

Spring Final Review



REcuperating Advanced Propulsion Engine Redesign

Customer: Air Force Research Lab

Advisor: Dr. Ryan Starkey

Team: Kevin Bieri, David Bright , Kevin Gomez, Kevin Horn, Becca Lidvall,
Carolyn Mason, Andrew Marshall, Peter Merrick, and Jacob Nickless



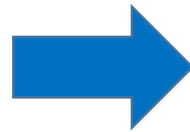
Presentation Agenda



- Project Overview
- Executive Summary
- Heat Exchanger & Model Validation
- Electronics & Engine Testing Validation
- Systems Engineering
- Project Management

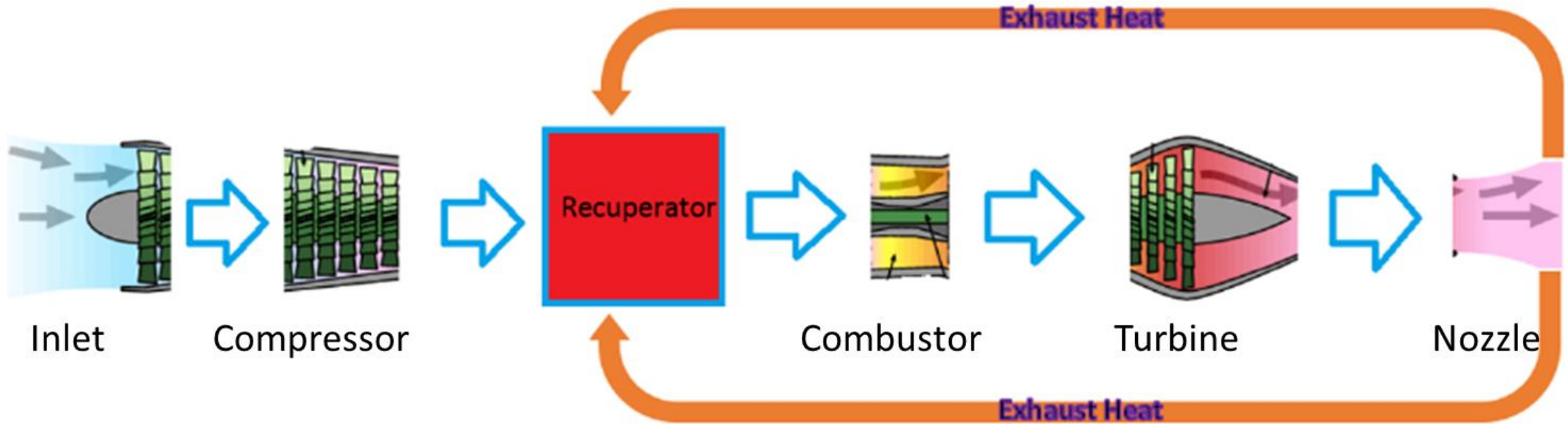
Field of Application

- Jet aircraft have a larger performance envelope than prop aircraft
- Jets burn more fuel making them less suited for long range applications.

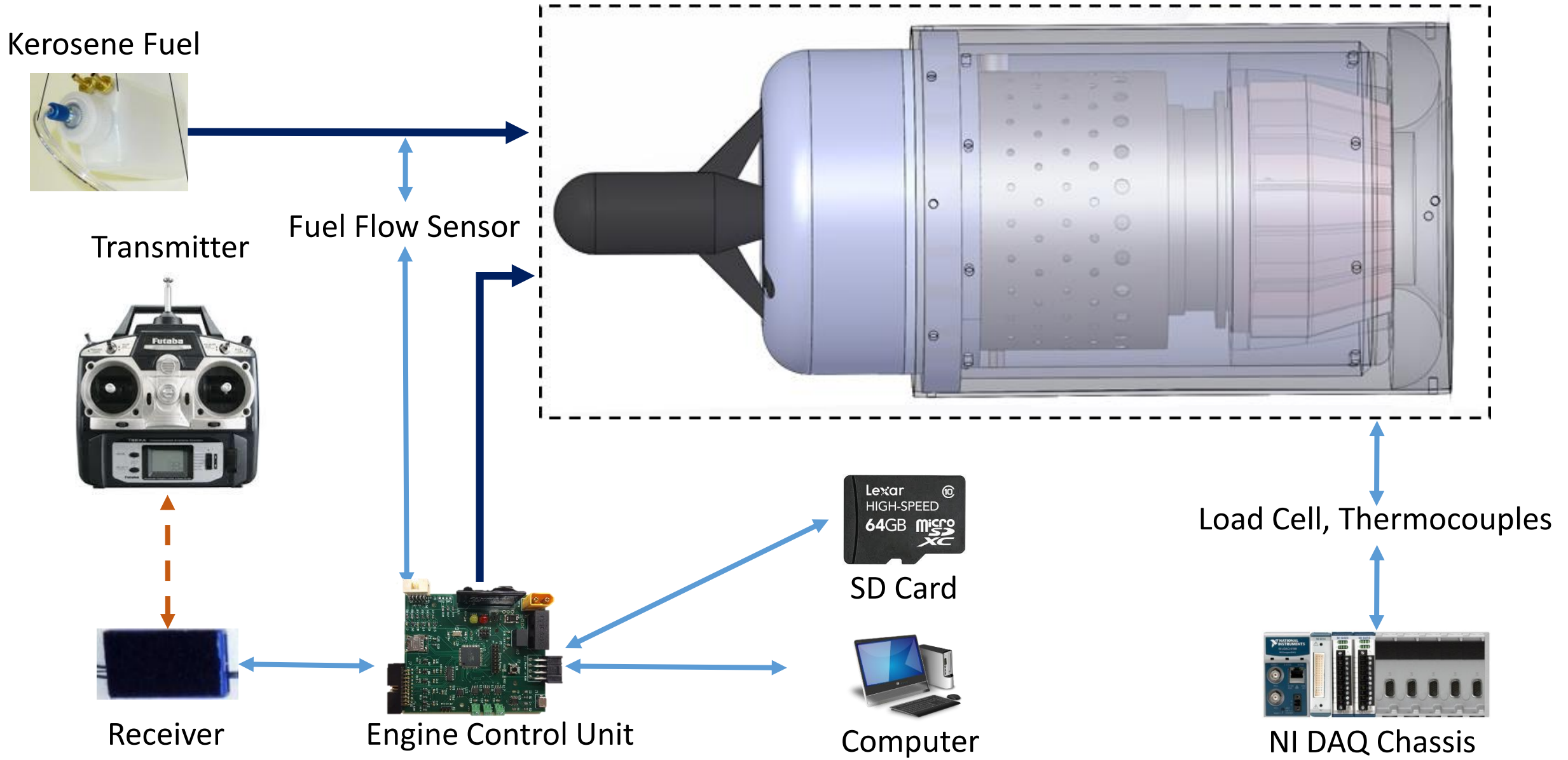


Project Mission

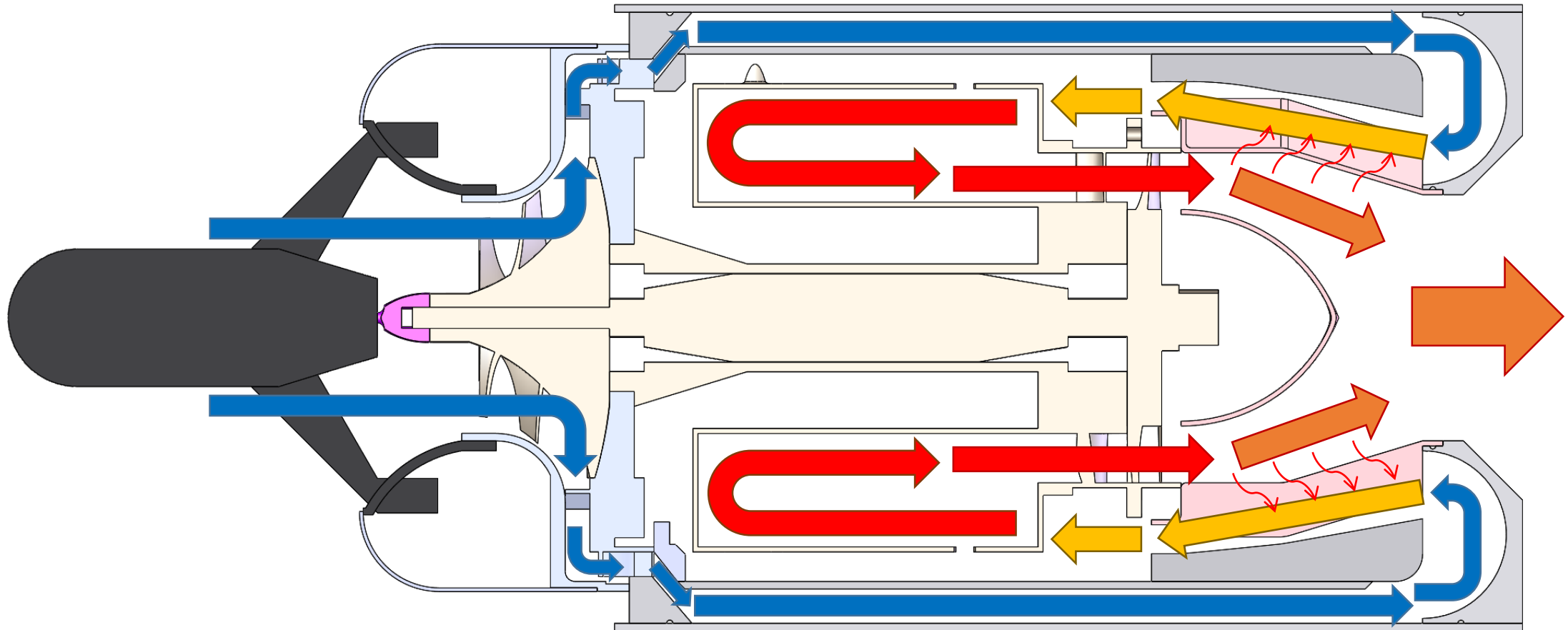
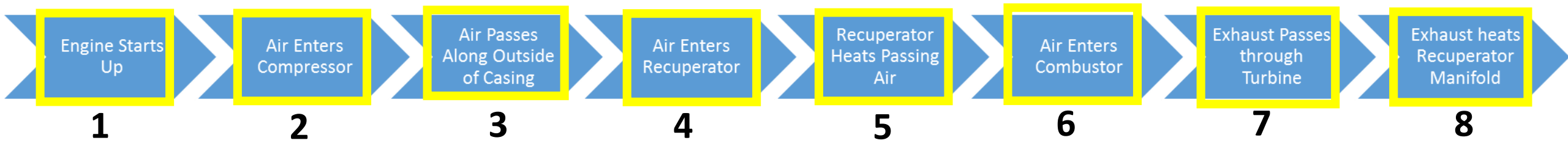
Model, build, implement, and verify an integrated recuperative system into a JetCat P90-RXi miniature turbojet engine for increased fuel efficiency from its stock configuration.



Ground based proof of concept for miniature turbojet



Baseline Design: Flow Path



CPE 1: Thermal-Fluid Modeling

- System **Characterization**

CPE 2: Heat Exchanger

- **Manufacturing**, Cost, Integration

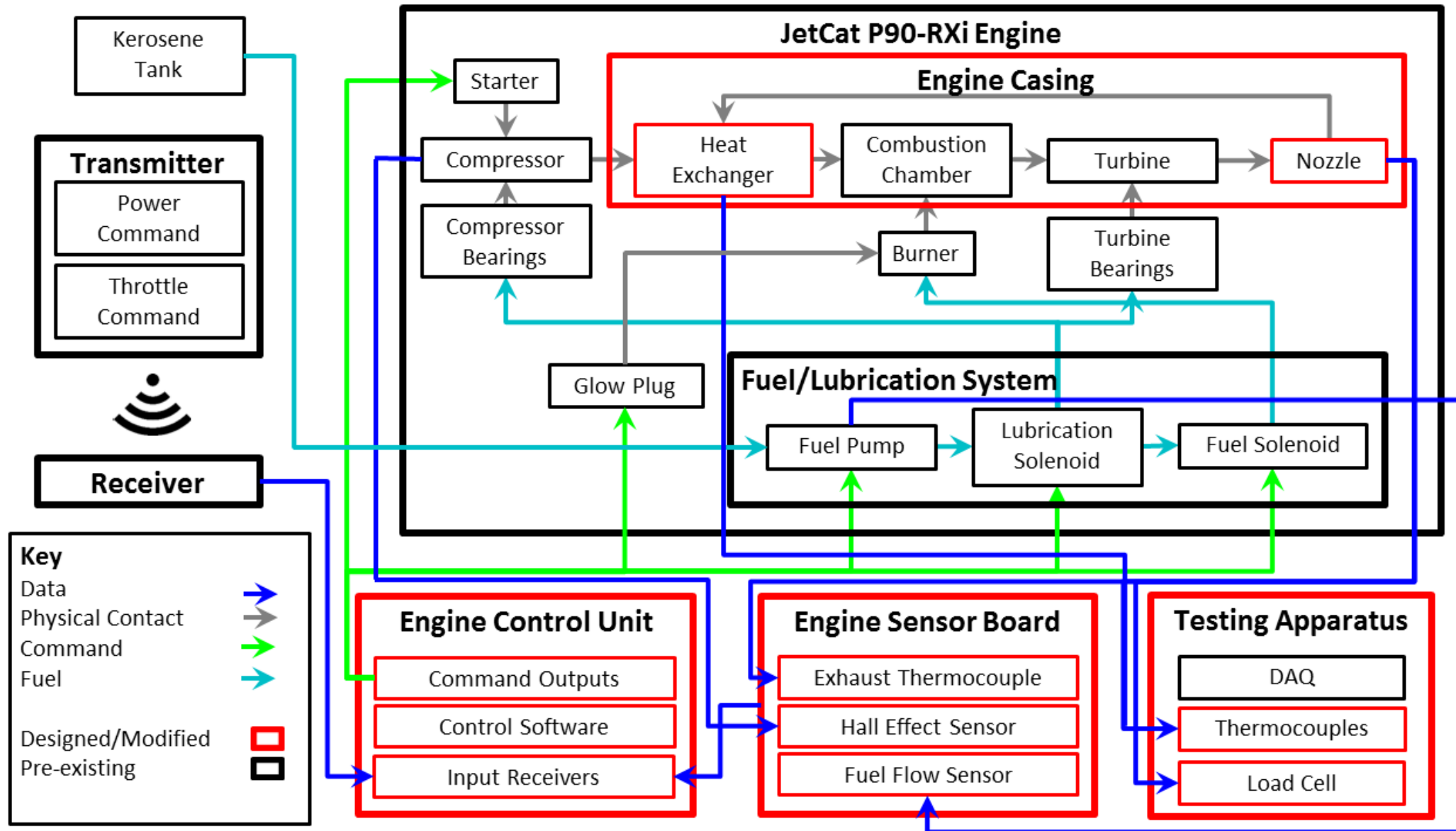
CPE 3: Engine Electronics

- **Control**, Safety, Sensors

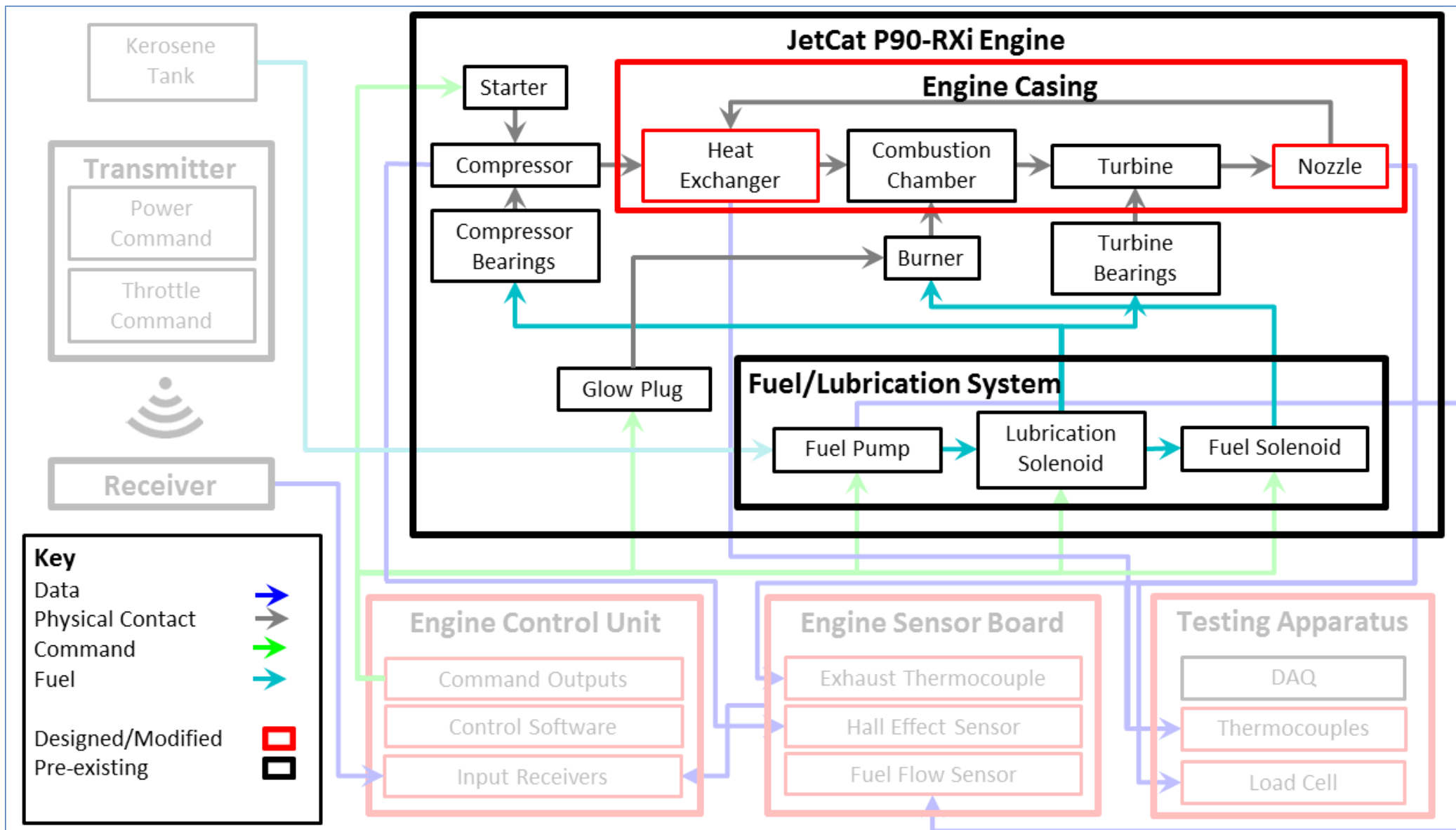
CPE 4: Testing

- **Model Validation**, System Verification, Sensors

Functional Block Diagram



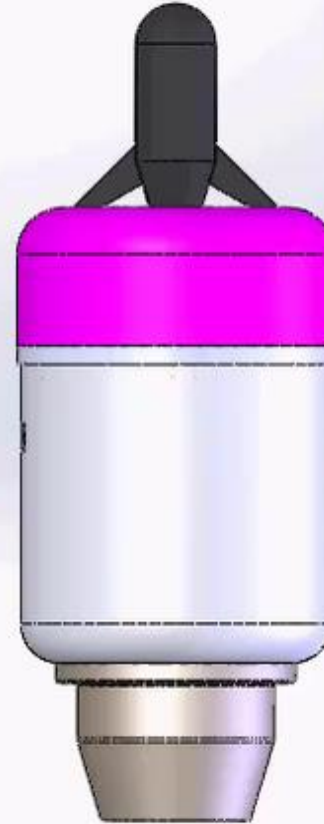
Mechanical FBD

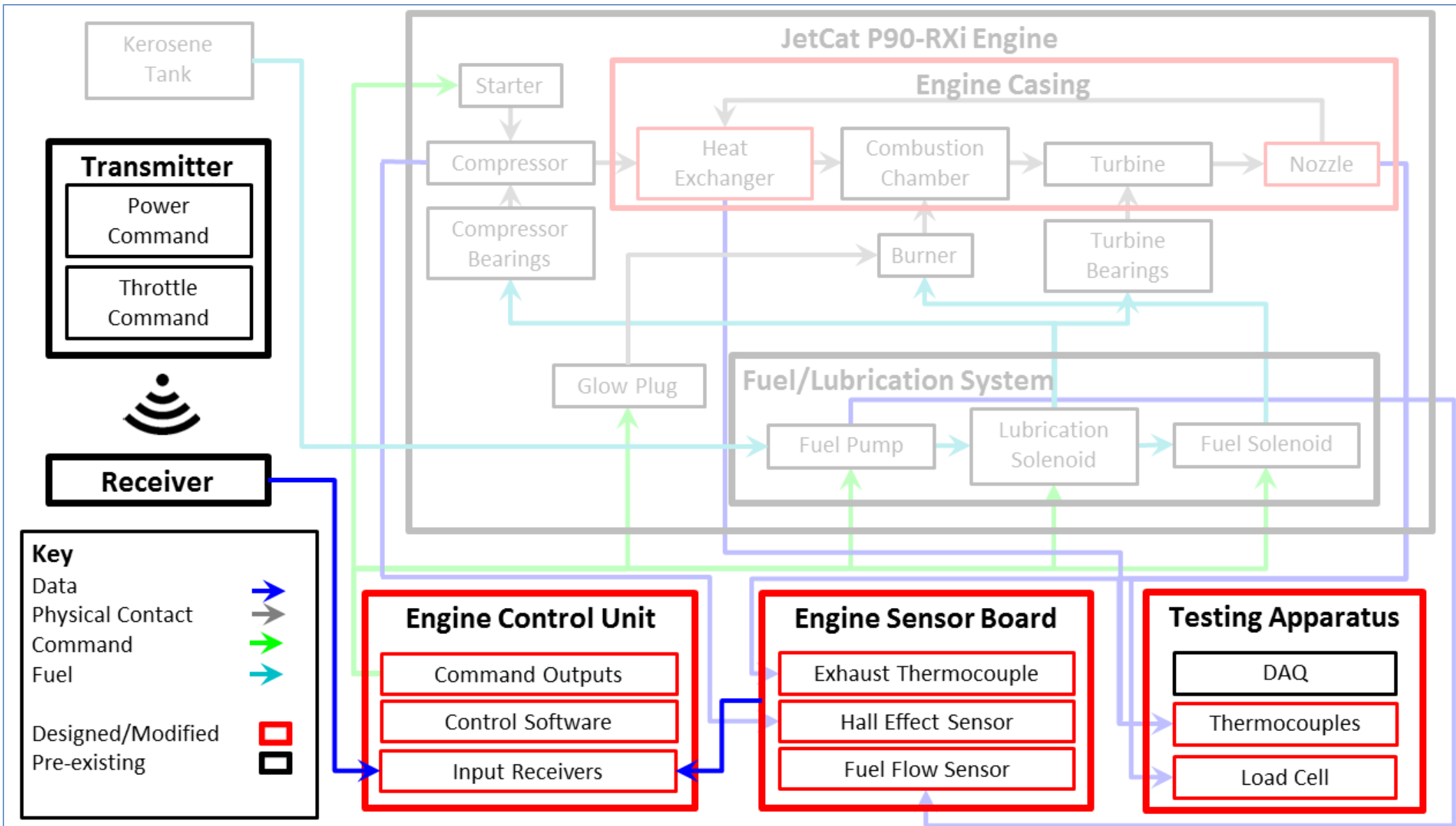


Forward Ring (x2)

Water Casing Blocks (x4)

