

Test Readiness Review



REcuperating Advanced Propulsion Engine Redesign

Customer: Air Force Research Lab

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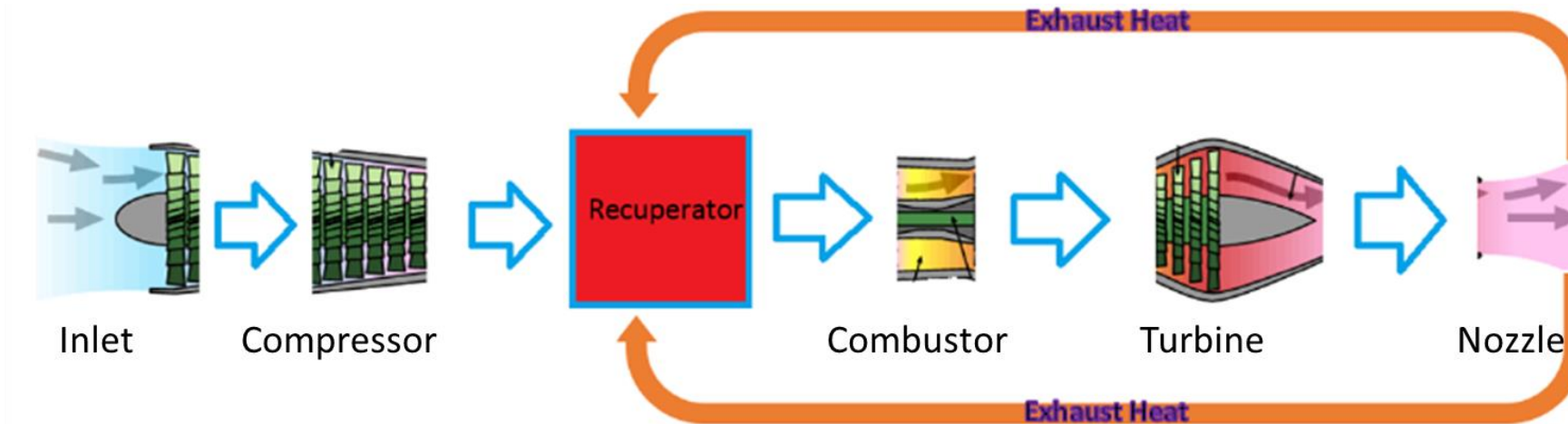


Presentation Agenda



- Project Overview
- Schedule
- Testing
- Budget

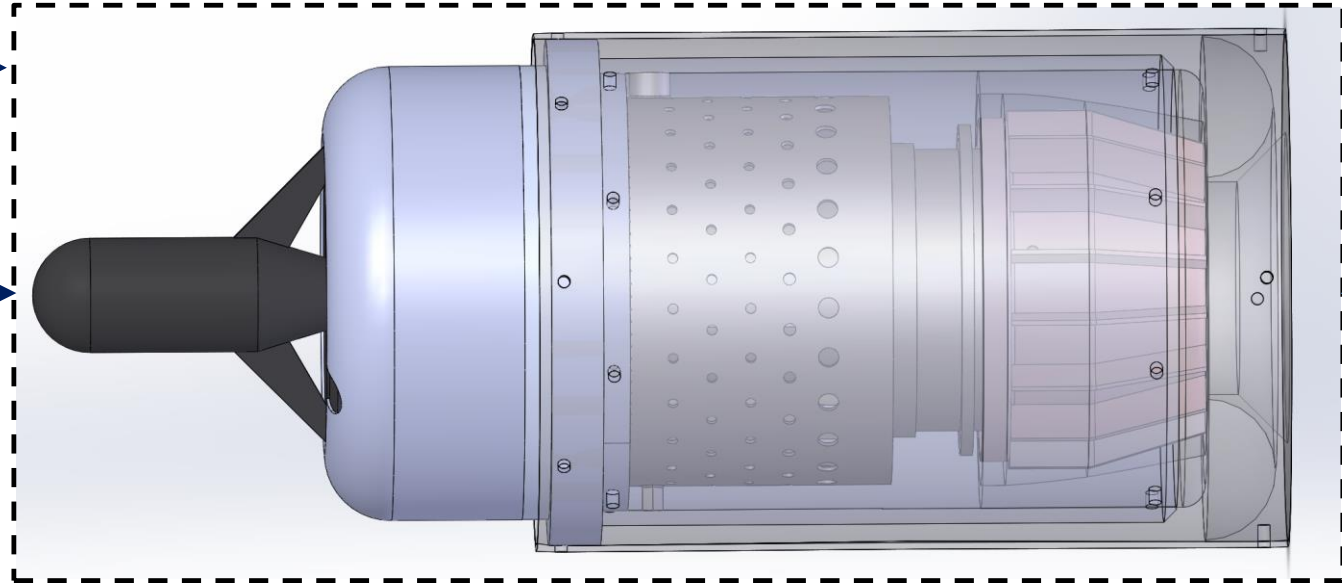
Model, build, implement, and verify an integrated recuperative system into a JetCat P90-RXi miniature turbojet engine for increased fuel efficiency from its stock configuration.



Kerosene Fuel



Modified P90-RXi



Fuel Flow Sensor



Transmitter



Receiver

Engine Control Unit



SD Card



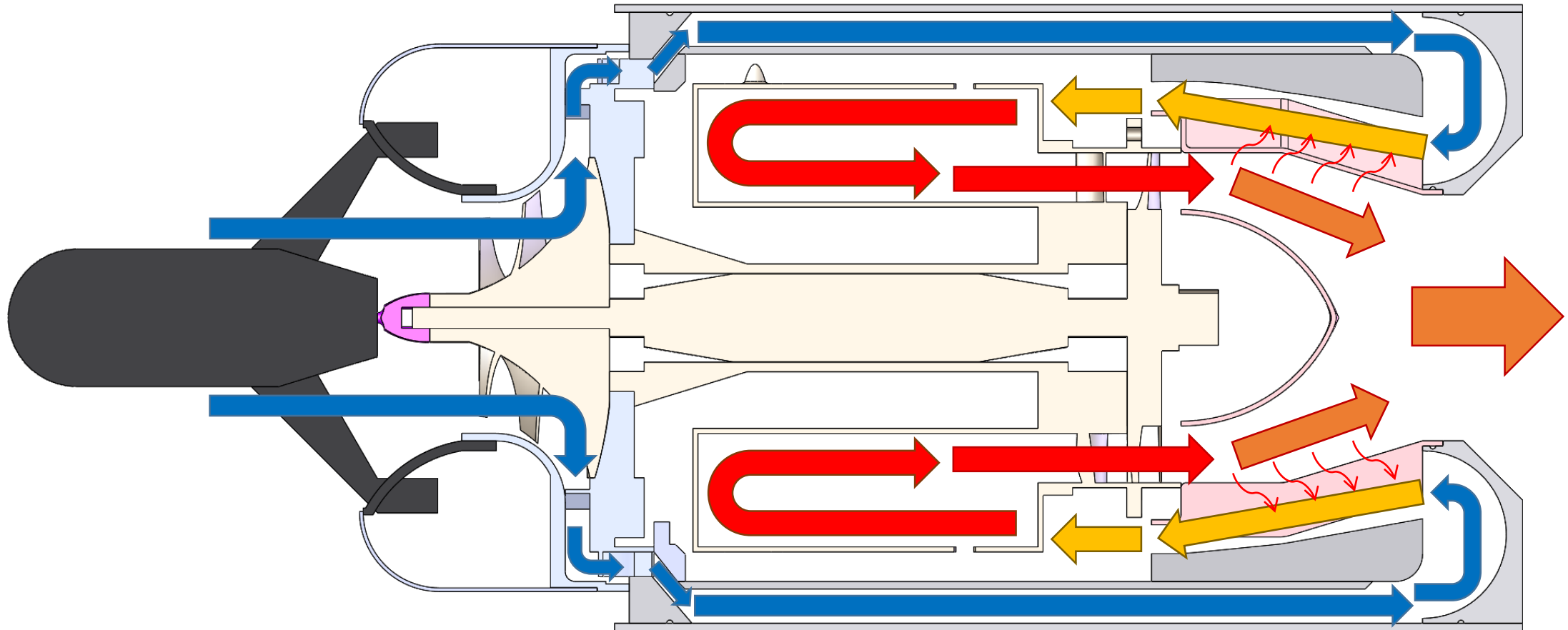
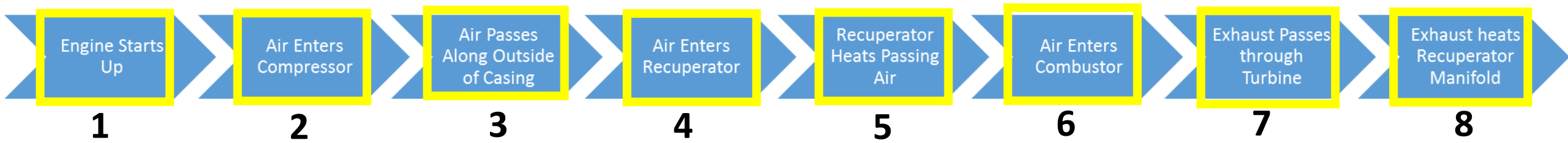
Computer

Load Cell, Thermocouples

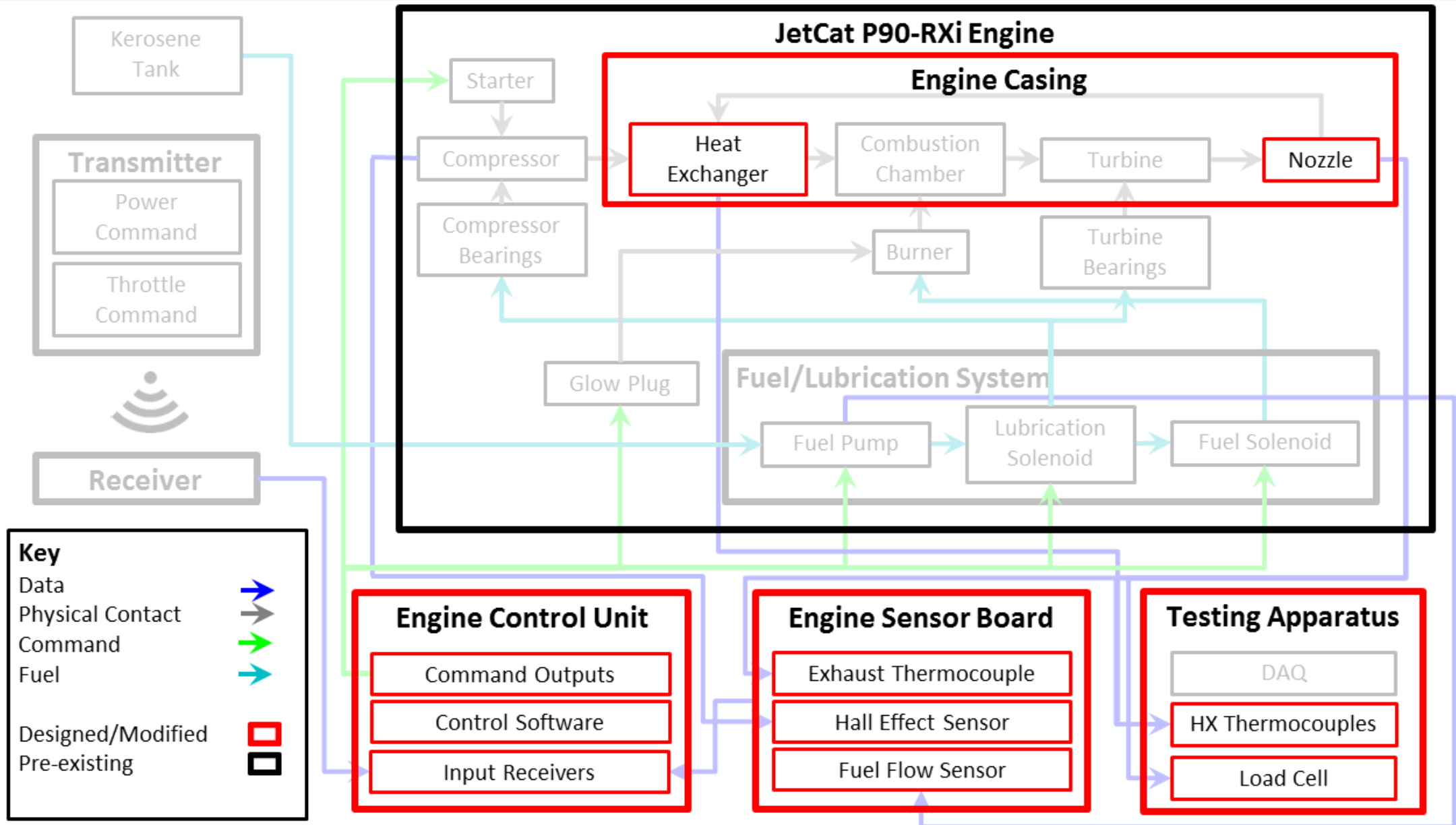


NI DAQ Chassis

Baseline Design: Flow Path



Functional Block Diagram



CPE 1: Thermal-Fluid Modeling

- System **Characterization**

CPE 2: Heat Exchanger

- **Manufacturing**, Cost, Integration

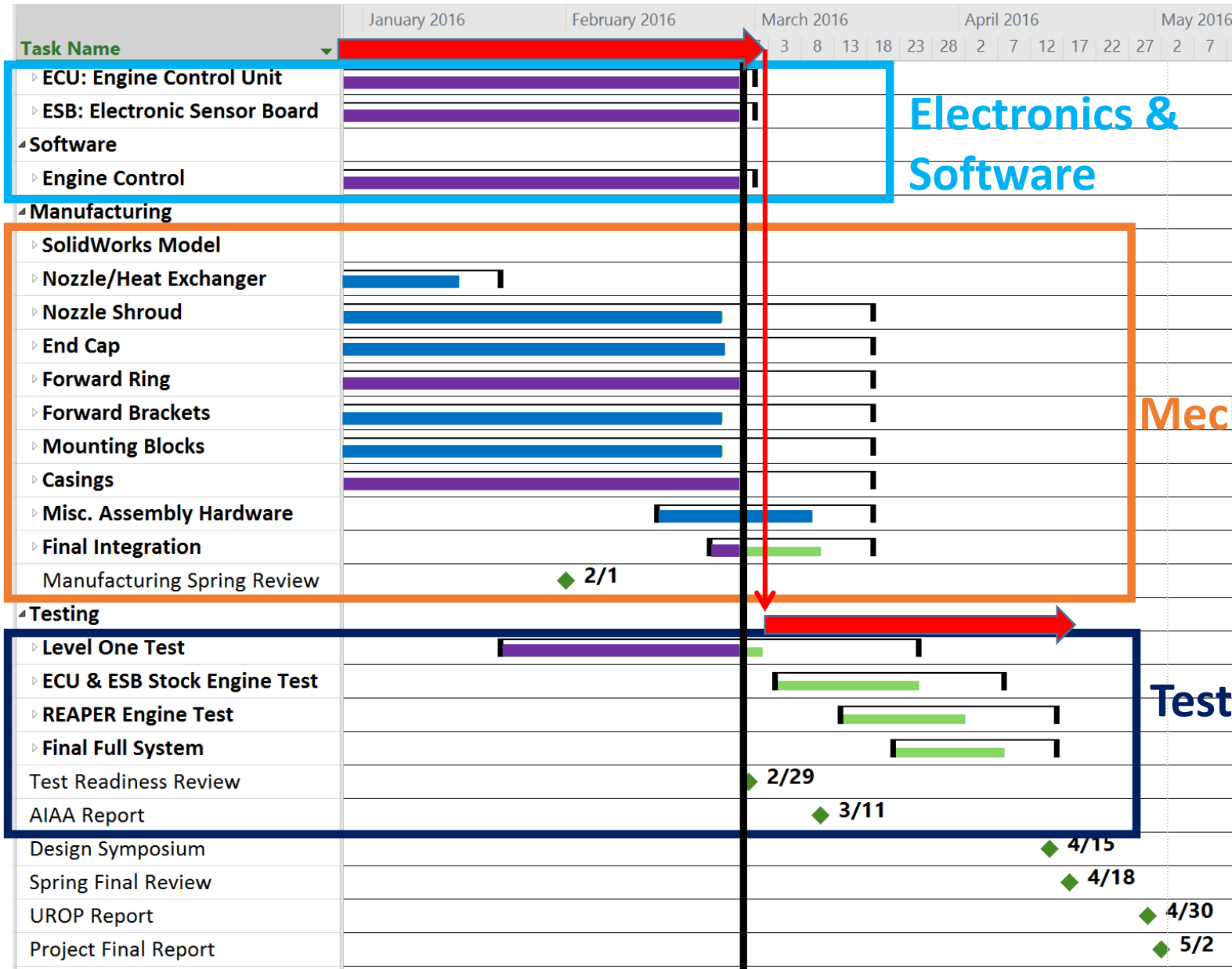
CPE 3: Engine Electronics

- **Control**, Safety, Sensors

CPE 4: Testing

- **Model Validation**, System Verification, Sensors

	Simulation	Recuperator
Level 1	<p>(CPE 1 - Model)</p> <ul style="list-style-type: none"> -Develop first order, steady state model -Model heat exchanger effectiveness, specific fuel consumption and thrust <p>✓</p>	<p>(CPE 2 – Heat Exchanger) (CPE 4 – Testing)</p> <ul style="list-style-type: none"> -Recuperator designed and manufactured -Recuperator verified with engine analog
Level 2	<ul style="list-style-type: none"> -Model transient characteristics <p>✓</p>	<p>(CPE 3 – Engine Electronics)</p> <ul style="list-style-type: none"> -Recuperator is integrated onto engine -Integrated engine system starts and runs
Level 3	<ul style="list-style-type: none"> -Develop CFD model -Model is verified with test data <p>✓</p>	<ul style="list-style-type: none"> -Engine system operates for throttle range -Engine system meets design requirements



Electronics & Software

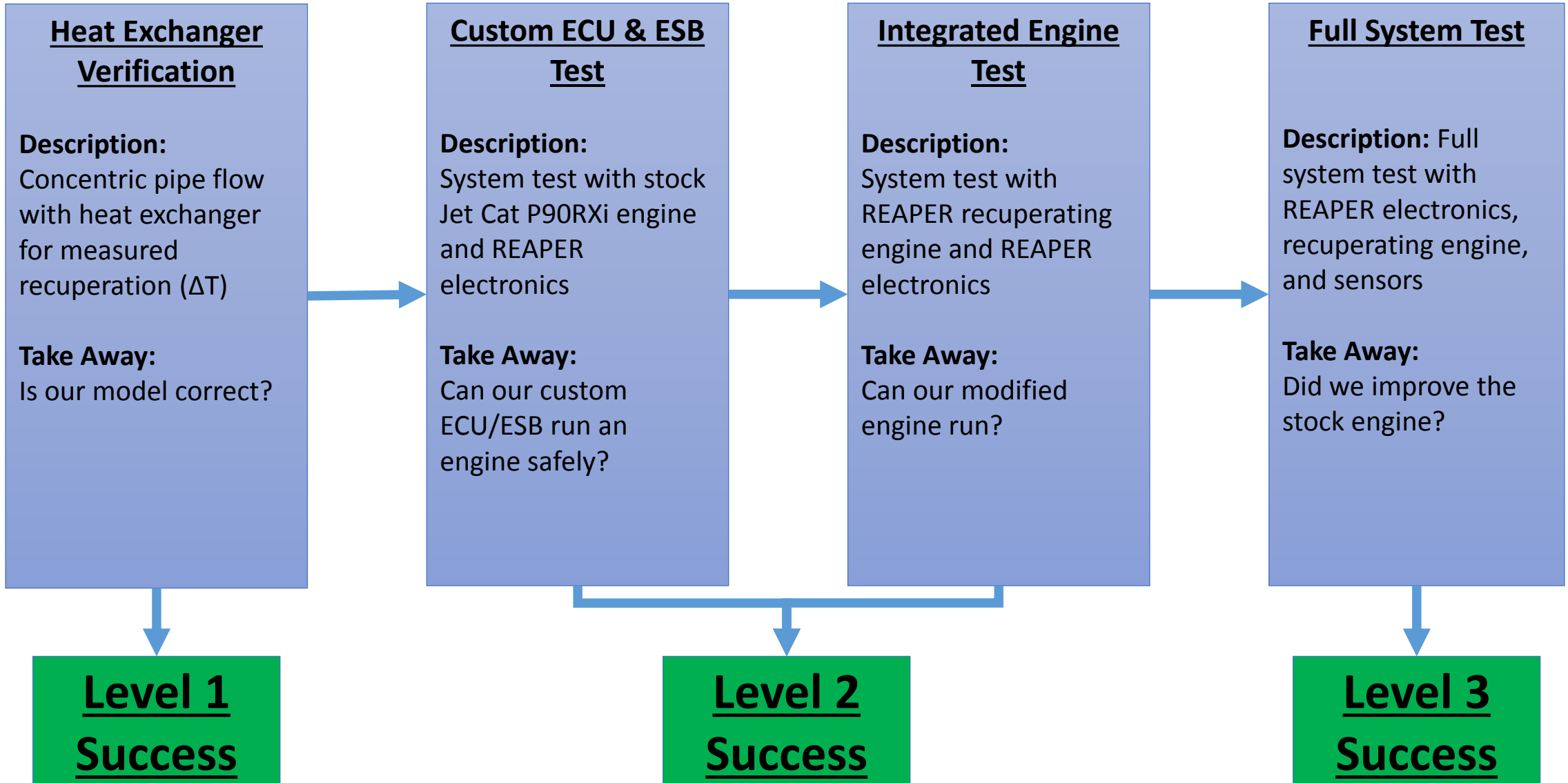
Mechanical

Testing

Key:
 Completed
 Current Progress
 Planned Time
 Margin



Testing



Heat Exchanger Verification Overview

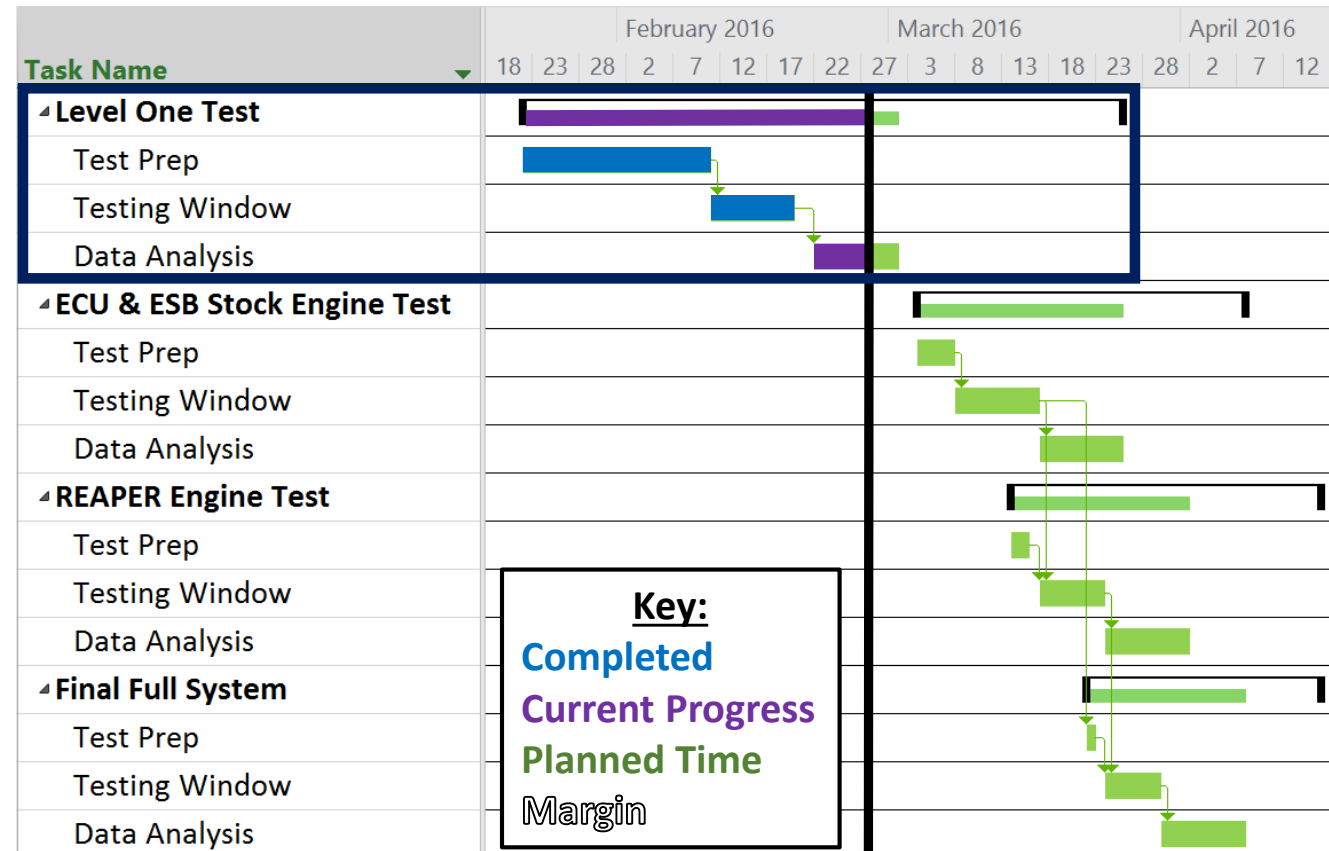
Test Dates: 2/11-2/19

Purpose:

