 FR.3 FR.4 FR.5 FR.6 FR.7 FR.8	April 16 th	Senior Projects Room Air Supply Wall Power Supply

Overview

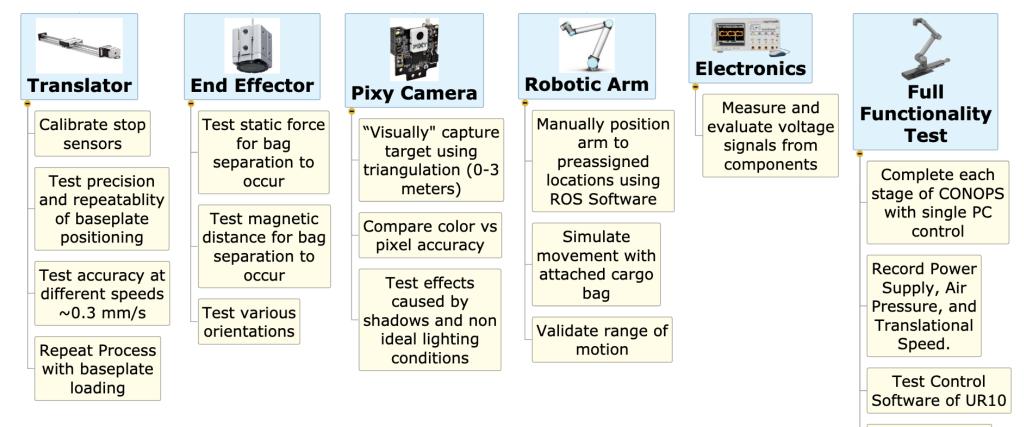
Project Management Risk

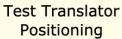
V&V Planning

Testing Tasks

Purpose







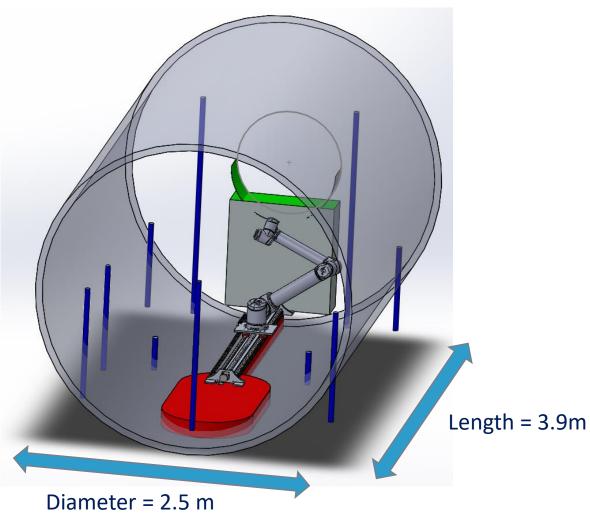
Test Camera System

Planning

Testing Set Up

Design

Purpose



SB | X e B

Capture Area: 0.2 square meters Release Area: 0.915 square meters Camera Stands

Cameras mounted using square, telescoping rods

Origin at center of hatch

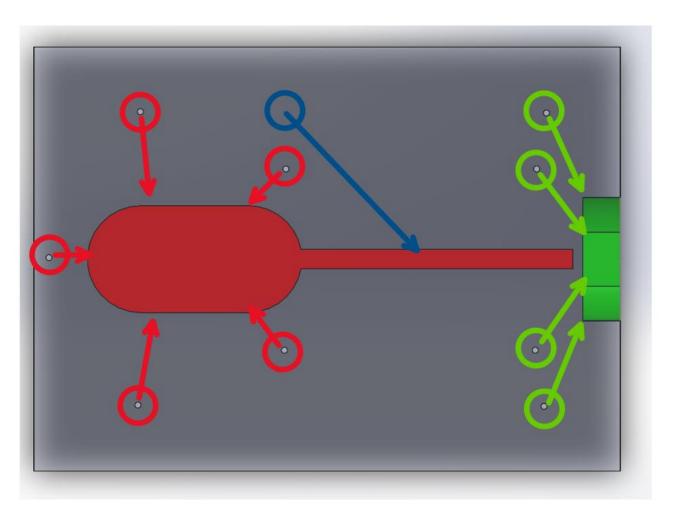
Overview

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Planning



Camera Set Up: Top Down



Location	Cameras	Symbol
Facing Capture Zone	4	0
Facing Release Zone	5	0
Facing Translator Path	1	0

Camera configuration centered about the middle of the Capture/Release Zones

• Each camera is 1.228 meters from this point

Translator camera is an average of 1.865 meters from the translator.