Forward Ring

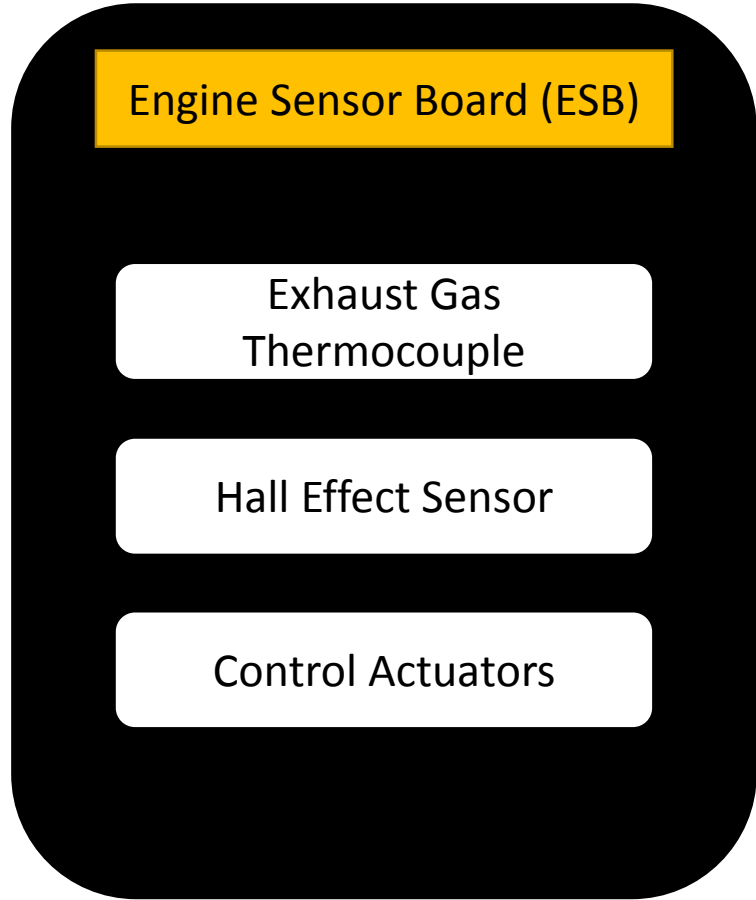
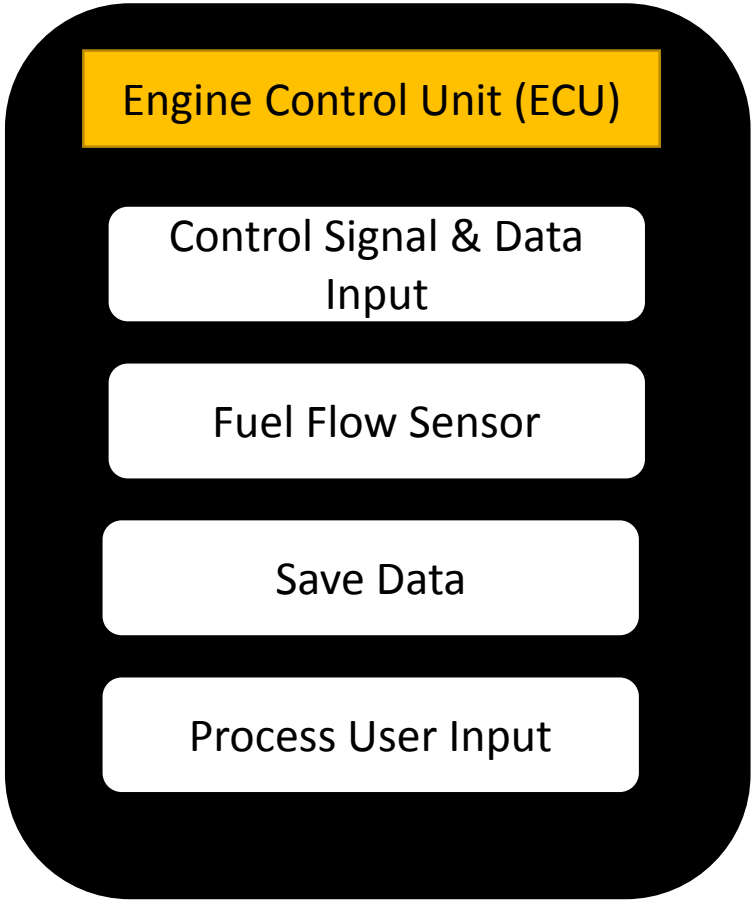




Custom printed circuit boards – based off MEDUSA design (~40%)

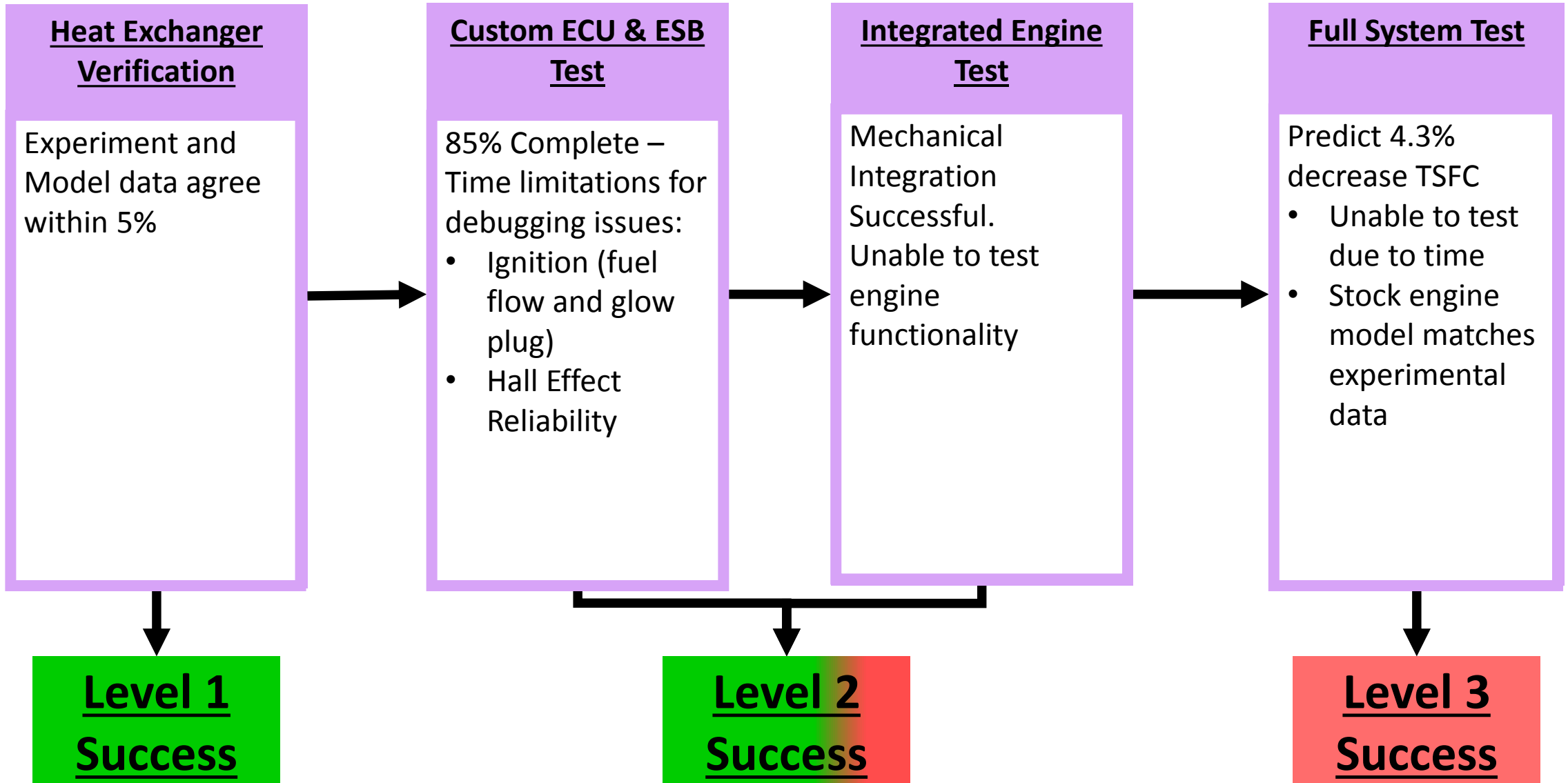


REAPER ECU



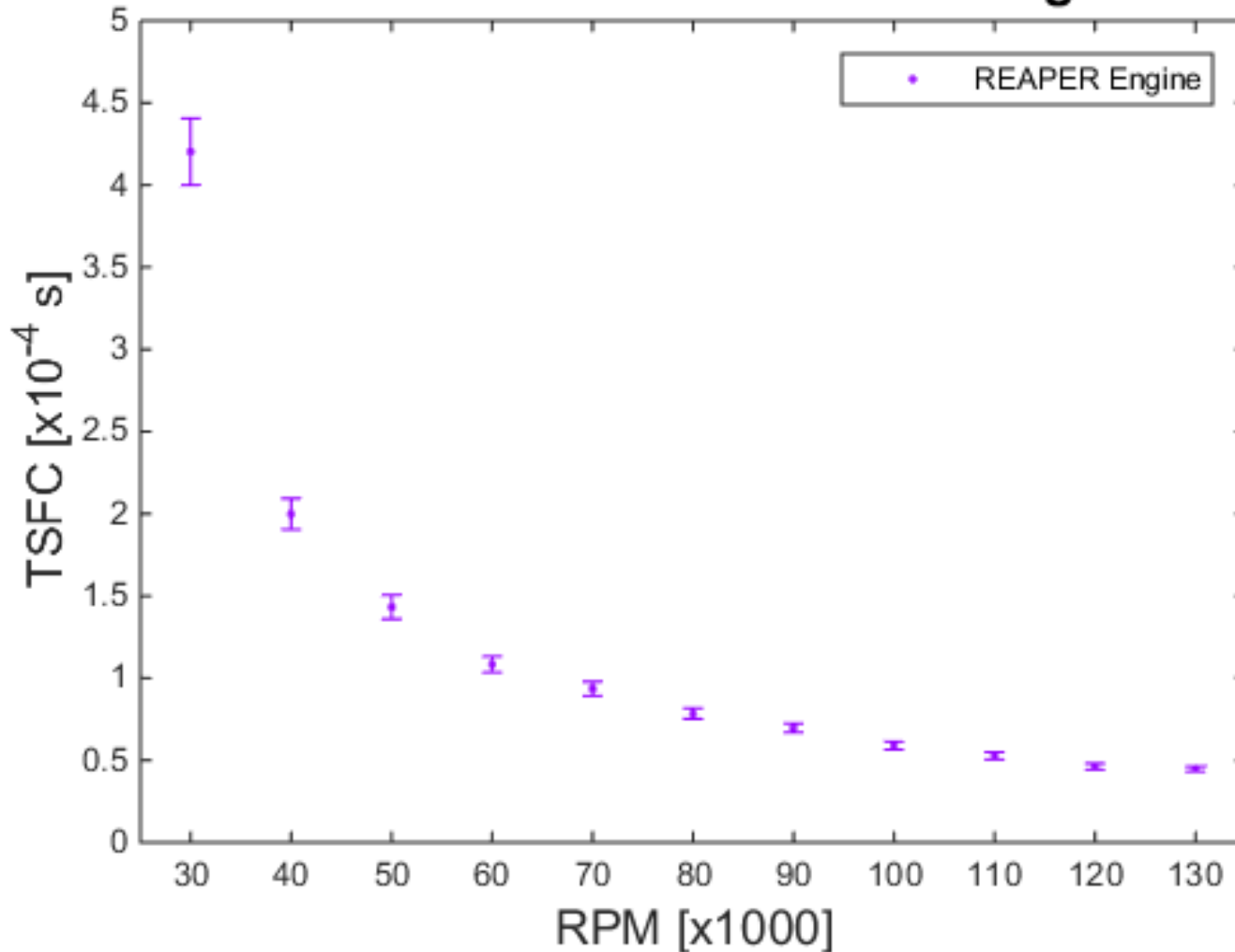
REAPER ESB

	Simulation	Recuperator
Level 1	<ul style="list-style-type: none"> -Develop first order, steady state model -Model heat exchanger effectiveness, specific fuel consumption and thrust <p style="text-align: right;">100%</p>	<ul style="list-style-type: none"> -Recuperator designed and manufactured -Recuperator verified with engine analog <p style="text-align: right;">100%</p>
Level 2	<ul style="list-style-type: none"> -Model transient characteristics <p style="text-align: right;">100%</p>	<ul style="list-style-type: none"> -Recuperator is integrated onto engine -Integrated engine system starts and runs <p style="text-align: right;">60%</p>
Level 3	<ul style="list-style-type: none"> -Develop CFD model -Model is verified with test data <p style="text-align: right;">90%</p>	<ul style="list-style-type: none"> -Engine system operates for throttle range -Engine system meets design requirements <p style="text-align: right;">0%</p>



Integrated Engine Test Prediction

Predicted TSFC for REAPER Engine



At Full Throttle:

- Stock Engine TSFC: $4.67 \times 10^{-4} [s^{-1}]$
- Predicted TSFC: $4.47 \times 10^{-4} [s^{-1}]$
- Percent Change in TSFC: **-4.3%**

Conclusions:

- Unable to meet FR 2 to decrease TSFC by 10% at maximum thrust
- Recuperation is better suited for shaft-work applications

Heat Exchanger & Heat Transfer Model Validation

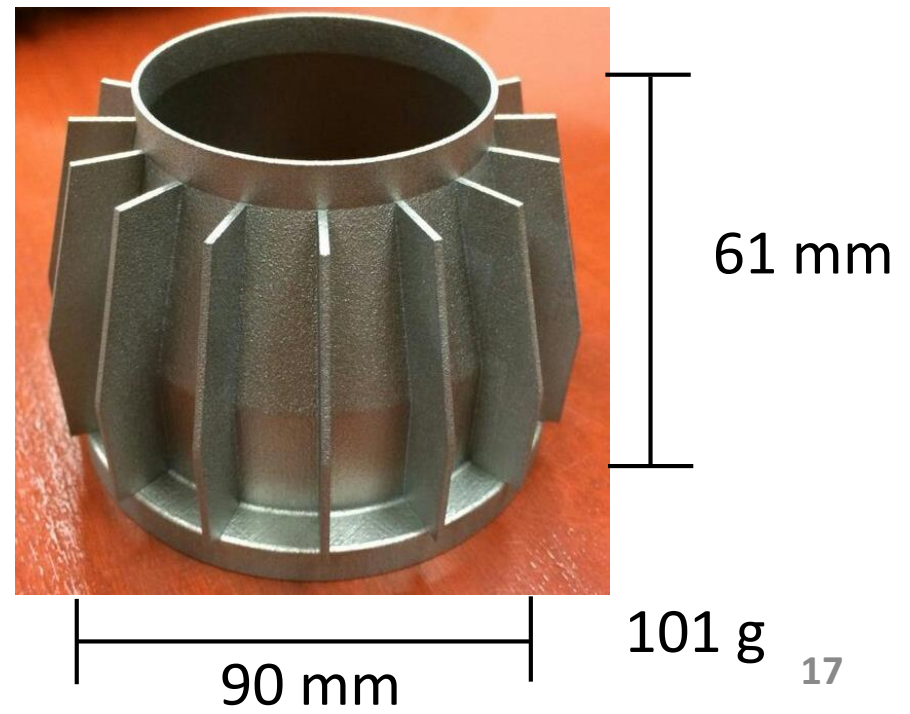
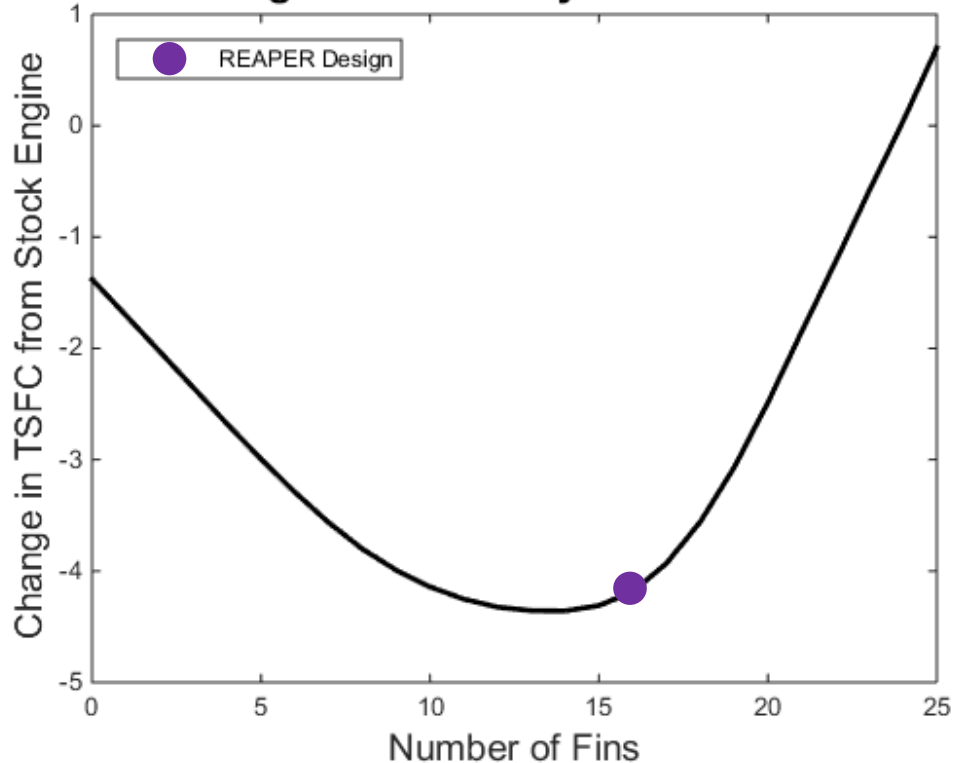
Goal: Verify heat exchanger design and heat transfer model

Motivation: Heat transfer from heat exchanger is the core aspect of the design

Heat Exchanger Design Overview

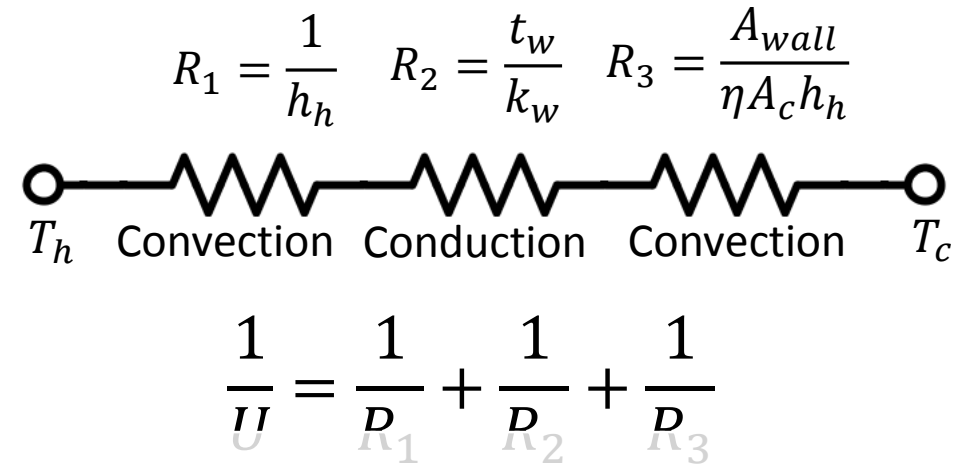
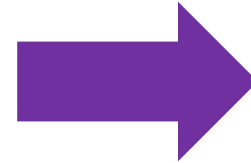
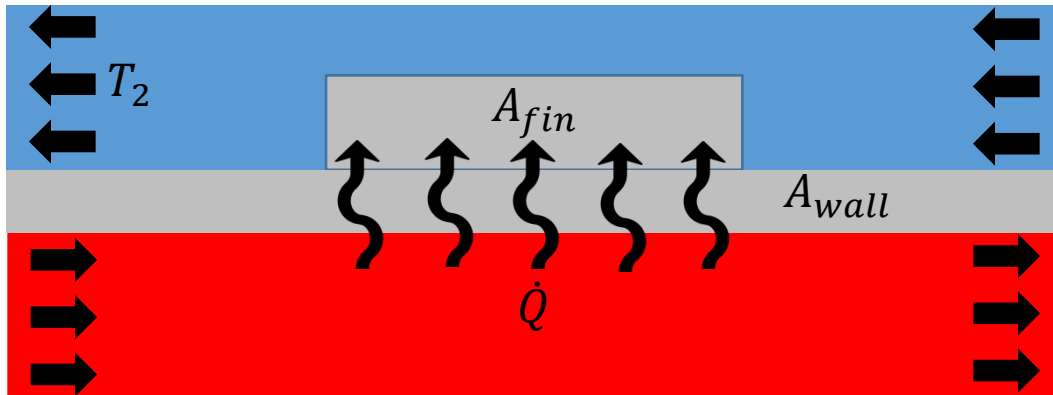
- Design obtained from parametric studies
- Interior fins and extended length considered but ultimately left out
- Direct Metal Laser Sintered by Protolabs
 - All dimensions within manufacturer tolerances ± 0.025 mm

Heat Exchanger Trade Study: Number of Cold Fins



Heat Transfer Model

$$C_p(T_2 - T_1) = UA_{wall}(T_h - T_c)$$



Gnielinski

ess

$$Nu_D = \frac{1}{(1 + 0.4 Pr)^{0.4} (1 + 0.1 Pr)^{0.4}}$$

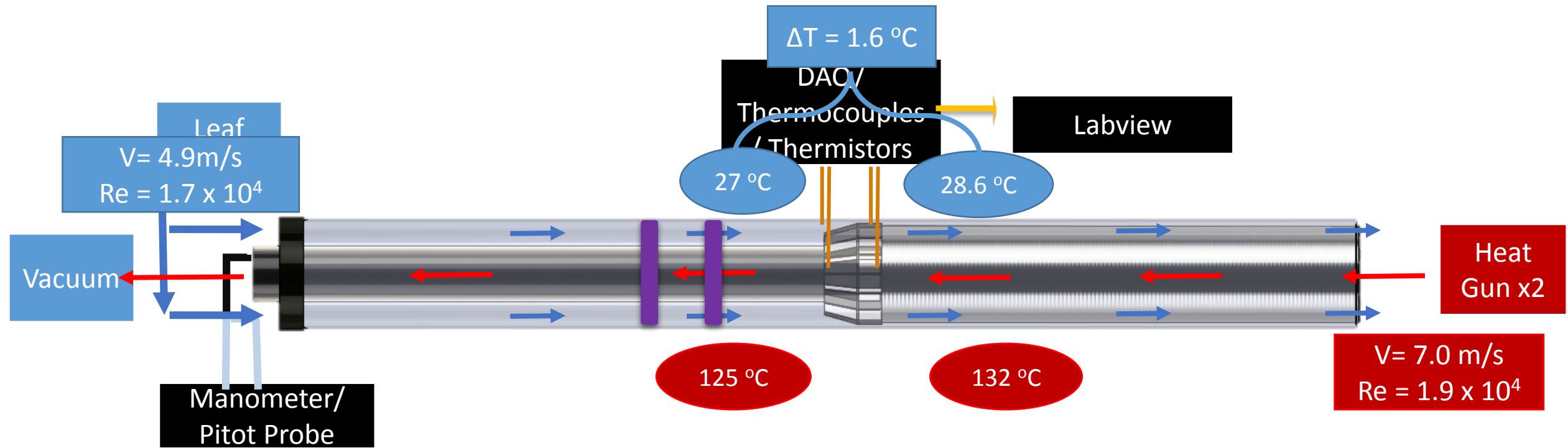
(η_f)