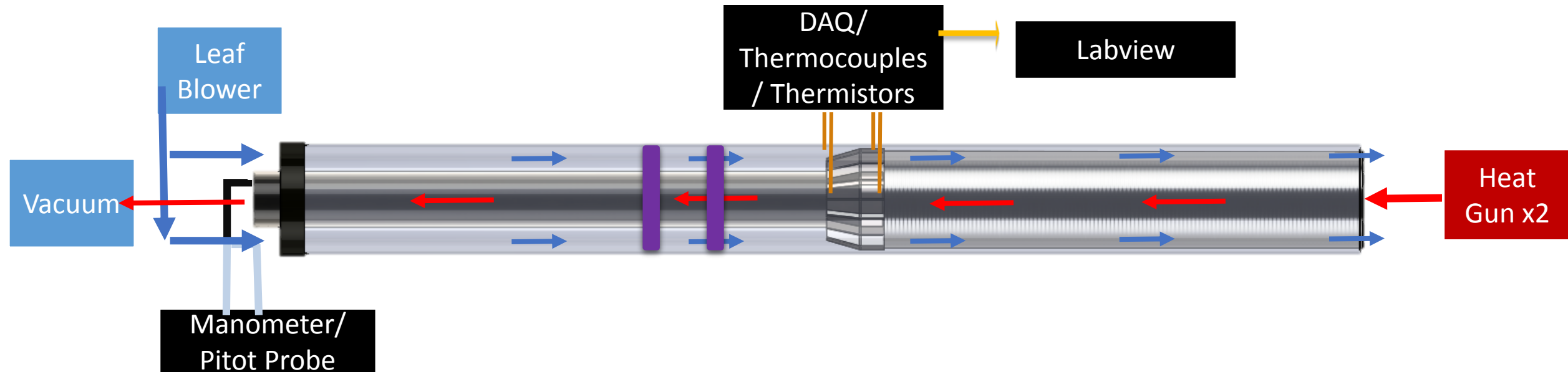
- Measure temperature change across concentric flow heat exchanger to validate model

Main Test Equipment:

- REAPER Nozzle-Heat Exchanger
- Thermistors (Cold side)
- K-Type Thermocouples (Hot side)
- Pitot Tube/Manometer

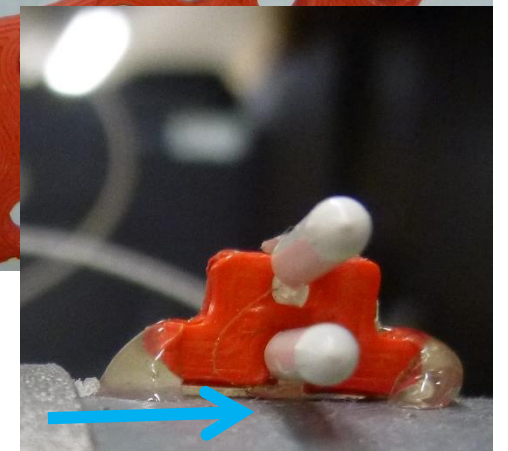
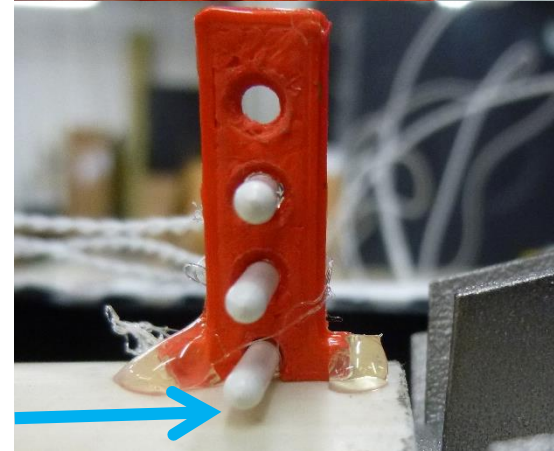
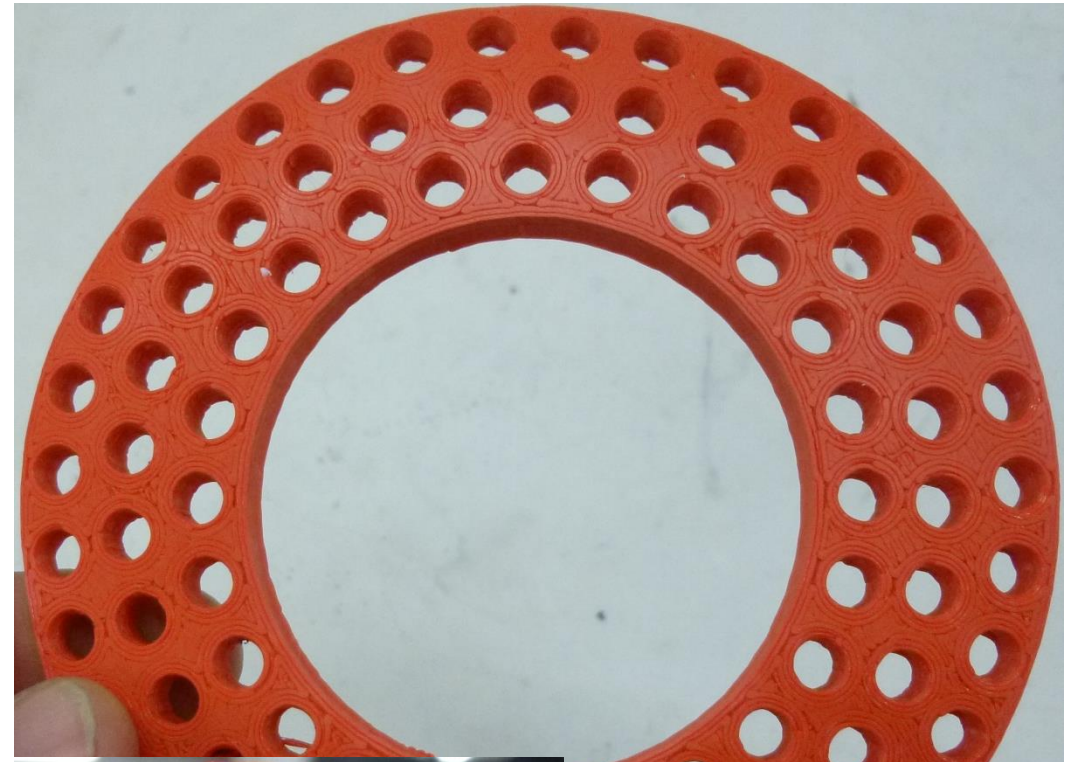
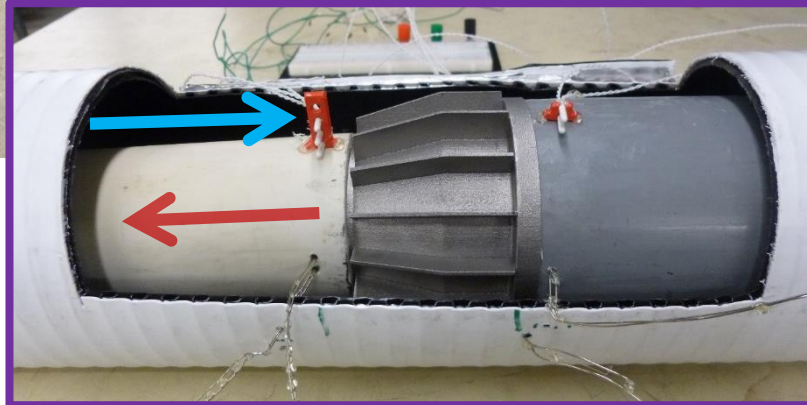
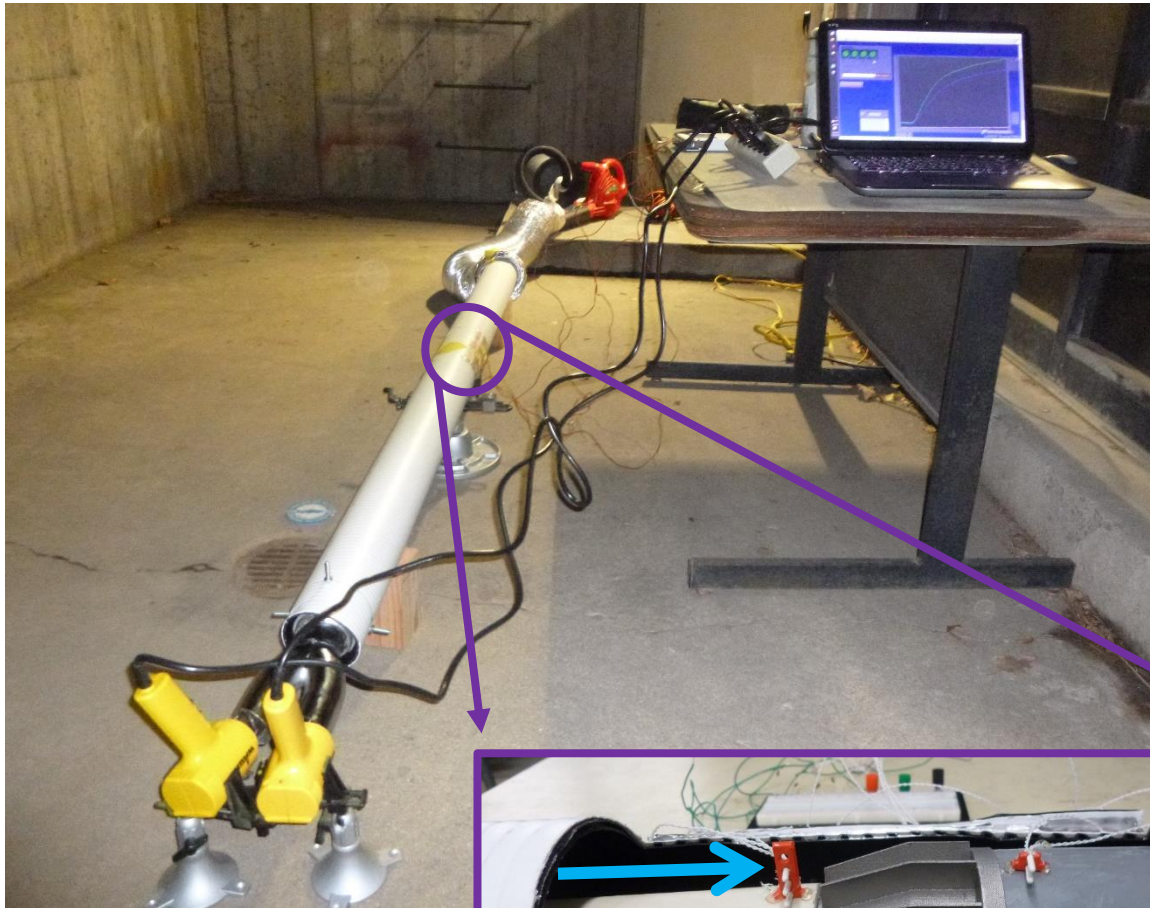


Estimated Hours Remaining: **10 hours**
 Workforce: **2**
 Scheduled Time after TRR: **15 hours**

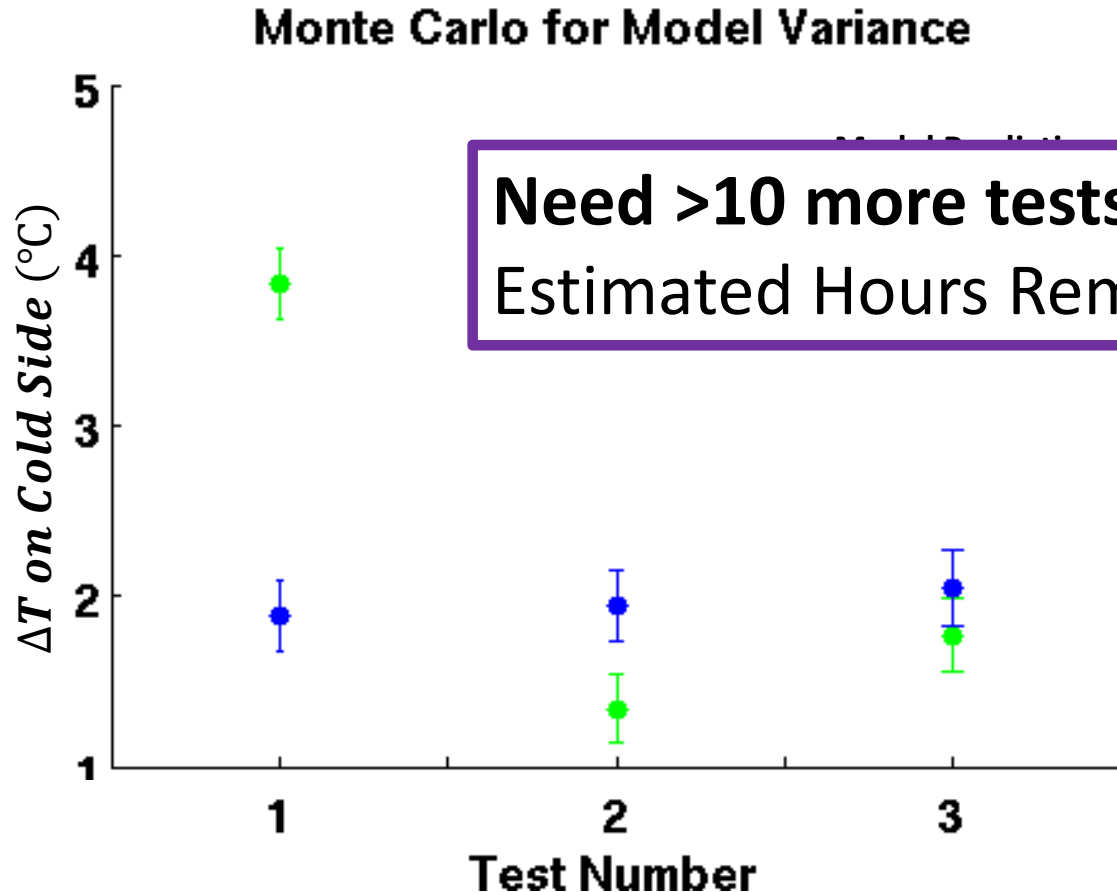
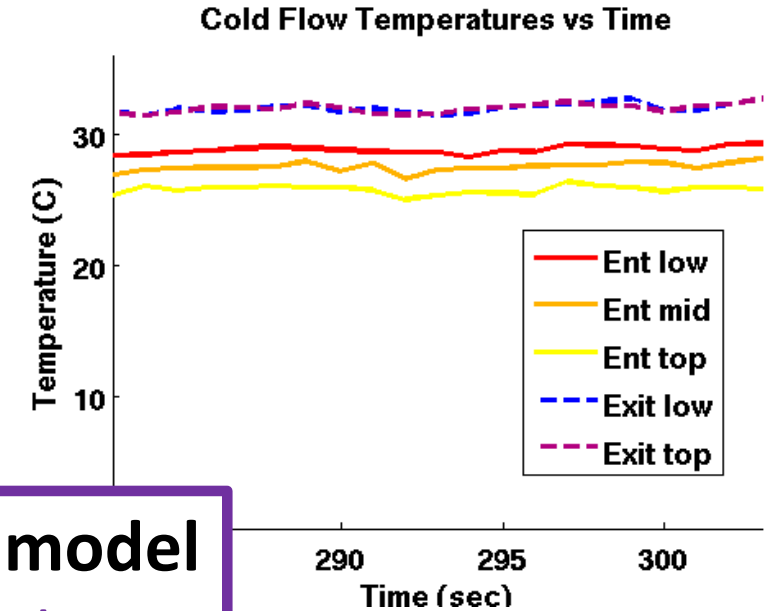


Sensor List	Error	Expected Sample Range	Sample Rate
Thermocouples	+/- 2°C	Hot Flow 100-300°C	1Hz
Thermistors	+/- 0.2°C	Cold Flow 10-40°C	1 Hz
Pitot Static Tube	+/- 1 m/s	5-40m/s	N/A

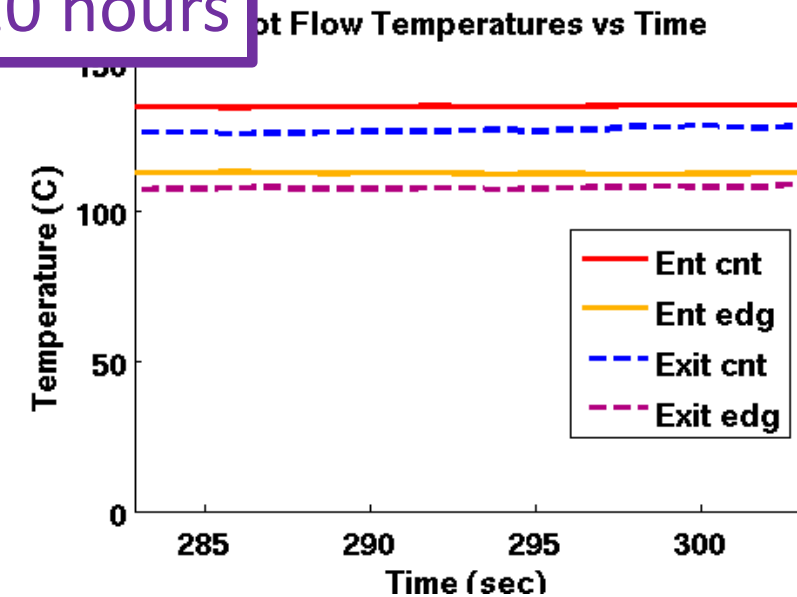
Heat Exchanger Verification



Test	Model	Experimental	Percent Difference
Test 1	1.9+/- 0.2 °C	3.83 +/-0.2°C	+102%
Test 2	2.0 +/-0.2 °C	1.34 +/-0.2°C	-32%
Test 3	1.8+/- 0.2 °C	1.77 +/-0.2°C	-14%