Design Requirements

Satisfaction Project

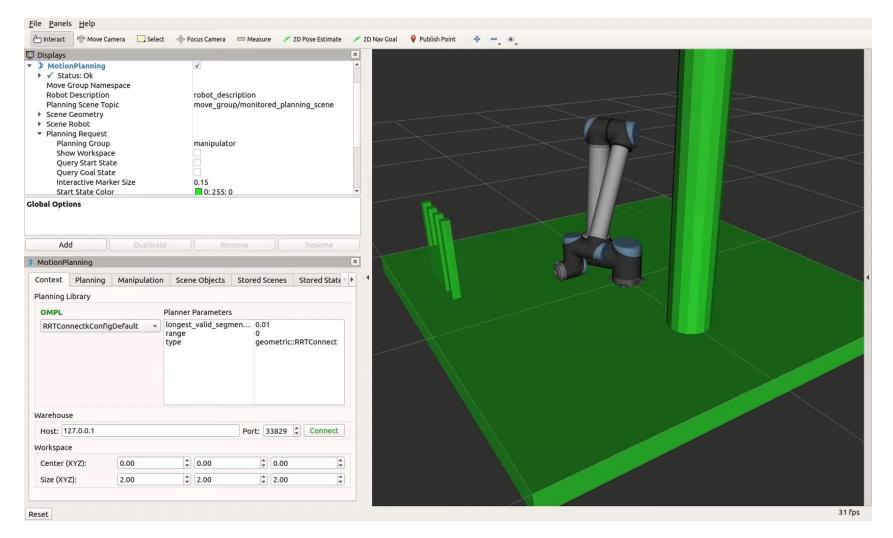
Project Management Risk

Planning

Image: Second se

V&V

RViz Demonstration

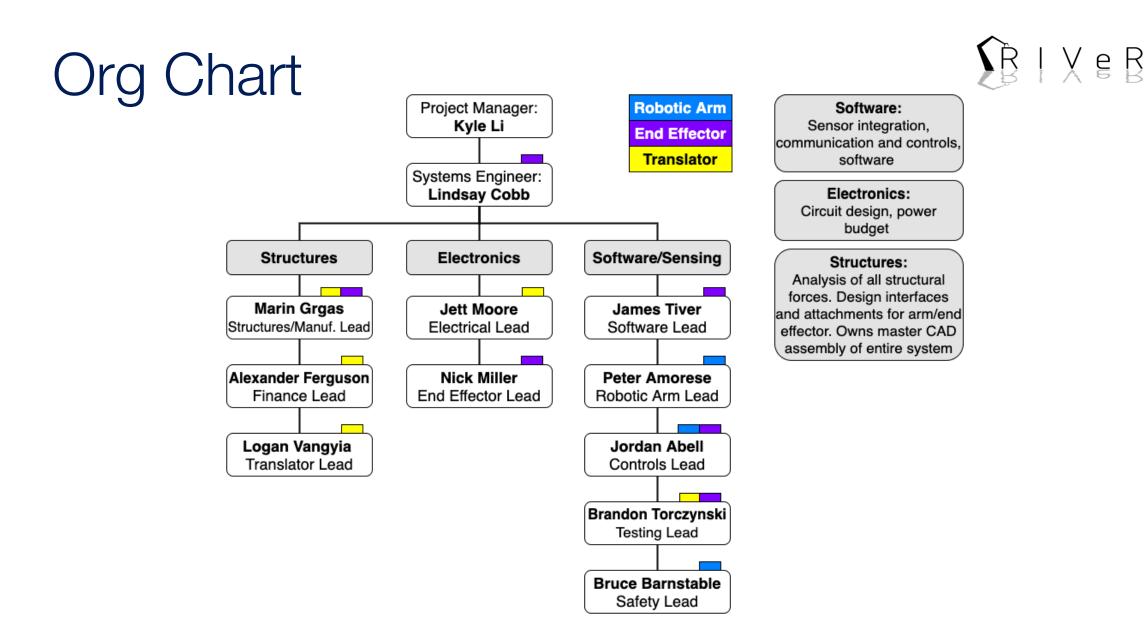


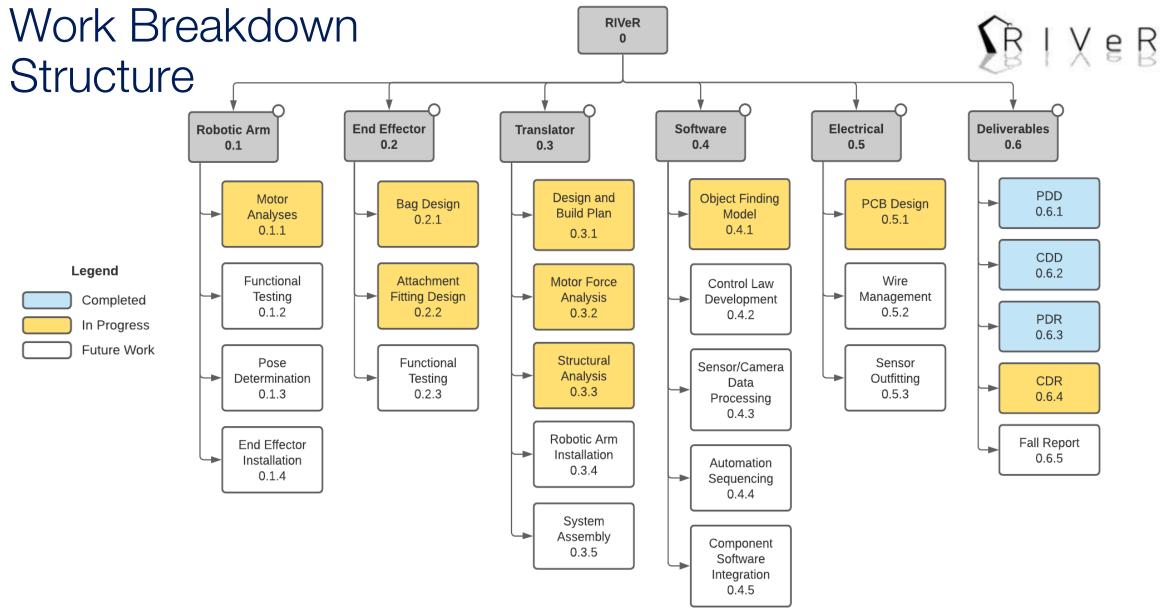
Overview

Project Planning

V&V Planning

Risk





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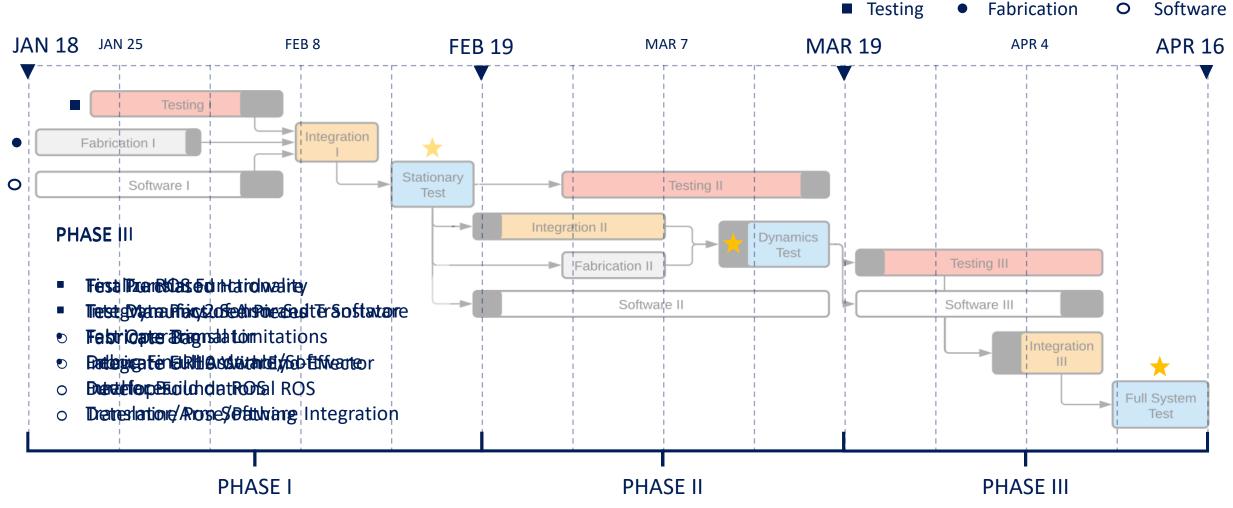
Software

Gantt Chart – Critical Path



Risk

Fabrication

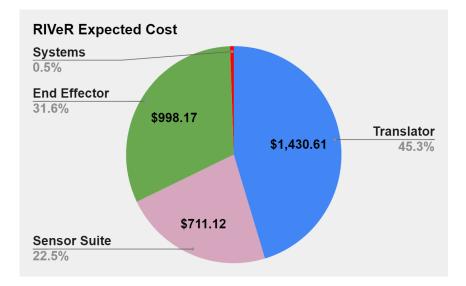


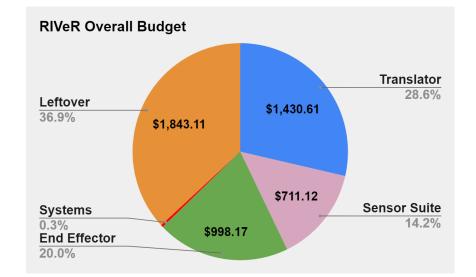


Cost Plan

Purpose

Subsystem	Expected Cost	Allocated Amount	Budget Margin
Translator	\$1,430.61	\$2200	\$769.39
End Effector	\$998.17	\$1600	\$601.83
Sensor	\$711.12	\$1100	\$388.88
Systems / Electrical	\$16.99	\$100	\$83.01
RIVeR Total	\$3,156.89	\$5000	\$1843.11





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52

Special Thanks

Sierra Nevada Corportation and Loren McDaniel Dr. Neogi CU Boulder Aerospace Department PAB





V&V Planning

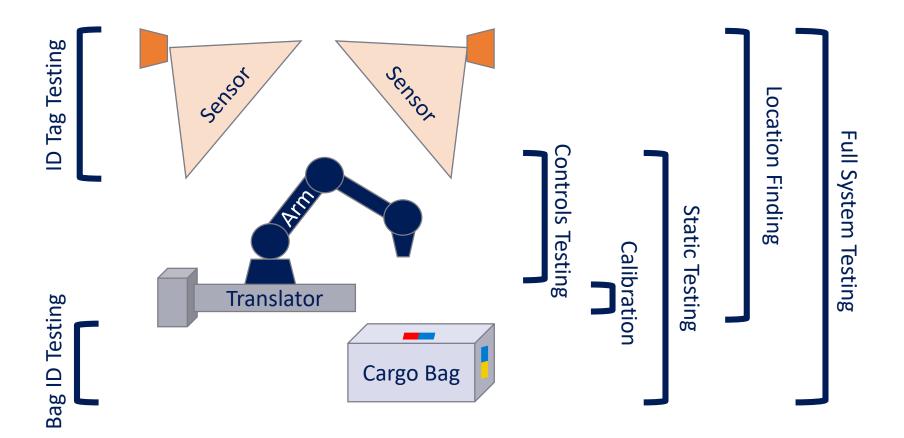


Roadmap

Purpose

Fall Semester

Spring Semester



SBIXeB

Gantt Chart – Overview I Fall

Nov 2020	Dec 2020	Jan 2021	Feb 2021
> CDR Tasks	-		
Fall Presentations/Assi			
CAD Models			
Fall Deliverables			
Testing			
Component Fabrication			
System Integration			
Dynamics Test Preparat			
Full Assembly Preparat			
Software Development		_	

SB | X e B

Risk

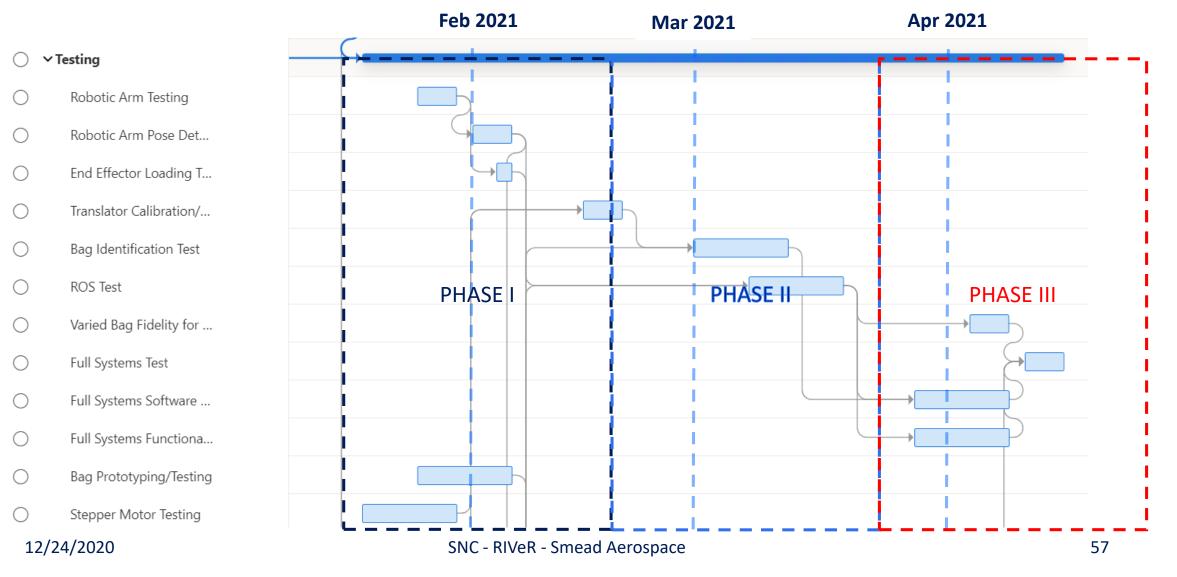
Gantt Chart – Overview II Spring

	Jan 2021	Feb 2021	Mar	2021	Apr 2021
> CDR Tasks					
> Fall Presentations/Assi		PHASE I	PHASE II	PHASE II	
> CAD Models					
> Fall Deliverables					
> Testing					
> Component Fabrication			_		
> System Integration					1
> Dynamics Test Preparat					
> Full Assembly Preparat.					
> Software Development					