Applicable for

$$Re_D \geq 3000$$

$$0.9 \leq Pr \leq 2000$$

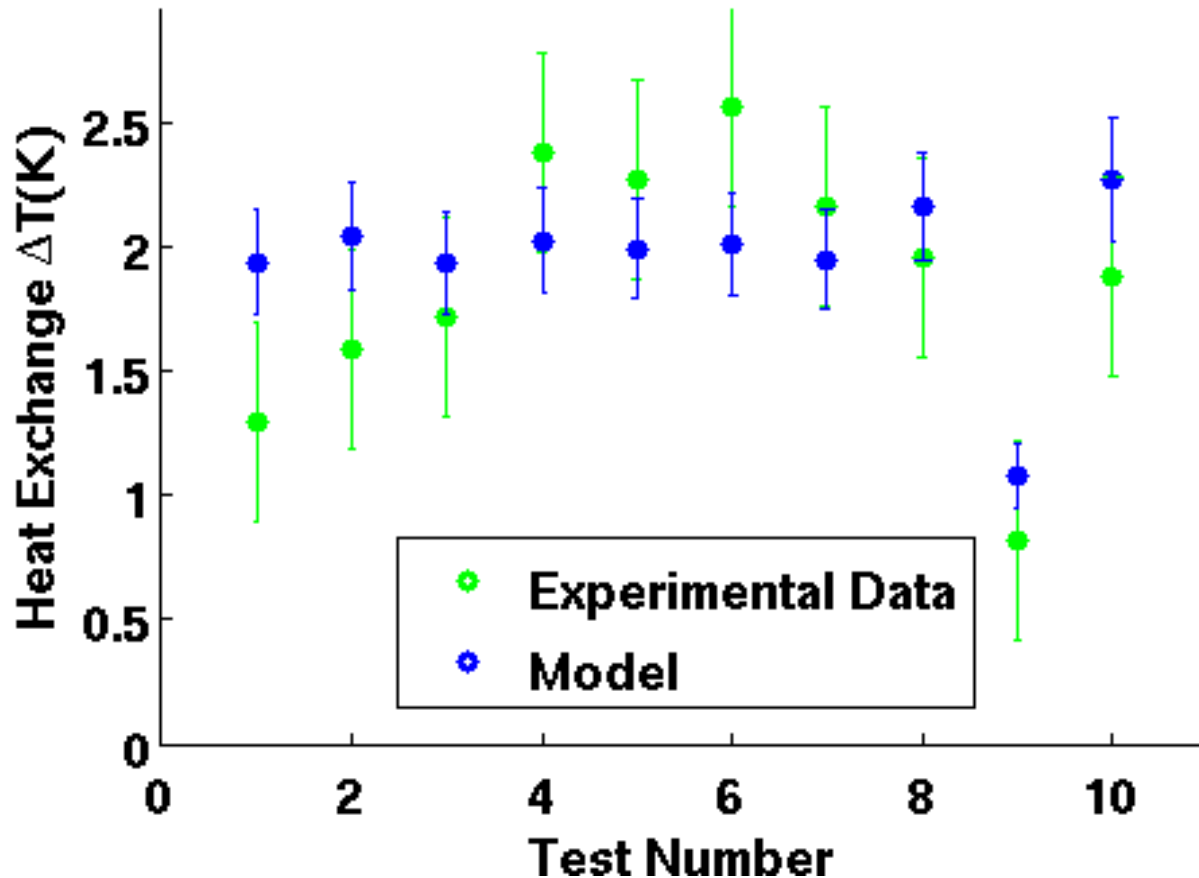
Verification of the heat transfer model is core to understanding recuperative engine cycle



Sensor List	Error	Expected Sample Range	Sample Rate
Thermocouples	+/- 2°C	Hot Flow 100-300°C	1 Hz
Thermistors	+/- 0.2°C	Cold Flow 10-40°C	1 Hz
Pitot Static Tube	+/- 1 m/s	5-40m/s	N/A

Heat Exchanger Test Results

Experimental Test Data vs Model Prediction for Heat Exchange (ΔT) Across Test Section



Data Comparison:

- 10 tests conducted
 - 9 of 10 tests within 2σ of each other
- On average model 5% error from experimental data

Conclusion:

- Heat exchanger functioned as designed
- Model predicts the heat exchanger performance

Control Volume Model Validation

Goal: Verify ability of engine model to predict engine performance

Motivation: Need to model engine performance to predict effect of heat exchanger

Conservation Laws

Mass:

$$\rho_1 A_1 V_1 = \rho_2 A_2 V_2$$

Momentum:

$$p_1 A_1 - p_2 A_2 + \tilde{P}(A_2 - A_1) - \left(\frac{\dot{W}_{shaft}}{V_m} + F_{fric} \right) = \dot{m}_2 V_2 - \dot{m}_1 V_1$$

Energy:

$$\left(\frac{\dot{Q} - \dot{W}_{shaft}}{\dot{m}} \right) - \frac{V_m^2}{2} K_L = C_{p,2} T_2 - C_{p,1} T_1 + \frac{1}{2} (V_2^2 - V_1^2)$$

Constitutive:

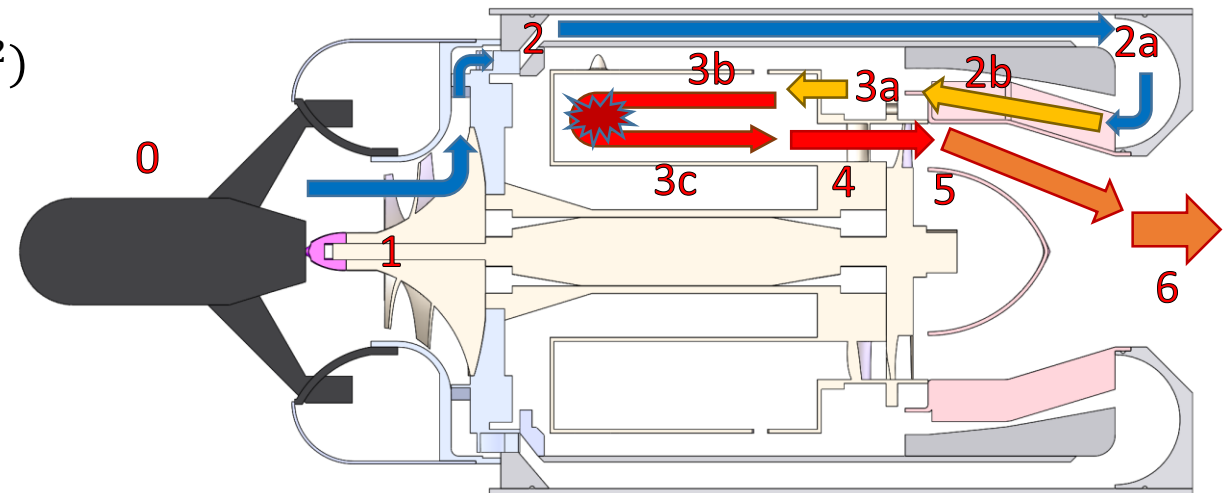
$$p = \rho RT$$

Loss Sources

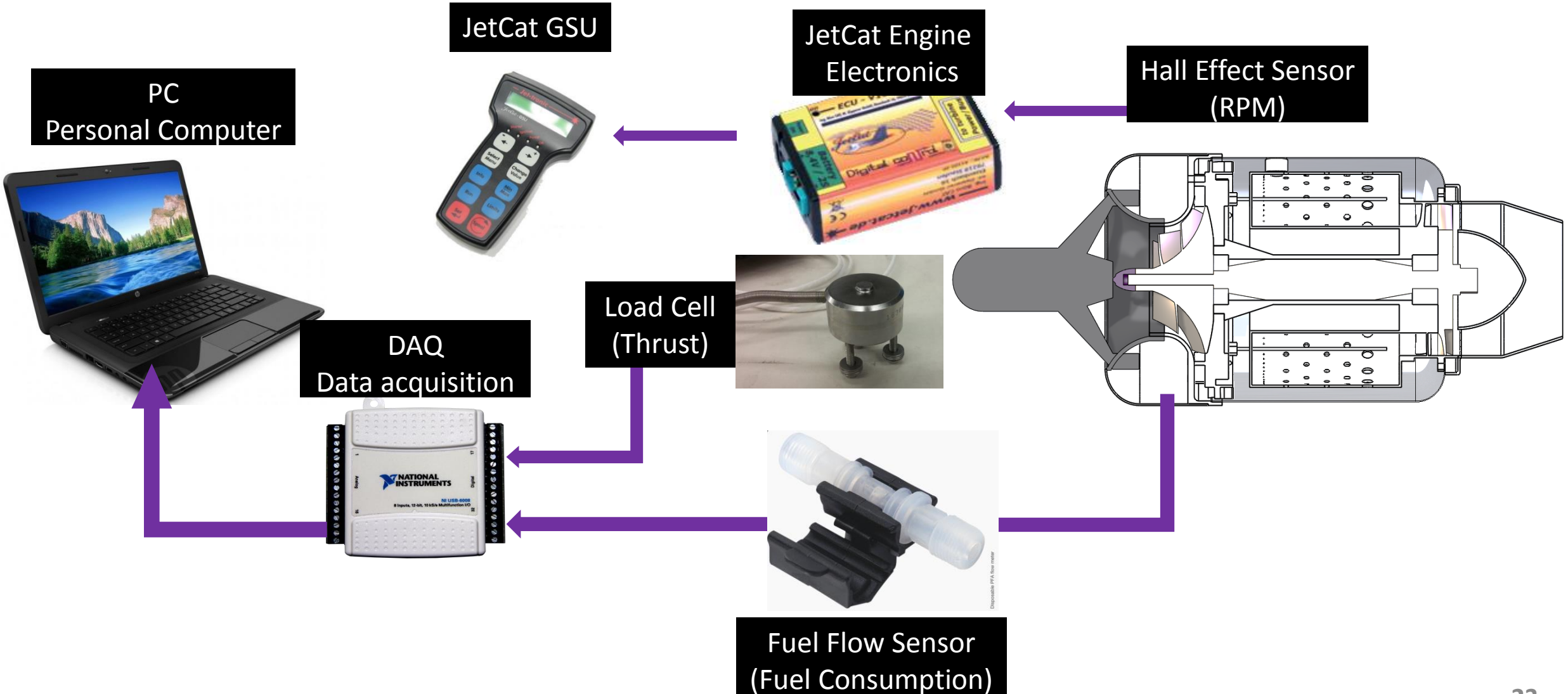
- Friction (Colebrook-White)
- Sudden expansion/contraction
- Gradual Expansion
- Turning the flow

Assumptions/Correlations

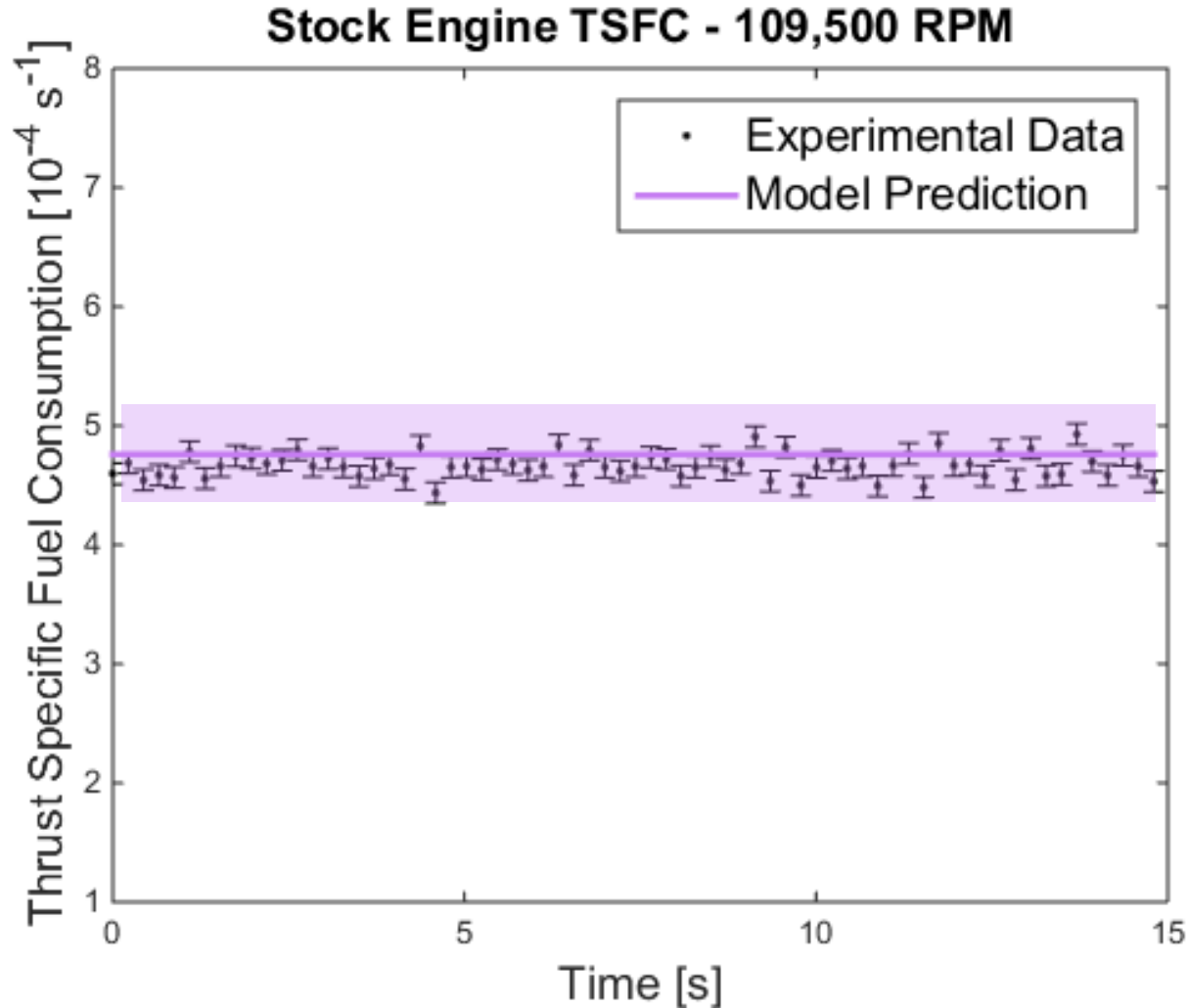
- Ideal, thermally perfect gas
- 1-D flow; fully turbulent
- Engine component efficiencies from MEDUSA/COMET component maps
- Colebrook-White friction correlation
- Gnielinski heat transfer correlation



Stock Engine Test Setup



Control Volume Model Validation: TSFC



Predicted TSFC: $4.8 \pm 0.3 * 10^{-4} [s^{-1}]$

Measured Average TSFC: $4.67 \pm 0.09 * 10^{-4} [s^{-1}]$

Percent Difference: 2.8%

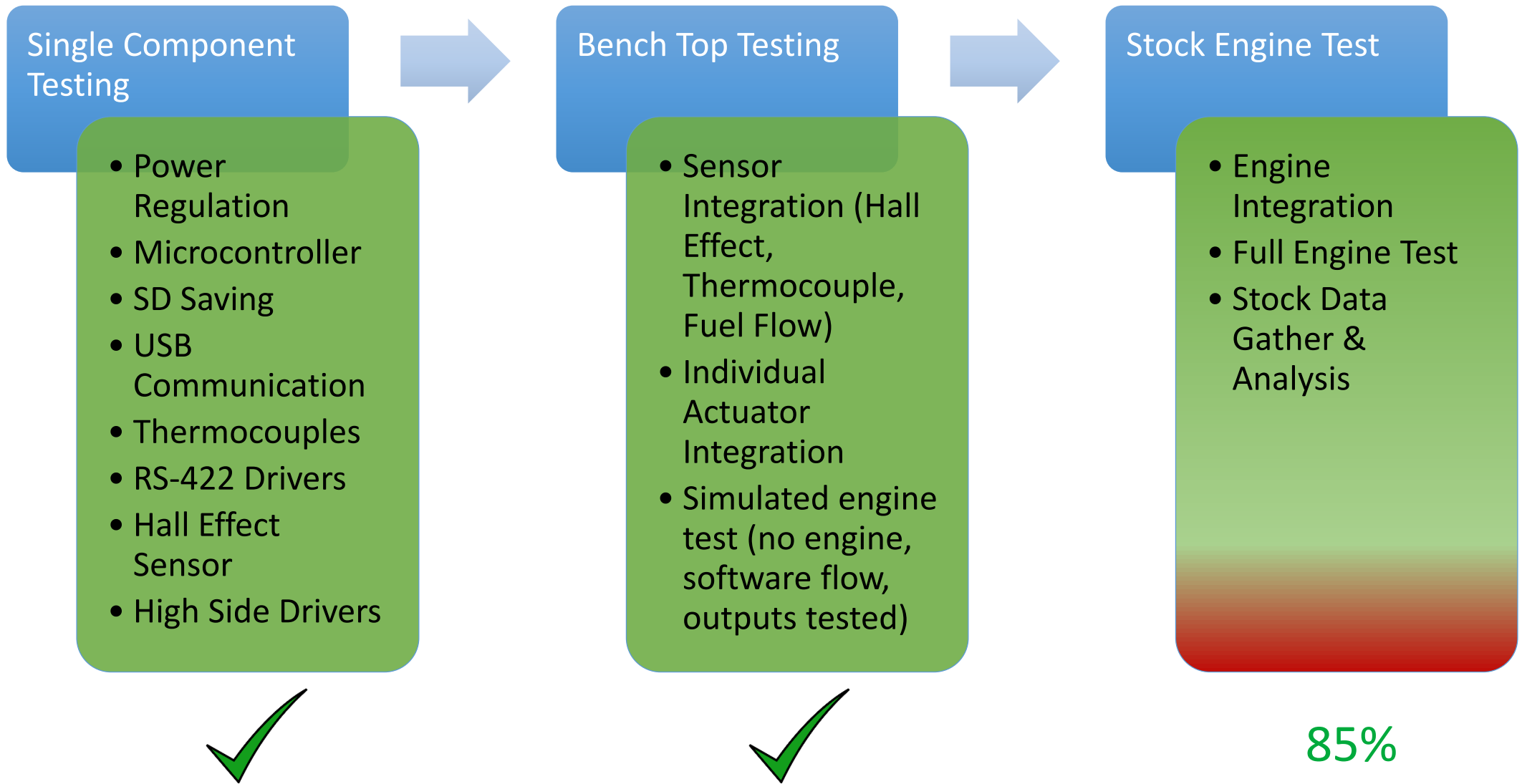
Conclusion:

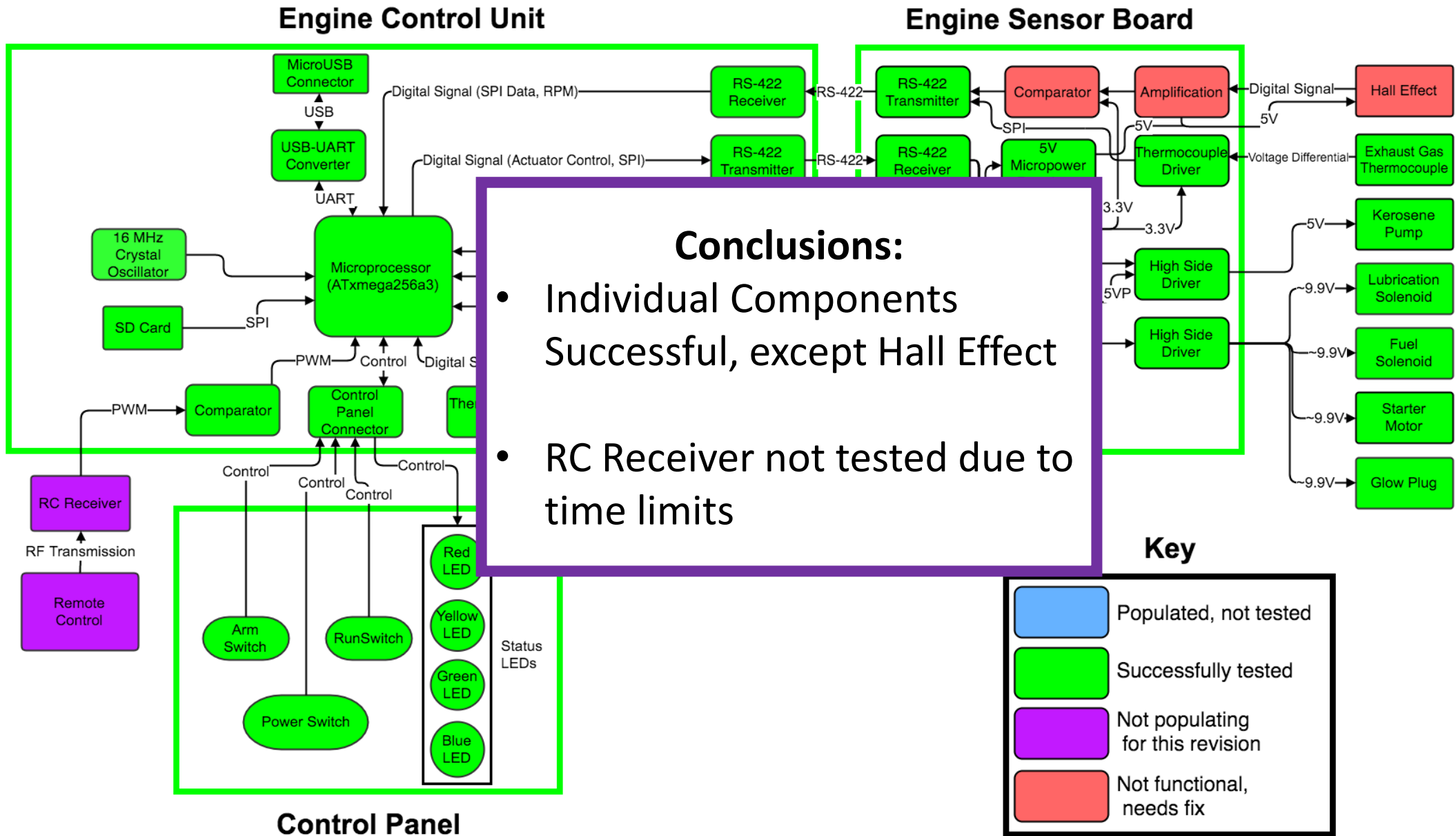
Control Volume model can predict the performance of the P90-RXi

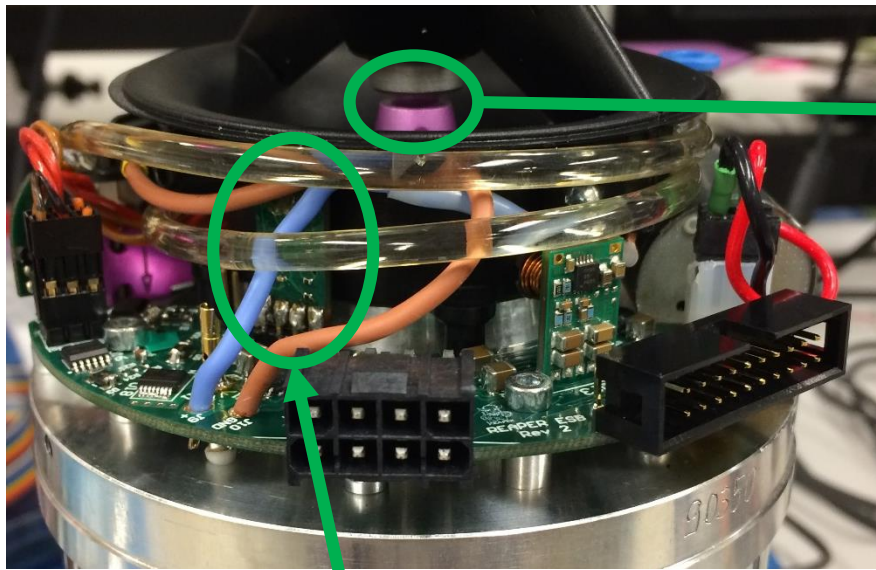
Engine Electronics

Goal: Safely control engine and save testing data

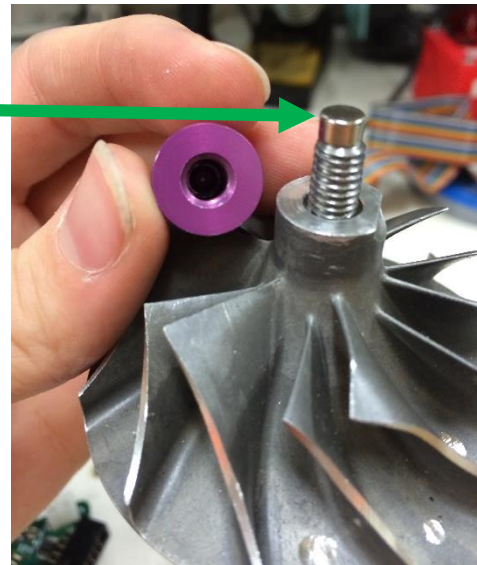
Motivation: Stock electronics cannot be modified to work with recuperating engine