Need >10 more tests to prove model
 Estimated Hours Remaining: 10 hours



ECU & ESB Stock Engine Test Overview

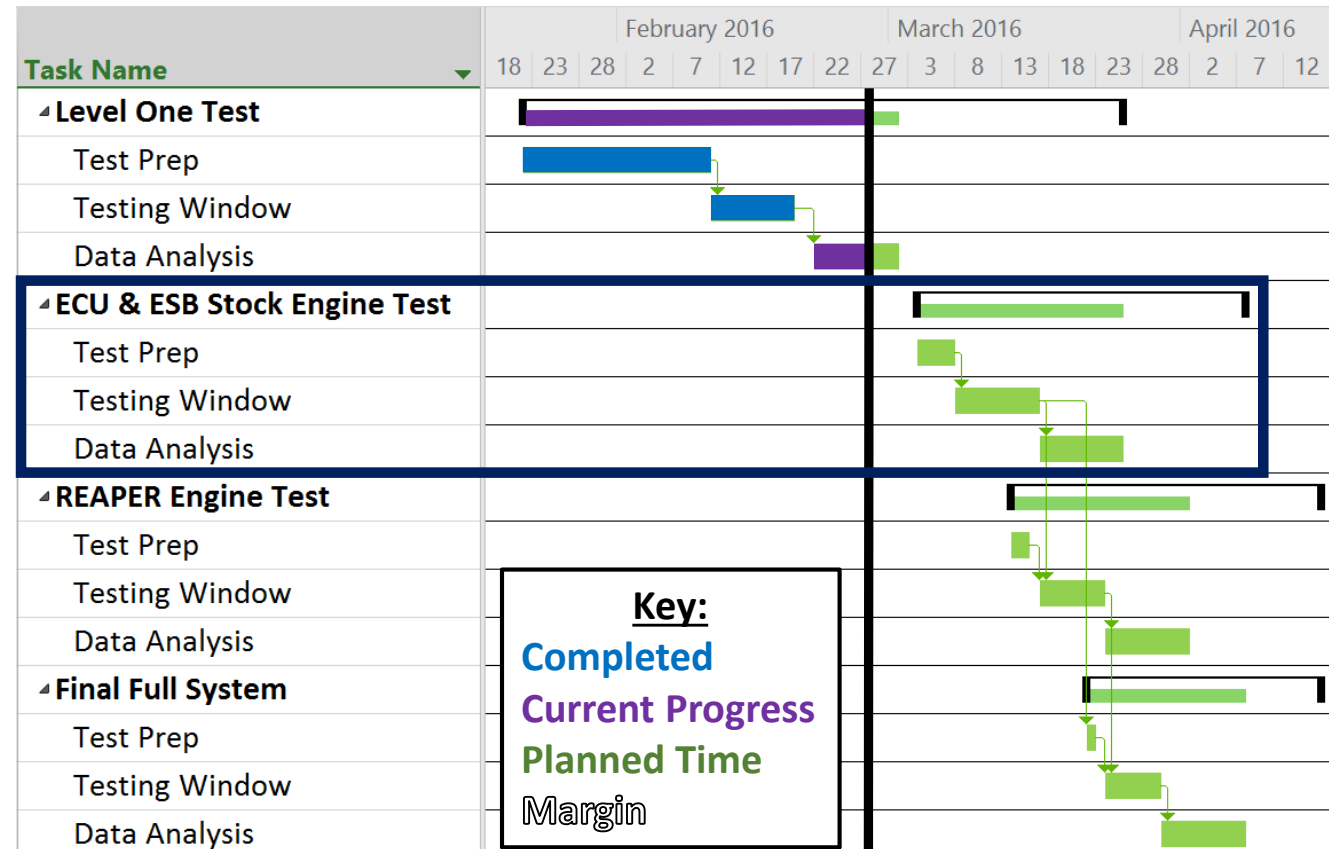
Test Dates: 3/8-3/16

Purpose

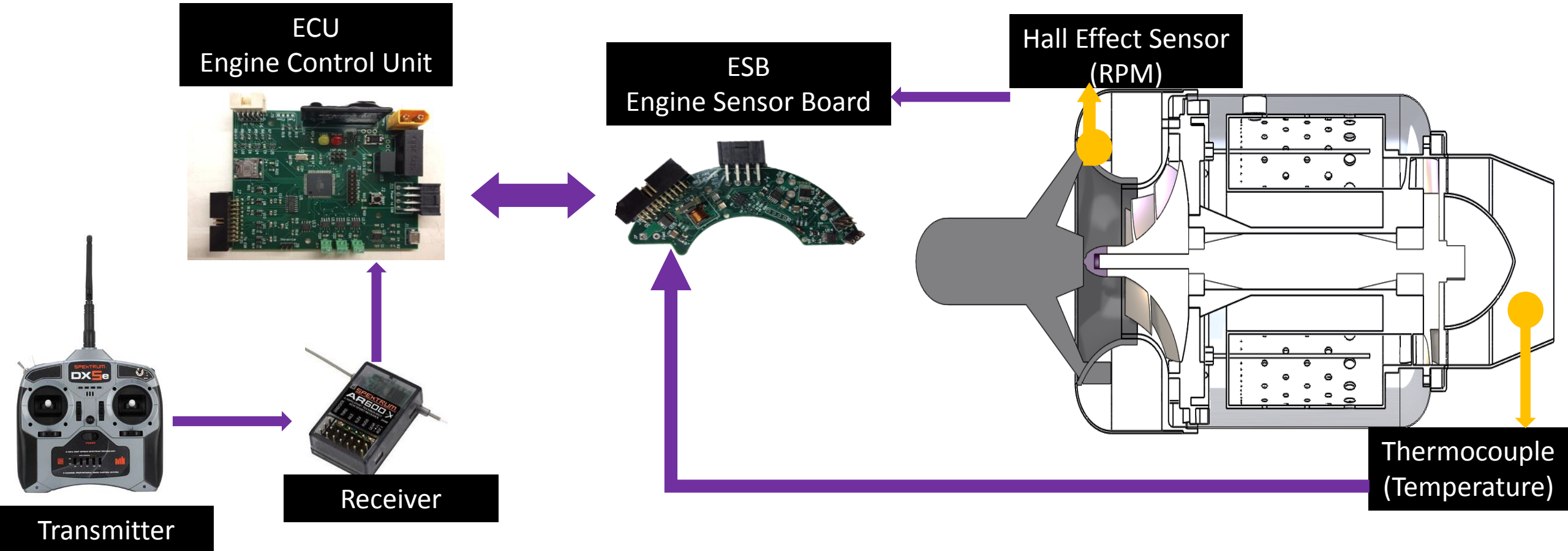
- Collect stock thrust and fuel consumption rate data
- Ensure custom ECU and ESB operates engine safety
- Partial Level 2 Success

Main Test Equipment

- JetCat stock P-90RXi engine
- Custom Engine Control Unit and Electronic Sensor Board



Estimated Hours Remaining: 25 hours
 Workforce: 4
 Scheduled Time after TRR: 35 hours



Sensor List	Error	Expected Range	Sample Rate
Thermocouple	± 2.5 °C	0-900 °C	31 Hz
Hall Effect	$\pm 0.05\%$	0- 130,000 rpm	31 Hz

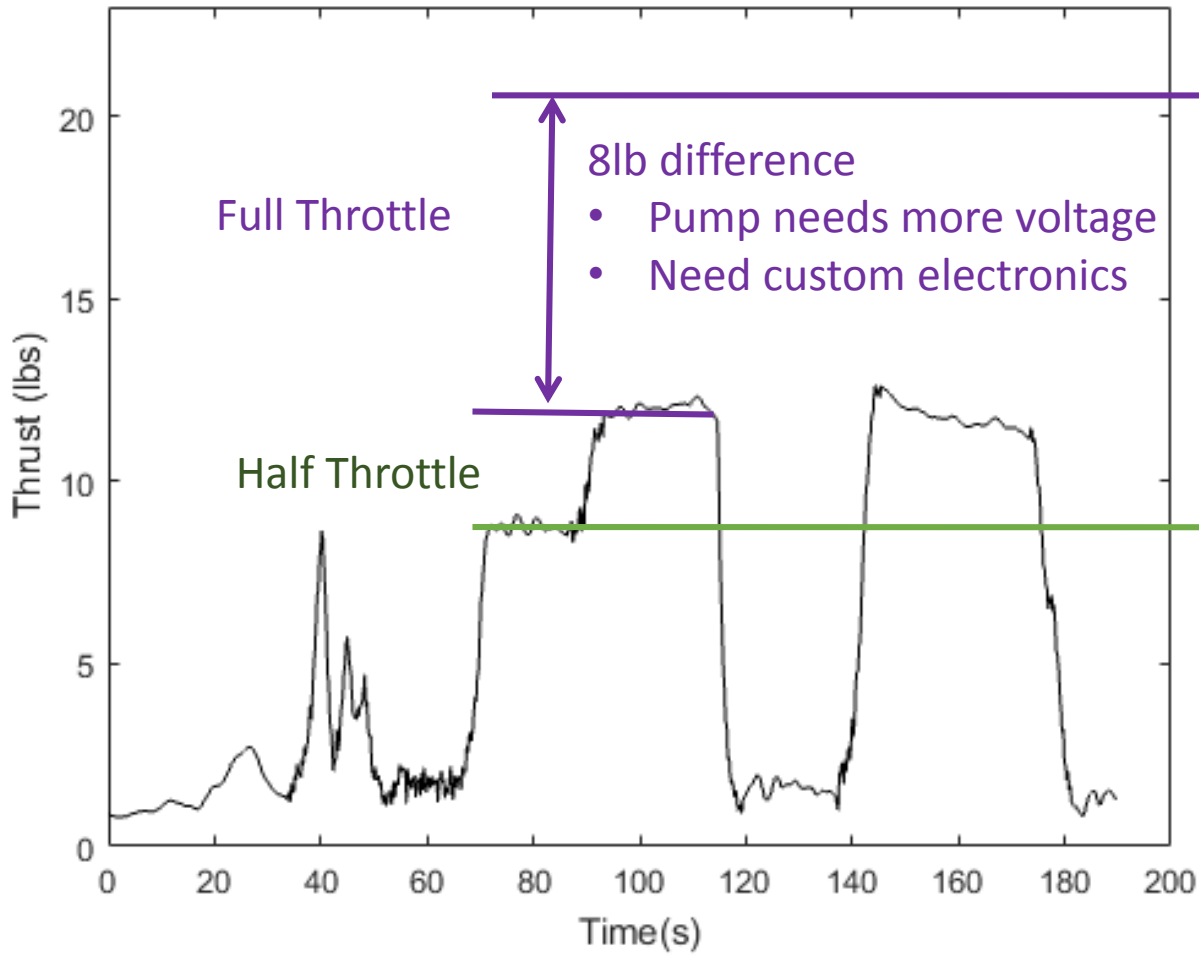
Preparation For Stock Engine Test

- Stock engine tests:
 - Show preparedness for ECU/ESB Engine Test
 - Show sensors used in TSFC are ready
- Progress
 - 2/26 full characterization of engine with fuel flow sensor and load cell
 - Efficient setup and trouble shooting issues
- Concerns
 - Weather- tests cut short due to wind and cold temperatures



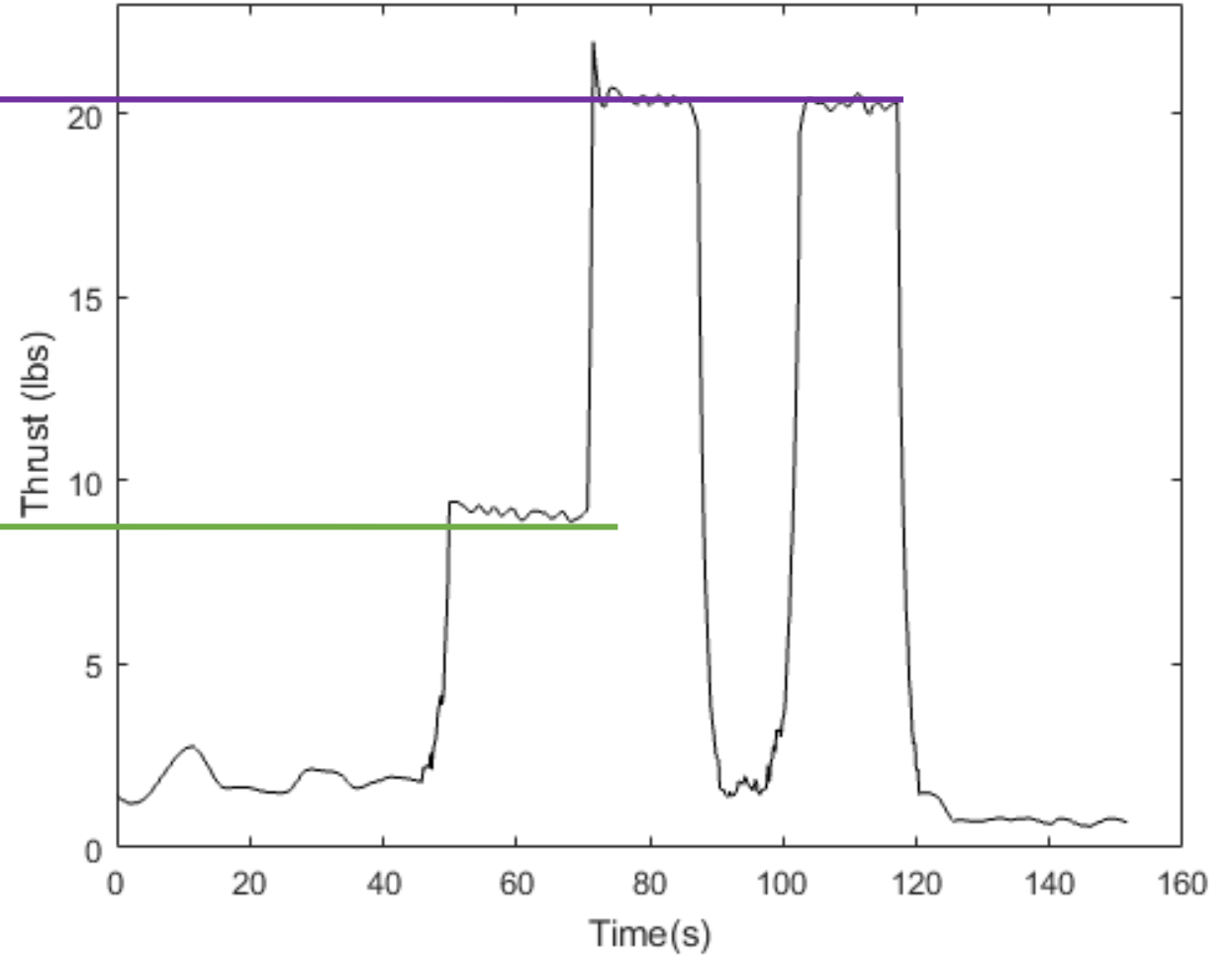
Stock Engine Thrust Data

With Fuel Flow Sensor



Max RPM = 109,500

Without Fuel Flow



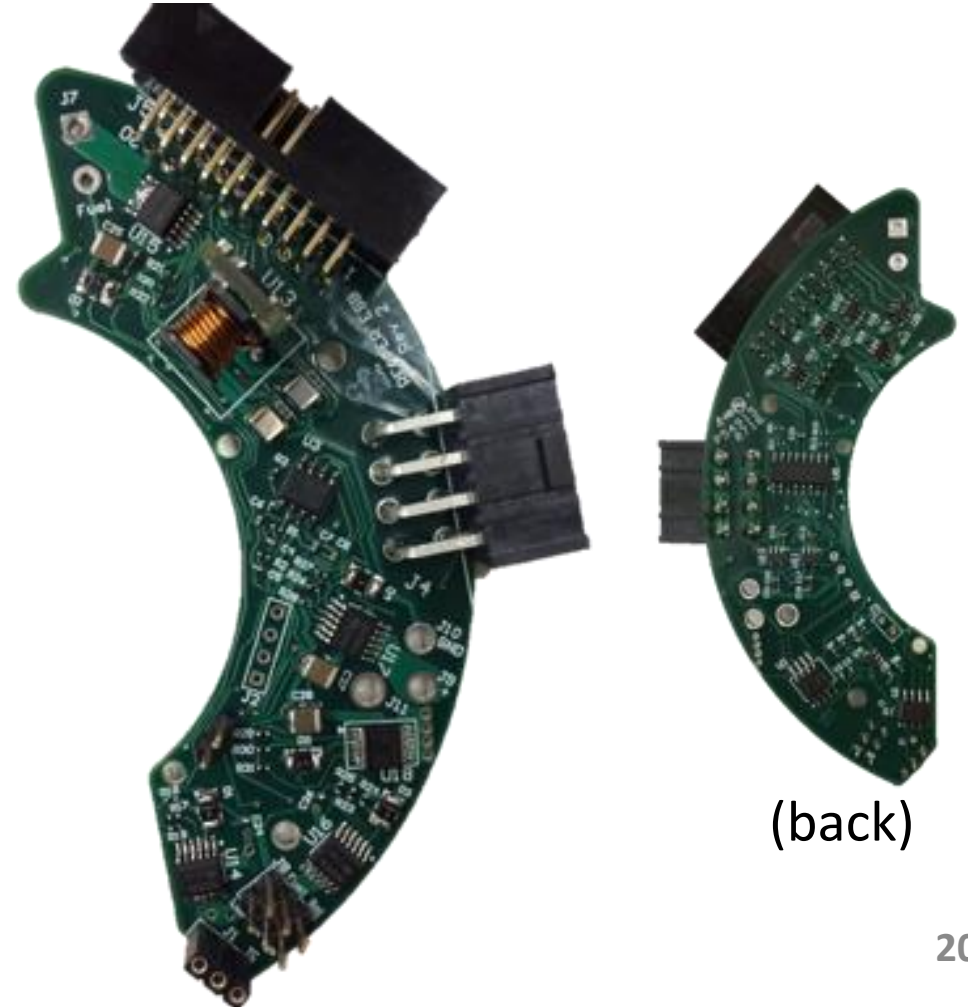
Max RPM = 130,000

- Two Custom Printed Circuit Boards:
 - Engine Control Unit (ECU)

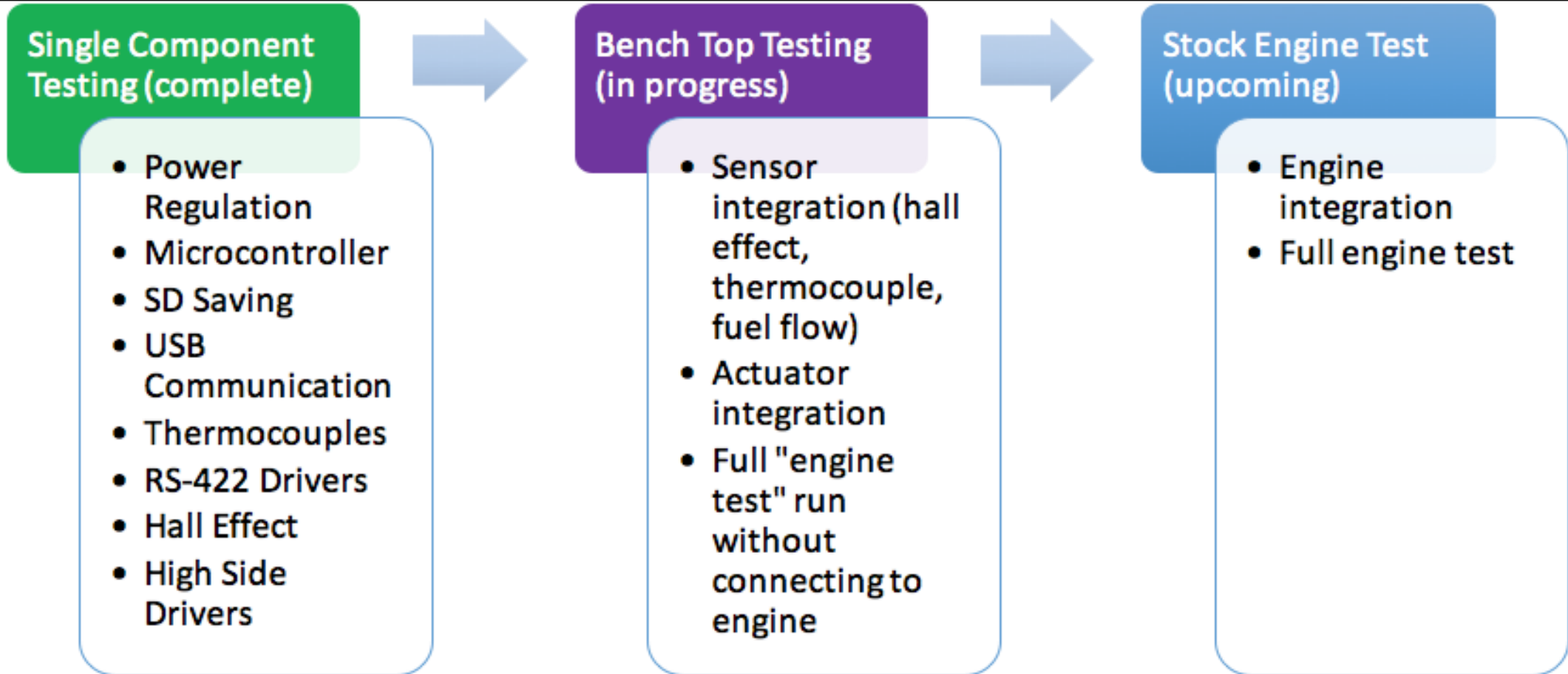


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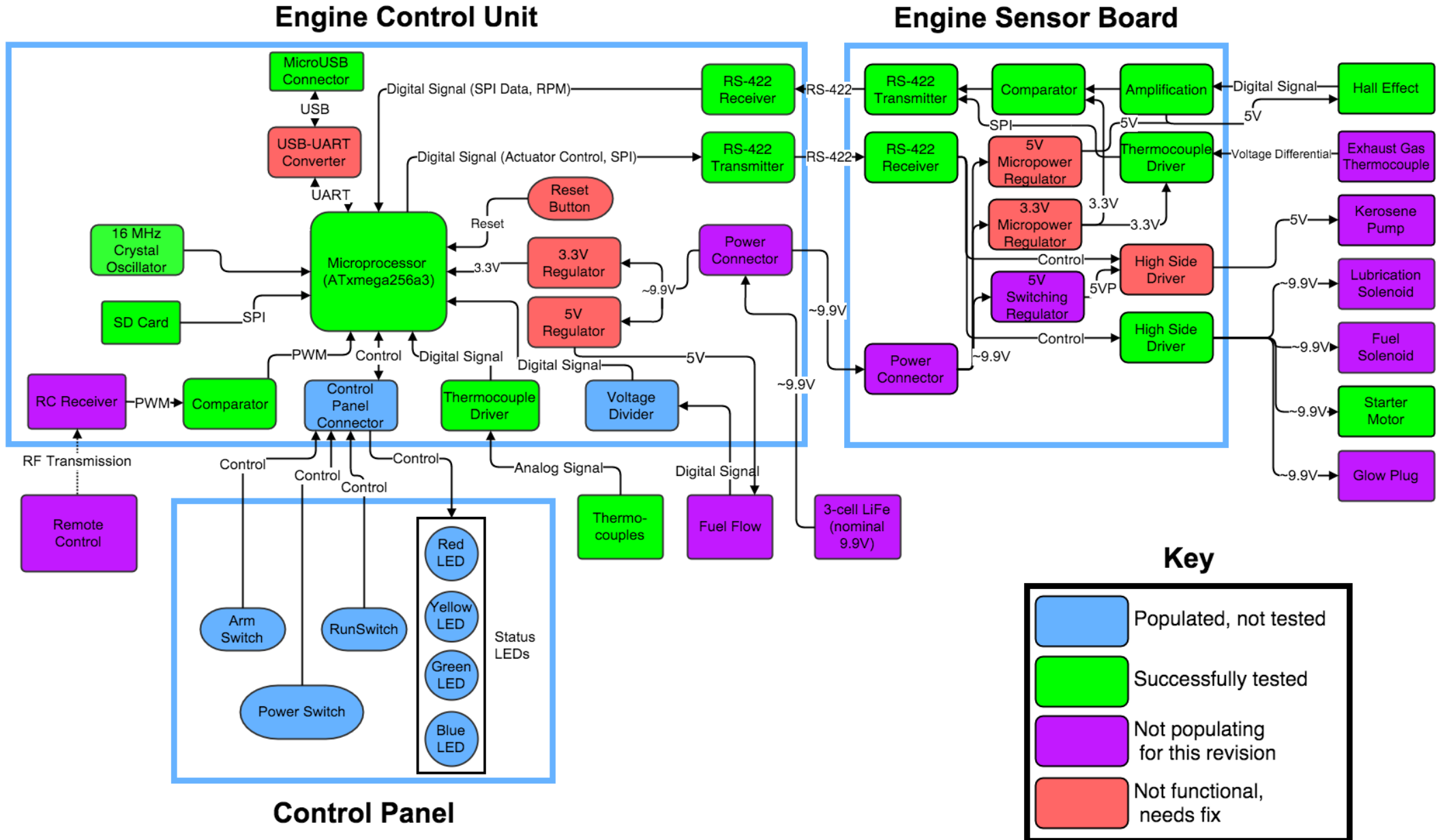
- Engine Sensor Board (ESB)