Overview

Gantt Chart - Testing



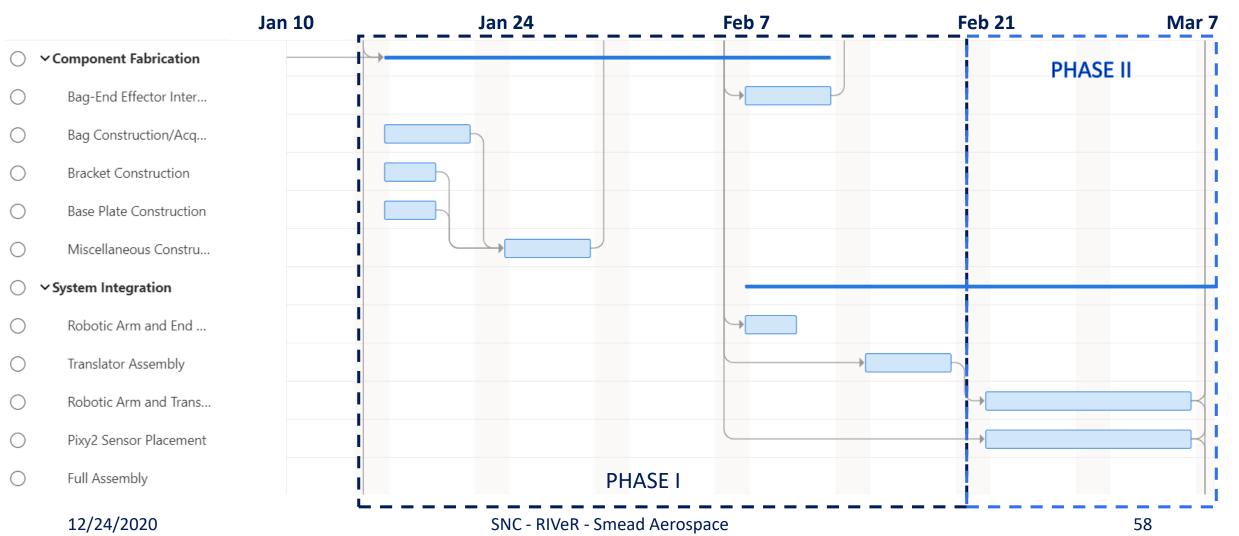


Satisfaction > Project Management

Risk V&V Planning

XeR

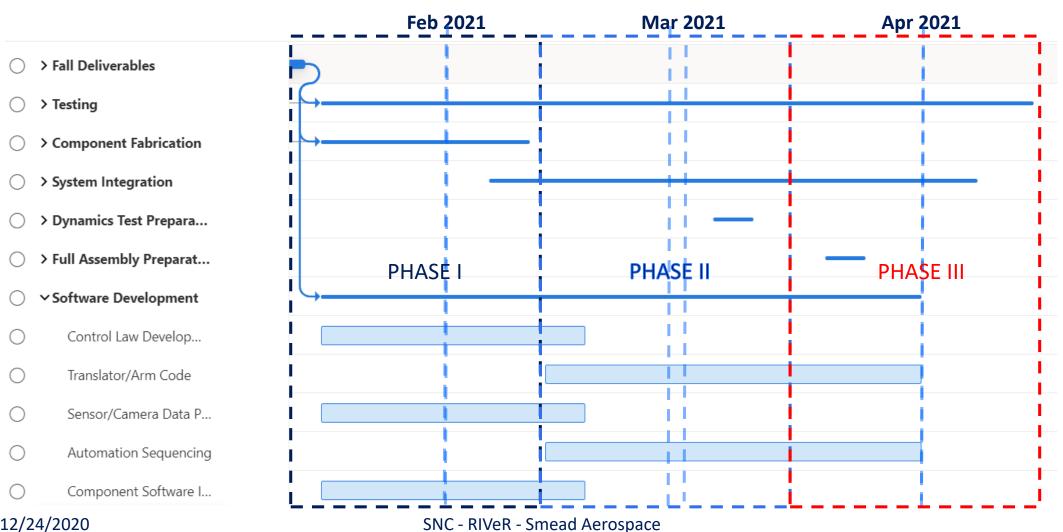
Gantt Chart – Component Fabrication and System Integration



Overview

Gantt Chart – Software





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Design Requirements that pertain to the Translator Subsystem

DR 1.1	The translation system shall be capable of translating the robotic arm, end effector, and cargo bag's combined mass.
DR 8.1	The system shall not deflect from any torques caused by motors.
DR.8.2	The rail system shall not experience any deflection that misaligns the threads.

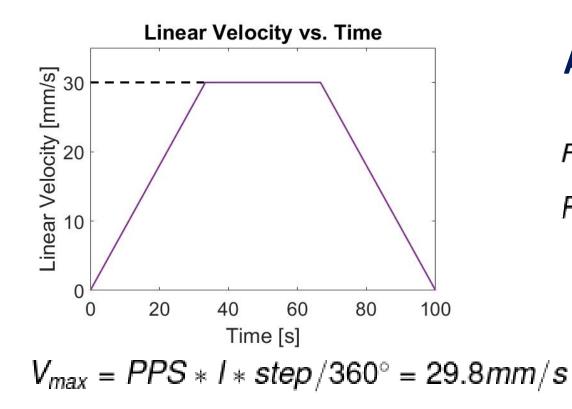
Motor Analysis

- Key Values:
 - Load mass
 - Holding Torque rating
 - Screw efficiency
 - Lead screw
 - Max microstep velocity
 - Max microstep acceleration
 - Microstep size
 - Static friction
 - Kinetic friction



[m]	= 38 kg
	= 1.22 N*m
[T _{rating}]	- 1.22 N III
[ŋ]	$= 90 \pm 5 \%$
[1]	= 5 ± 0.03 mm
[PPS]	= 305,175 steps/s
[α]	= 6.104*10 ⁶ steps/s^2
[step]	= 7.031*10 ⁻³ °/step
[µ _s]	= 1.96
[µ _k]	= 1.87

Motor Analysis



SB | X e B

Axial Force
$$F_a = F_m + F_f - F_l$$

$$F_{static} = F_m + F_{f,static} = F_m + mg * \mu_s = 729.7N$$

$$F_{sliding} = F_m + F_{f,kinetic} - F_l = F_m + m(g\mu_k - a) = 673.5N$$

Motor Analysis - Tolerances



- Assumption:
 - Screw Efficiency: Ball screw efficiency typically between 85% and $95\% = 90 \pm 5\%$
- From translator_data_shestmm
 - Lead screw:

Motor Analysis - Tolerances



- Error Propagation:
 - Acceleration: $\frac{\delta a}{|a|} = \sqrt{\left(\frac{\delta \alpha}{\alpha}\right)^2 + \left(\frac{\delta n}{n}\right)^2 + \left(\frac{\delta l}{l}\right)^2} = 0.6\% = 0.0036m/s^2$
 - Sliding Force: $\frac{\delta F_{a,m}}{|F_{a,m}|} = \sqrt{(\frac{\delta a}{a})^2 + (\frac{\delta m}{m})^2 + (\frac{\delta \mu_k}{\mu_k})^2} = 0.6\% = 4.041 \text{ N}$
 - Moving Torque: $\frac{\delta T_{a,m}}{|T_{a,m}|} = \sqrt{(\frac{\delta F_{a,m}}{F_{a,m}})^2 + (\frac{\delta I}{I})^2 + (\frac{\delta \eta}{\eta})^2} = 5.62\% = 0.0335$ Nm
 - Static Torque: $\frac{\delta T_{a,s}}{|T_{a,s}|} = \sqrt{\left(\frac{\delta F_{a,s}}{F_{a,s}}\right)^2 + \left(\frac{\delta I}{I}\right)^2 + \left(\frac{\delta \eta}{\eta}\right)^2} = 5.59\% = 0.0361 \text{ Nm}$

• Linear Velocity:
$$\frac{\delta V_{max}}{|V_{max}|} = \sqrt{(\frac{\delta stepsize}{stepsize})^2 + (\frac{\delta I}{I})^2 + (\frac{\delta PPS}{PPS})^2} = 0.6\% = 0.178 mm/s$$

Motor Analysis – Limit Tolerance



- Some variables for Torque analysis have unknown tolerances
 - Solution: find limit values for these variables to prove feasibility through the Torque rating of the motor (T_{rating} = 1.22 N*m)