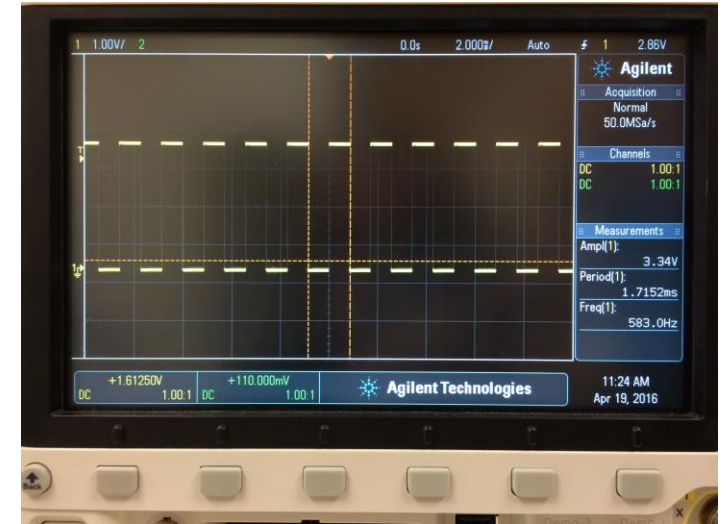




Hall Effect Integration

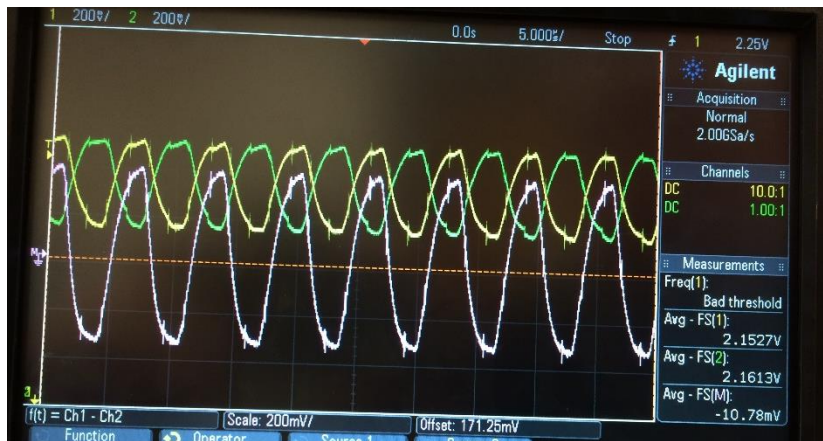


Internal Magnet



Initial Testing – Successful

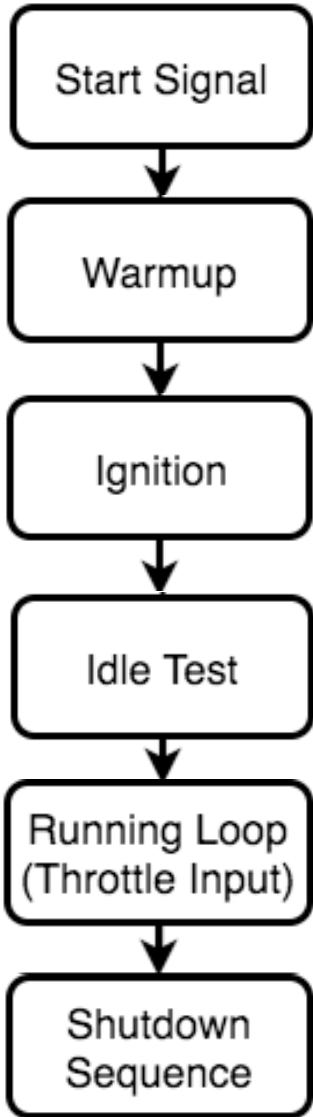
~20mV
Difference →
Amplified for
microcontroller



Raw Differential Output



Issue Encountered after Testing – Signal not square



Wait for ARM and RUN signals from Control Box

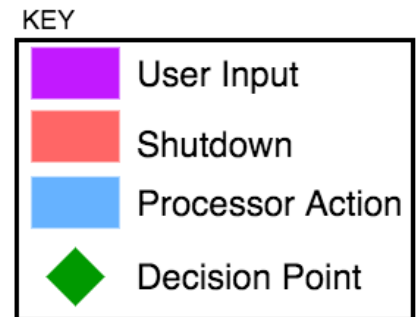
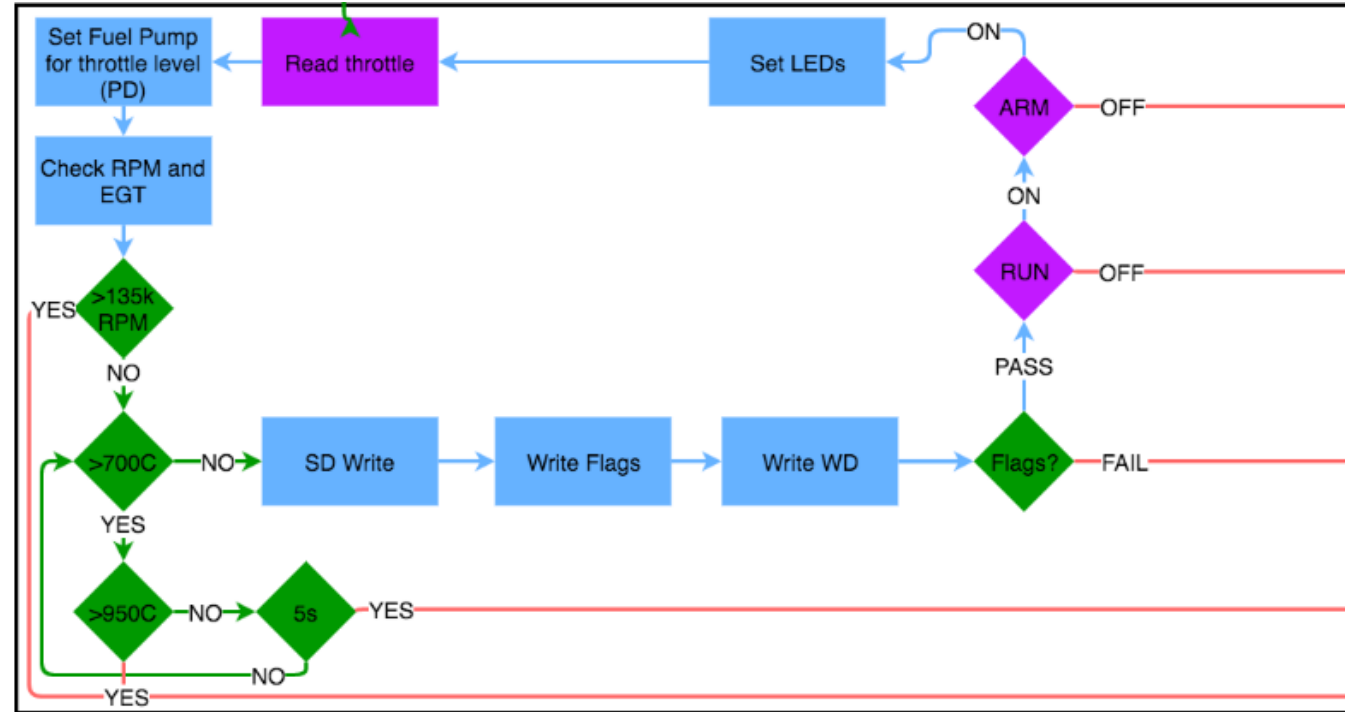
Spin starter motor to start compression

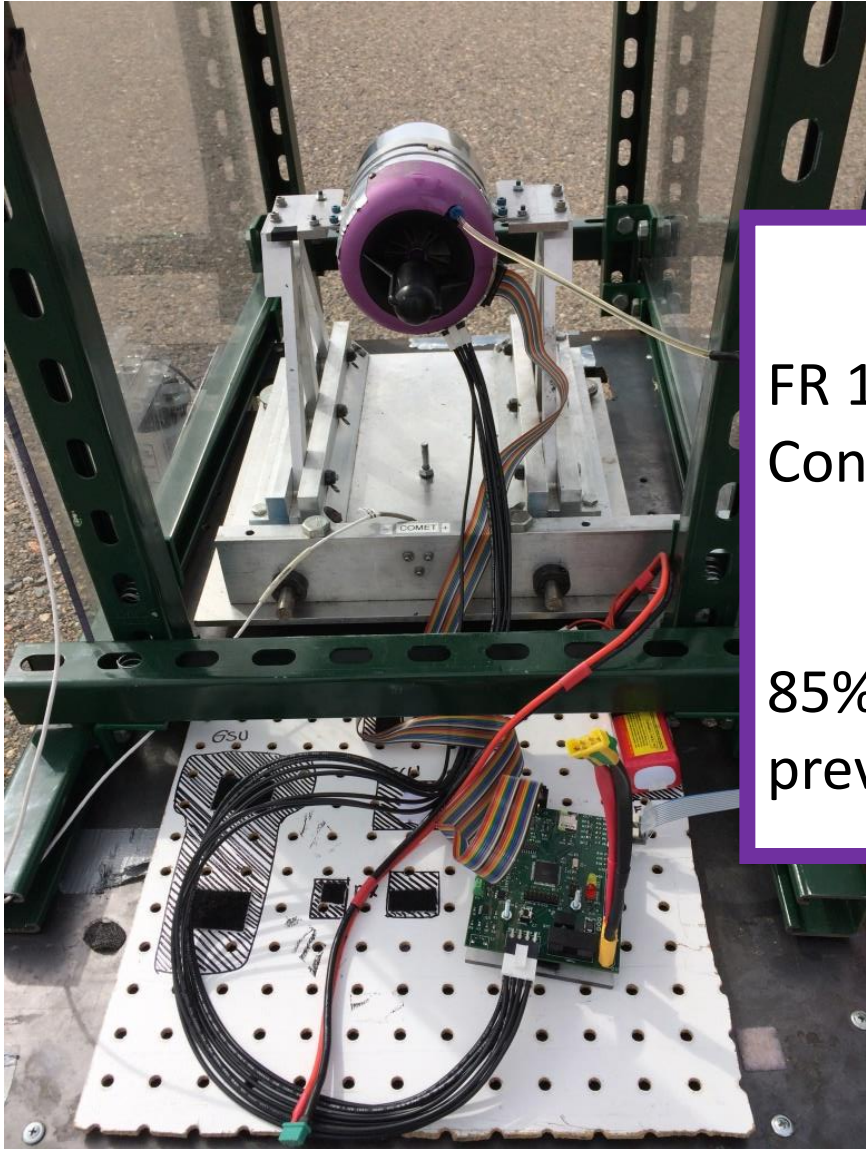
Heat glow plug; add fuel; check temperature and RPM for combustion

Set fuel pump to idle; tweak as needed until idle RPM (35,000) is reached

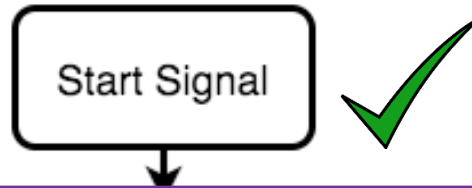
Set fuel pump to reach RPM correlating with throttle level; check safeties and switches

Run starter motor until engine is below 80°C

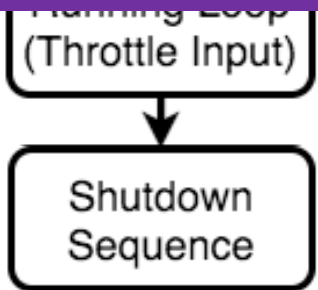




Engine Test at Boulder Airport



Conclusions:
FR 1: Engine Electronics Shall Control the Engine.
↓
85% complete – Time limitations prevent full verification

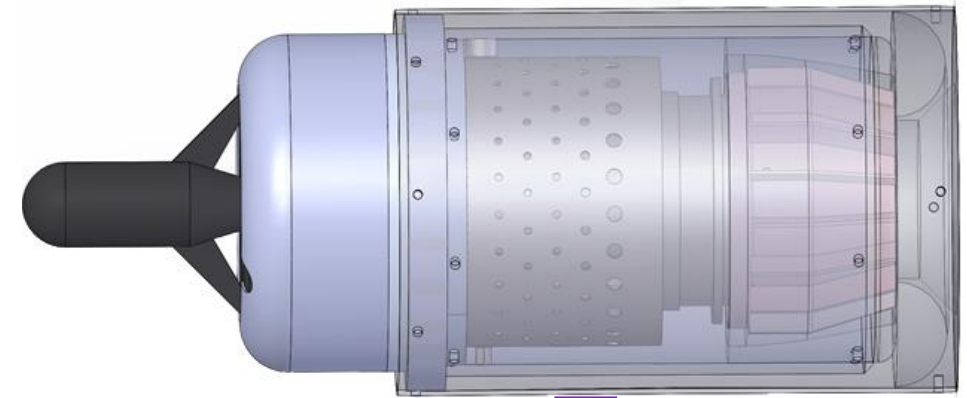


- Actuators ON ✓
- RPM Readings ✓
- Temperature Readings ✓
- Fuel Ignition X

- Possibly due to:
- Under/over fueling
 - Glow plug heat too low

Systems Engineering

- **Design Solution: Top Down**
 - Customer Design Requirement
 - Levels of Success and Functional Requirements
 - Design Concept Selection
 - Heat Exchanger/Engine Control Trade Study
 - Risk Analysis
 - Engine Control Trade Study
 - Full Subsystem Design
 - CAD model, Component/Material Selection
- **Development, Integration, Testing: Bottom Up**
 - Benchtop Testing, Mechanical Fit Check
 - Heat Exchanger Validation
 - Full System Test



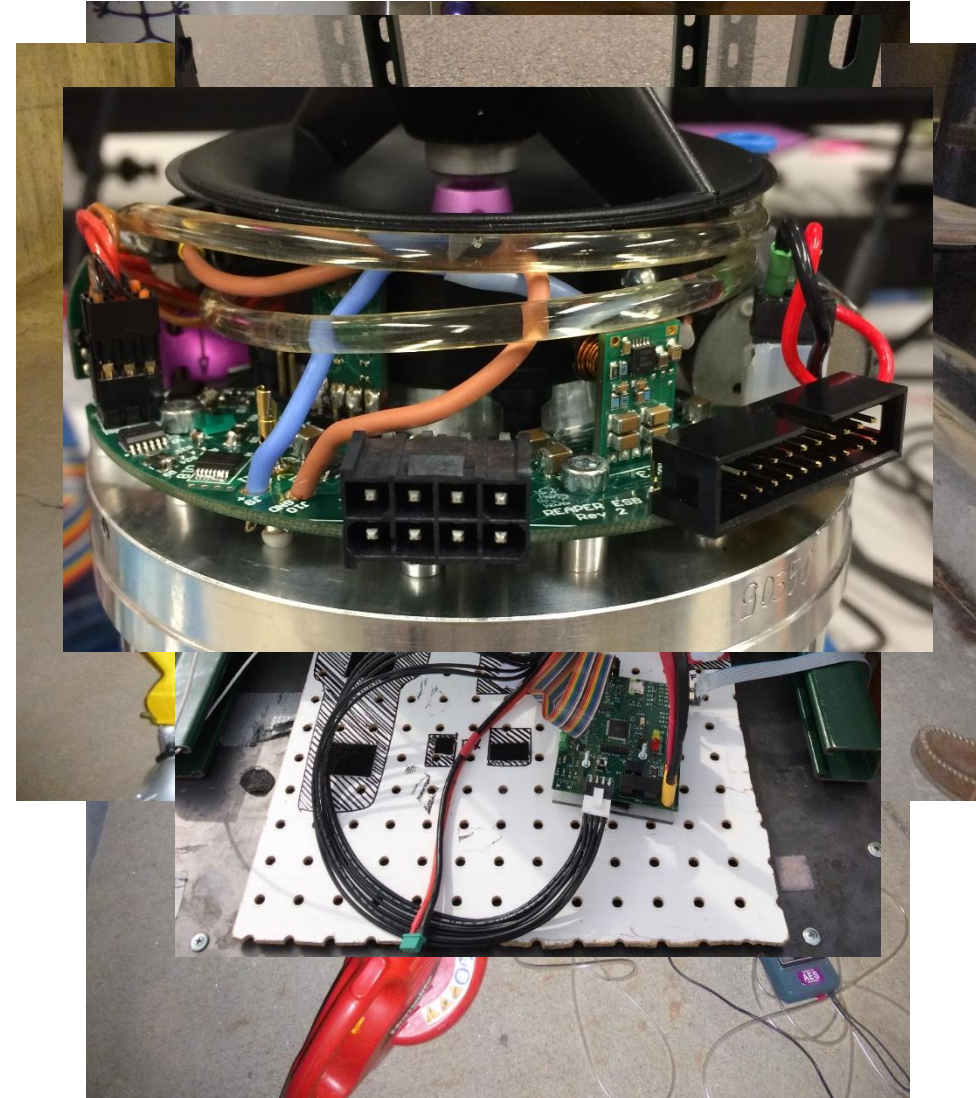
- Key Trade Study

- Engine Control → Custom Engine Control Unit and Engine Sensor Board
- Heat Exchanger → Gas to Gas Heat Transfer

	Weight	Stock	Custom PCB	Programmable	
	Weight	Heat Pipe	Gas-Gas Multi-pass	Gas-Gas Single Passed Finned	Gas-Gas Counter Flow
Mass	10	1	2	4	1
Volume	10	3	2	3	3
Manufacturability/ Cost	30	1	3	4	3
Integrity	30	4	1	2	2
Flow Impedance	20	5	4	5	1
Total	100	2.9	2.4	3.5	2.1

- Increase weight of development time
- Increase weight of flow impedance
- Will not change overall outcome
- Potential change in trade outcome

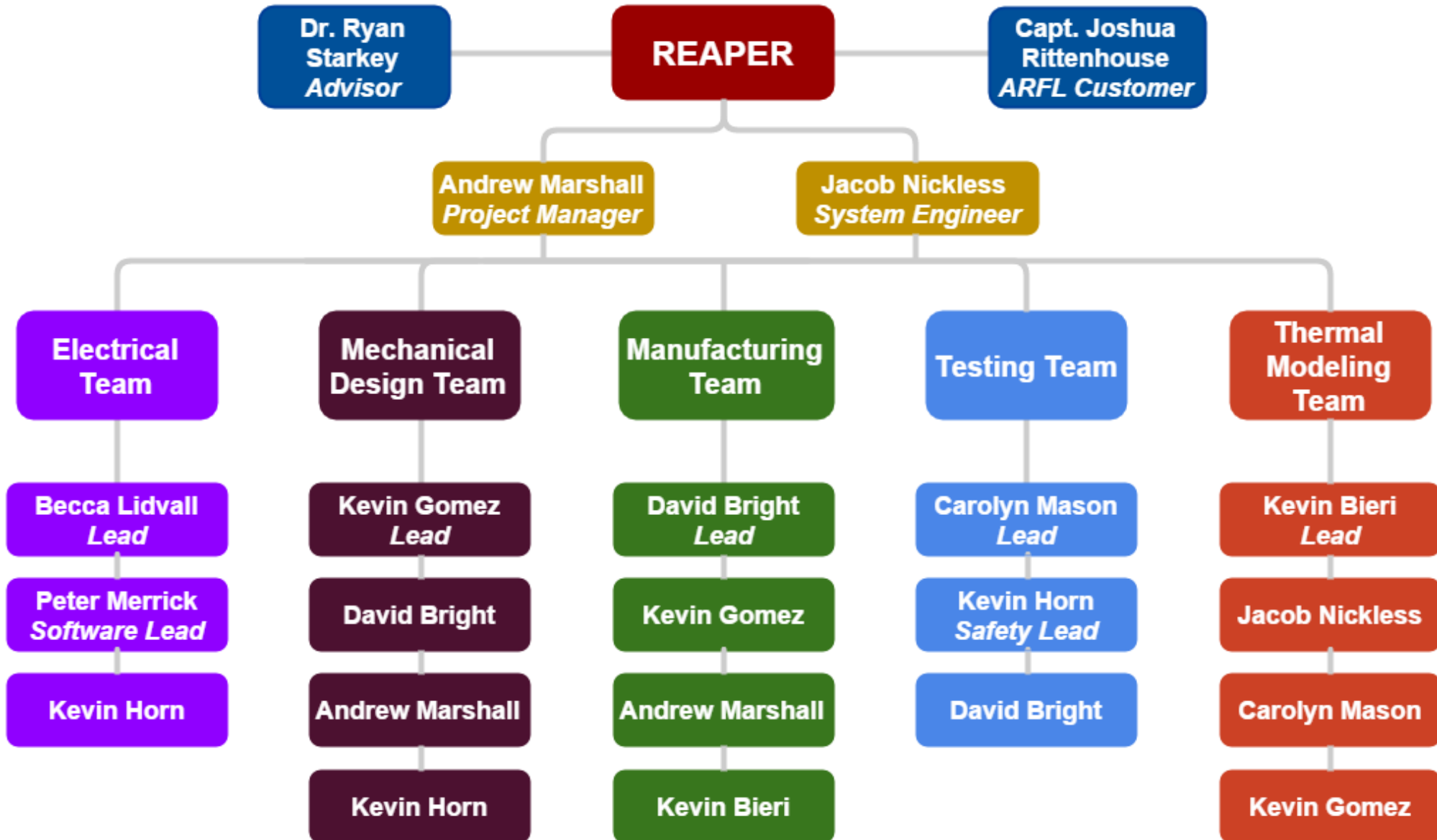
- Expect System Integration Problems
 - Custom electronics took longer to test and integrate
 - Sensors issues caused scheduling slippage
- Plan for Iterations & Allocated Resources Early
 - Iterations were needed to prove model
 - Became main focus of project success
- Risks developed in CDR did not address the electronics and testing scheduling slippage



- Turbo Jet Recuperator Proof of Concept
 - Weight increase of **230%** paired with **4.3%** decrease in TSFC
 - Different manufacturing method and material selection
 - Reduce the weight of recuperator
- Recuperation on Mini-turbo jet turbine
 - Initial findings show recuperation may not be applicable to turbo jet
 - Possible application to shaft work engine
- Future Work
 - Hall Effects sensor debugging
 - Full stock engine characterization
 - Recuperator integration testing
 - Iteration of high level design → Heat Pipes