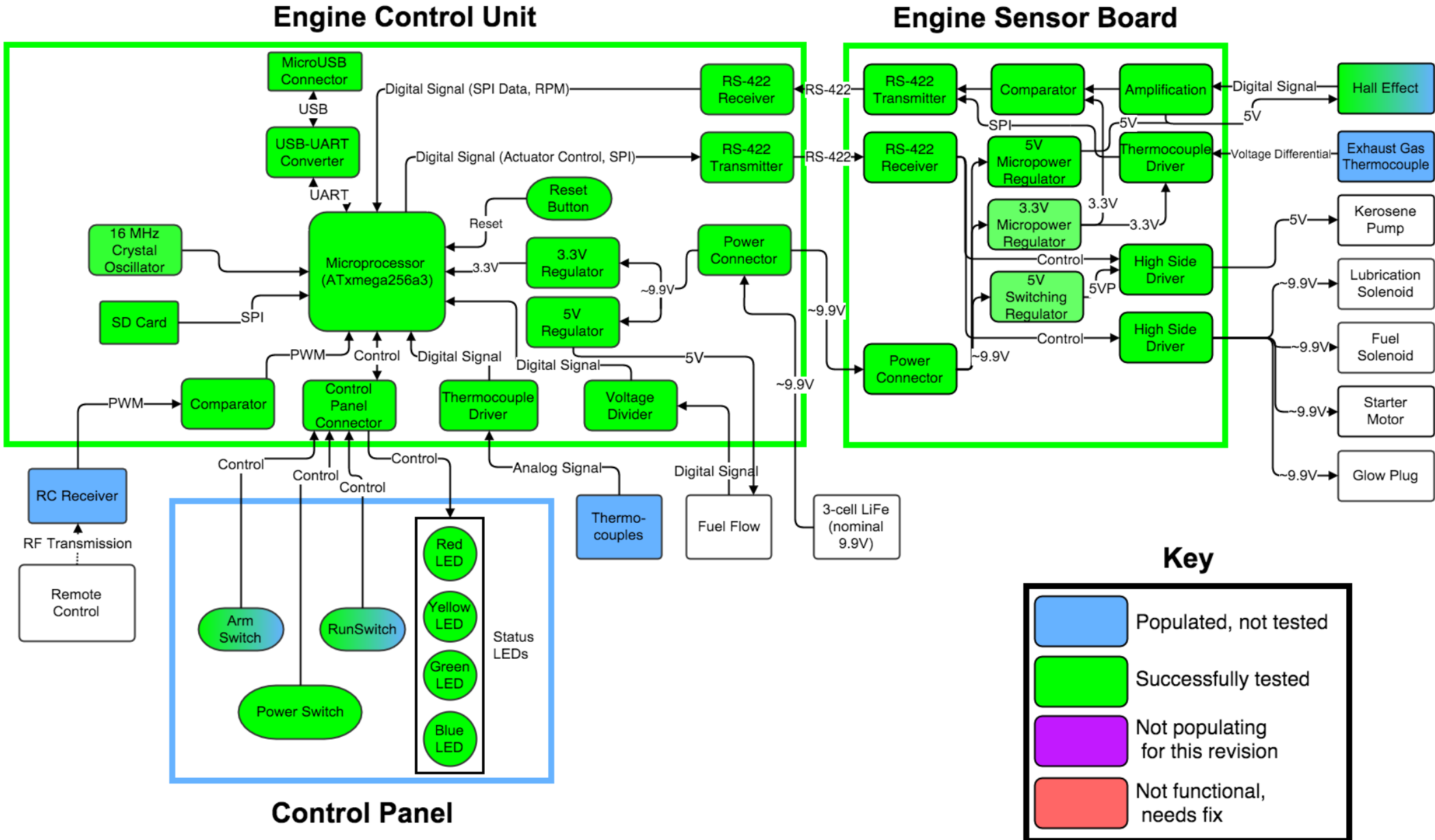


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Estimated Hours Remaining: 15 hours
Workforce: 2
Scheduled Time after TRR: 20 hours





Engine Electronics: Software Progress

High Level

Final Implementation

KEY

Validated

Written

Incomplete

Hardware Interface Layer

SD Card

Hall Effect

Thermocouples

Fuel Flow

Glow Plug

Starter motor

Low Level Interface

SPI

Oscillator

Interrupts

USART

PWM

Estimated Hours Remaining: 12 hours

Workforce: 1

Scheduled Time after TRR: 15 hours

Integrated Engine Test Overview

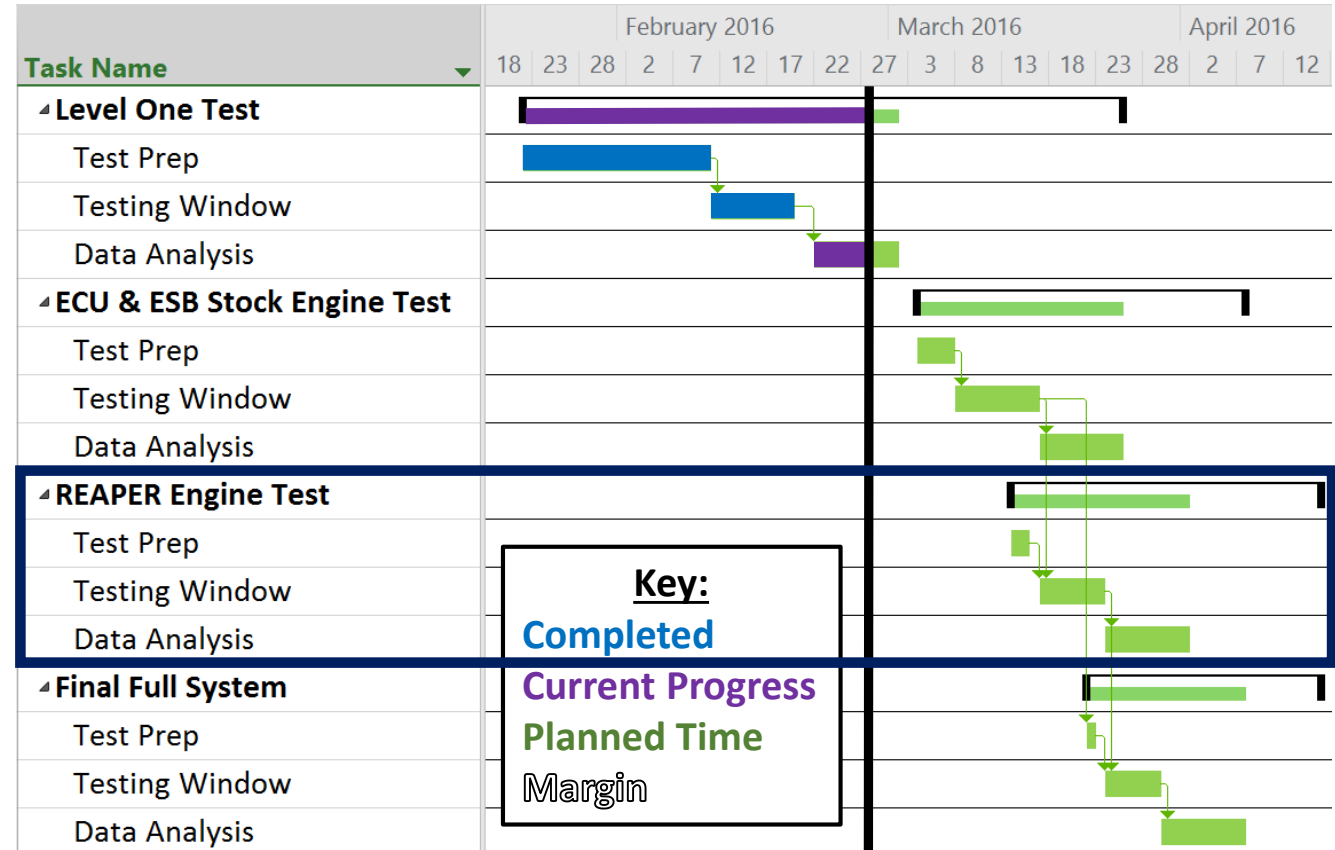
Test Dates: 3/17-3/23

Purpose

- Ensure REAPER engine starts
- Ensure custom ECU and ESB operates engine safety
- Reach Level 2 Success

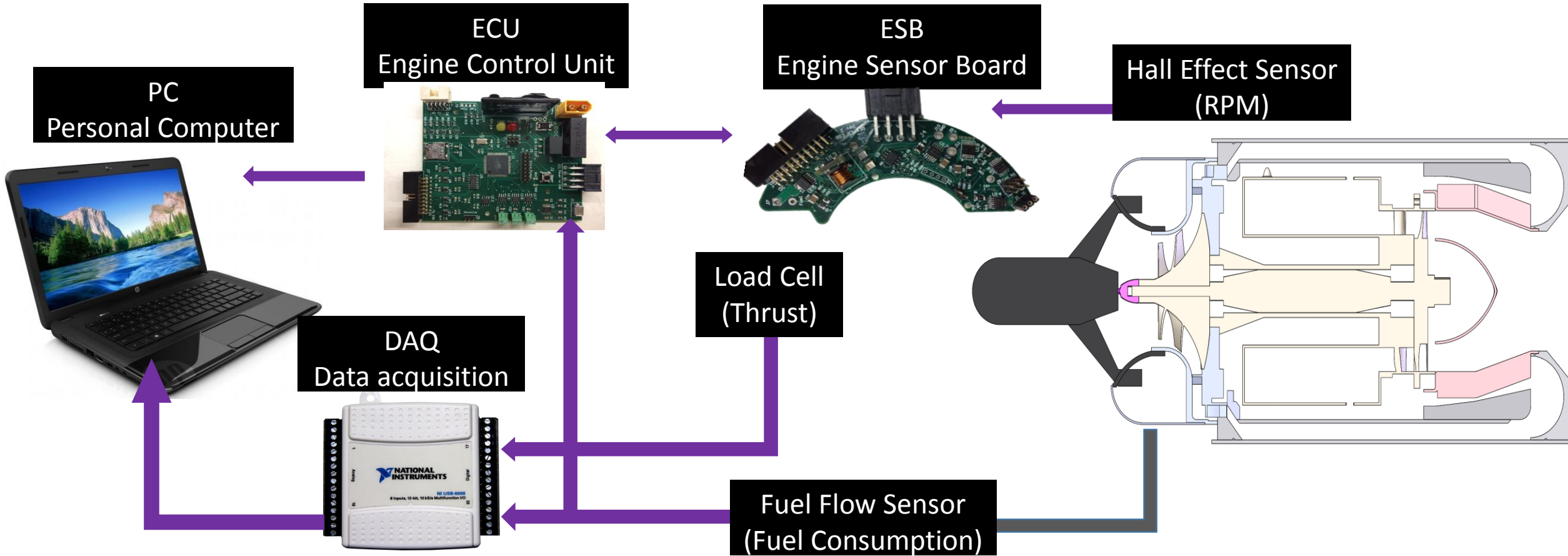
Main Test Equipment

- Modified P-90RXi engine
- Custom Engine Control Unit and Electronic Sensor Board



Estimated Hours Remaining: 25 hours
 Workforce: 4
 Scheduled Time after TRR: 35 hours

Integrated Engine Test Validation



Sensor List	Error	Expected Range	Sample Rate
Fuel Flow Sensor	±1%	0-5 mL/s	31 Hz
25lb Load Cell	±0.2%	0- 22 lbs	1 Hz
Hall Effect	±0.05%	0- 130,000 rpm	31 Hz

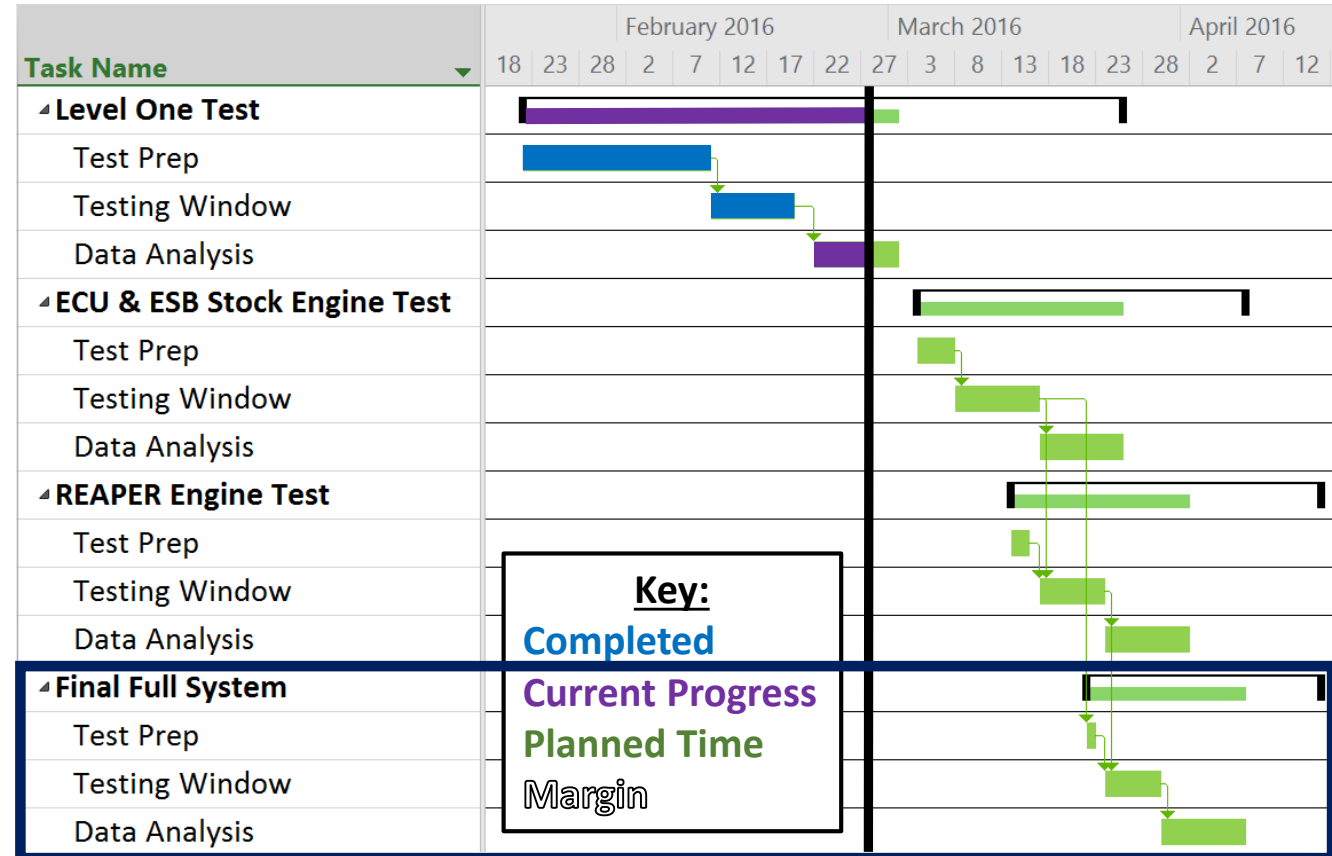
Test Dates: 3/24-3/29

Purpose

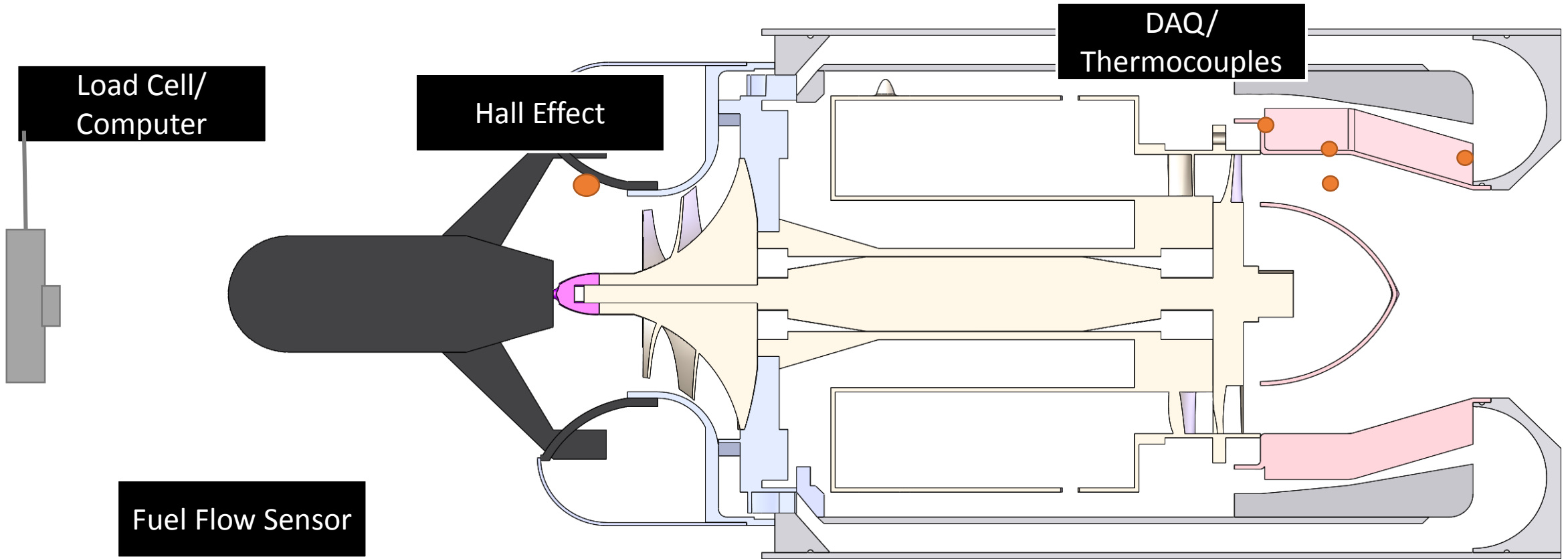
- Ensure REAPER engine starts
- Collect TSFC data
- Reach Level 3 Success

Main Test Equipment

- Modified P-90RXi engine
- Custom Engine Control Unit and Electronic Sensor Board
- Fuel Flow Sensor
- Load Cell



Estimated Hours Remaining: 25 hours
 Workforce: 4
 Scheduled Time after TRR: 35 hours



Sensor List	Error	Expected Range	Sample Rate
Fuel Flow Sensor	±1%	0-5 mL/s	31 Hz
25lb Load Cell	±0.2%	0-22 lbs	1 Hz
Hall Effect	±0.05%	0-130,000 rpm	31 Hz
Thermocouples	±2.5 °C	0-900 °C	31 Hz

Conservation Laws

Mass: $\rho_1 A_1 V_1 = \rho_2 A_2 V_2$

Momentum: $p_1 A_1 - p_2 A_2 - \left(\frac{\dot{W}_{shaft}}{V_m} + F_{fric} \right) = \dot{m}_2 V_2 - \dot{m}_1 V_1$

Energy: $\left(\frac{\dot{Q} - \dot{W}_{shaft}}{\dot{m}} \right) - \frac{V_m^2}{2} K_L = C_{p,2} T_2 - C_{p,1} T_1 + \frac{1}{2} (V_2^2 - V_1^2)$