Screw Efficiency:
$$\eta_{lim} = \frac{F_{sliding}*I}{2\pi T_{rating}} = 43.9 \%$$

• Kinetic friction:

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•

$$\mu_{s,lim} = \frac{F_{rating}}{m * g} - 1 = 2.711$$

$$m_{lim} = \frac{F_{rating}}{m * g} = 48.12 \text{ km}$$

 $\mu_{k,lim} = \frac{F_{rating}/m-a}{q} - 1 = 2.651$

• Load Mass:

$$m_{lim} = \frac{F_{rating}}{a+g(1+\mu_k)} = 48.12 \text{ kg}$$

• Machining Force: $F_m = F_{rating} - F_{static} = 652.0 \text{ N}$

Overview

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Procured Components

Stepper Motor

Purpose

- Silverpak 23 C
- Ethernet Connection
- Built in driver/controller and Encoder



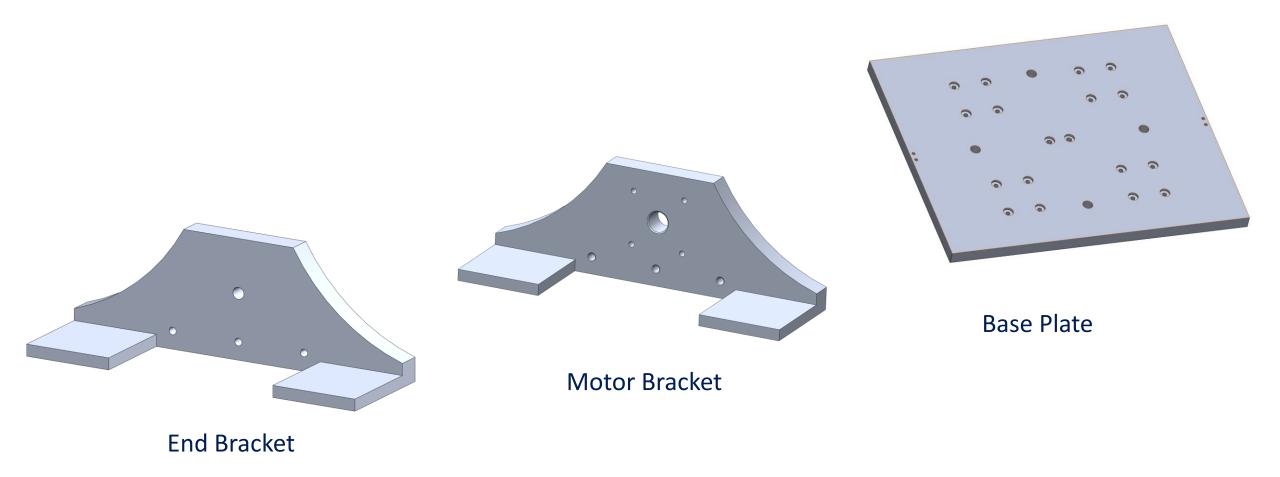
- ACT-PG-150-BS-20-5-N34
- Coupler
- Limit Switch
 - WS0850101F050SA





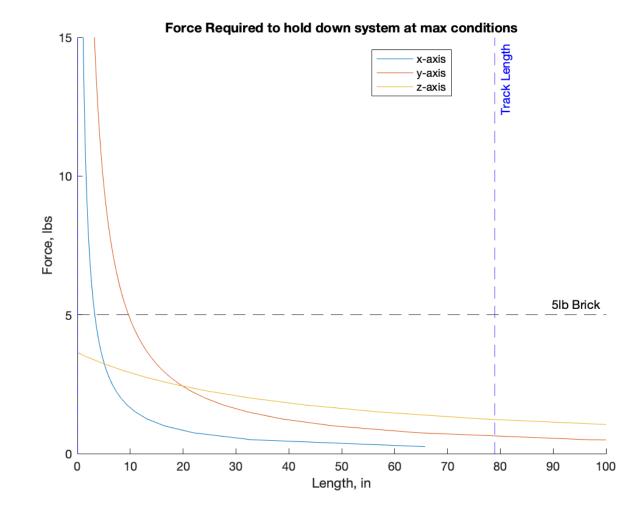
Manufactured Parts





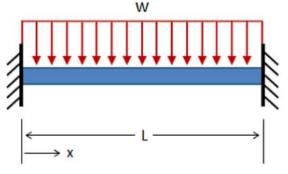
Feasibility of Mounting



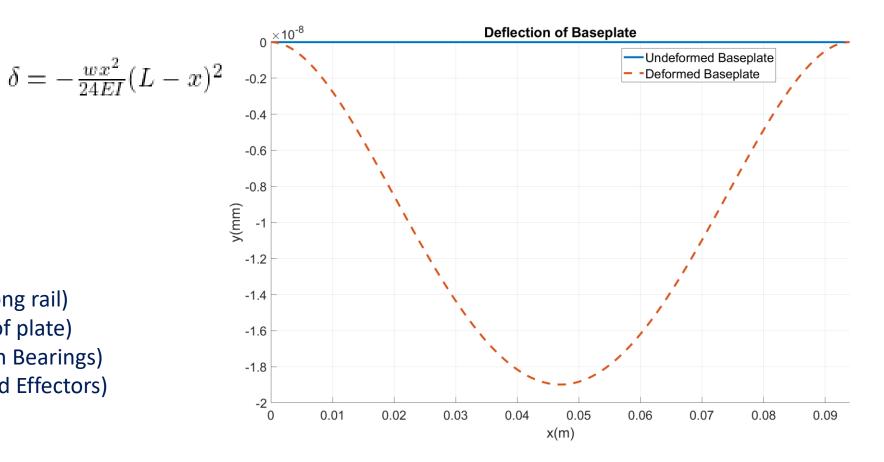


Baseplate Beam Calculation





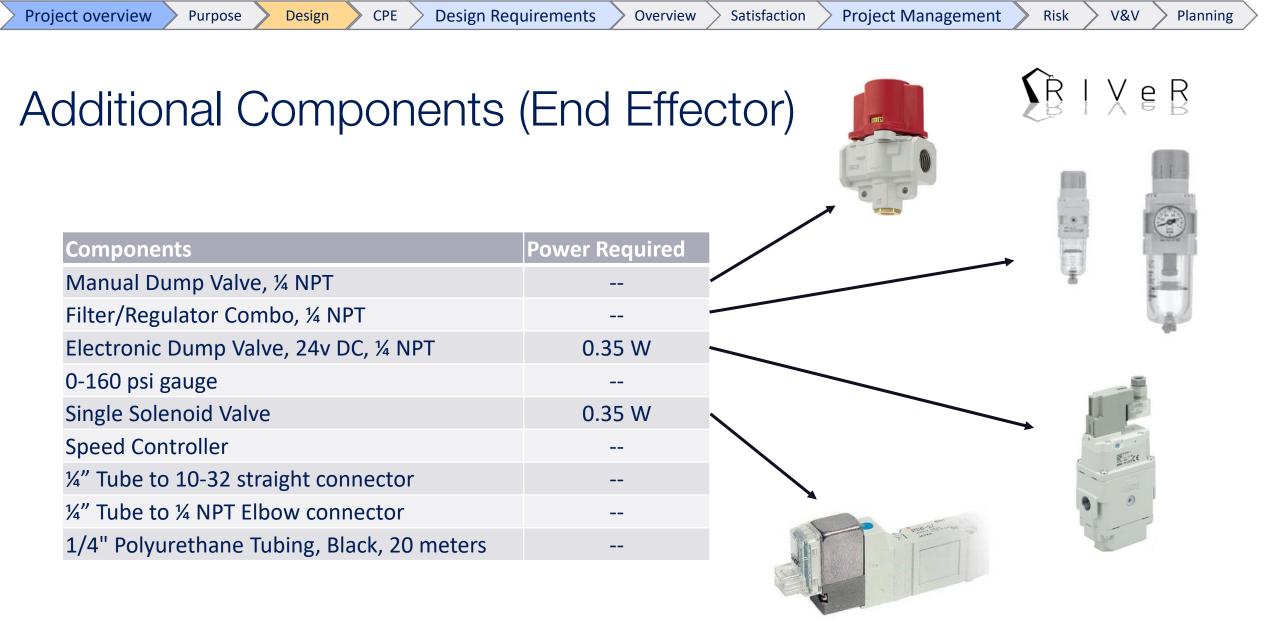
- E = 69 GPa
 - 6061 Aluminum
- I = (b•d^3)/12 = 5.12e-8 m^2
 - b= 300 mm (Distance along rail)
 - D= 1.27 mm (Thickness of plate)
- L = 94 mm (Distance Between Bearings)
- w= 330 N (Weight of Arm/ End Effectors)



Torque Analysis Assumptions



- Gravitational moment distributed among farthest bearings.
- Max robotic motor torque 330 Nm evenly distributed amongst bearings.
 - Won't be running on max torque.
- Over estimate proves stage viability