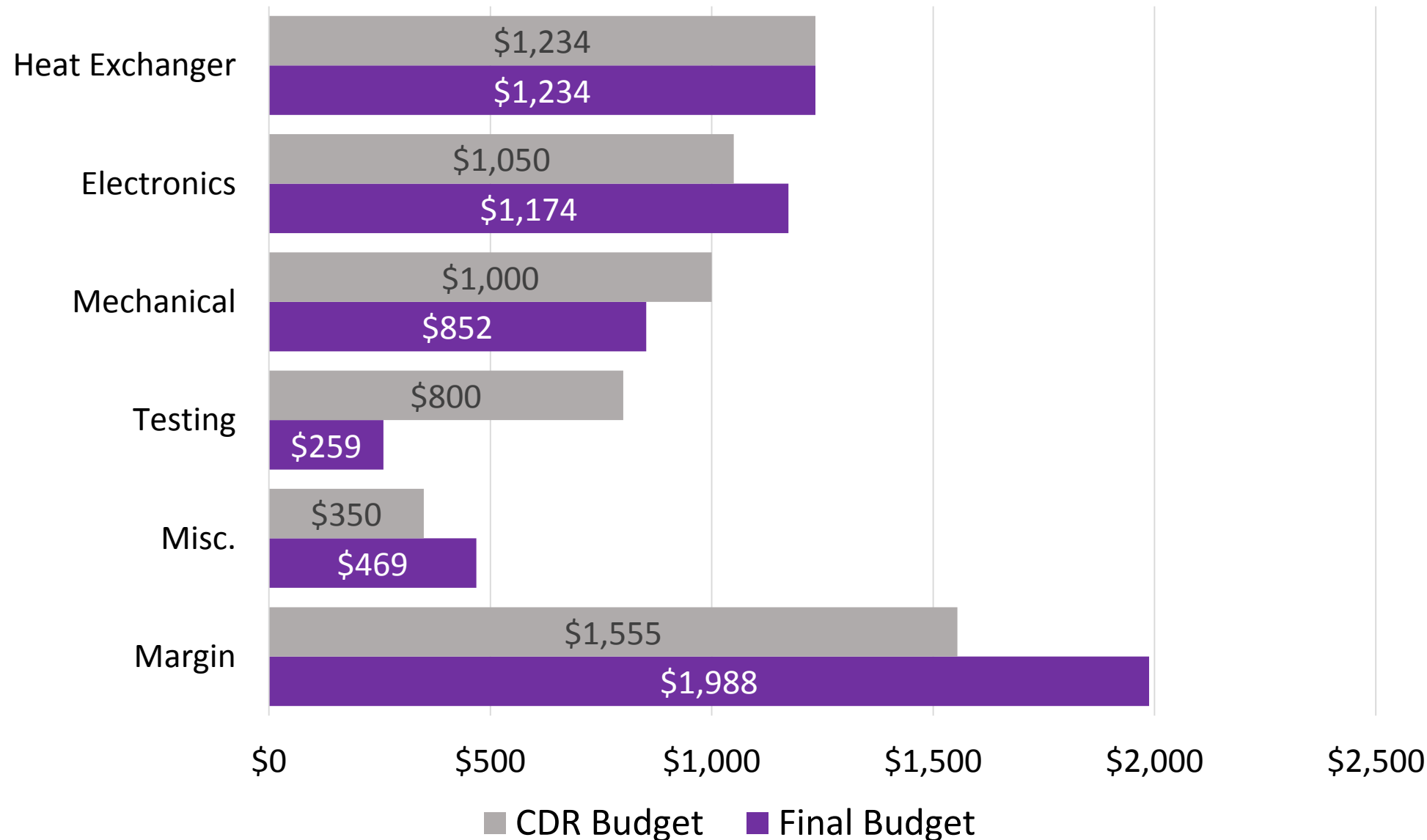


Project Management



- Weekly Meetings
 - Prepared agenda based on previous meetings to cover
 - Summarize meeting/action items
- Centralized team communication with GroupMe messenger
 - Extremely effective for real-time updates
 - Provided scheduling ability for testing-day attendance RSVP's
- Utilized Microsoft Project to track project progress
 - Extremely versatile and powerful project tracking
- Centralized budget and financial obligations to CFO
 - Streamlined purchases and provided flexibility with last minute purchases

- Weekly Meetings
 - Having an agenda is most effective
 - Keep track of and follow up on action items frequently
 - Ensure team members always have a task to work on
- Microsoft Project
 - Should have been continuously updated
 - Sometimes difficult to use
- JetCat
 - Unreliable with impractical lead times



CDR Budget

- Budget: \$5,975
- Expenses: \$4,420

Final Budget

- Spent: \$3,987

Difference from CDR:

- \$446 unspent

EEF Contribution:

- \$1,131.20

Engine purchase:

- \$2,240

Assumptions:

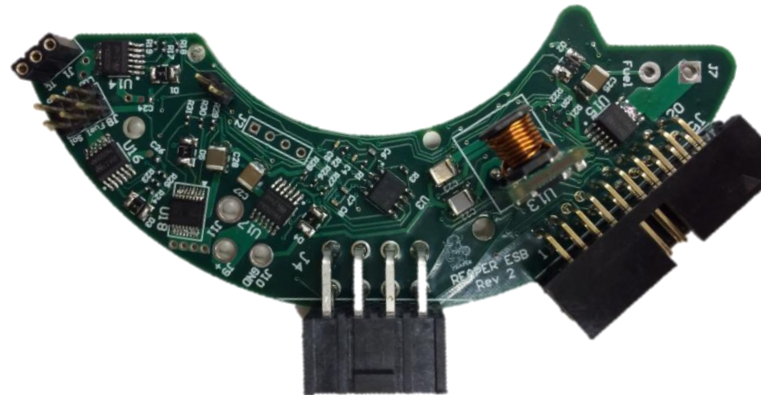
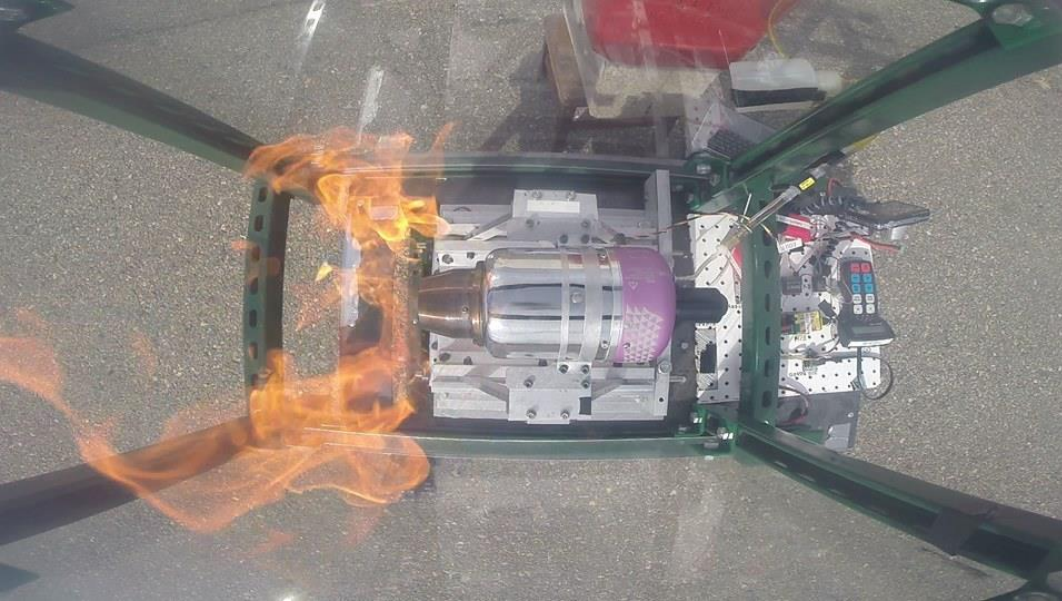
\$65,000 annual salary of entry-level aerospace engineers
Full Time Equivalent of 2080 hours/year
+Overhead rate of 200%

Total Hours	4169.4 hours
Total Direct Labor Cost	\$130,293.75
Overhead Rate	200%
Overhead Cost	\$260,587.50
Material Cost	\$7,000
Total Industry Cost	\$397,881.25

REAPER would like to thank:

- The Project Advisory Board
- Professor Ryan Starkey
- Course Assistant, Thomas Green
- Trudy Schwartz, Bobby Hodgkinson, Matt Rhode
- Previous engine teams (MEDUSA, COMET)
- Boulder Municipal Airport
- Air Force Research Lab

Questions?





Backup Slides



Mechanical Backup Slides

Full Mechanical System

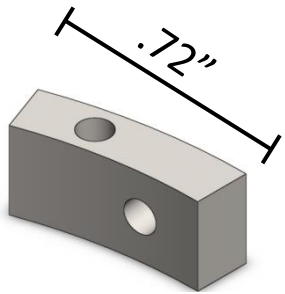


Total Added Weight: 3.36 kg

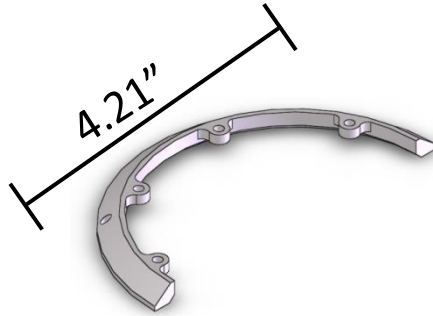
234 % Mass Increase

Different Materials or total redesign needed
to meet 50% mass increase requirement
(130% increase all Titanium)

Other Mechanical Components



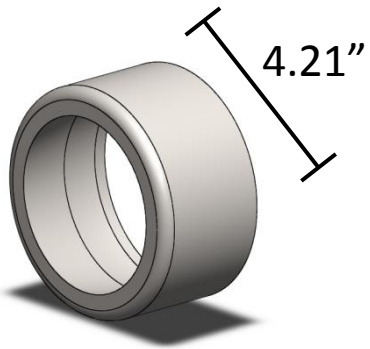
Mounting Blocks (x4)
4.5 g



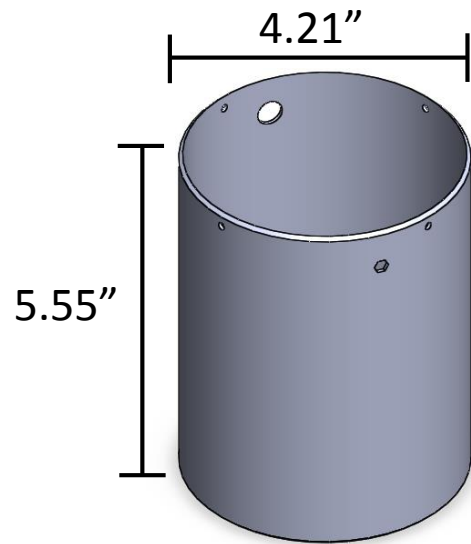
Mount Brackets (x2)
44.5 g



Forward Ring
220 g

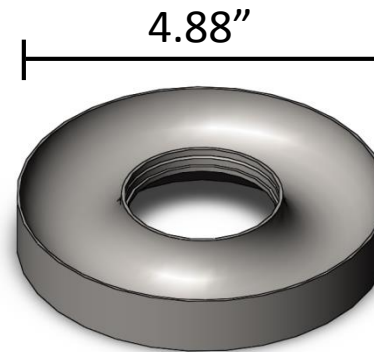


Nozzle Shroud



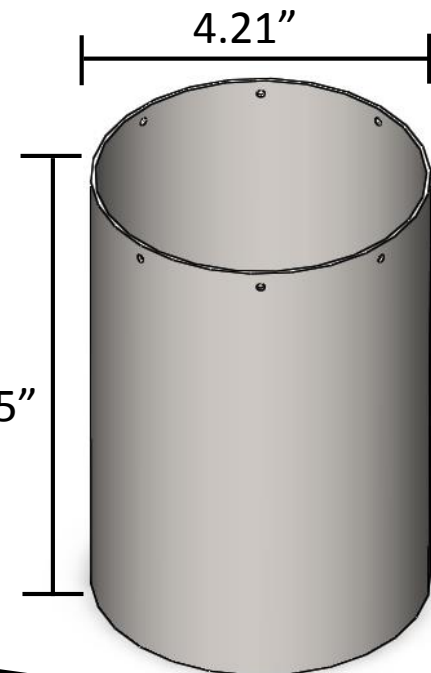
Inner Casing

1.68 kg



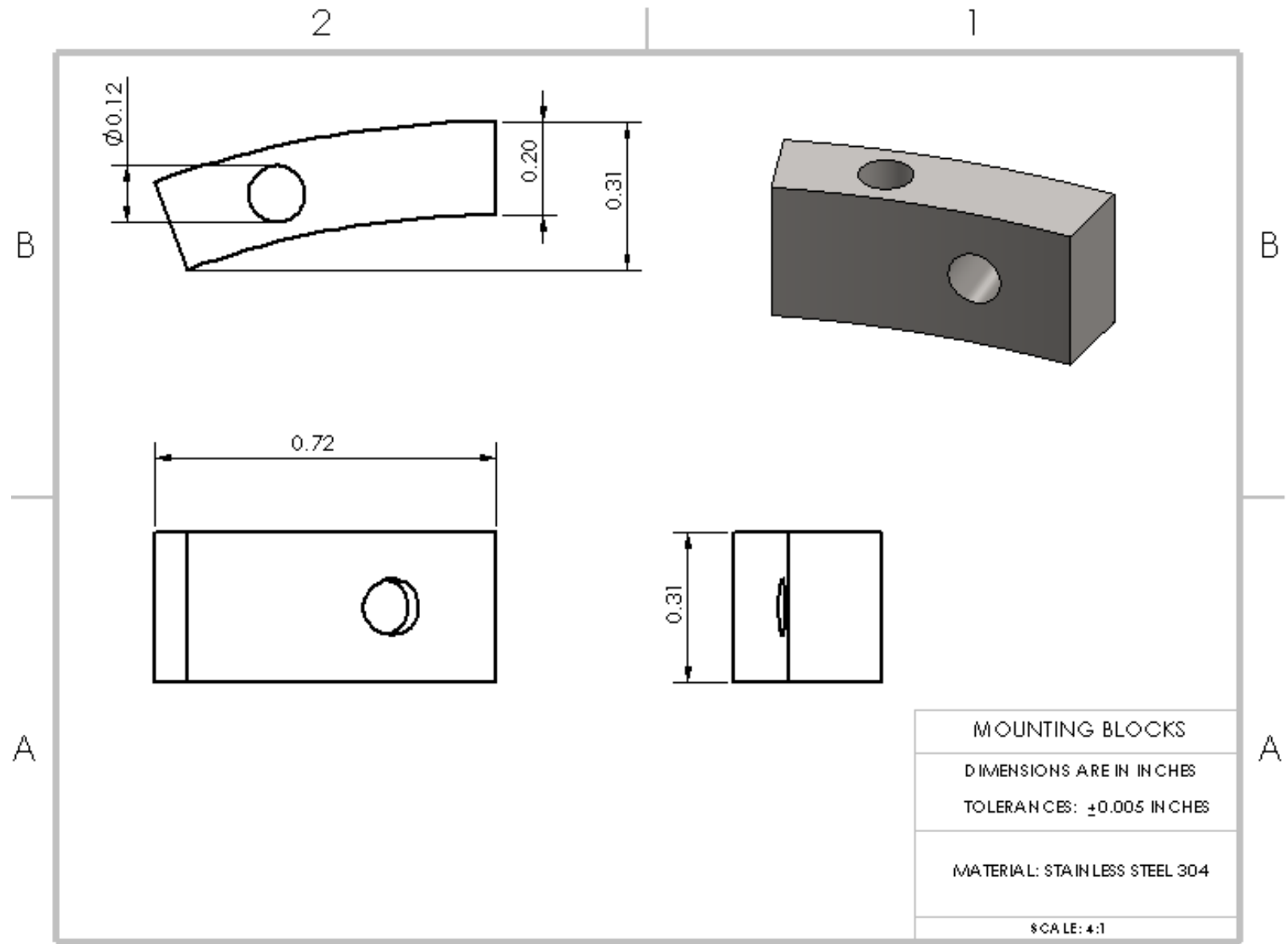
End Cap

1.33 kg

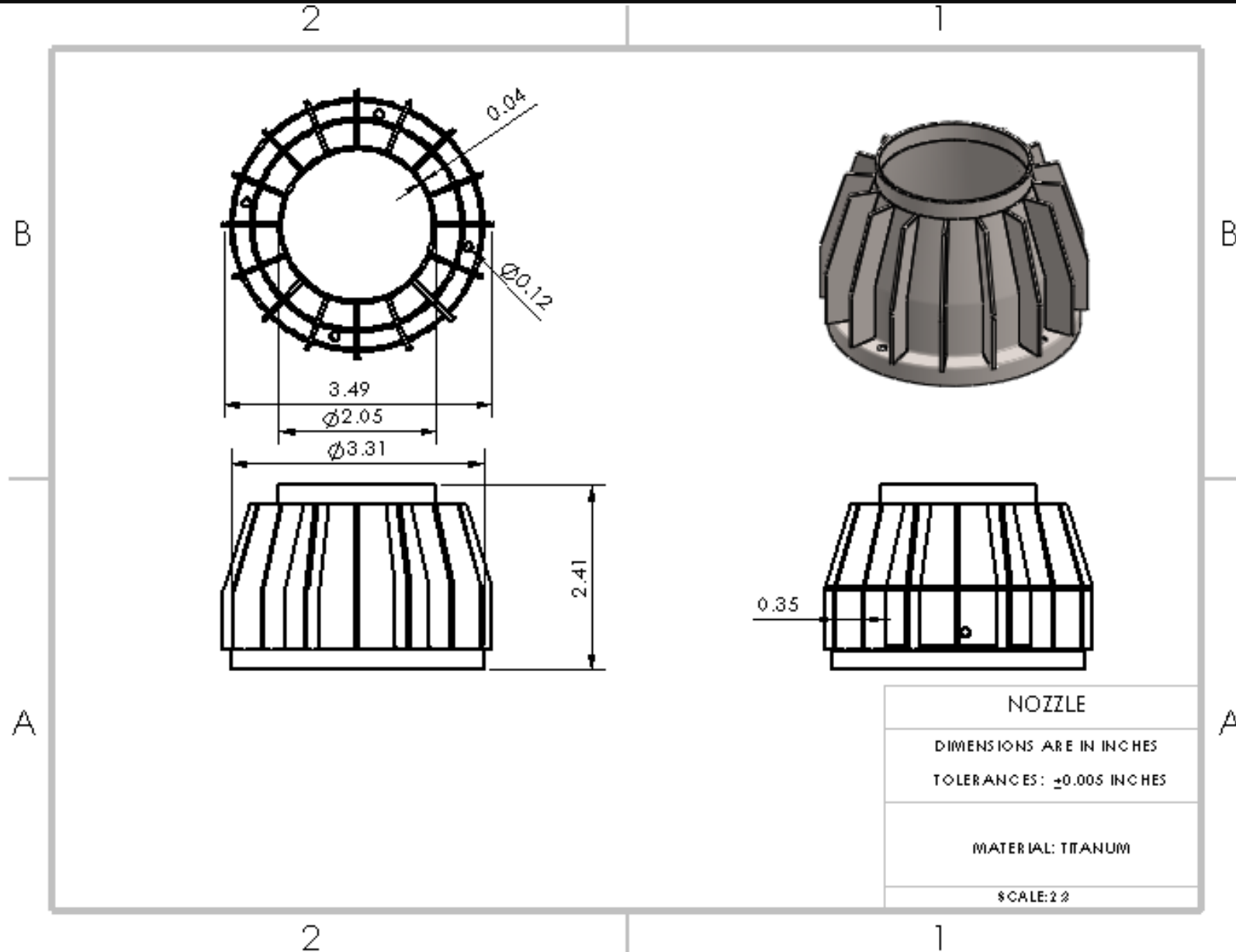


Outer Casing

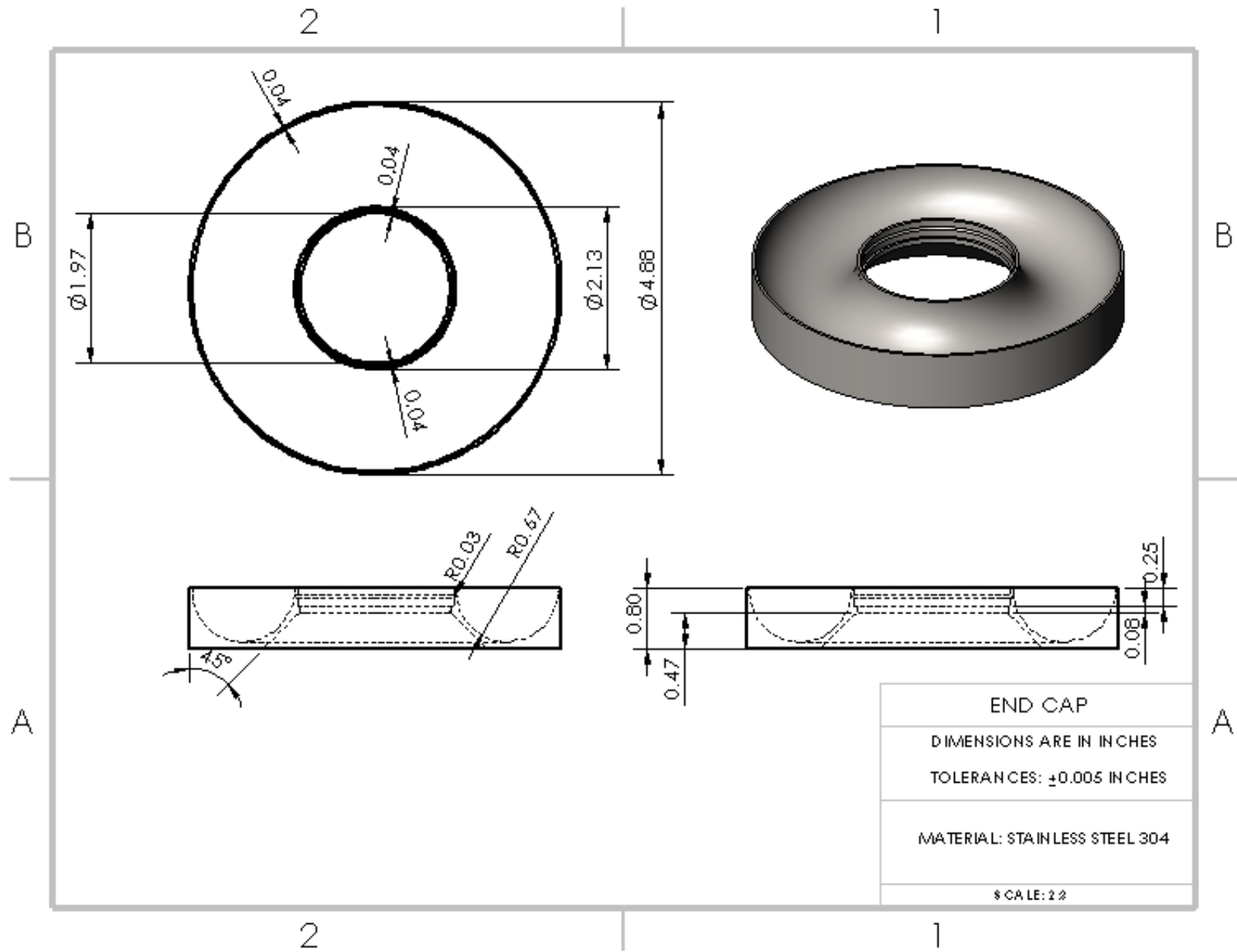
Mounting Blocks: Dimensioned Drawing



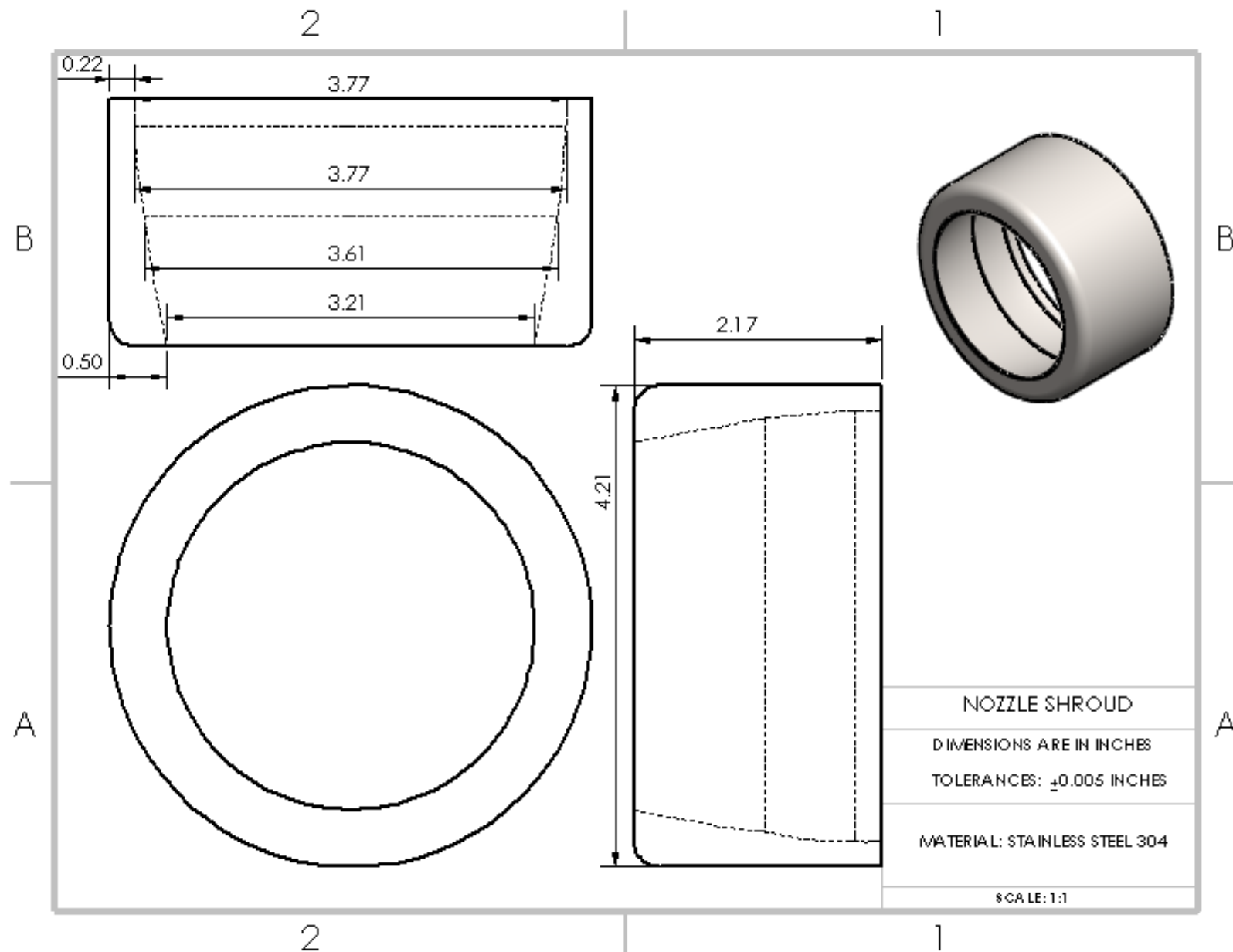
Nozzle/Heat Exchanger: Dimensioned Drawing