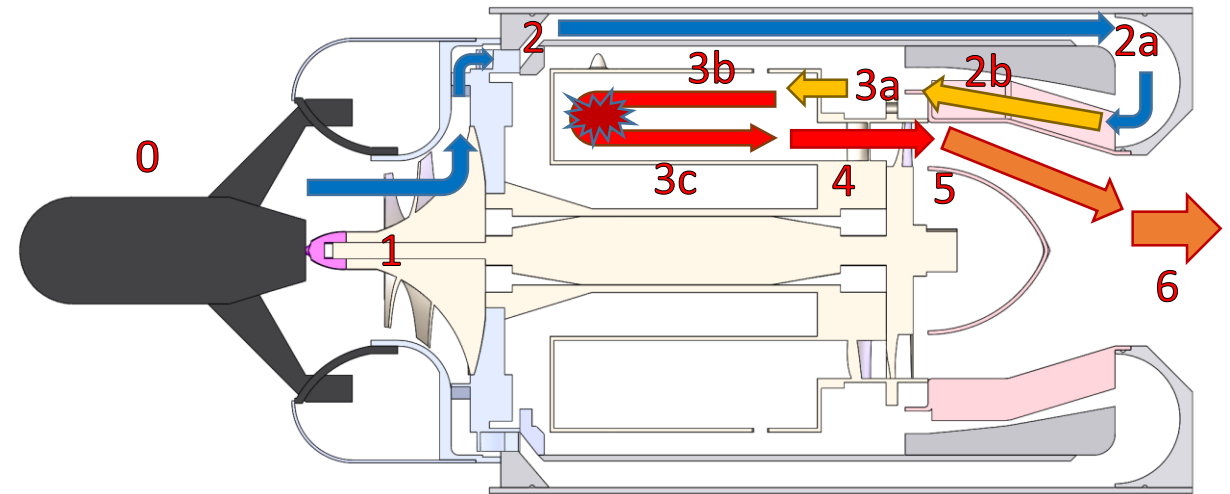
Constitutive: $p = \rho R T$

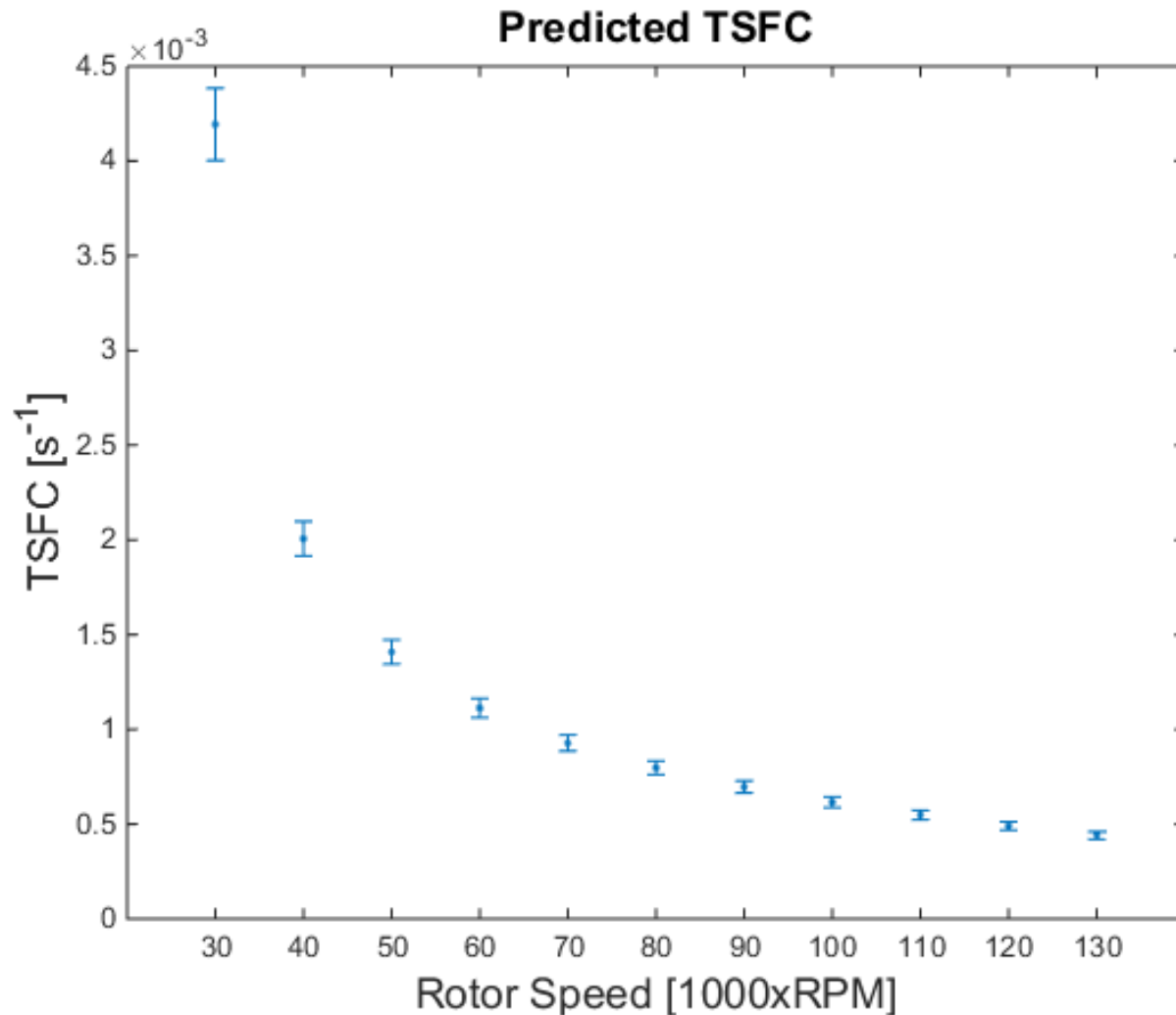
Loss Sources

- Friction (Colebrook-White)
- Sudden expansion/contraction
- Gradual Expansion
- Turning the flow

Assumptions/Correlations

- Ideal, thermally perfect gas
- 1-D flow; fully developed
- Engine component efficiencies from MEDUSA/COMET tests
- Colebrook-White friction correlation
- Gnielinski heat transfer correlation





Monte Carlo Simulation

Sensitivity Variables

- Fuel consumption increases linearly
- Thrust increase exponentially
- Engine RPM
- Error concentrated on fuel consumption prediction
- Compressor Efficiency
- Turbine Efficiency
- Combustor Efficiency
- Heat Transfer Coefficients (x2)
- Friction Coefficients (x6)
- Expansion/Contraction Coefficients (x3)
- Flow Diversion Coefficients (x4)
- Environmental conditions

Assume Normal Distribution

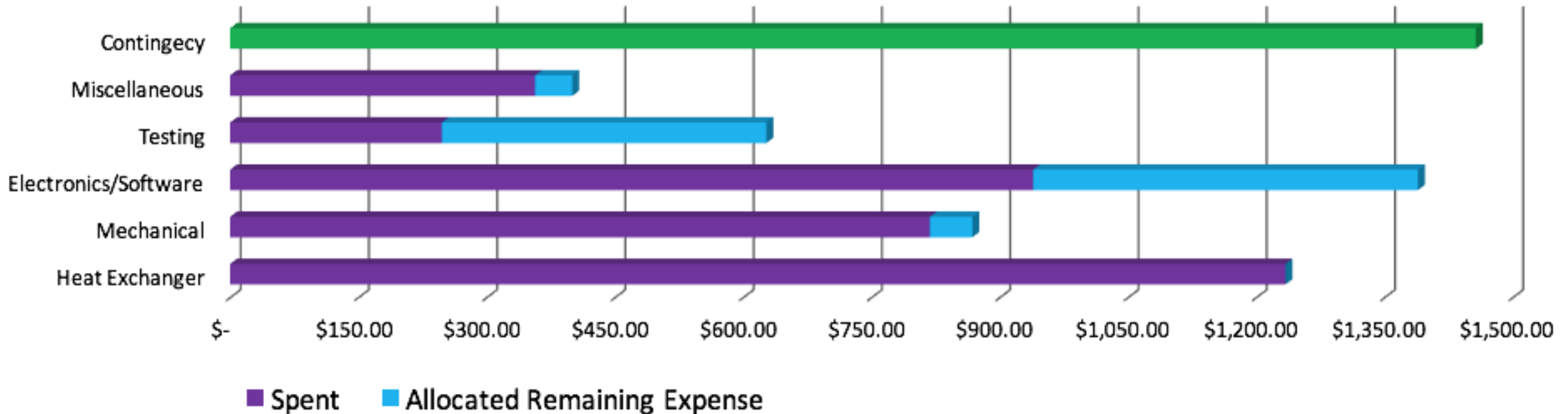
$$x = \bar{x} + N(\bar{x}, \sigma)$$



Budget



Budget



Total Budget **\$5,975**
 Total Spent **\$3,595**
 Remaining Expenses **\$880**
 Contingency **\$1,500**

Remaining Expected Expense	Total Cost
Fuel Flow Inserts	\$330
Misc. Integration Hardware	\$50
Misc. Electronics Components	\$50
Spare Parts for Final Testing	\$450
Total	\$880

Questions?



- [1] http://pillars.che.pitt.edu/student/slide.cgi?course_id=10&slide_id=13.0
- [2] Kays, W.M. and London, A.L., *Compact Heat Exchanger Design*, R.R. Donnelley & Sons, 1984.
- [3] Titanium Ti-6Al-4V (Grade 5), Annealed," American Society for Materials. MatWeb Database. Web. Accessed 11 Oct. 2015. <<http://asm.matweb.com/search/SpecificMaterial.asp?bassnum=MTP641>>.
- [4] Contreras-Garcia, Julia, Emily Ehrle, Eric James, Jonathan Lumpkin, Matthew McClain, Megan O'Sullivan, BenWoeste, and Kevin Wong, "COMET Project Final Report", 2014.
- [5] Ma, Huikang, Daniel Frazier, Crawford Leeds, Corey Wilson, Carlos Torres, Alexander Truskowski, Christopher Jirucha, Abram Jorgenson, and Nathan Genrich, "MEDUSA Project Final Report", 2015. 09 Sept. 2015.
- [6] RMI Titanium Company. "Titanium Alloy Guid." (n.d.): n. pag. Jan. 2000. Web. 28 Nov. 2015. <<http://www.rtiintl.com/Titanium/RTI-Titanium-Alloy-Guide.pdf>>.
- [7] Nickel Development Insitute. "HIGH-TEMPERATURE CHARACTERISTICS OF STAINLESS STEELS." (n.d.): n. pag. *Nickel Insitute*. American Iron and Steel Institute. Web. 28 Nov. 2015. <http://www.nickelinstitute.org/~Media/Files/TechnicalLiterature/High_TemperatureCharacteristicsOfStainlessSteel_9004_.pdf>.
- [8] Johnson, Carl R., and John D. Grimsley. *Short-time Stress Rupture of Prestressed Titanium Alloys under Rapid Heating Conditions*. Washington, D.C.: National Aeronautics and Space Administration, 1970. *National Technical Reports Server*. National Aeronautics and Space Administration. Web. 28 Nov. 2015. <<http://ntrs.nasa.gov/archive/nasa/casi.ntrs.nasa.gov/19710002194.pdf>>.
- [9] Kadoya, K., M. Matsunaga, and A. Nagashima. "Viscosity and Thermal Conductivity of Dry Air in the Gaseous Phase." *Journal of Physical Chemistry* 14.4 (1985): 947-56. *National Technical Reference Database*. Web. 30 Nov. 2015. <<http://www.nist.gov/data/PDFfiles/jpcrd283.pdf>>
- [10] Lemmon, Eric W., Richard T. Jacobsen, Steven G. Penocello, and Daniel G. Friend. "Thermodynamic Properties of Air and Mixtures of Nitrogen, Argon, and Oxygen From 60 to 2000 K at Pressure to 2000 MPa." *Journal of Physical Chemistry* 29.3 (2000): 331-56. *National Technical Reference Database*. Web. 30 Nov. 2015. <<http://www.nist.gov/data/PDFfiles/jpcrd581.pdf>>.
- [11] "Stainless Round 304/304L 5 inch." *OnlineMetals.com*. Web. Accessed 29 Nov. 2015. <https://www.onlinemetals.com/merchant.cfm?pid=127&step=4&showunits=inches&id=6&top_cat=1>
- [12] "Stainless Round 304/304L 4.25 inch." *OnlineMetals.com*. Web. Accessed 29 Nov. 2015. <https://www.onlinemetals.com/merchant.cfm?pid=124&step=4&showunits=inches&id=6&top_cat=1#>
- [13] "Stainless 2B Sheet 304 Annealed." *OnlineMetals.com*. Web. Accessed 29 Nov. 2015. <http://www.onlinemetals.com/merchant.cfm?pid=6828&step=4&showunits=inches&id=233&top_cat=1>
- [14] "Stainless Redtangle 304/304L." *OnlineMetals.com*. Web. Accessed 29 Nov. 2015. <https://www.onlinemetals.com/merchant.cfm?pid=4420&step=4&showunits=inches&id=25&top_cat=1>

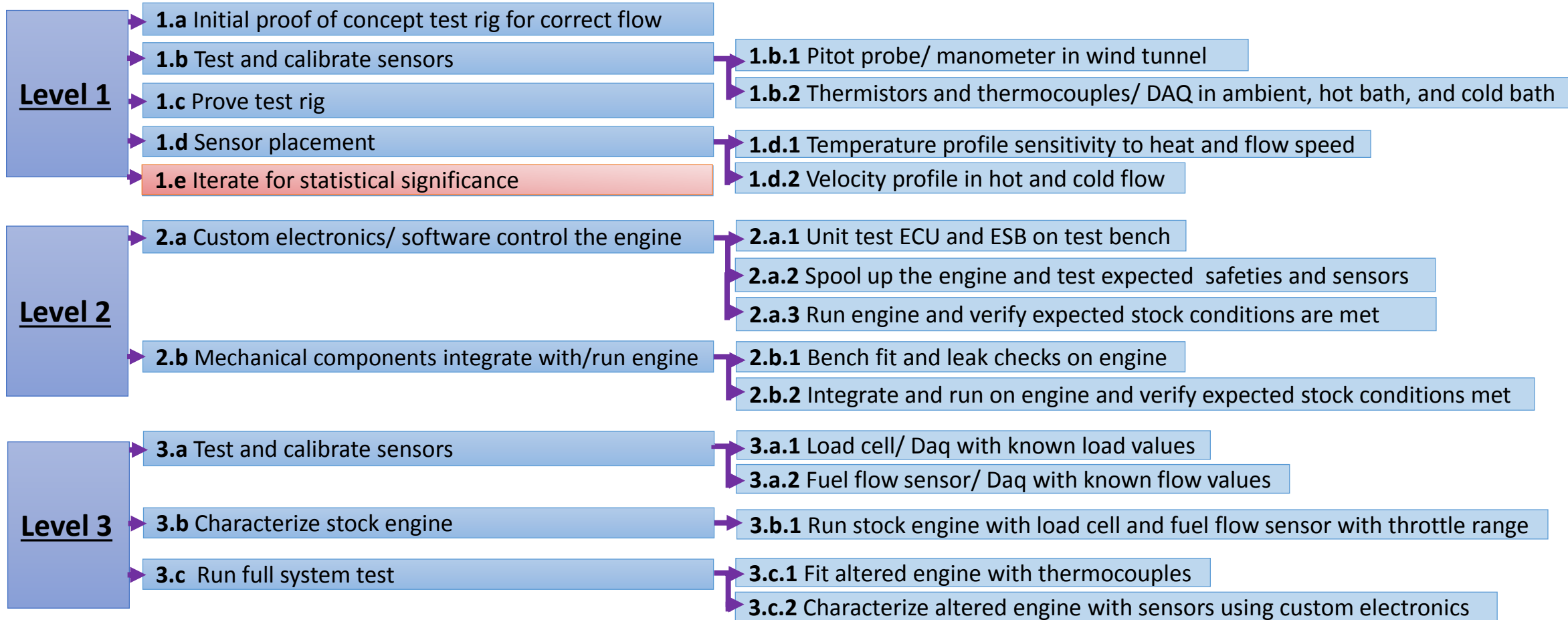


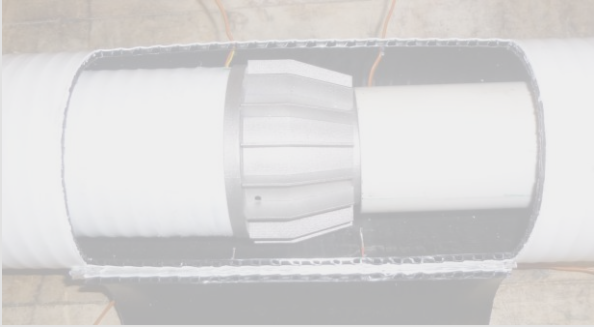
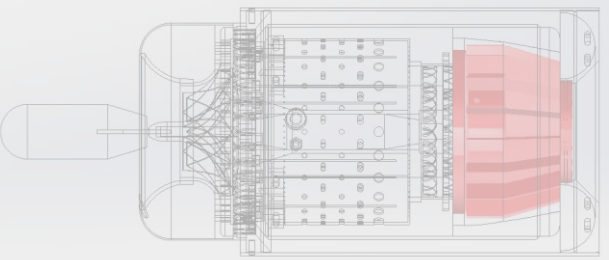
Backup Slides



Testing Overview

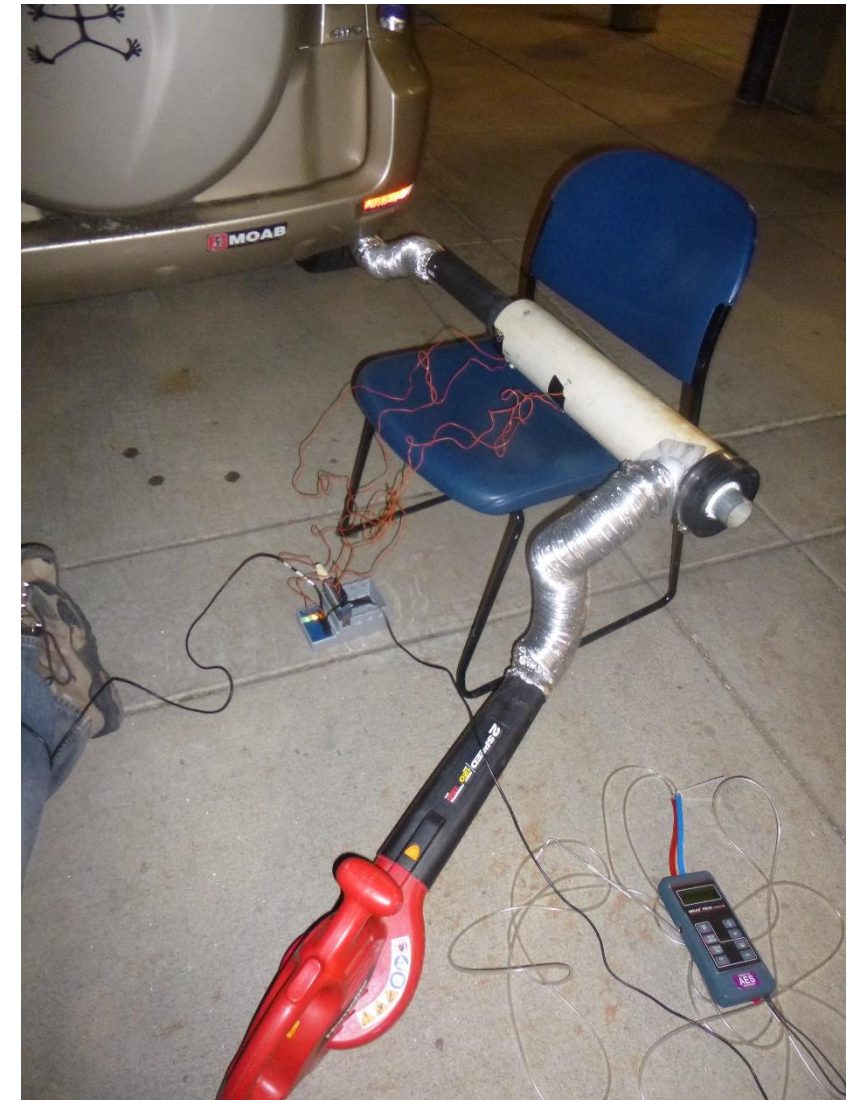
Backup Slides



Test	Purpose	Required Setup	Status
	<ul style="list-style-type: none"> • Level 1 success • Recuperator operates without critical failure • Verifies heat transfer from model 	<ul style="list-style-type: none"> • Concentric pipe test rig with recuperator integrated • Use heat guns, leaf blowers, thermocouples, and pitot probe from Level 0 testing • Use manometer and Daq/Labview for data collection 	<ul style="list-style-type: none"> • Built and withstands high heat tests • Matlab model complete • Analysis underway for Level 1 success
	<ul style="list-style-type: none"> • Level 3 success • Engine runs • Meet Throttle time • Effectiveness, Thrust Specific Fuel Consumption (TSFC), and thrust reduction match model 	<ul style="list-style-type: none"> • Manufacturing complete with recuperator integrated onto the engine • Use REAPER electronics • Use thermocouples and pitot probe from Level 0 testing • Use load cell, fuel flow sensors, and hall effect sensor 	<ul style="list-style-type: none"> • Manufacturing and electronics on track • Labview GUIs created and tested for thermocouples and load cell • Matlab and CFD models complete

Heat Exchanger Verification Backup Slides

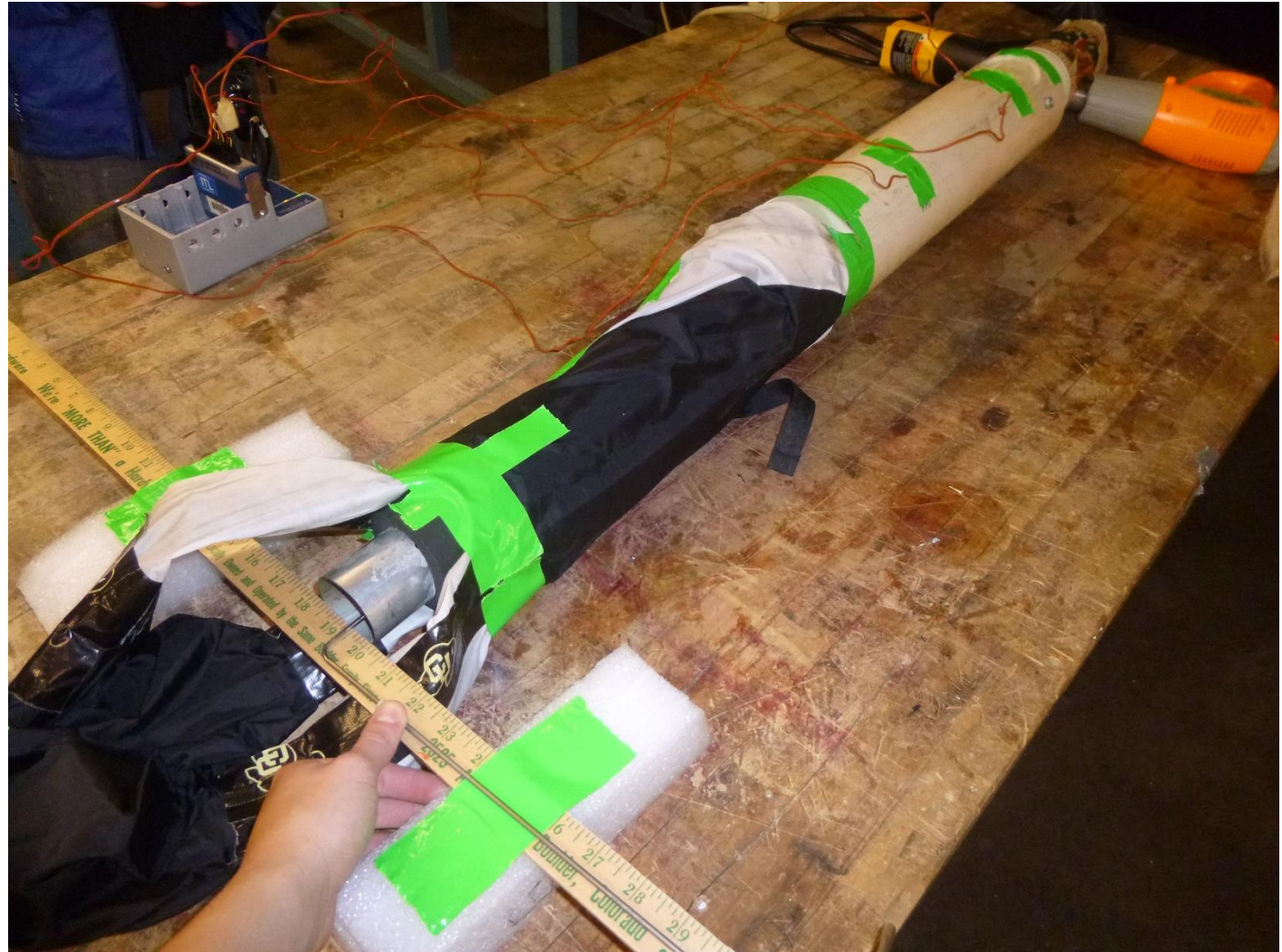
- Description
 - Concentric pipe flow
 - Hot flow from car exhaust
- Lessons Learned
 - Car exhaust is not hot/ fast enough for turbulent flow
 - Not a sustainable test, takes too long to reach steady state
 - Difficult to set up and tear down