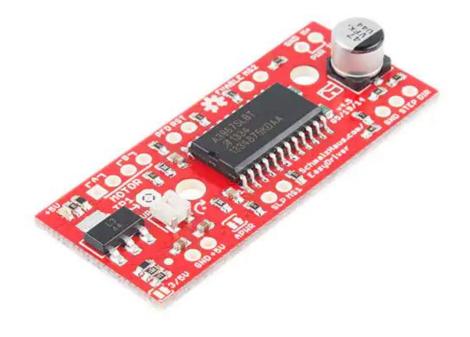


Solenoid Driver

• ROB-12779

- Arduino Compatible
- Will use digital Logic from Arduino
- Enable line to Solenoid
- Powered from 24 V
 - Included with End Effector in power budget





Design Requirements

Overview

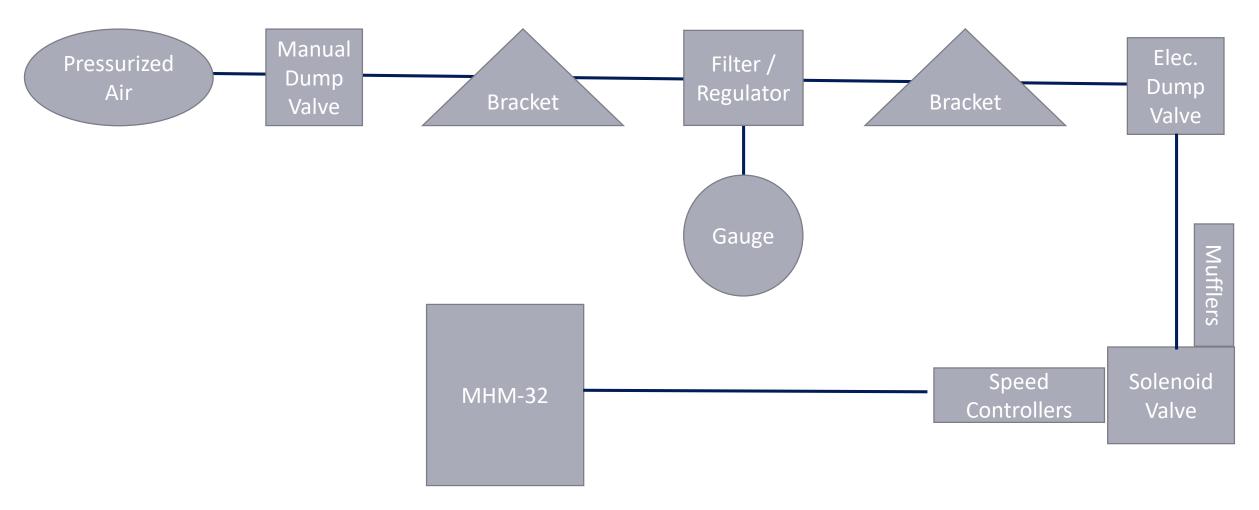
Satisfaction > Project Ma

Project Management Risk V&V

/ > Planning

<u>Ř</u> I V e B









Planning

DR #	Req(s)
DR 1.2	Arm shall be able to maintain security of bags with a force of 10N
DR 6.1	Secure cargo for the duration of transit from the origin to the end of the track system.

• Show previous analysis for torque stall

Overview

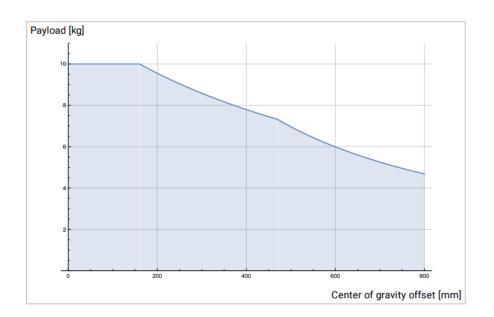
Risk V&V Planning



Motor Torque-Speed Analysis

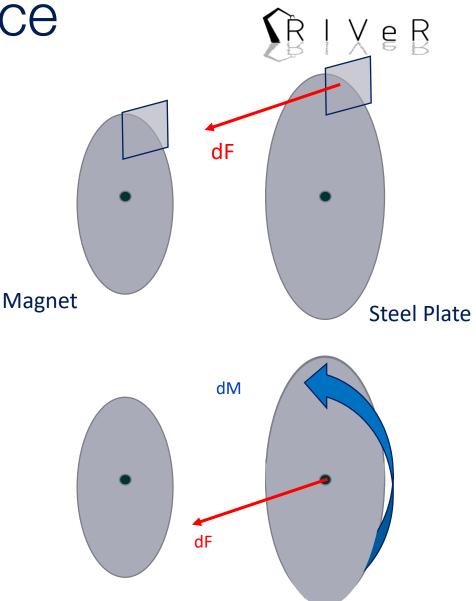
- Max speed is limited by manufacturer
 - Joint size 2,3: 180 deg/sec
 - Joint size 4: 120 deg/sec
- Motors are rated such that max speed is viable through the continuous torque range
- Max payload is dependent on the *center of gravity of offset*
 - *C.O.G. Offset:* Distance b/t payload c.o.g. and center of tool flange
 - With the given 1 kg payload the c.o.g offset can be up to .8 m, well within our parameters

Working range	Maximum speed
± 360°	± 120°/s
± 360°	± 120°/s
± 360°	± 180°/s
	± 360° ± 360° ± 360° ± 360° ± 360°



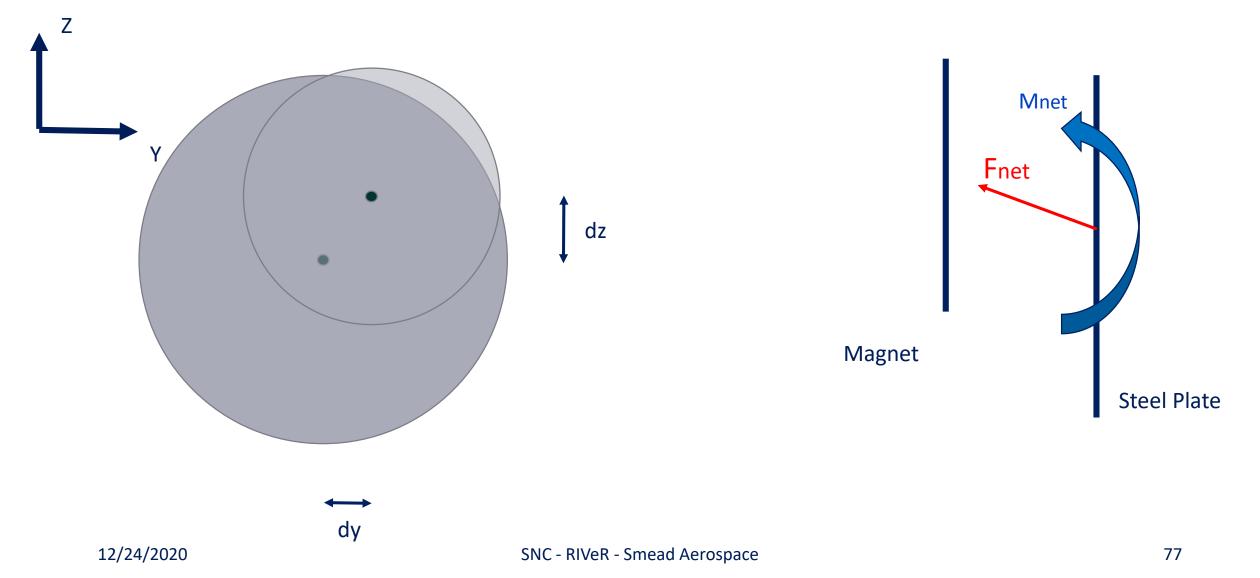
End Effector Magnetic Force Analysis

- Discretize magnet and steel plate
- Compute the force between each gridpoint of the magnet to each gridpoint of the steel plate
- Make an equivalent Force-Moment representation to get a net Force and net moment



End Effector Reaction Force Analysis





End Effector Reaction Force Analysis



• Reaction Force Form: p(y,z) = az + by + c

• Solve for c

$$\int \int p(g)$$

$$\int \int p(y,z) dy dz = F_x$$
 Pad

• Centroids:
$$\bar{z} = \frac{\int \int zp(y,z)dydz}{\int \int p(y,z)dydz}$$
 $\bar{y} =$

$$\bar{y} = \frac{\int \int yp(y,z)dydz}{\int \int p(y,z)dydz}$$

Solve for a and b

$$\bar{y} \int \int p(y,z) dy dz = M_z$$
 Pad

$$\bar{z} \int \int p(y,z) dy dz = M_y$$

Pad

12/24/2020

Design Requirements

Overview

Satisfaction

0.0

0.0

0.0

23.5

Y Axis [mm]

-23.5 -23.5

-23.5 -23.5

-23.5 -23.5

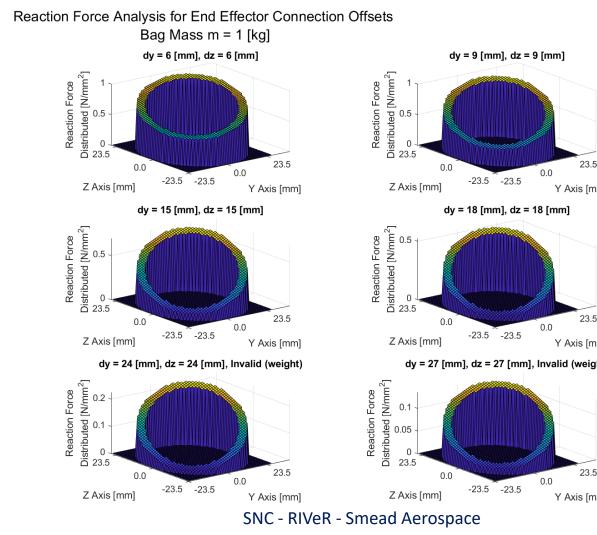
Project Management Risk Planning

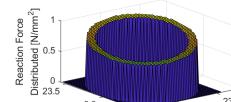


V&V

	DR #	Req(s)
nm]	DR 1.2	Arm shall be able to maintain security of bags with a force of 10N
[mm] 23.5 Y Axis [mm] valid (weight)	DR 6.1	Secure cargo for the duration of transit from the origin to the end of the track system.