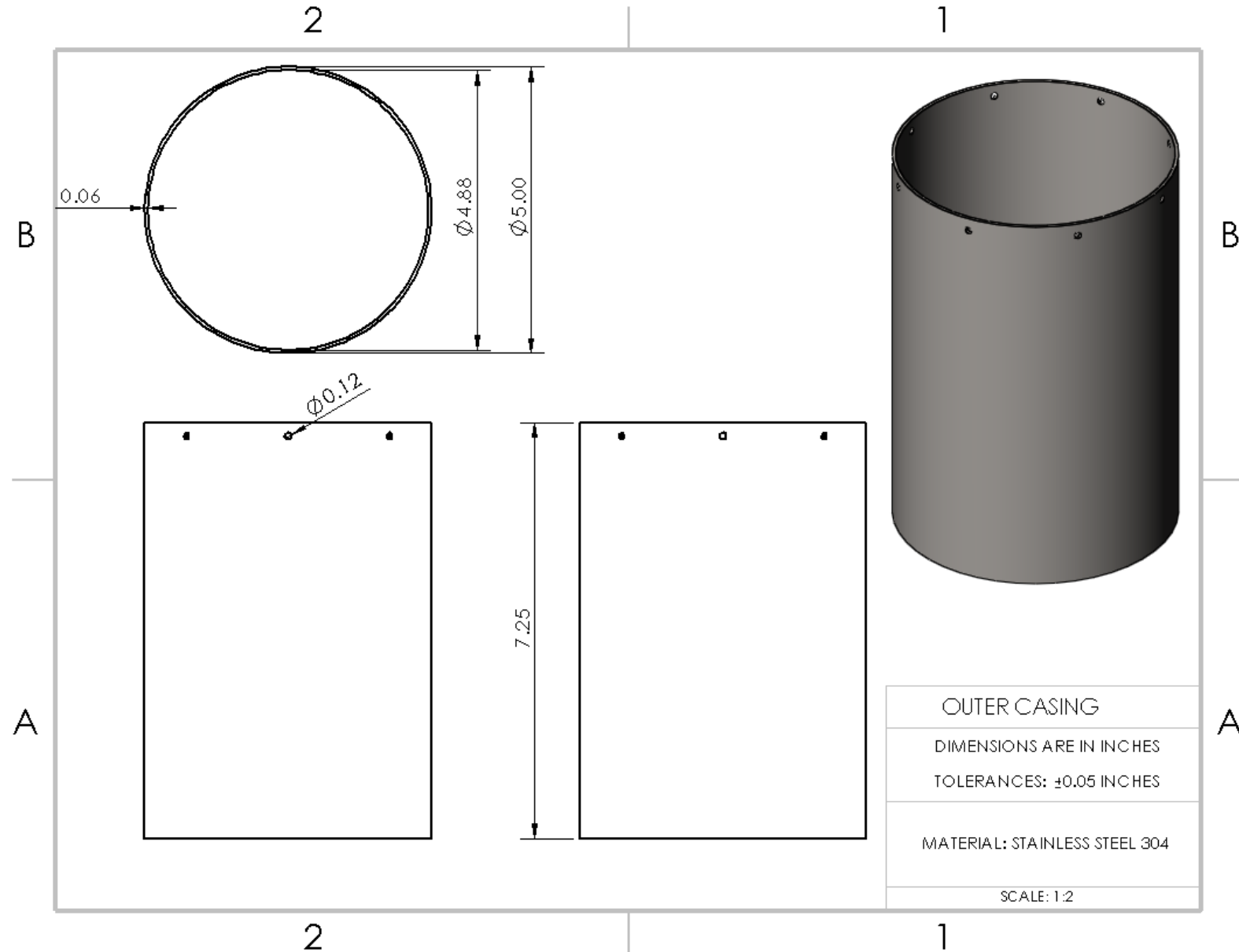
End Cap: Dimensioned Drawing



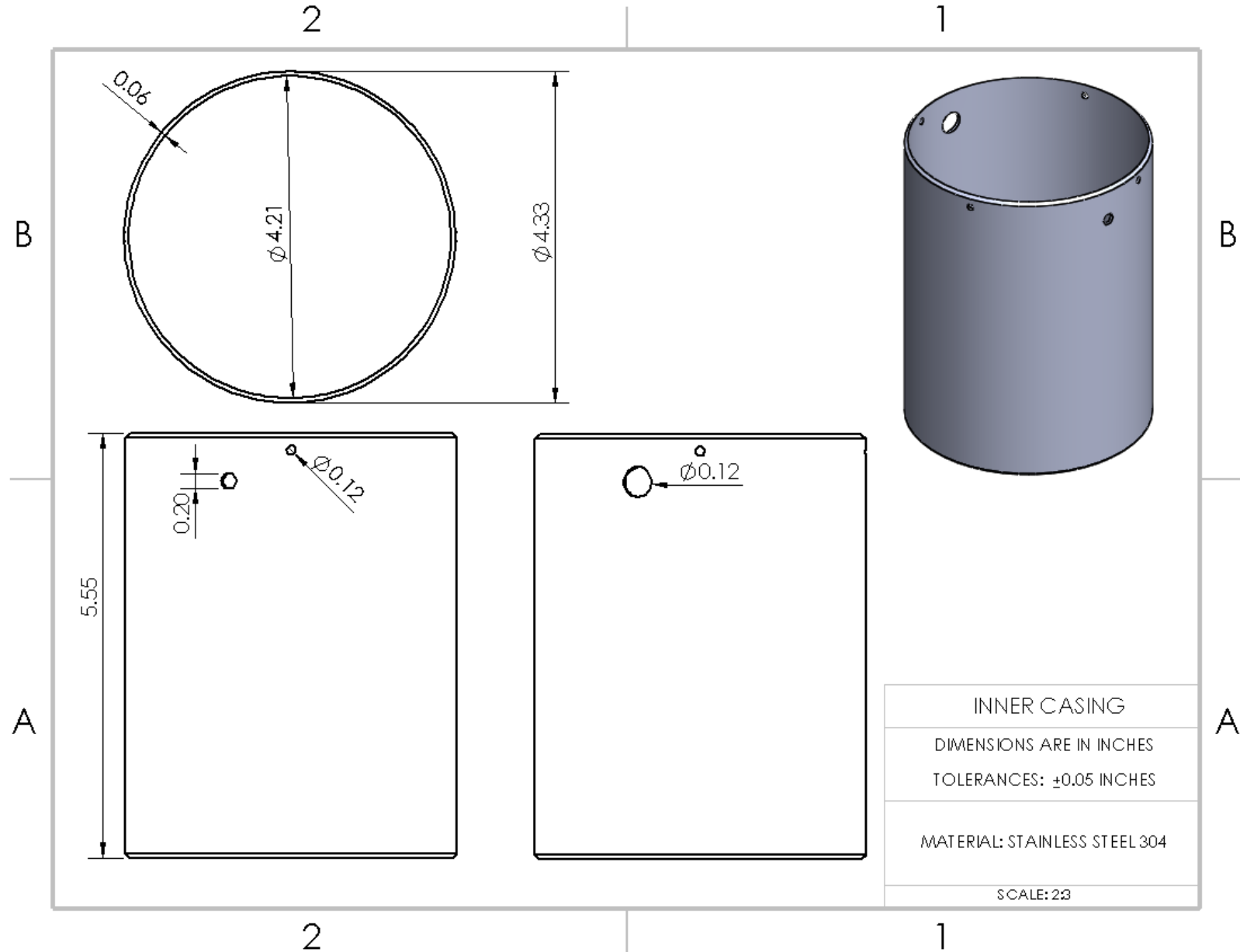
Nozzle Shroud: Dimensioned Drawing



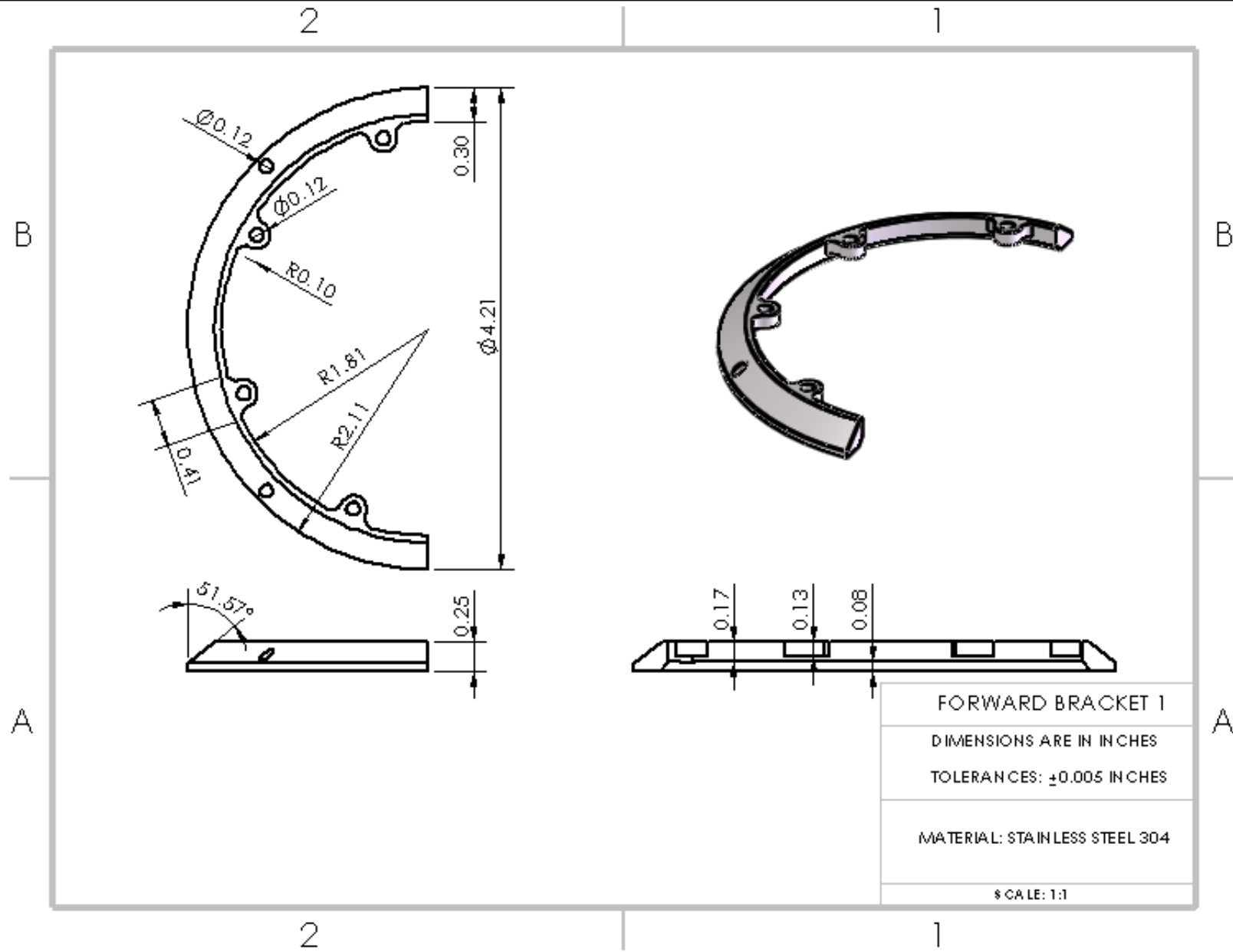
Outer Casing: Dimensioned Drawing



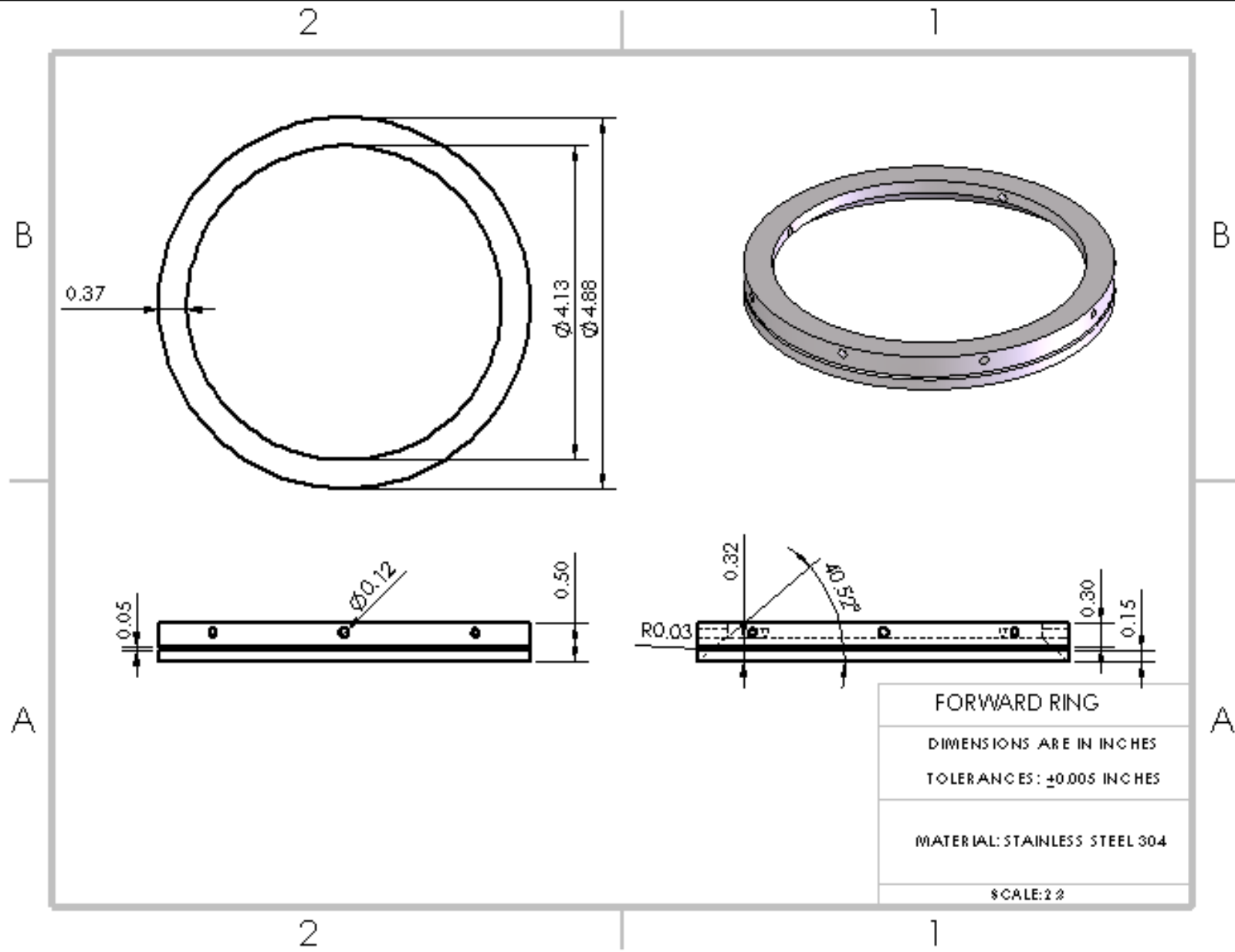
Inner Casing: Dimensioned Drawing



Forward Brackets: Dimensioned Drawing



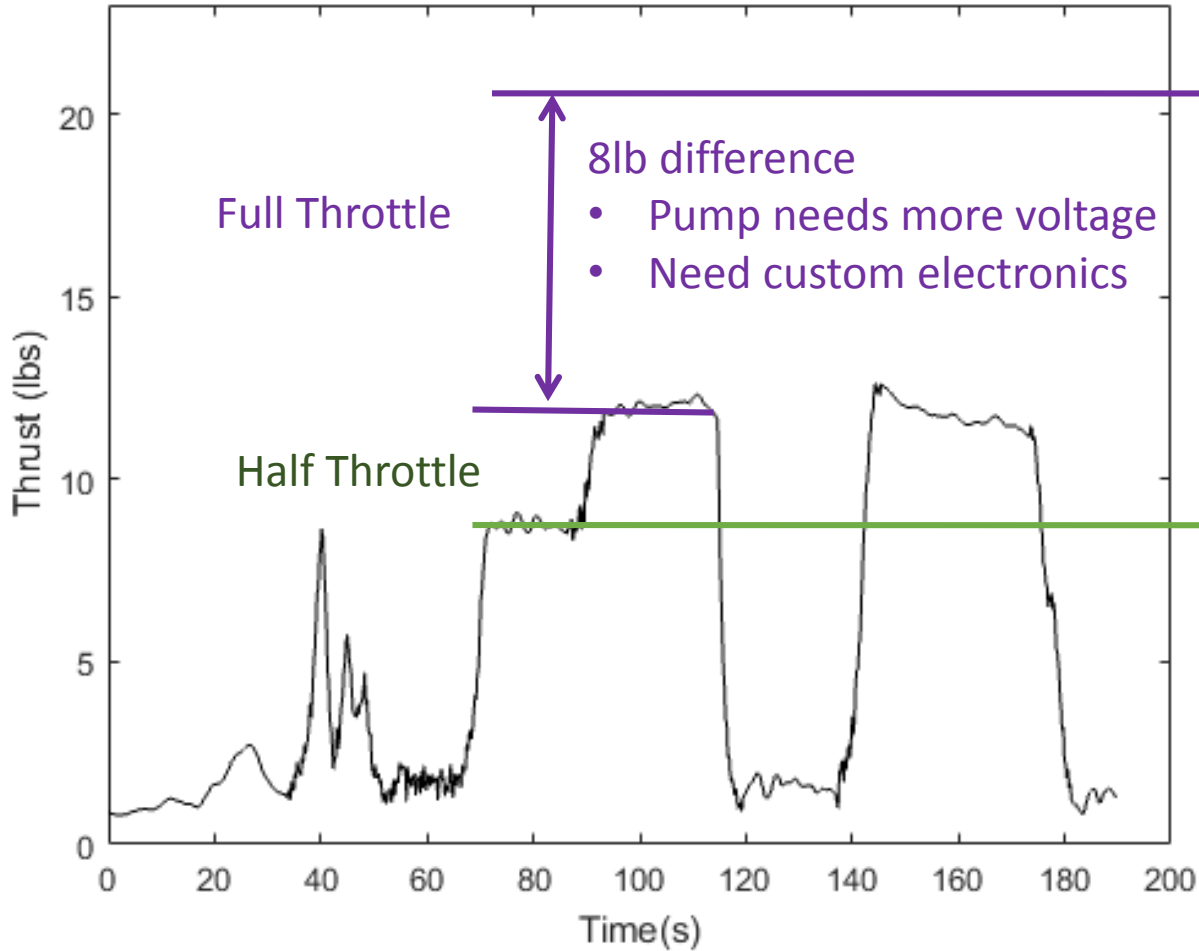
Forward Ring: Dimensioned Drawing





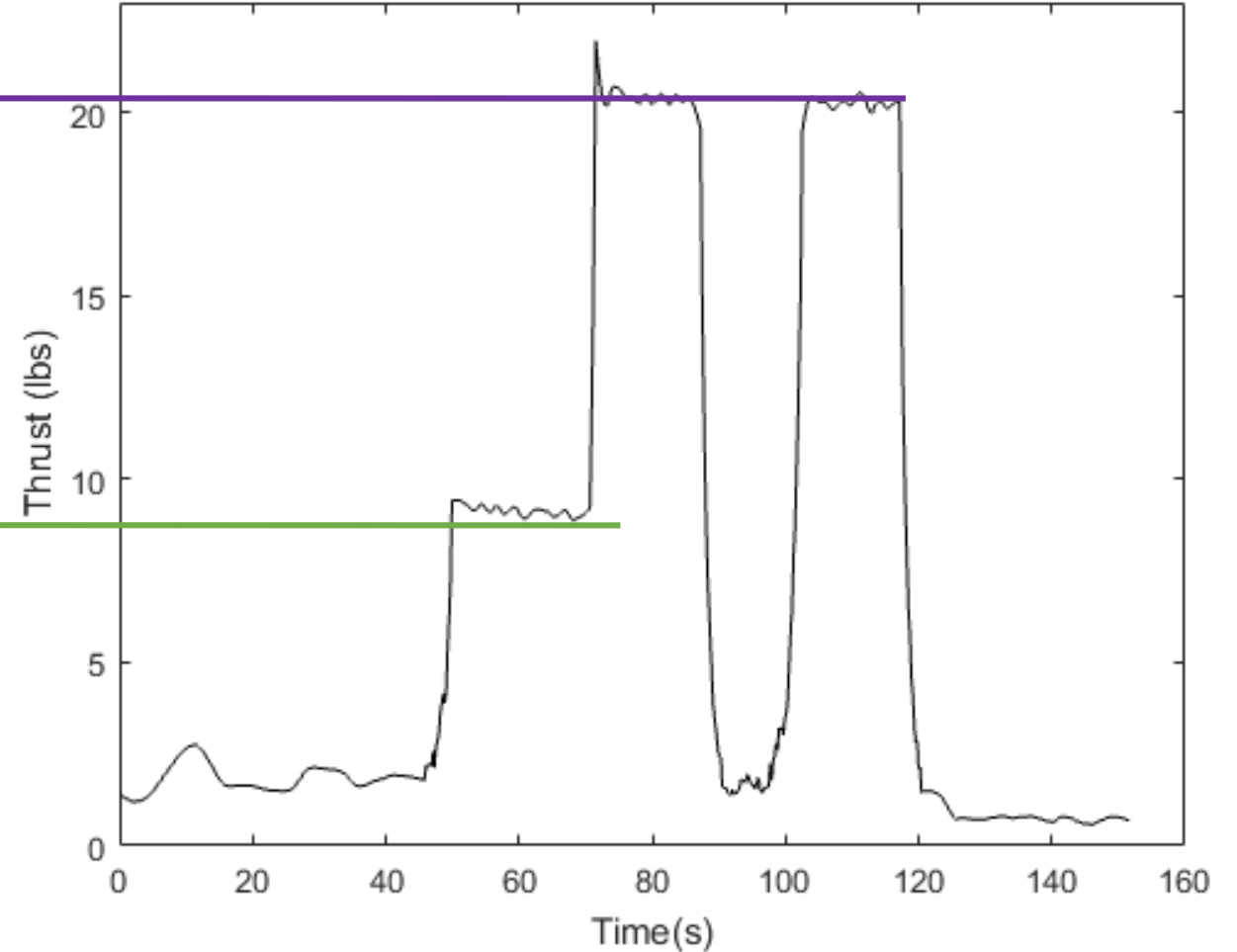
Electrical Backup Slides

With Fuel Flow Sensor



Max RPM = 109,500

Without Fuel Flow



Max RPM = 130,000

Sensor	Measures	Error	Use	Error Effect
Thermocouple	Exhaust Gas Temp	± 3 °C	Engine Status during Test	Low
Hall Effect	Shaft RPM	$\pm 0.5\%$	Engine Stats during Test	Low
Load Cell	Engine Thrust	$\pm 3\%$	Thrust Data for Analysis	High
Fuel Flow	Fuel Flow	$\pm 1\%$	Fuel Flow Data for Analysis	Medium