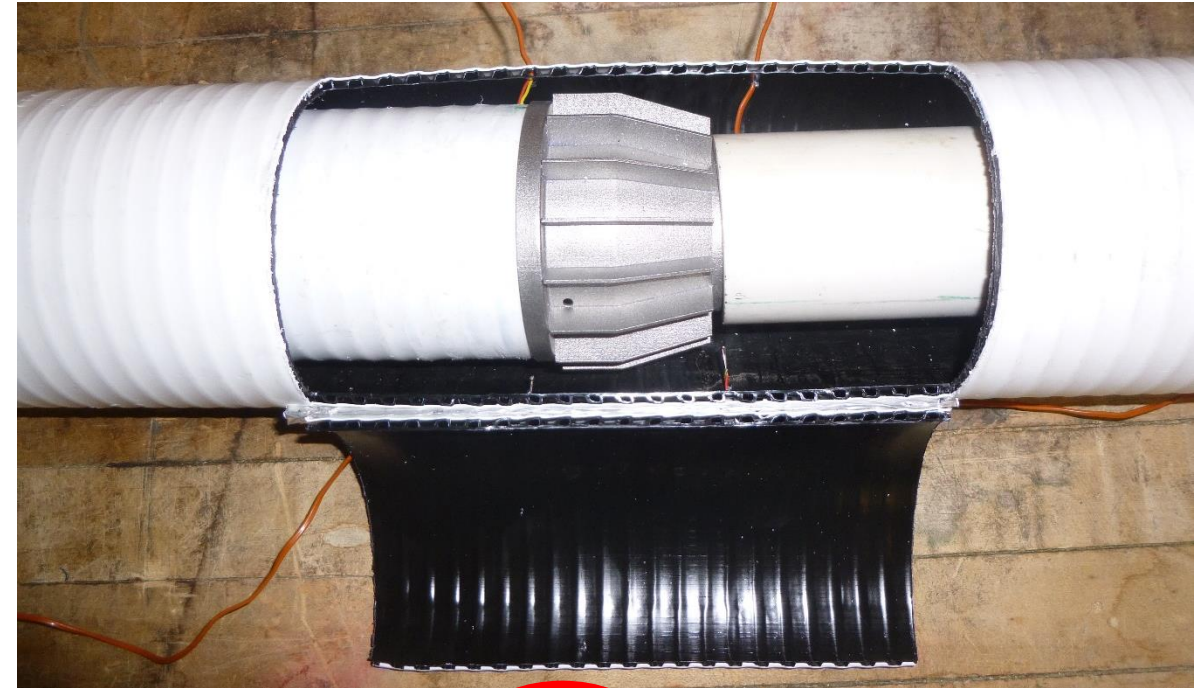
- Description:
 - Concentric pipe flow
 - Single heat gun for hot flow
- Lessons Learned:
 - Flow is uneven in the cold flow since the leaf blower is coming in from the side
 - Test section not long enough for fully developed turbulent flow
 - Results are difficult to quantify since the heat exchange is small. Need more heat



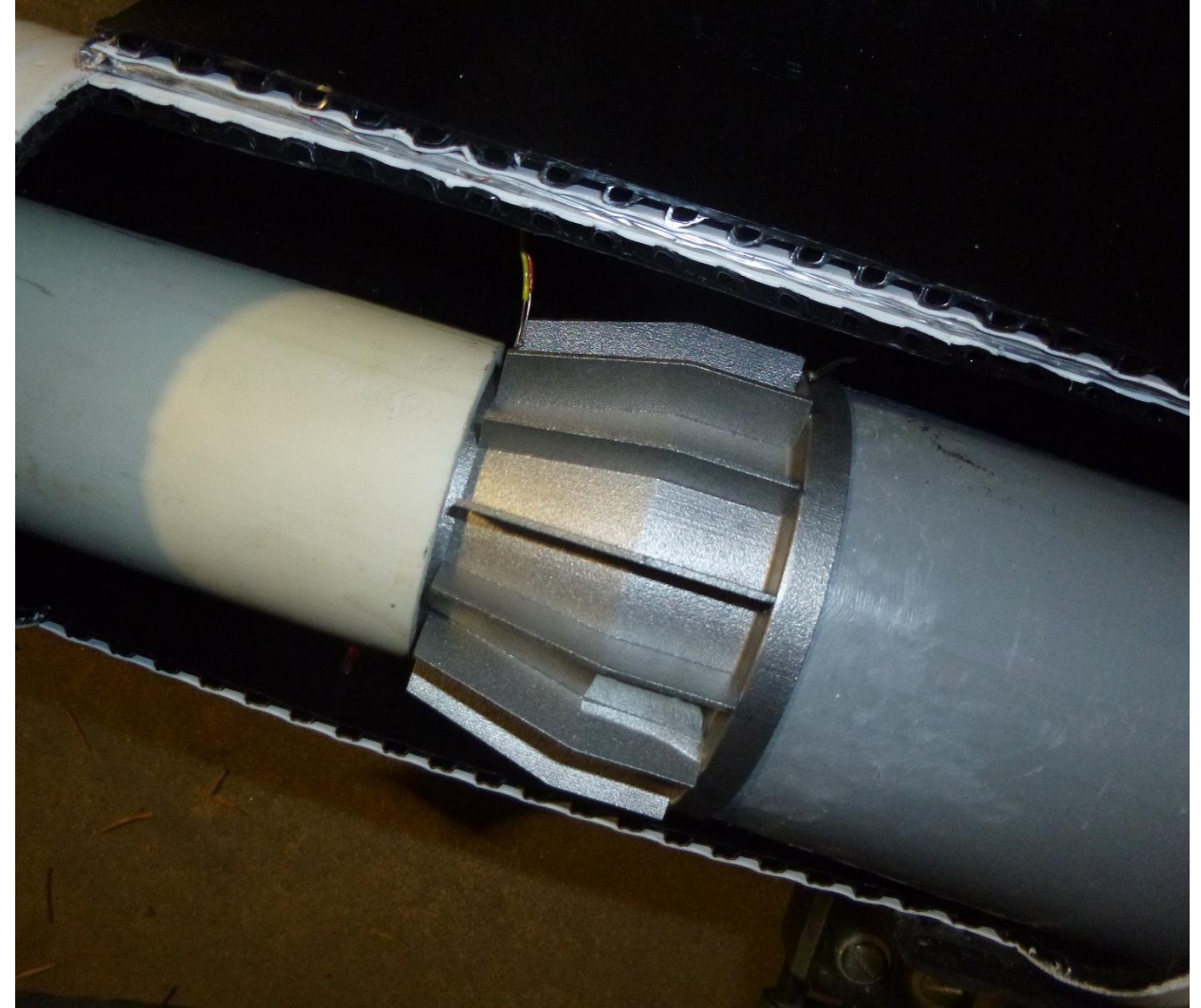
- Description:
 - Concentric pipe flow
 - Cold flow straightened via flow diverter/ shroud
 - Cold flow has longer to develop
 - Two heat guns and additional flow for greater temperature
- Lessons Learned:
 - Heat guns over heated, because hot air was flowing back through them
 - Thermocouples difficult to integrate in flow since the pipe is closed



- Description:
 - Concentric pipe flow with heat exchanger
 - Longer heat pipes for developed flow
 - Door cut for easier access to heat exchanger and thermocouples
 - Hot flow pulled down the pipe using a sucking fan, allowing for higher Reynolds number, hotter flow, and less risk for the heat guns
- Lessons Learned:
 - Extra heat from heat guns caused severe melting and weird results from unknown melting sections



- Description:
 - Concentric pipe flow with heat exchanger
 - New hot flow entrance pipe, with metal interior and pvc exterior to take the heat better, but still provide insulation to the flow
- Lessons Learned:
 - The new pipe held up, but the heat guns melted the Y-pipe so that it was unusable. Plastic is a bad idea



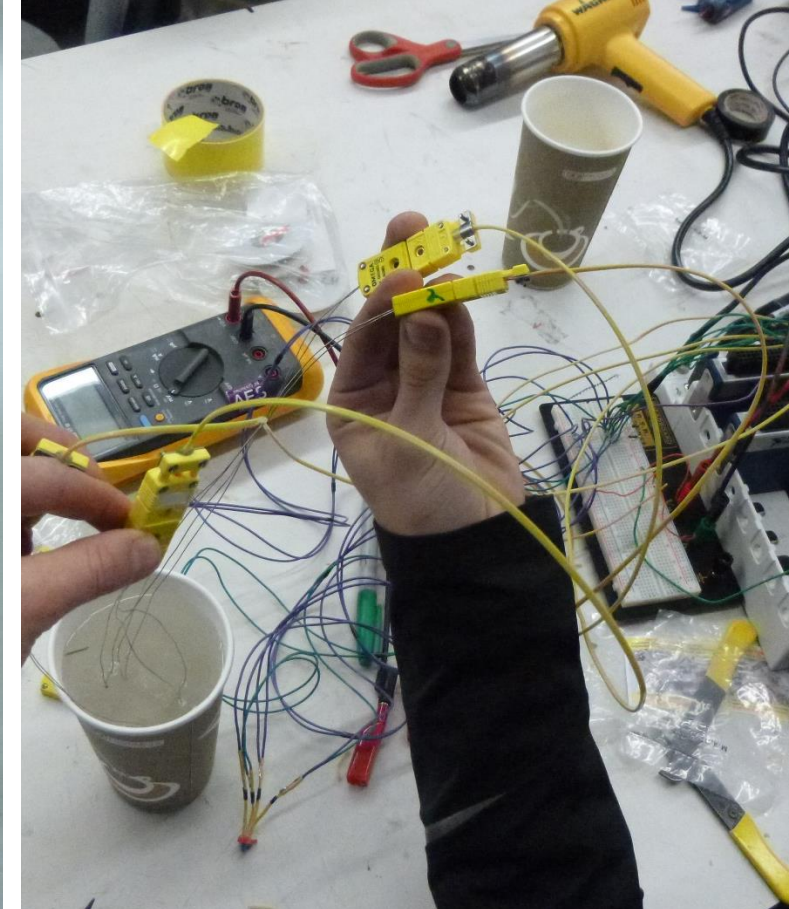
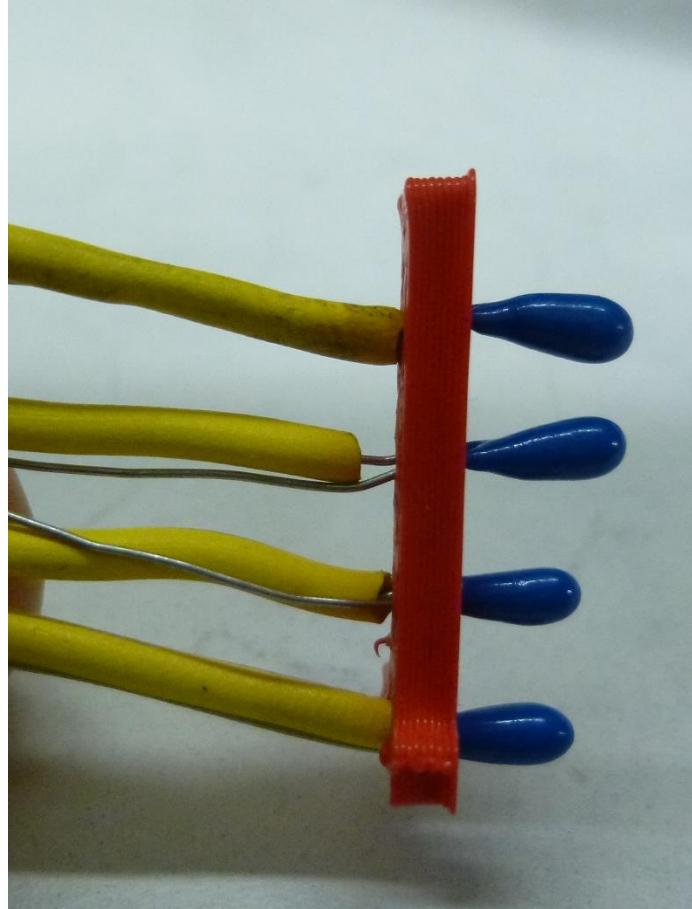
- Description:
 - Concentric pipe flow with heat exchanger
 - Replaced Y-pvc pipe with a Y-car exhaust pipe
- Lessons Learned:
 - A temperature profile is necessary for the cold flow because the thermocouples are very sensitive to placement



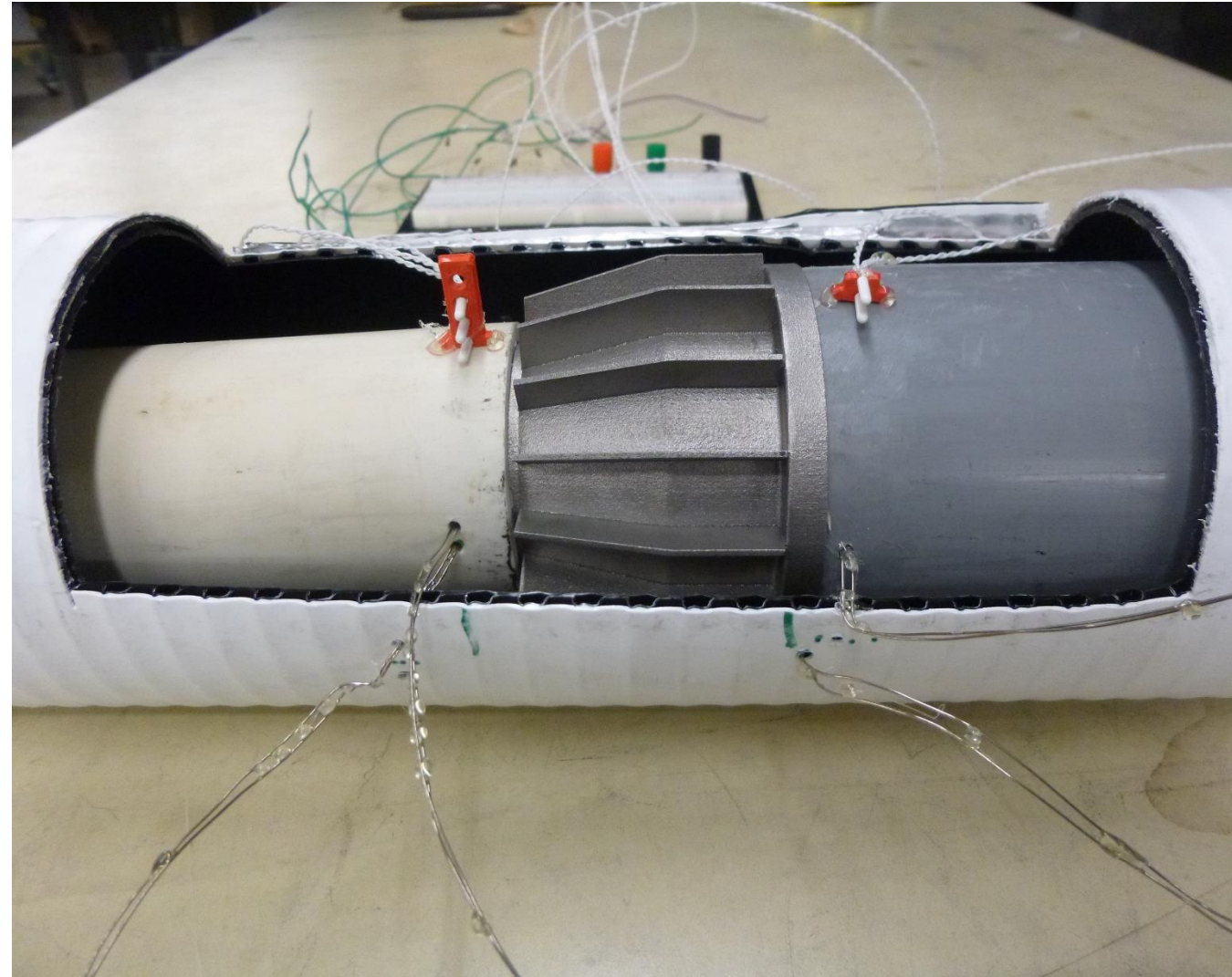
- Description:
 - Used level 0 setup to get a temperature profile in concentric pipe flow
 - Found experimental profile for different leaf blower and sucker speeds
- Lessons Learned:
 - Leaf blower low, sucker low
0.37°/mm (radial)
 - Leaf blower high, sucker low
0.74°/mm (radial)
 - A temperature profile is needed for conclusive results
 - Thermistors should be used instead of thermocouples, because they have less error



- Description:
 - Concentric pipe flow with heat exchanger
 - 3D printed profile insert for thermistors
 - Made in-house thermocouples with bare wire for easier integration and testing with the Daq
- Lessons Learned:
 - Bare wires are difficult to work with and created poor data when test was run since wires kept touching in flow



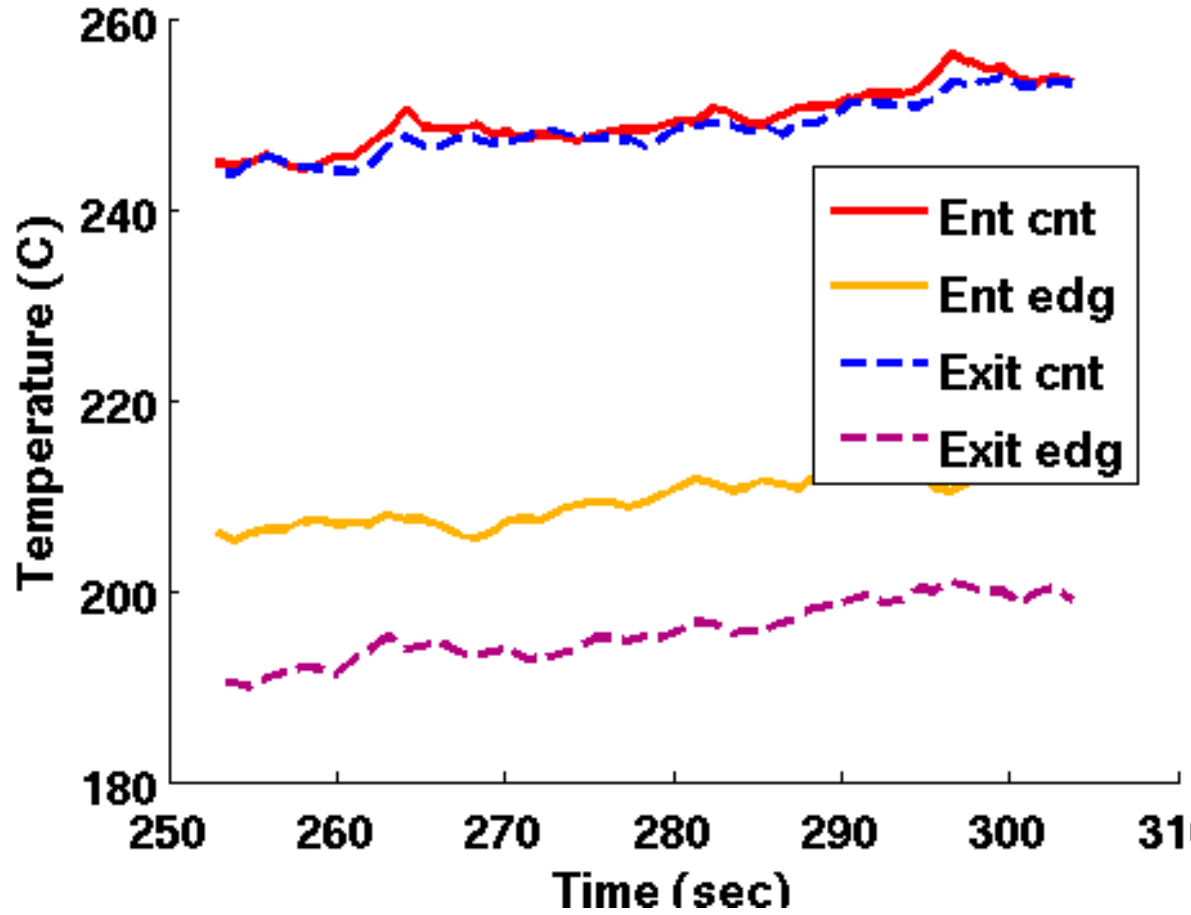
- Description:
 - Concentric pipe flow with heat exchanger
 - Using covered thermistors to prevent wires touching
 - Beaded in-house thermocouples with hot glue to prevent wires touching
- Lessons Learned:
 - Results inconclusive due to: spiraling flow (unexpected stream lines), pressure drops/ unintentional mixing due to leaks, wrongly assumed resistors all have the same resistance
 - Important to take bulk temperatures and velocities in Matlab analysis
 - Need to wait longer between tests to prevent melting