Steel Plate: d = 40 [mm] μ = 0.1





0.0

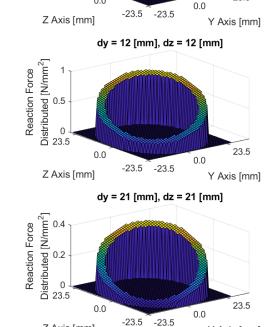
Z Axis [mm]

dy = 3 [mm], dz = 3 [mm]

Purpose

23.5

Y Axis [mm]



12/24/2020

79

Robotic Arm Tech Specs



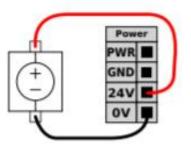
- Communication:
 - 500 Hz Control frequency
 - Modbus TCP
 - PROFINET
 - Ethernet/IP
 - USB 2.0, USB 3.0
- Operating Temperature Range 0-50°C

Extra Power to UR-10





If more current is needed, an external power supply can be connected as shown below.



- 24V 3A Power Supply Attached
 - Adds to 2 A included
- Total Power From 24V Rail
 - 5 A
 - 120 W
- Includes free wire adapter

USB Power

- Arduino
 - Includes 1 Meter USB
 2.0
 - .05 A 5 VDC
- Pixy 2 Cameras
 - Micro USB
 - 1 Meter Included
 - .14 A 5 VDC
- USB Power Supply
 - 2.4 A per port for multiple devices





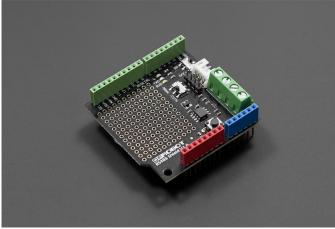
Power Budget Cont.



4VDC Rail					5 VDC Ra	ul			
Part	Current [A]	Voltage[VDC]	Number of Parts	Power[W]	Part	Current [A]	Voltage[VDC]	Number of Part	
Power Supply	3	24	1	72	USB Power Supp	bly 20) 5	5	
UR-10	2	24	1	48	Arduino	-0.05	5 5	5	
Stepper Motor	-3	24	1	-72	Pixy2	-0.14	4 ÷	5 10	
Limit Switch	-0.1	24	. 2	-4.8	Total				
MHM 25	-0.8233333333			-20.72					
Total	1.076666667	,		22.48					
MHM 25 Brea	kdown					D evite			
					Voltage Rails				
Part	Current [A]	Voltage[VDC]	Number of Parts	Power[W]	24 V	MHM 25, Stepper, Limit Switch			
D-M9PWV	-0.04	24	2	-1.92	12 V				
Solenoid Driver	-0.75	24	1	-18					
Solenoid	-0.01458333333	24		-0.35	5 V	Pixy 2, Arduino			
Solenoid SY	-0.01875	24		-0.45	30 V				
Total	-0.8233333333			-20.72					

Stepper Motor

- RS-485
 - Differential signal
- Arduino used as PLC
 - Serial commands converted from UART to RS-485
 - Receives corrected encoder data
- RS-485 Shield





Silverpak 23C and 23CE INTEGRATED STEP MOTOR, DRIVER AND CONTROLLER(CE)

(23CE With optional encoder feedback – closed loop)



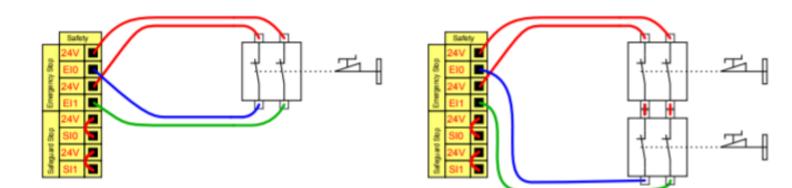
Limit Switch

- 2 Limit Switches
- Connected to
 emergency stop
- 2 Pin outs
- 24V limit switch selected.



4.3.2.2 Connecting emergency stop buttons

In most applications it is required to use one or more extra emergency stop buttons. The illustration below show how one or more emergency stop buttons.



SB | X e B

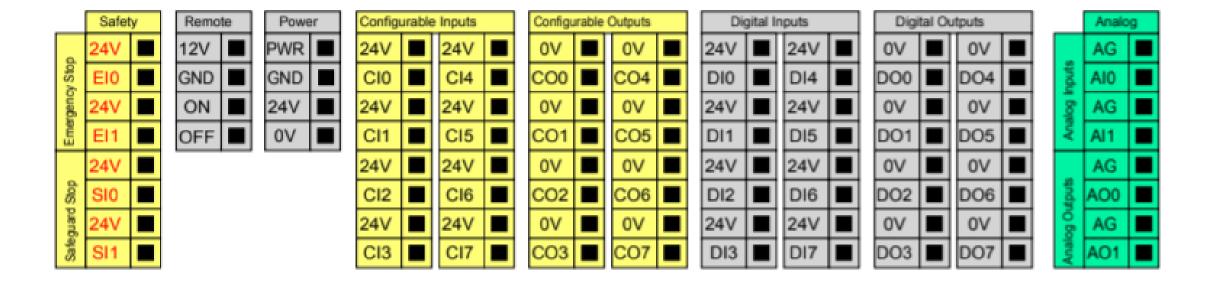
Wiring

- 75 ft needed
 - 180 ft accounted for
- 24 Gauge Wire Selected
- 30 T2 connectors to split I2C and power lines



UR-10 Electronics Interface





Arduino Uno Pin Out

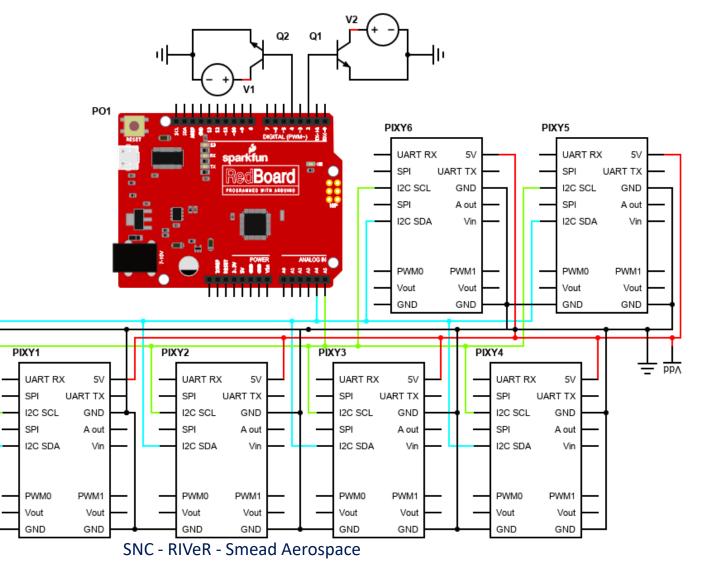


Pin	Function	Device
RX0 (Pin 1)	UART RX	RS-485 Shield
TX0 (Pin 2)	UART TX	RS-485 Shield
Digital 3	Logic High/Low	Solenoid Driver
Digital 4	Logic High/Low	Auto Switch
Digital 10	SS	Ethernet Shield
Digital 11	MOSI	Ethernet Shield
Digital 12	MISO	Ethernet Shield
Digital 13	SCK	Ethernet Shield
Analog 4	SDA	Pixy2 Cameras
Analog 5	SCL	Pixy2 Cameras

Arduino Pin Out







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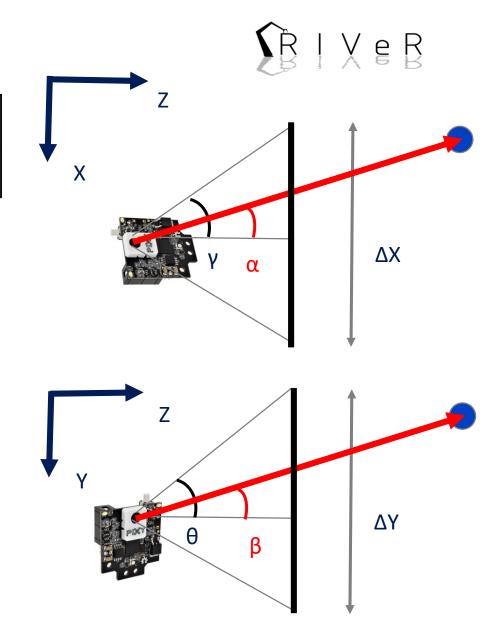
89