Thermocouple



Hall Effect



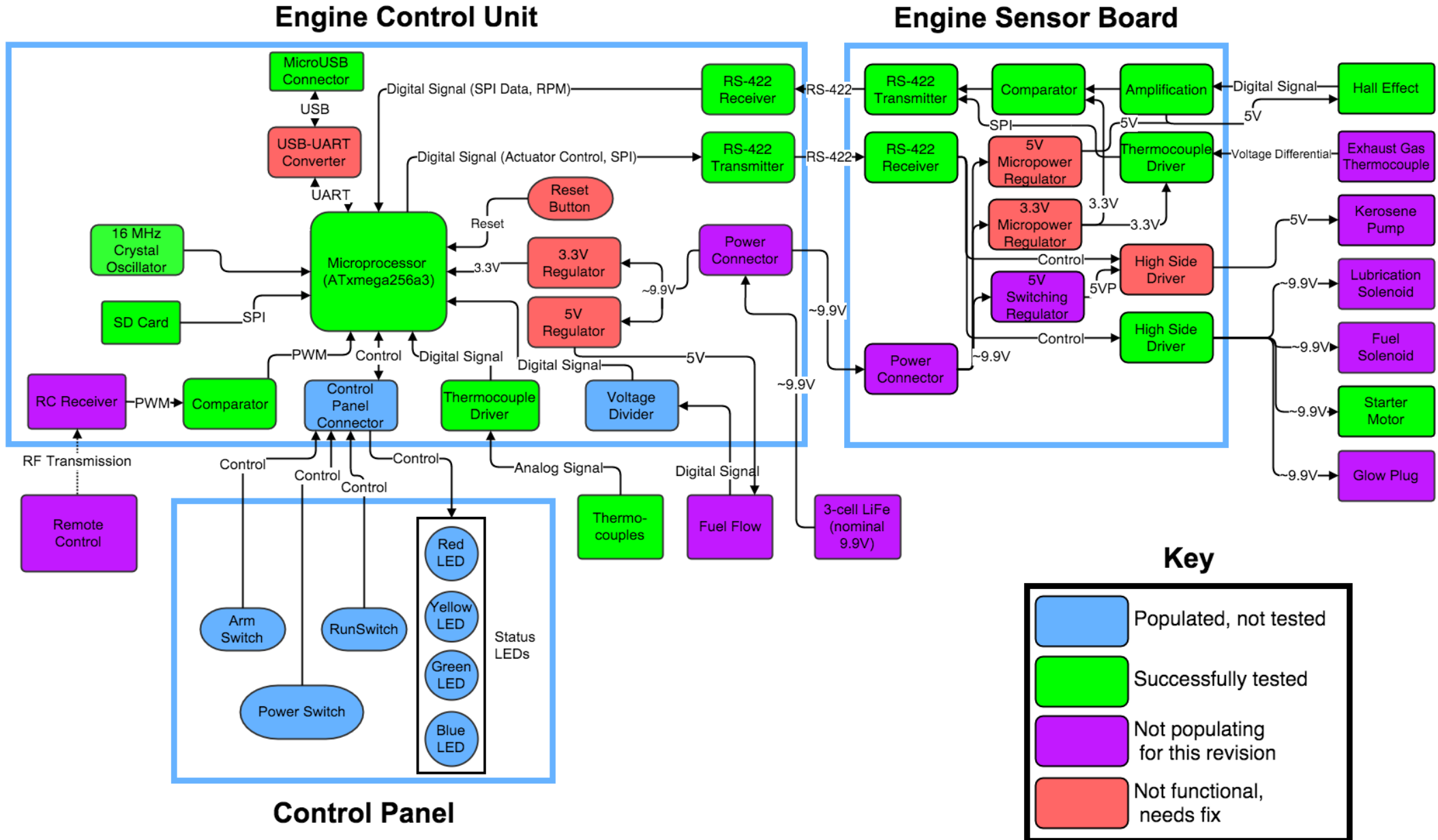
Fuel Flow



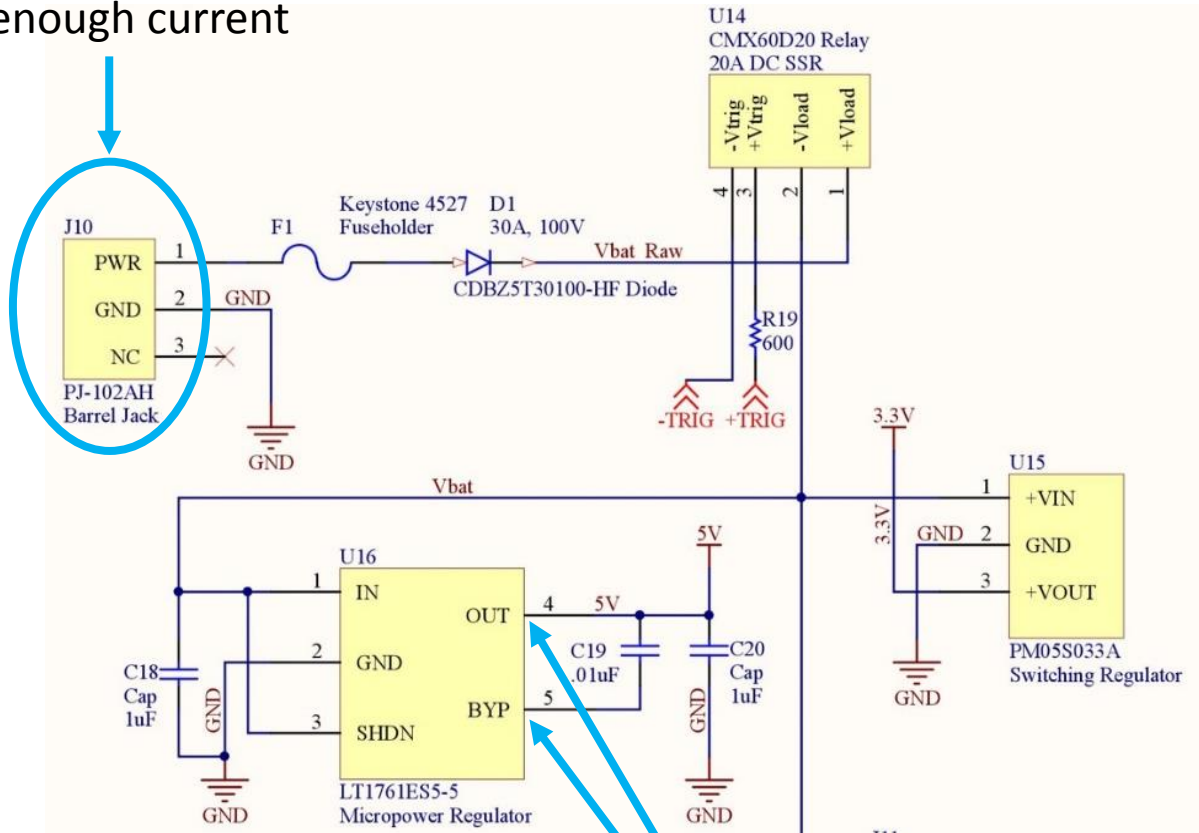
Actuator	Duty Cycle	PWM Frequency	Approx. Voltage	Current (approx.)**	Power	Time On (5 min test)	Energy Draw
Starter Motor	25%*	20 Hz	2.5 V	4.25 A	10.6 W	2 min	142 mAh
Glow Plug	27%*	20 Hz	2.7 V	5.5 A	14.9 W	0.50 min	46 mAh
Lubrication Solenoid	100%	20 Hz	9.9 V	0.3 A	3.0 W	5 min	25 mAh
Fuel Solenoid	100%	20 Hz	9.9 V	0.3 A	3.0 W	5 min	25 mAh
Fuel Pump	20%*	20 Hz	2.0 V	2.0 A	4.0 W	4 min	133 mAh

* Duty cycle changes during time on, so average listed

** Approximation, not measured directly during testing



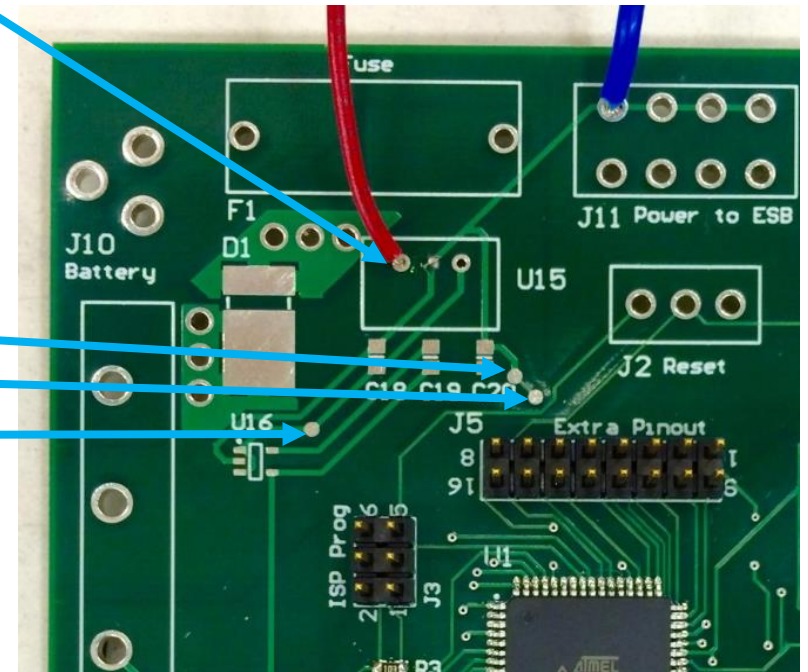
Can't source enough current

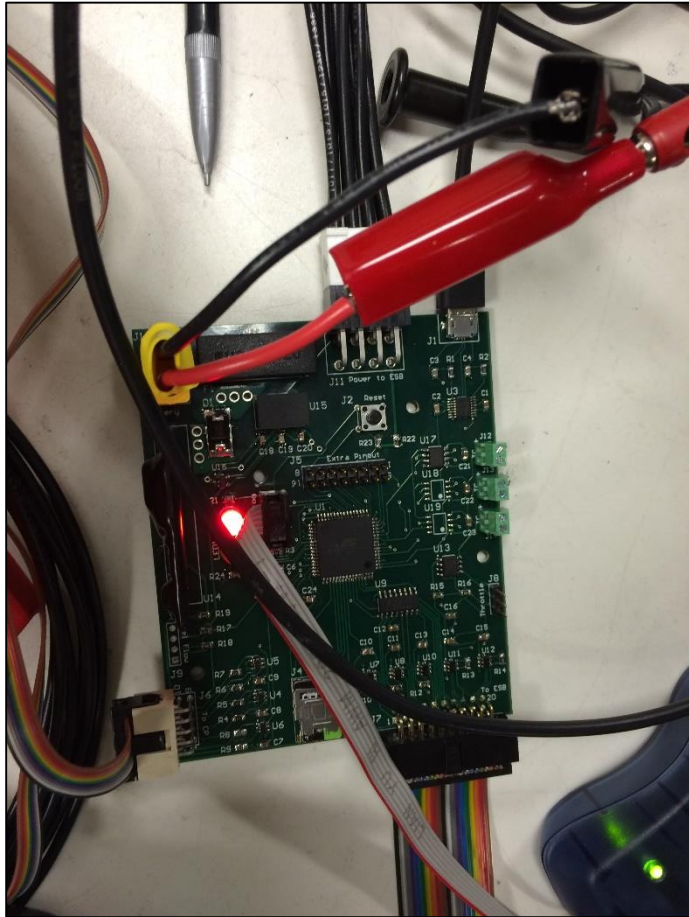


Swapped pins on footprint

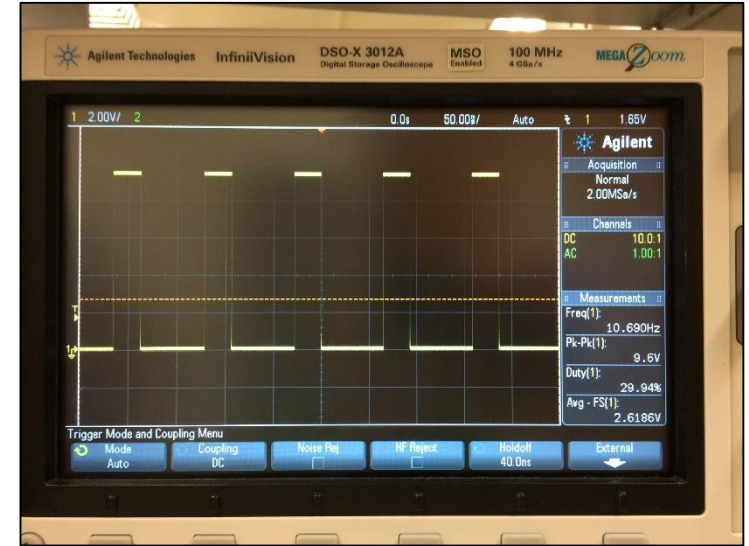
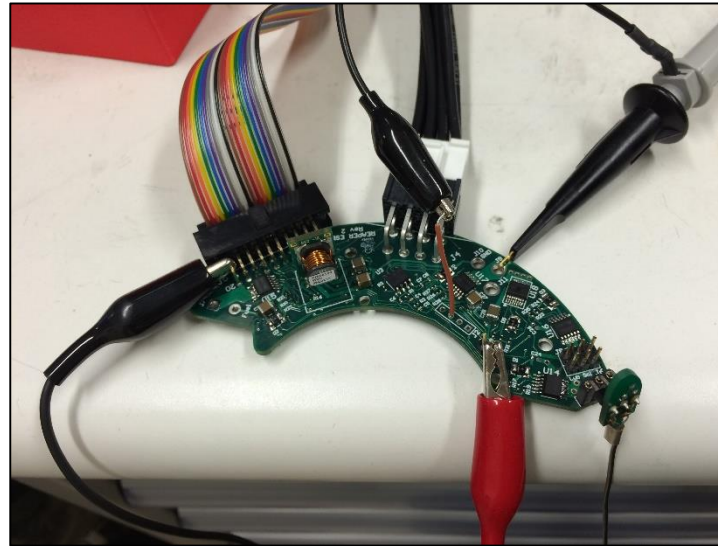
Power Plane Issue

Incorrectly Designed Vias

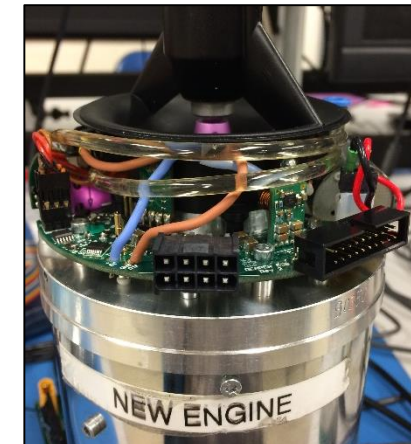
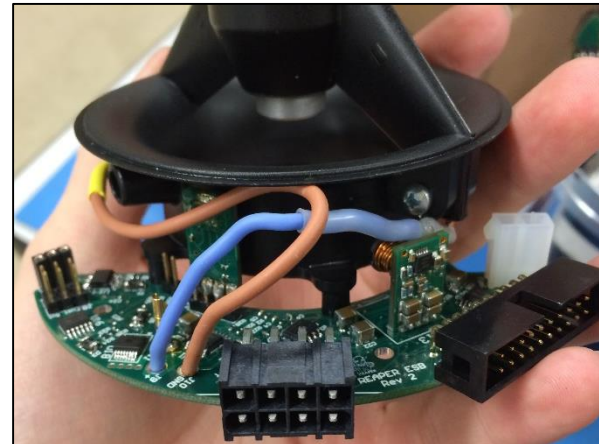




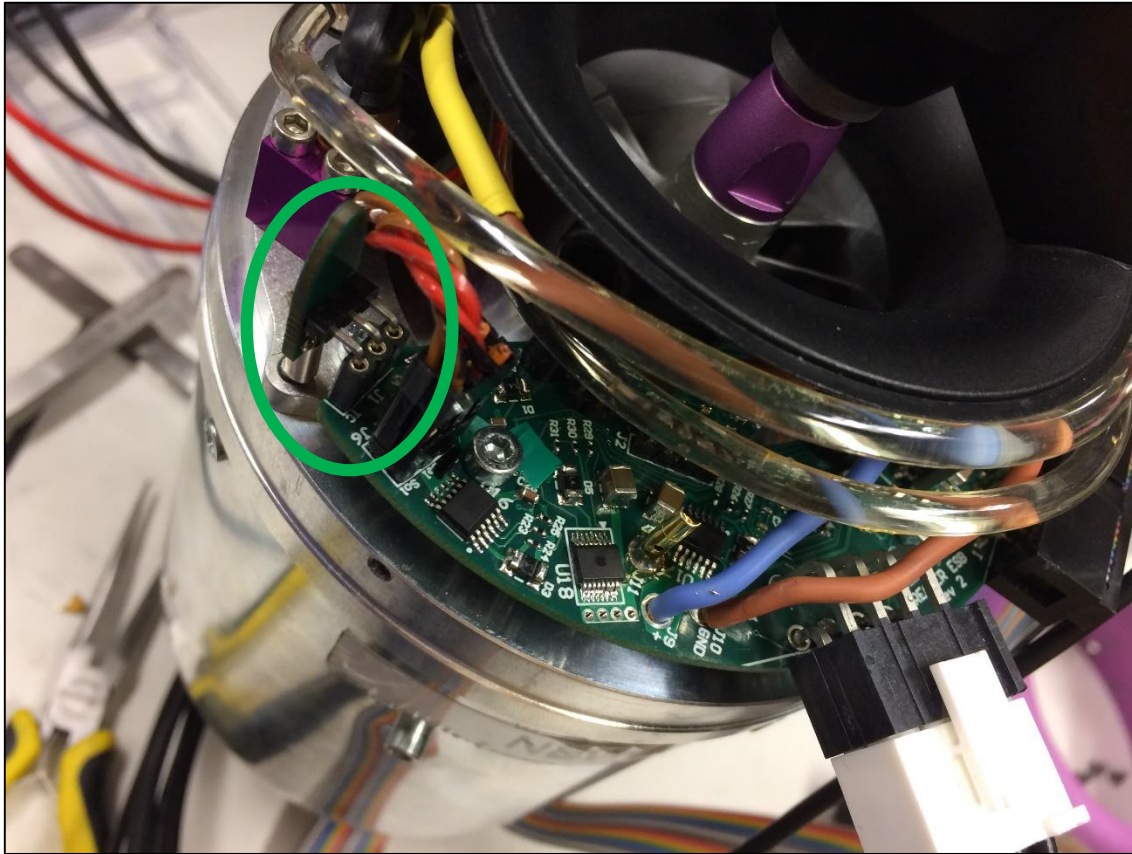
Individual Components Verification - Success



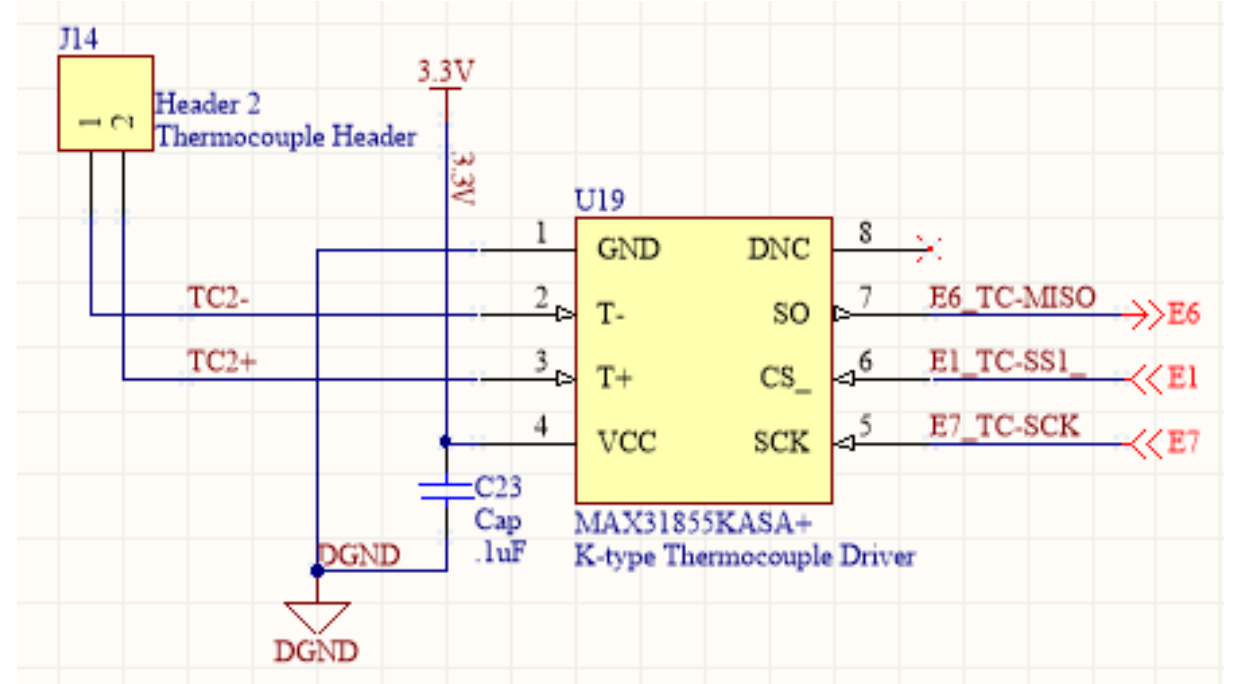
Actuator Signals Verification - Success



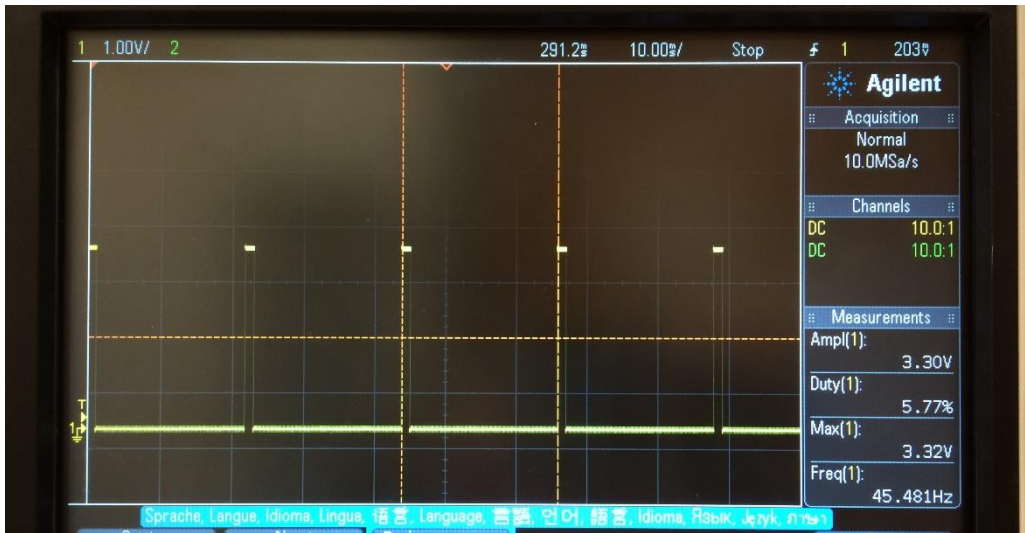
Actuators Integrated and Individually Tested - Success