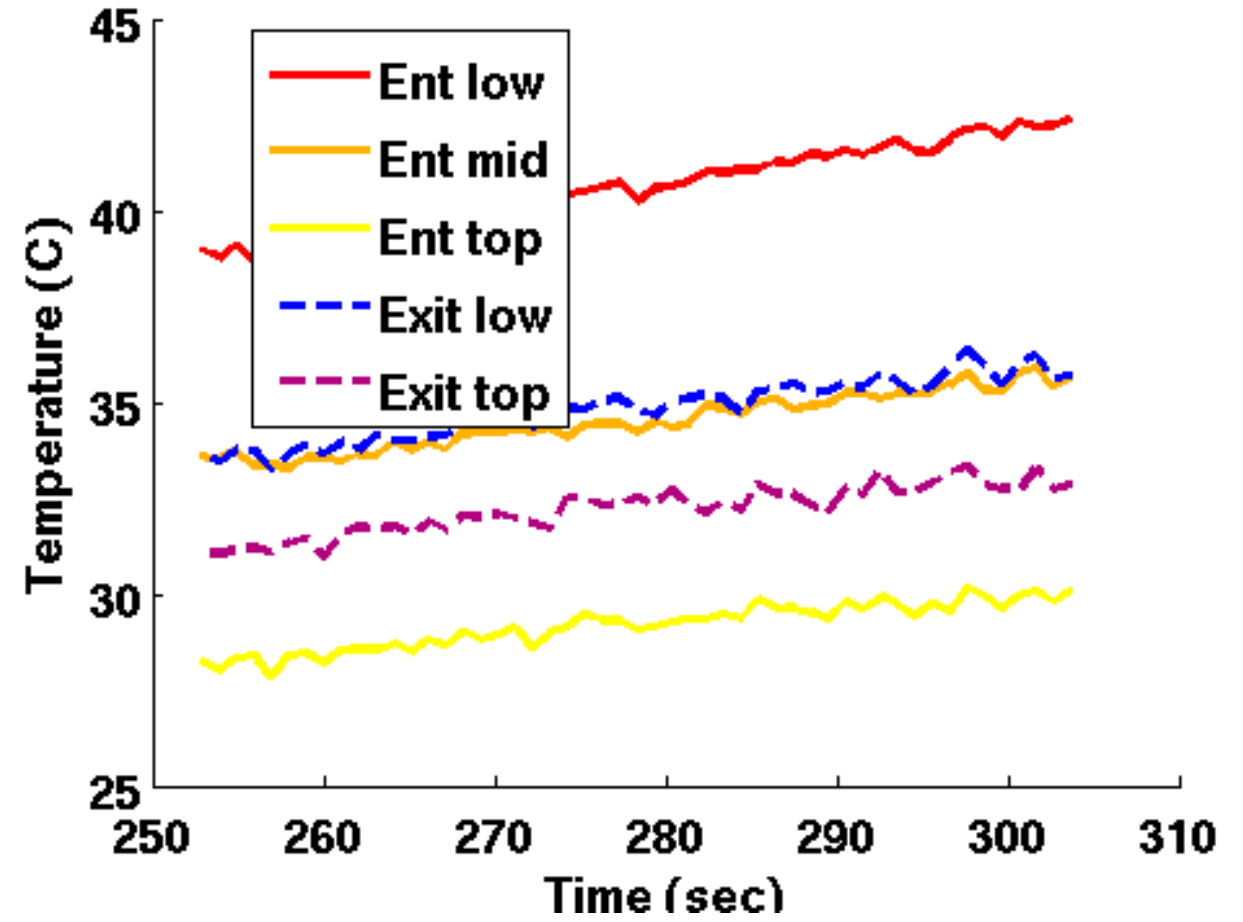
Iterations/ Lessons Learned: Level 1.4

Result: -5 °C across heat exchanger

Hot Flow Temperatures vs Time

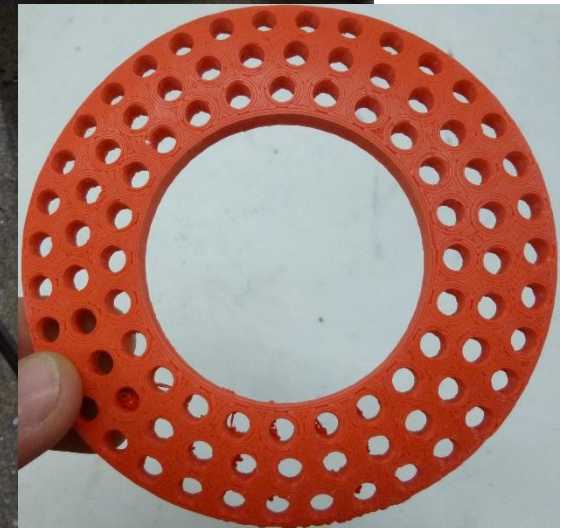


Cold Flow Temperatures vs Time



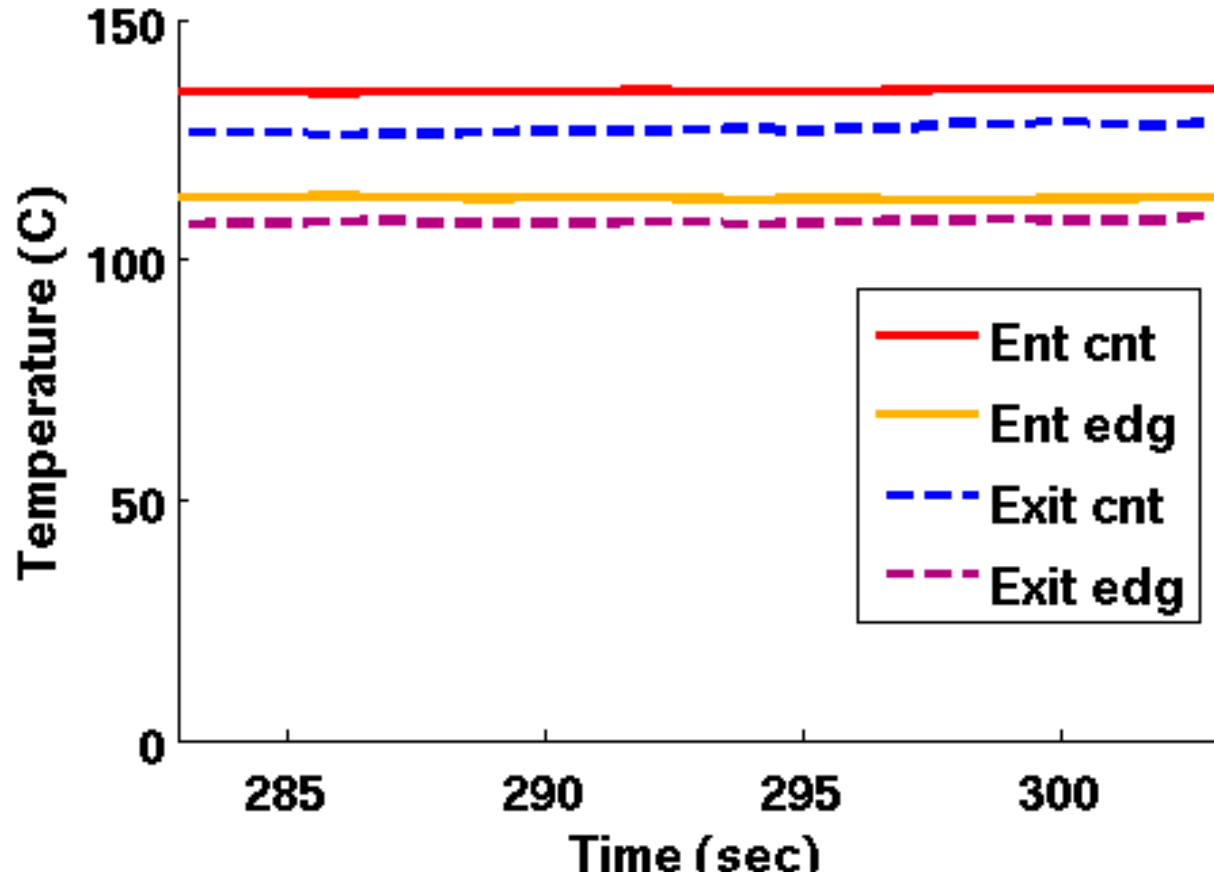
- Description:
 - Concentric pipe flow with heat exchanger
 - Created flow straightener inserts to place in cold incoming flow
 - Secured ducting around the leaf blower to prevent uneven flow and unnecessary pressure drops
 - Place temperature profile inserts with thermistors in different streamlines

- Lessons Learned:
 - Ran 3 tests and found similar data. Need to run more tests for statistical assurance

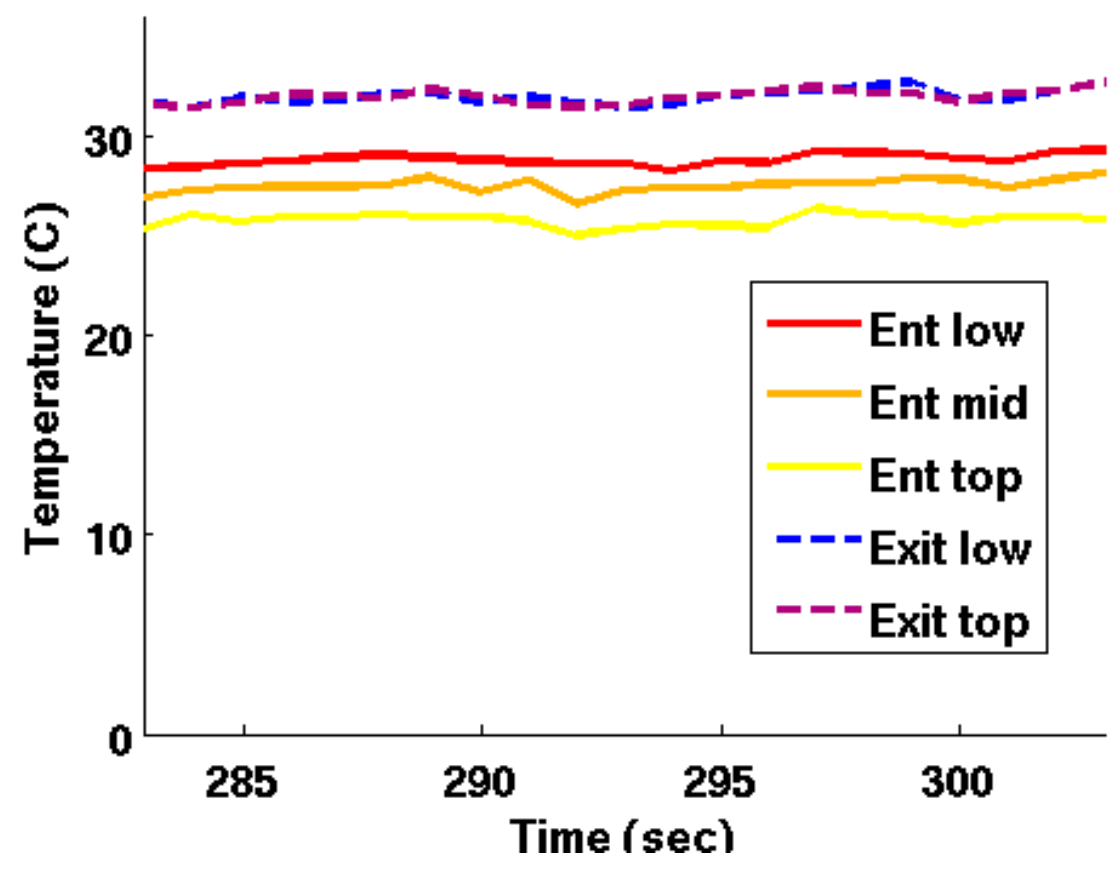


Result: +3.83 °C across heat exchanger

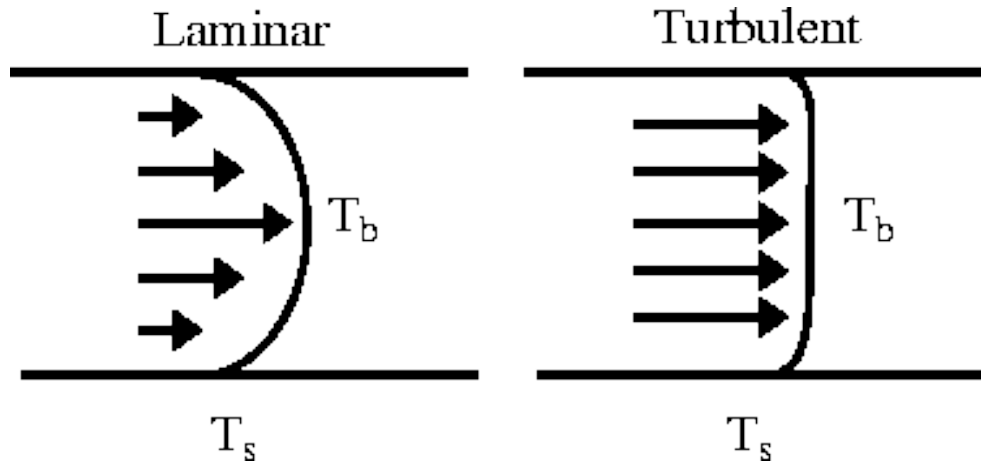
Hot Flow Temperatures vs Time



Cold Flow Temperatures vs Time



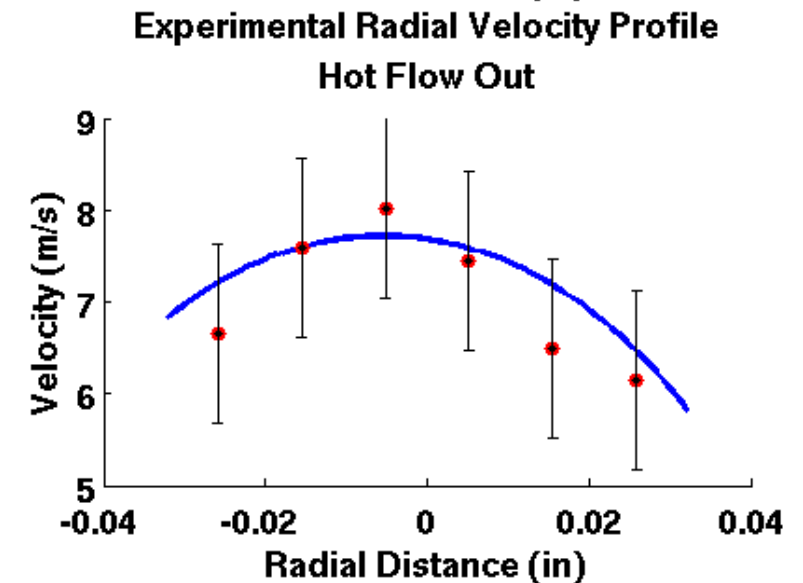
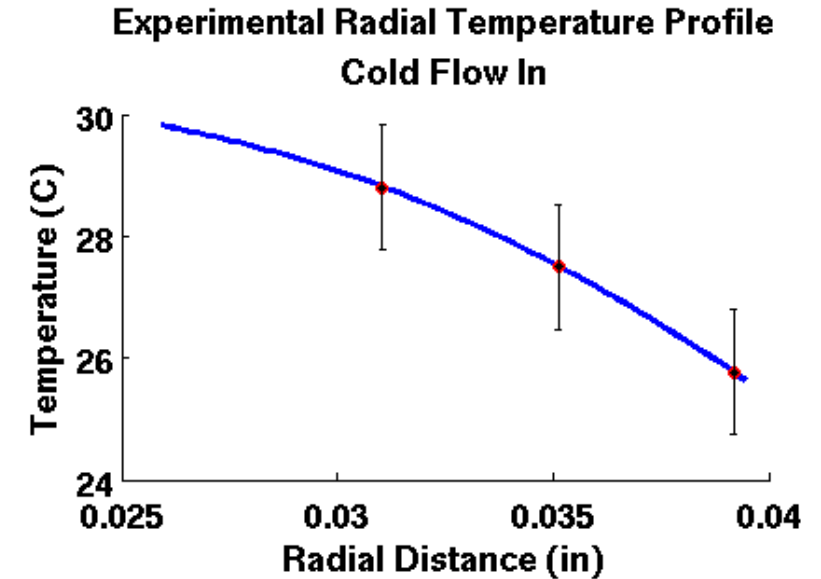
- Expected Results and Considerations:
 - Velocity profiles [1]



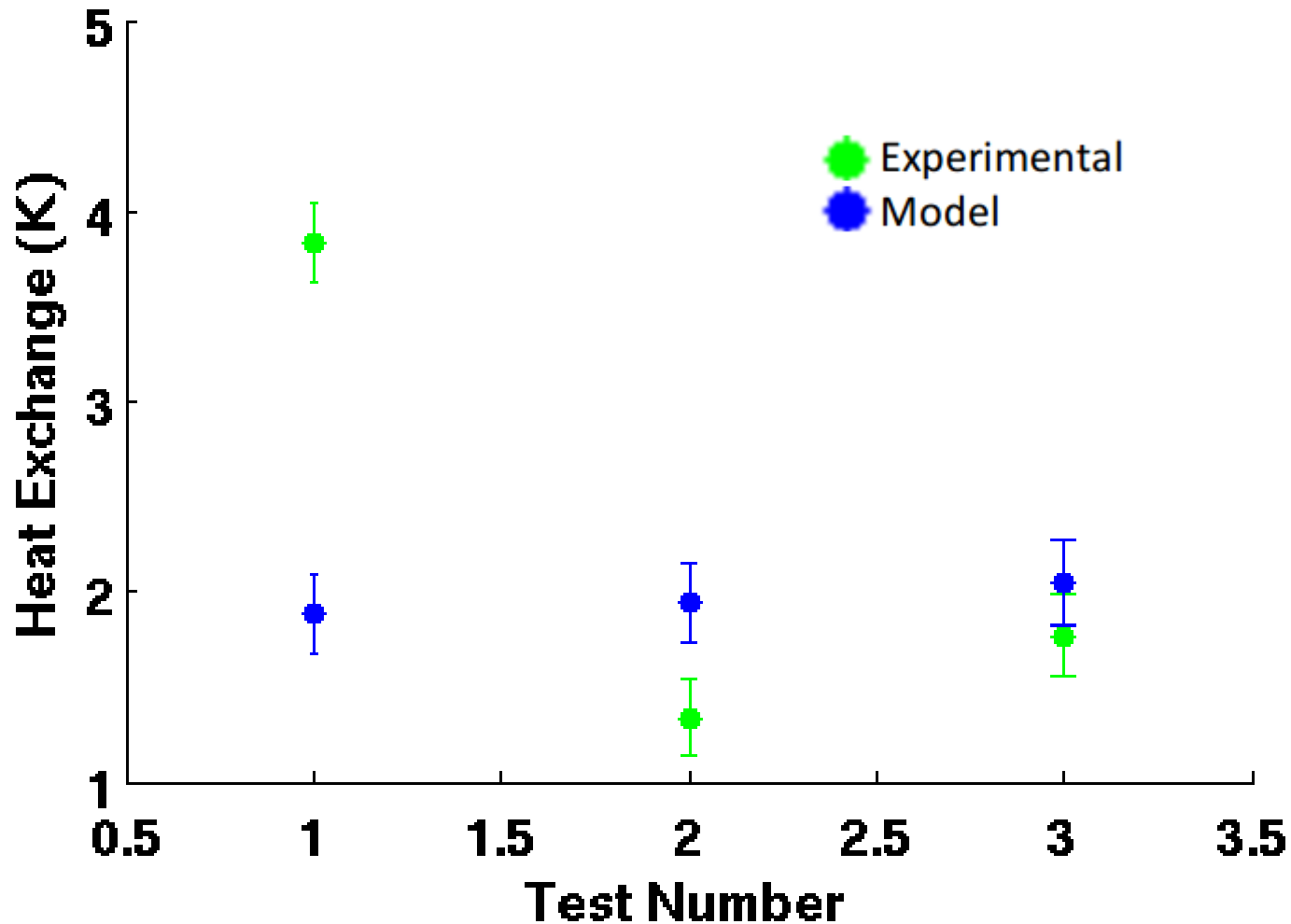
- Take bulk velocity and temperature

$$T_b = \frac{2}{U_m r_o^2} \int_0^{r_o} u T r dr$$

$$U_m = \frac{2}{r_o^2} \int_0^{r_o} u r dr$$



Monte Carlo for Model Variance



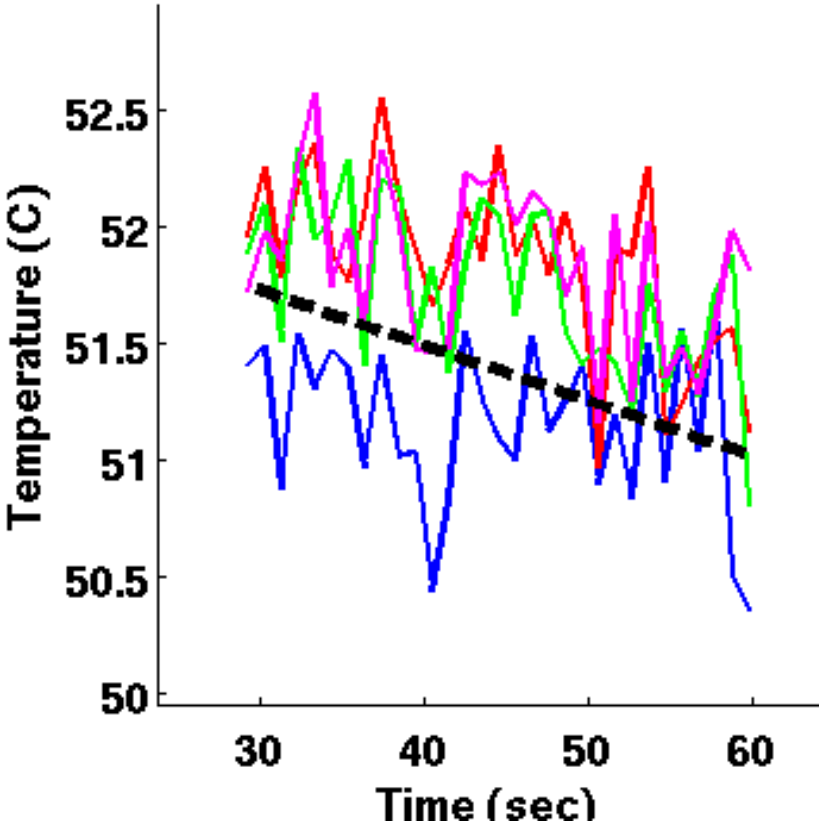
Monte Carlo Simulation Sensitivity Variables

- Temperature
 - Cold flow in
 - Hot flow in
 - Hot flow out
- Velocity
 - Hot
 - Cold