Sensor State Estimation $T = \begin{bmatrix} \tan(\gamma) & 0 & 0 \\ 0 & \tan(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad \Delta = \begin{bmatrix} \frac{2}{\Delta x} & 0 \\ 0 & \frac{2}{\Delta y} \\ 0 & 0 \end{bmatrix} \quad \vec{i} = \begin{bmatrix} 1 \\ 1 \\ -1 \end{bmatrix} \quad \mathbf{x}$

 $C = \begin{bmatrix} \hat{x}_C & \hat{y}_C & \hat{z}_C \end{bmatrix} = \text{ Core Coordinate Frame} \\ \text{ Definition Matrix} \end{cases}$

$$\vec{s} = \begin{bmatrix} x_s & y_s & z_s \end{bmatrix} =$$
 Sensor Position Vector

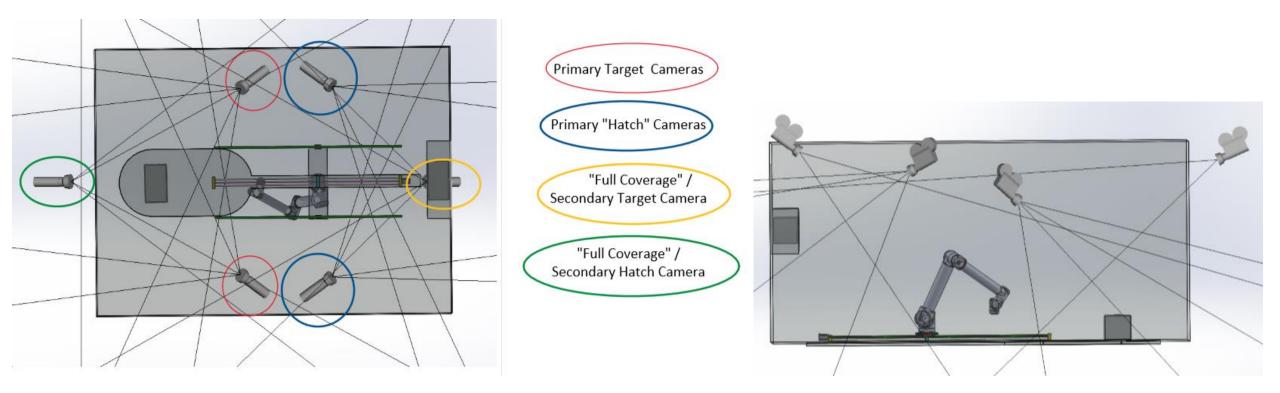
 $a = \hat{z}_s C^T (\mathbf{x} - \vec{s}) = \text{Proportionality Constant}$ $\hat{y}(k) = (\Delta^T \Delta)^{-1} \Delta^T (\frac{1}{a} T^{-1} S^T C^T (\mathbf{x} - \vec{s}) + \vec{i})$



12/24/2020



Pixy2 Placement: 6-Cam System



Pixy Locations



				Camera 4					
X (meters)	+0.50	+0.56	+0.56	+0.50	+2.23	3.21	3.8	3.19	2.22
Y	-0.55	+0.52	+0.52	-0.55	-1.16	-0.54	-0.22	-0.54	-1.16
Z	-0.98	-0.60	+0.60	0.98	0.61	0.98	0	0.99	-0.6

0.25 m into the center of the hatch

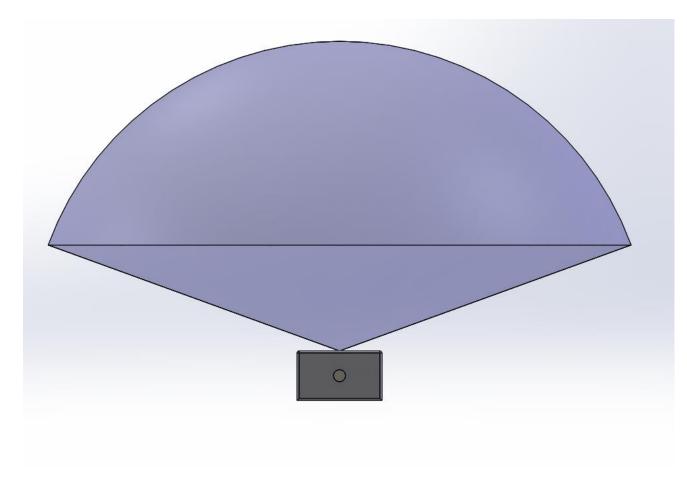
Pixy Locations – Center of Hatch



				Camera 4					
X (meters)	+0.25	+0.31	+0.31	+0.25	+1.975	2.96	3.55	2.94	1.975
Y	-0.55	+0.52	+0.52	-0.55	-1.16	-0.54	-0.22	-0.54	-1.16
Z	-0.98	-0.60	+0.60	0.98	0.61	0.98	0	0.99	-0.6

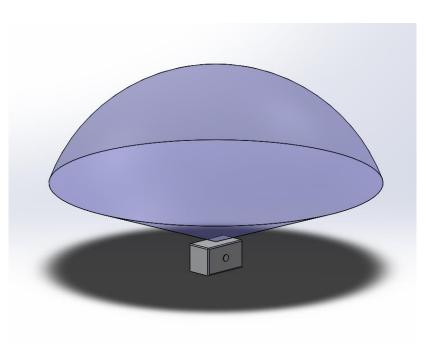
X is normal to hatch-planeY is vertical up down in hatch-planeZ is horizontal left-right in hatch-plane

Viewing Regions

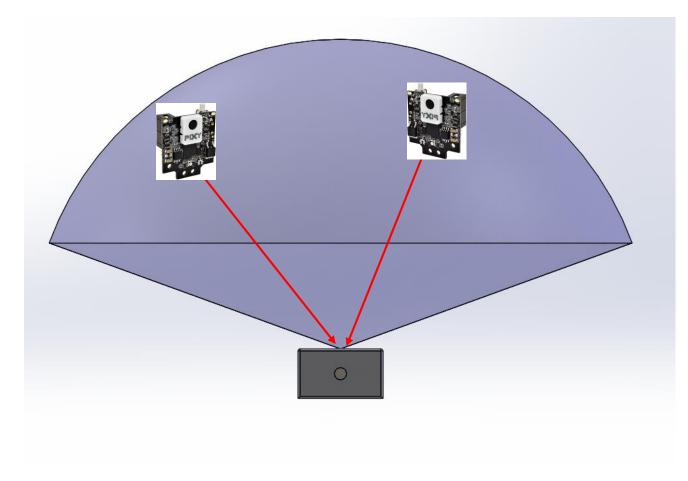




- Dependent on viewing distance and maximum incident angle
- Regions repeat every 90 degrees

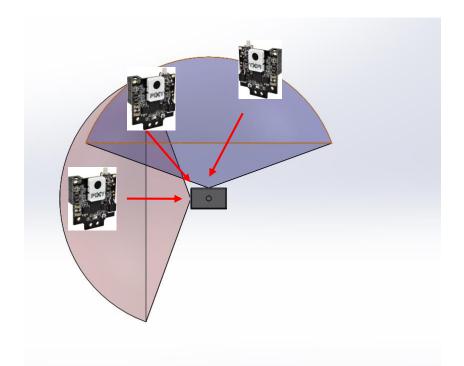


Camera Angles





- 2 Cameras in the same region will see the same face
- Angle between 2 Cameras must be less than 90 degrees







DR.3.1	The system shall identify a cargo bag with its orientation and position.	
DR.3.2	The system shall be able to determine if the cargo has reached the target location	
DR.3.3	The operating system shall be able to determine if the cargo is irretrievable.	
DR.3.4	The system shall give feedback if the transportation has failed and cease operations.	
DR.6.1	The end-effector shall secure cargo for the duration of all translation and rotation required for a task.	