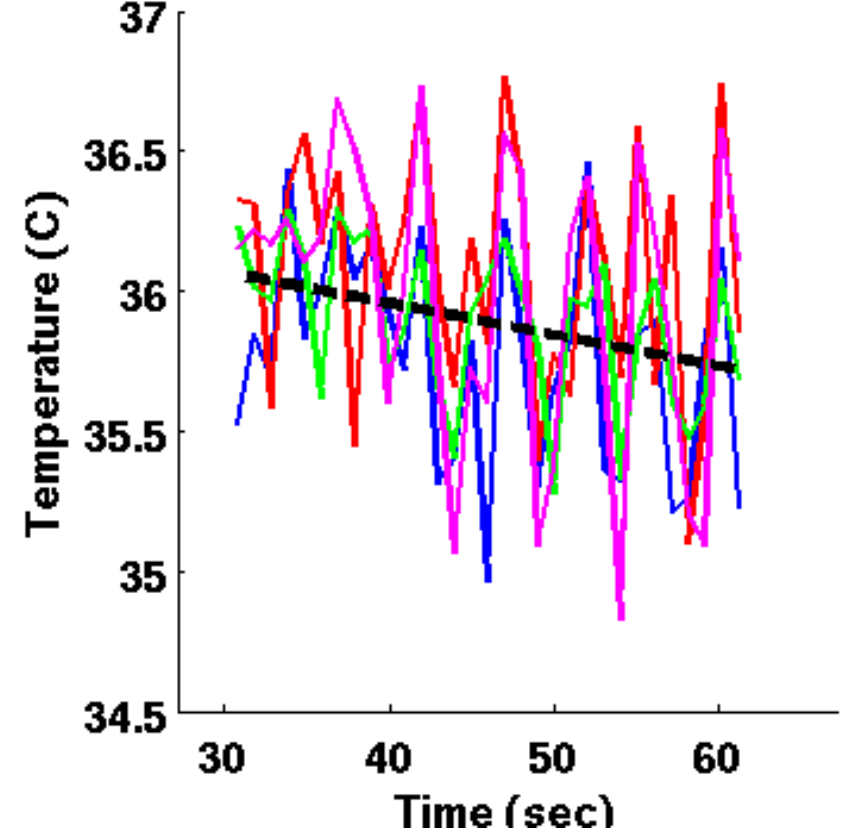
**Need to run at least ten tests
to prove model**

Estimated Hours Remaining: 10
hours

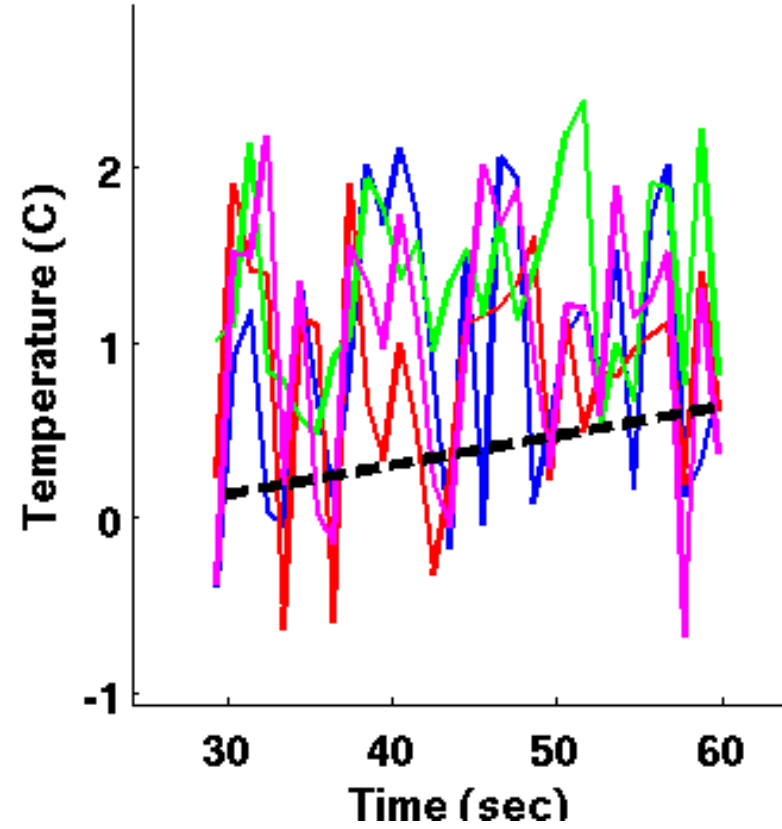
HotWaterComparison



LukeWarmWaterComparison

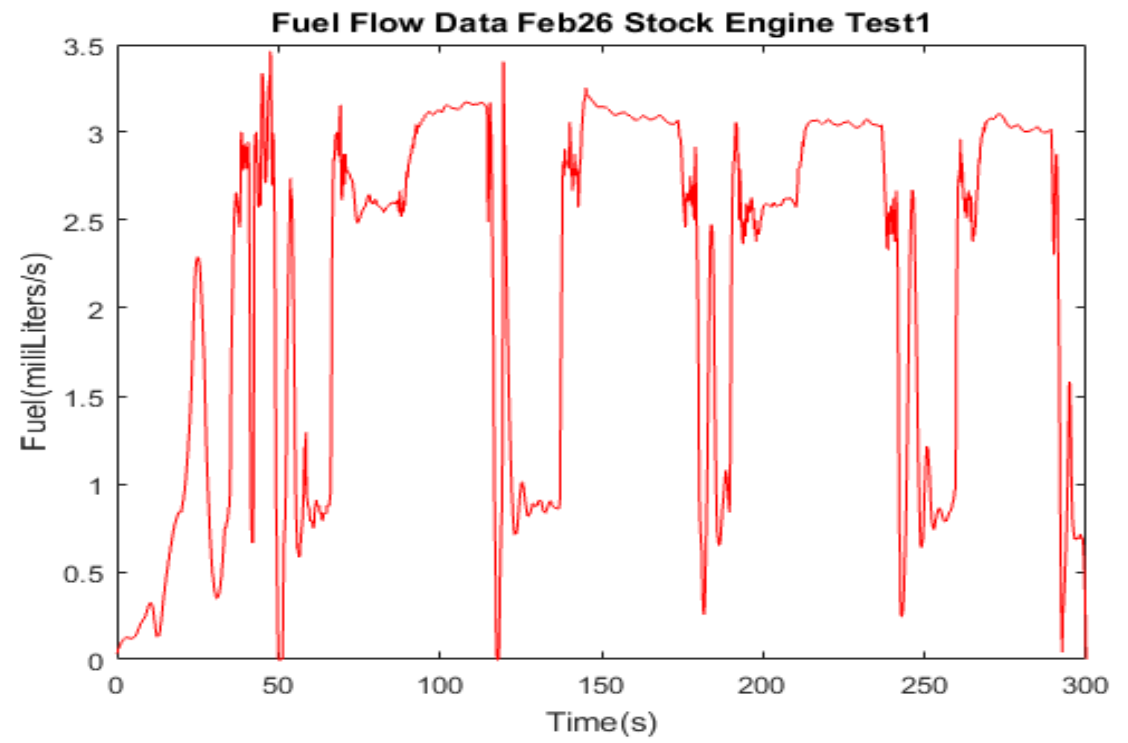
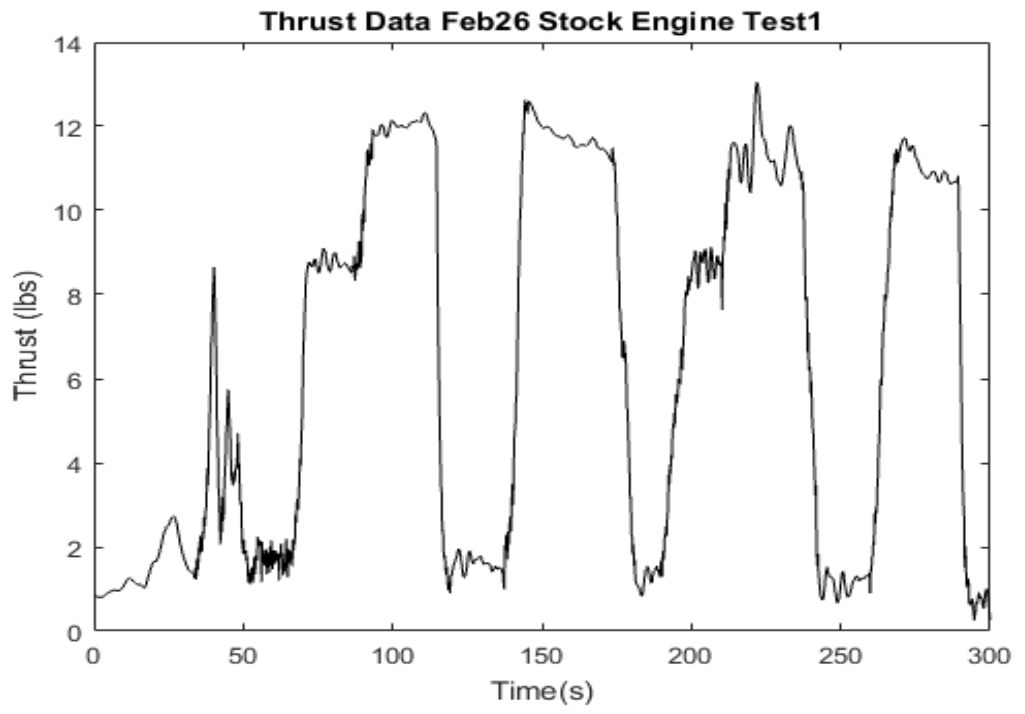


ColdWaterComparison



ECU & ESB Stock Engine Test Backup Slides

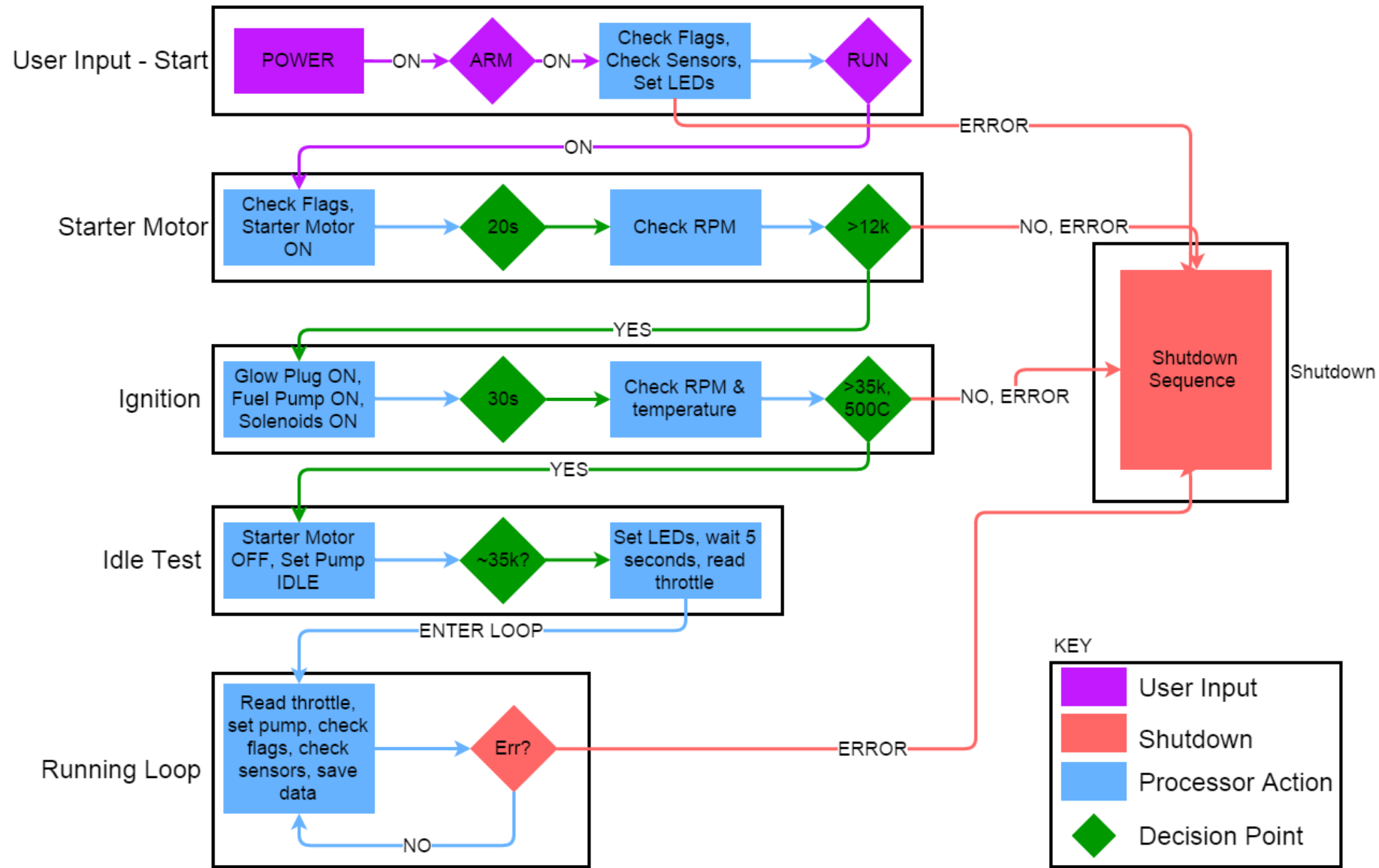
Stock Engine Characterization (TSFC)



TSFC (1/s) *1E-4			
	Idle	Half	Full
Test 1*	14.4 ± 0.9	5.2 ± 0.3	4.7 ± 0.3

*During Test 1 Throttle max = 109,500 RPM (Should be ~130,000)

EE: Engine Test Flow Chart



Integrated/Full System Test Backup Slides

HORN_Thermocouples_and_Thermistors.vi Front Panel

Temperature in Degrees C

Thermocouples?

Thermistors?

STOP Program

Notes:

Hot_Ent_Cent
Hot_Ent_Edg
Hot_Exit_Cent
Hot_Exit_Edg
Cold_Ent_Low
Cold_Ent_Med
Cold_Ent_High
Cold_Exit_Low
Cold_Exit_High

0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00
0.00

Voltage on Thermistors
0

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HORN_Thermocouples_and_Thermistors.vi Block Diagram

Thermistors

Expression Node

Temperature (C)

Write Comment

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REAPER_FUEL_AND_THRUST.vi Front Panel

NOTE: The USB-6009 should be listed as Dev 1

STOP & SAVE DATA

Calibrated by Kevin on 2/5/2016 for our 25lb load cell
Calibration Constant at 2820 Offset at .0077
Offset can be changed whenever, doesn't effect calibration

Calibration Constant was at 4530
Calibration Constant 2820 Offset 0.0077

Total milliliters Time (minutes)
0.000 0.000

Load Cell Force

Force (lbs)

Samples

Raw Load Cell Measurement
0

Total Total Pulses
0.000

Fuel Flow (milliliters)

Total fuel (mL)

Samples

Flowmeter Calibration Constant (pulses/L)
110000

Calibrated by Kevin on 2/5/2016 for our equiflow sensor
Calibration Constant at 110000

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REAPER_FUEL_AND_THRUST.vi Block Diagram

Potential Problem with this VI: The VI re-initializes all of it's channels with every data acquisition. This causes software based timing problems. The ideal solution would be to create a single VI that runs continuously and samples from all channels to ensure contant data flow.

Time (minutes)

Conversion into min

Flowmeter Calibration Constant (pulses/L)

Conversion to Seconds

Conversion to seconds

Total Total Pulses

Total milliliters

Fuel Flow (milliliters)

Conversion to minutes

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To Be Completed

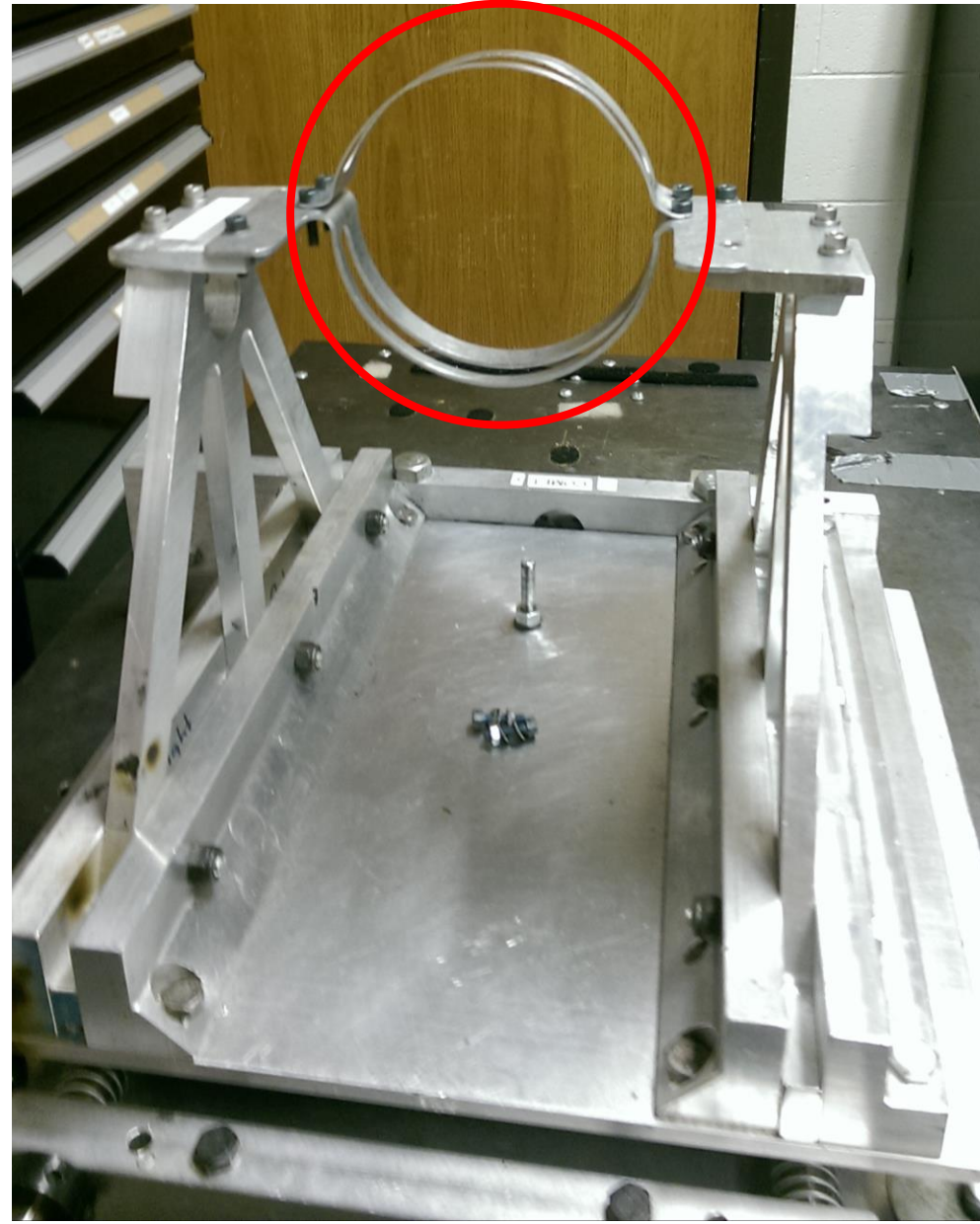
Part	Remaining Hours
Forward Ring	1
Outer Casing	2
Inner Casing	3
Nozzle	0.5

To Be Started

Part	Remaining Hours
Component Integration	4
Test Stand Alteration	6

Total Remaining Hours: **16.5**

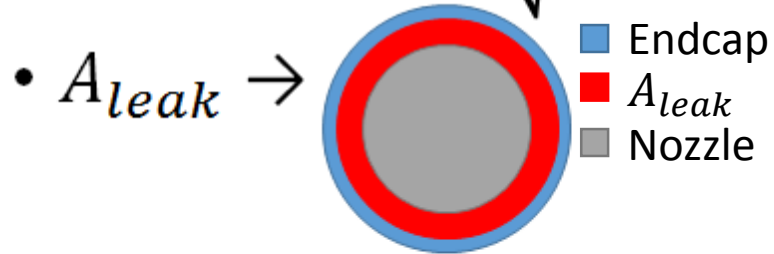
Engine Run Test: Test Stand Alteration



Pressure Leak: Magnitude

- Most likely to occur at joint of Endcap and Nozzle

- $\dot{m} = C * A_{leak} \sqrt{2\rho_{engine} (P_{engine} - P_{atm})}$



$$A_{leak} = \pi((r_{Nozzle} + gap)^2 - r_{Nozzle}^2)$$

$$A_{leak} = 2E^{-5} m^2$$

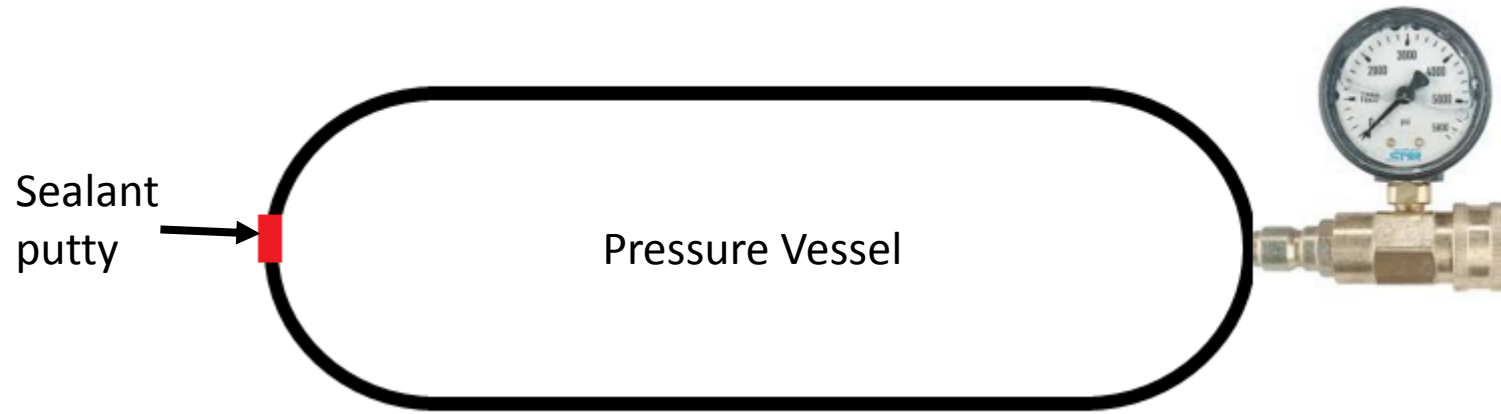
- $\rho_{engine} = 2.3 \frac{kg}{m^3}$

- $P_{engine} = 2.6 atm = 263445 Pa, P_{atm} = 1 atm = 101325 Pa$

- $C = .625 \rightarrow$ hole flow coefficient, between .6 and .65

- $\dot{m} = 0.011 \frac{kg}{s}$

Leak Analysis – Test Setup



Assume Ideal Gas → $\rho = \frac{P}{RT}$

$$\dot{m} = V \frac{\partial \rho}{\partial t} = V \left(\frac{\partial \rho}{\partial P} \frac{\partial P}{\partial t} + \cancel{\frac{\partial \rho}{\partial R} \frac{\partial R}{\partial t}} + \cancel{\frac{\partial \rho}{\partial T} \frac{\partial T}{\partial t}} \right)$$

$$\dot{m} = V \left(\frac{1}{RT} \frac{\partial P}{\partial t} \right)$$