Overview

- Satisfaction of the above dependent upon Pixy 2 uncertainty
 - Setup -<u>60°</u> <u>40°</u> <u>Test Setup</u> <u>60°</u> <u>60°</u>

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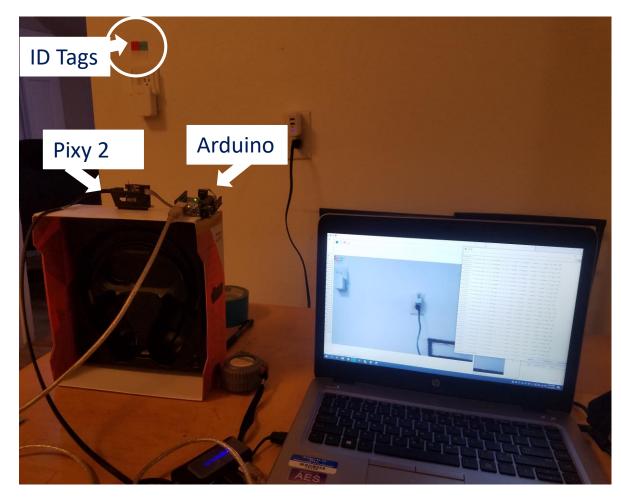
Risk > V&V > Planning

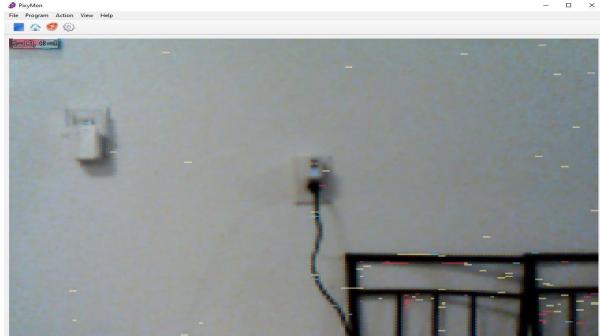


Test Setup

Design

Purpose





Detected 1

block 0: CC block sig: 12 (10 decimal) x: 15 y: 5 width: 26 height: 6 angle: -4 index: 218 age: 255 Detected 1

- block 0: CC block sig: 12 (10 decimal) x: 16 y: 4 width: 28 height: 5 angle: -11 index: 218 age: 255
 Detected 1
- block 0: CC block sig: 12 (10 decimal) x: 15 y: 4 width: 26 height: 5 angle: 0 index: 218 age: 255 Detected 1
- block 0: CC block sig: 12 (10 decimal) x: 15 y: 4 width: 26 height: 5 angle: 0 index: 218 age: 255 Detected 1

block 0: CC block sig: 12 (10 decimal) x: 15 y: 5 width: 26 height: 6 angle: -11 index: 218 age: 255
Detected 1

block 0: CC block sig: 12 (10 decimal) x: 14 y: 4 width: 28 height: 5 angle: 4 index: 218 age: 255

Uncertainty Results



1) Test #	2) Distance to wall [in]	3) Individual Tag Dimensions [in]	4) Plane Width [in]	5) Physical Tag Width %	6) Pixel coordinate	7) Pixel Tag Width %	8) Error [%]
1	27.5"	1" x 7/8"	31.75"	3.149%	10.22	3.245%	3.05%
2	41.125"	1" x 7/8"	47.487"	2.125%	7.667	2.433%	13.2%
3 (old settings)	41.125"	2" x 7/8"	47.487"	4.25%	14.83	4.709%	10.8%
4 (new settings)	41.125"	2" x 7/8"	47.487"	4.25%	12.65	4.016%	5.50%
5	61"	2" x 7/8"	70.437"	2.839%	9.45	3.000%	5.67%
6	61"	2" x 1 3/8"	70.437"	2.839%	9.25	2.937%	3.45%
7	85.5"	3" x 1 3/8"	98.727"	3.039%	10.15	3.222%	6.03%

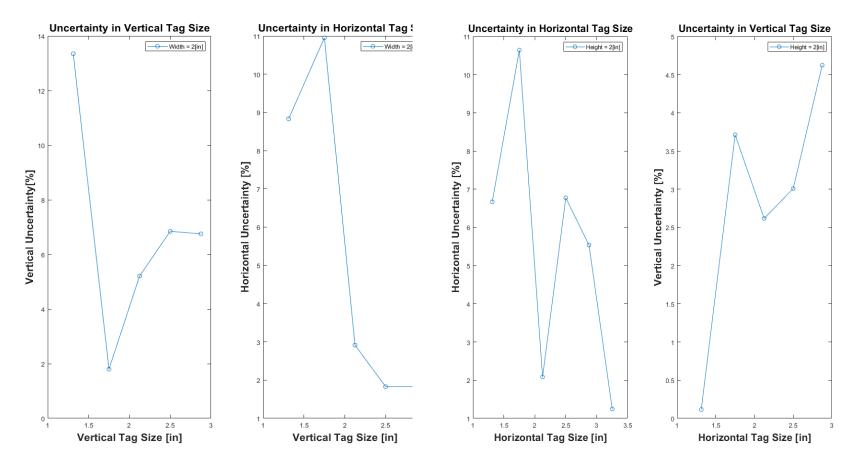
Overview

Uncertainty Based on Tag Size



Varying Height With Constant Width

Varying Width With Constant Height



Horizontal accuracy proportional to tag width and height
Vertical accuracy dominantly proportional to tag height
Tests evaluated with default
sensitivity settings
Accuracy can still be improved
Tweak sensitivity and range
Improved Lighting

Better test setup

Design Requirements

Satisfaction > Project Management

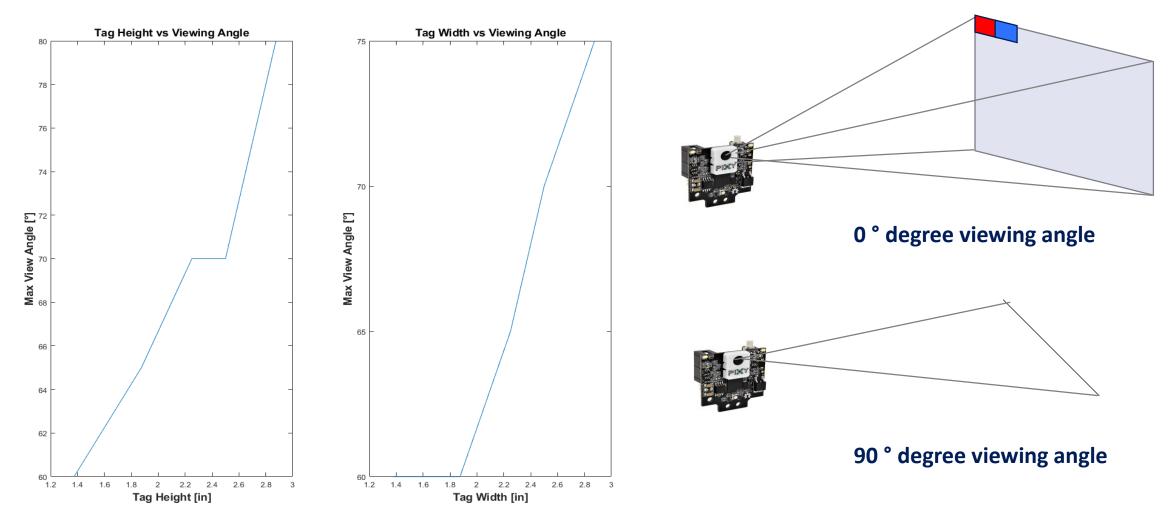
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/ > Planning

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Pixy Viewing Angle Determination



Overview

Overview

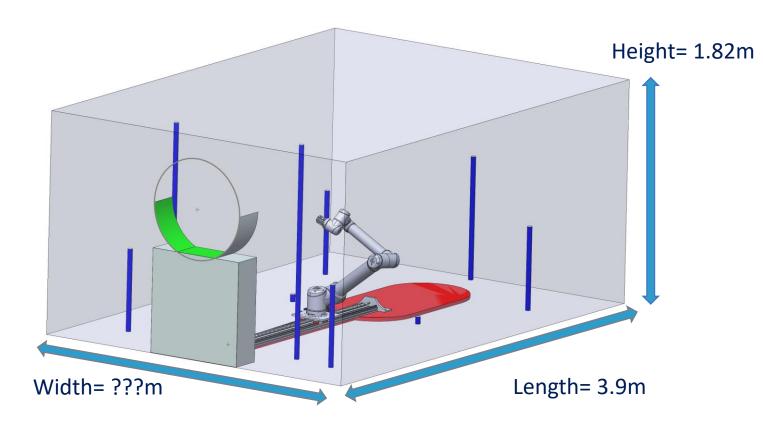
Satisfaction > Project Management

ent Risk V&V

Planning

IXeB

Testing Set Up Version 1



Capture Area Release Area Camera Stands

Cameras mounted using square, telescoping rods

Overview

Measurements

Purpose



Measurement	Key Issues	Design Solution
Cargo Bag Images	Image coverage must include at least 3 faces of the bag for orientation determination	Allocate 4-5 cameras for the capture and release locations
	Resolution of bag	Pixy2 Cameras are placed within 1.3 meters of the capture and release locations
	Microcontroller processing limits for data from 10 cameras	Arduino is capable of handling around 15 Pixy2 Cameras
Environment Images	Obstructions to camera views and arm's path	Combination of camera views of entire environment and RViz
Translator: Encoder/ Push Sensor Data	Microcontroller can process limits for translator in addition to sensor system	Arduino is capable of processing data from translator in addition to the 10 cameras

Overview



Objective:

Purpose

- 1. Test Sensory Modeling
- 2. Verify Arduino can handle heavy processing power

Camera System Verification

Plan:

- Vary Cargo Bag orientations and positions with the capture and release locations
- Simultaneously communicate data from all the Pixy2 Cameras to the Arduino