Thermocouple Integration and Testing - Success



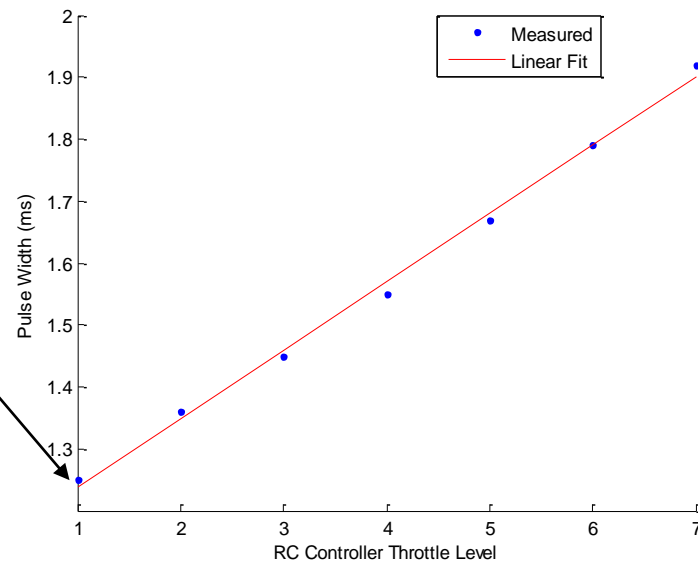
Schematic for Thermocouple circuit



Low Throttle: 5.77% Duty Cycle (1.26 ms pulse)



Full Throttle: 8.75% Duty Cycle (1.92 ms pulse)

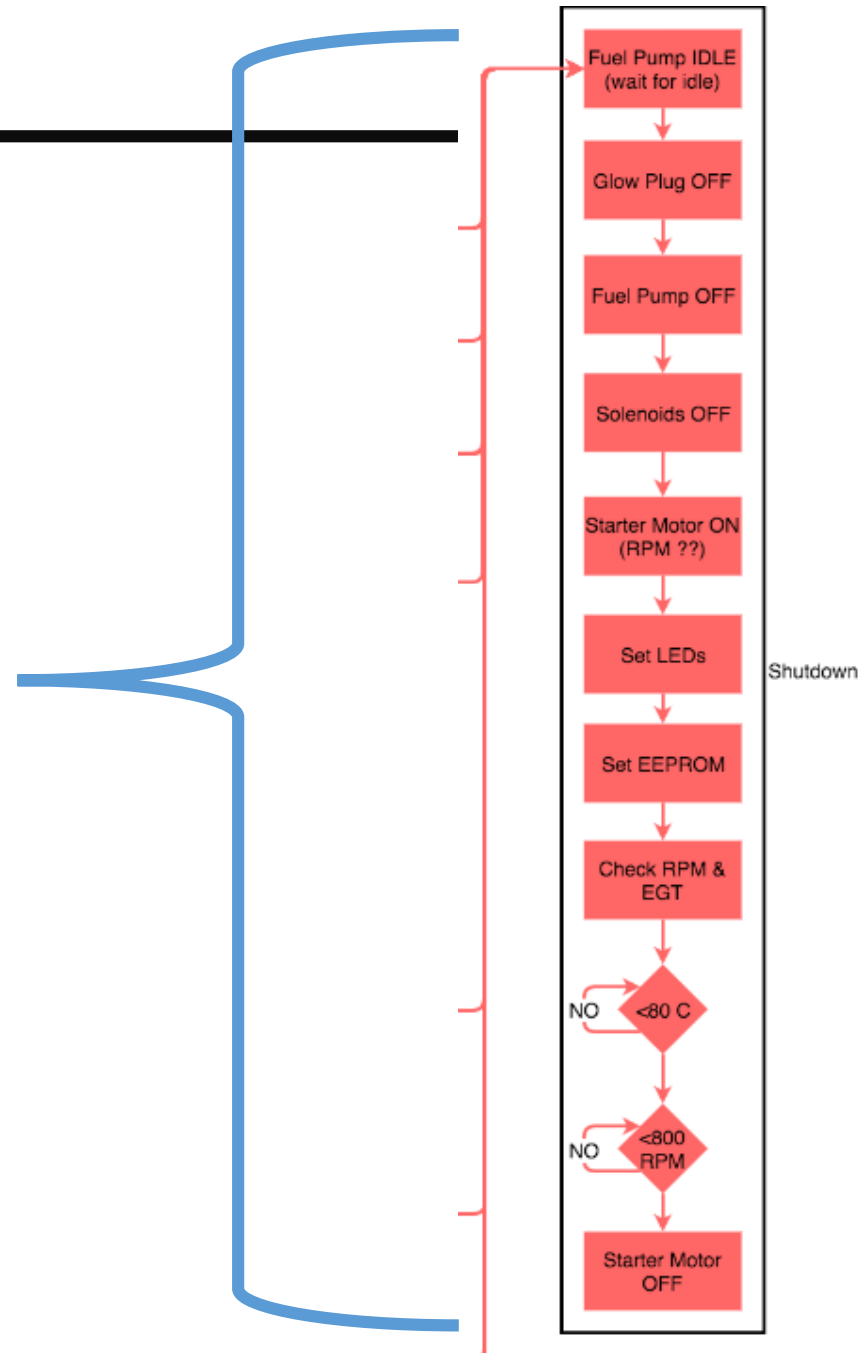


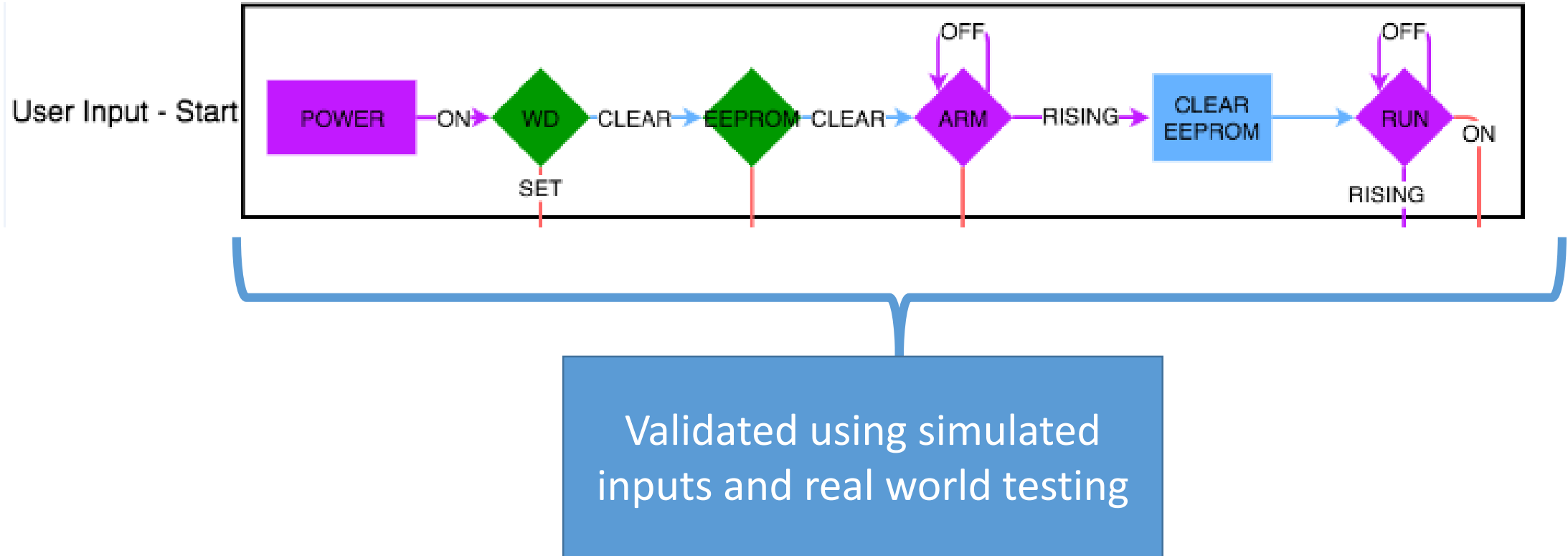
Very small difference – required more timers and interrupt for high fidelity, but did not have time to test after completion of software changes

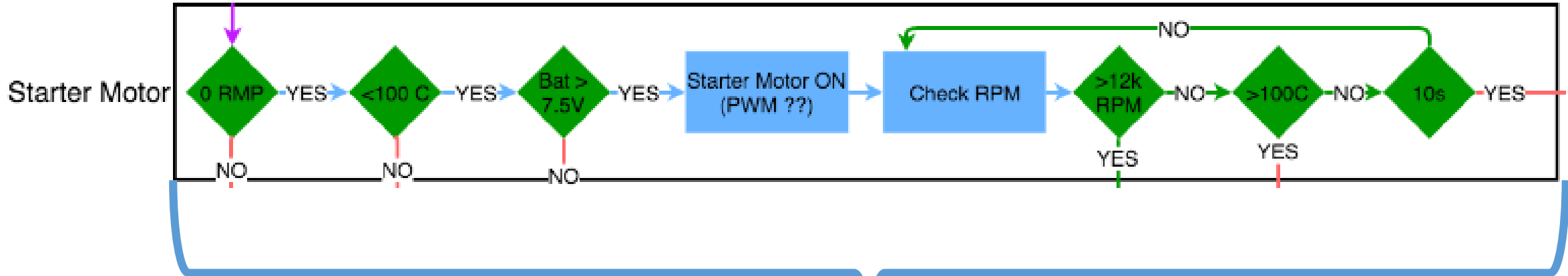


Software Backup Slides

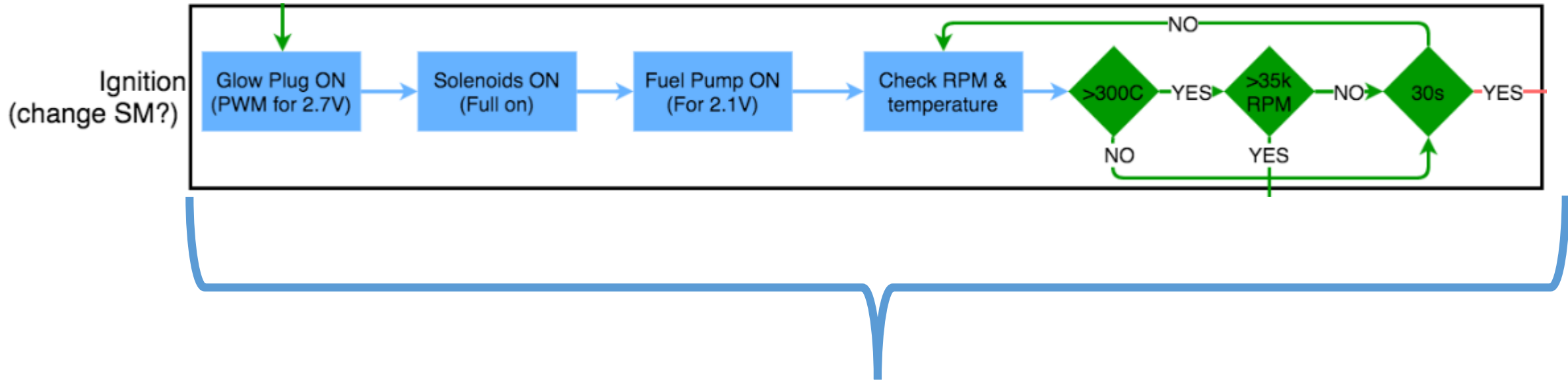
Validated using
simulated inputs
and real world
testing



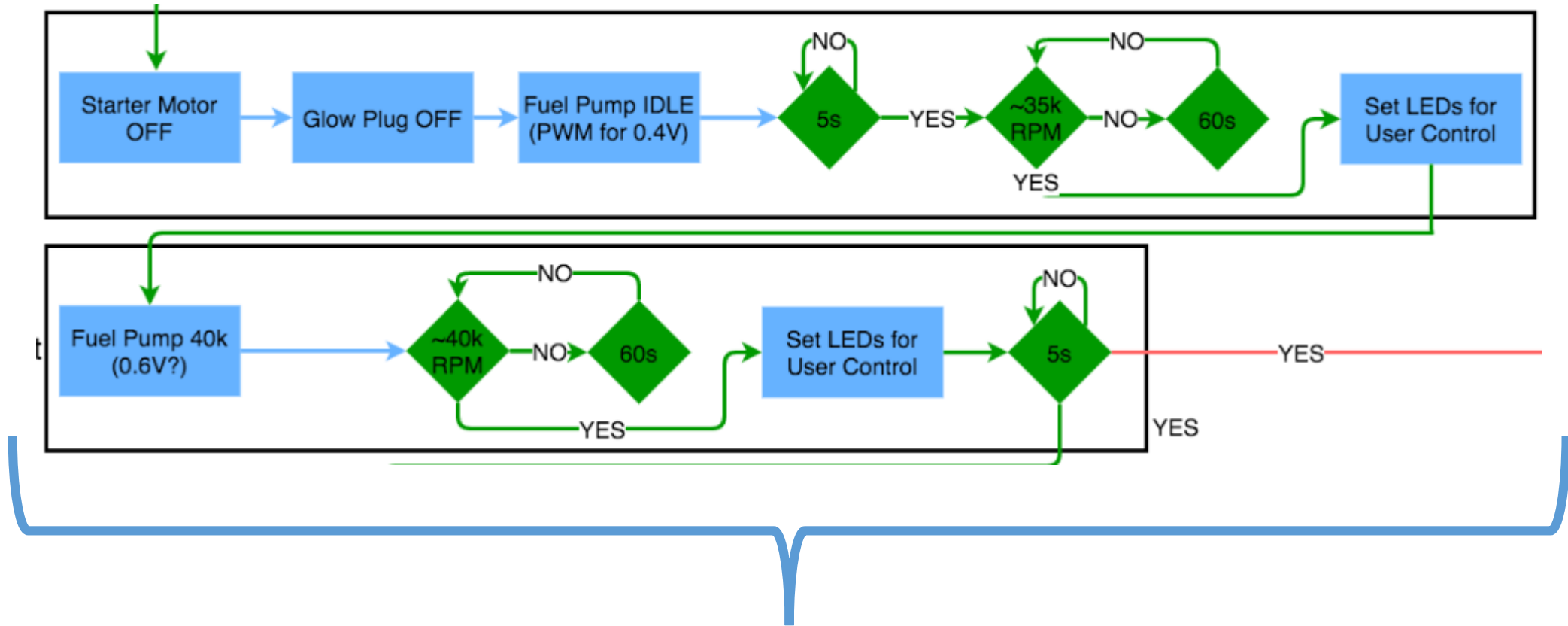




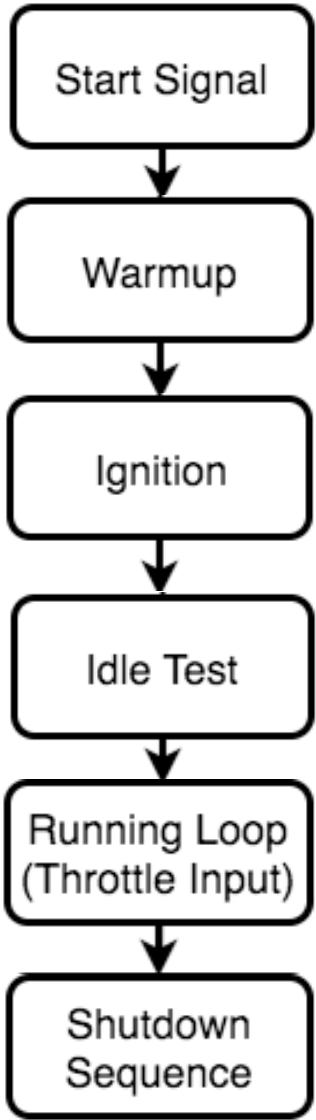
Validated using simulated inputs and real world testing



Validated using simulated inputs



Validated using simulated Inputs



Wait for signals from sensors

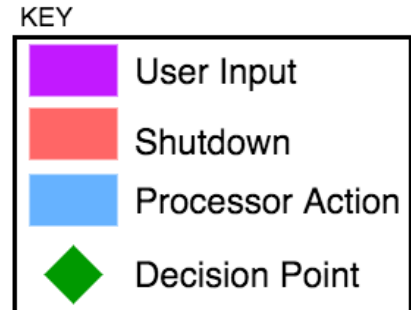
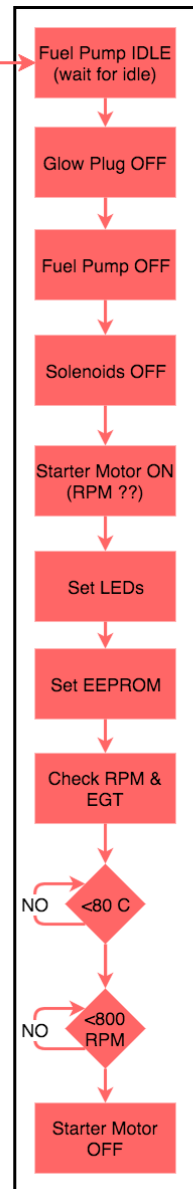
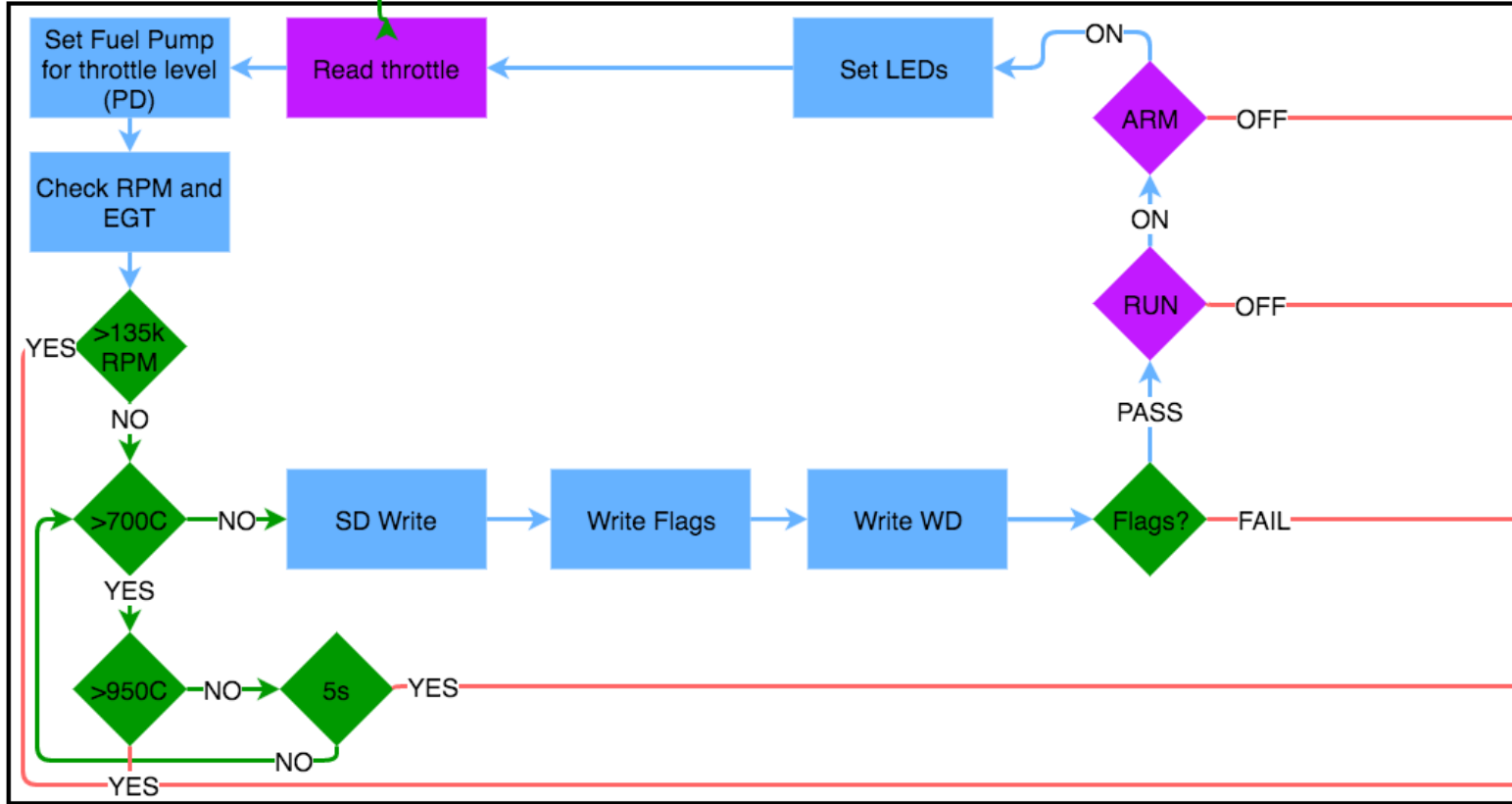
Spin starter compressor

Heat glow temperature

Set fuel pump until idle

Set fuel pump to reach RPM correlating with throttle level; check safeties and switches

Run starter motor until engine is below 80°C

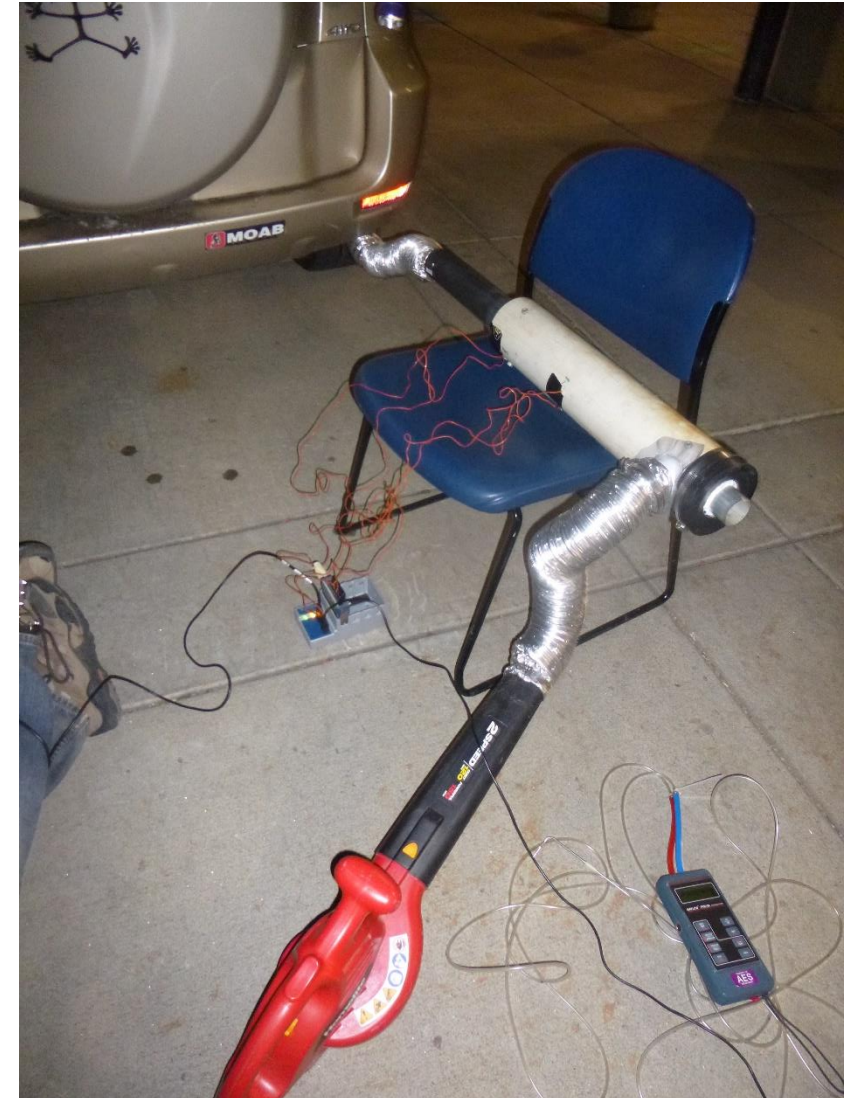


Shutdown



Testing Backup Slides

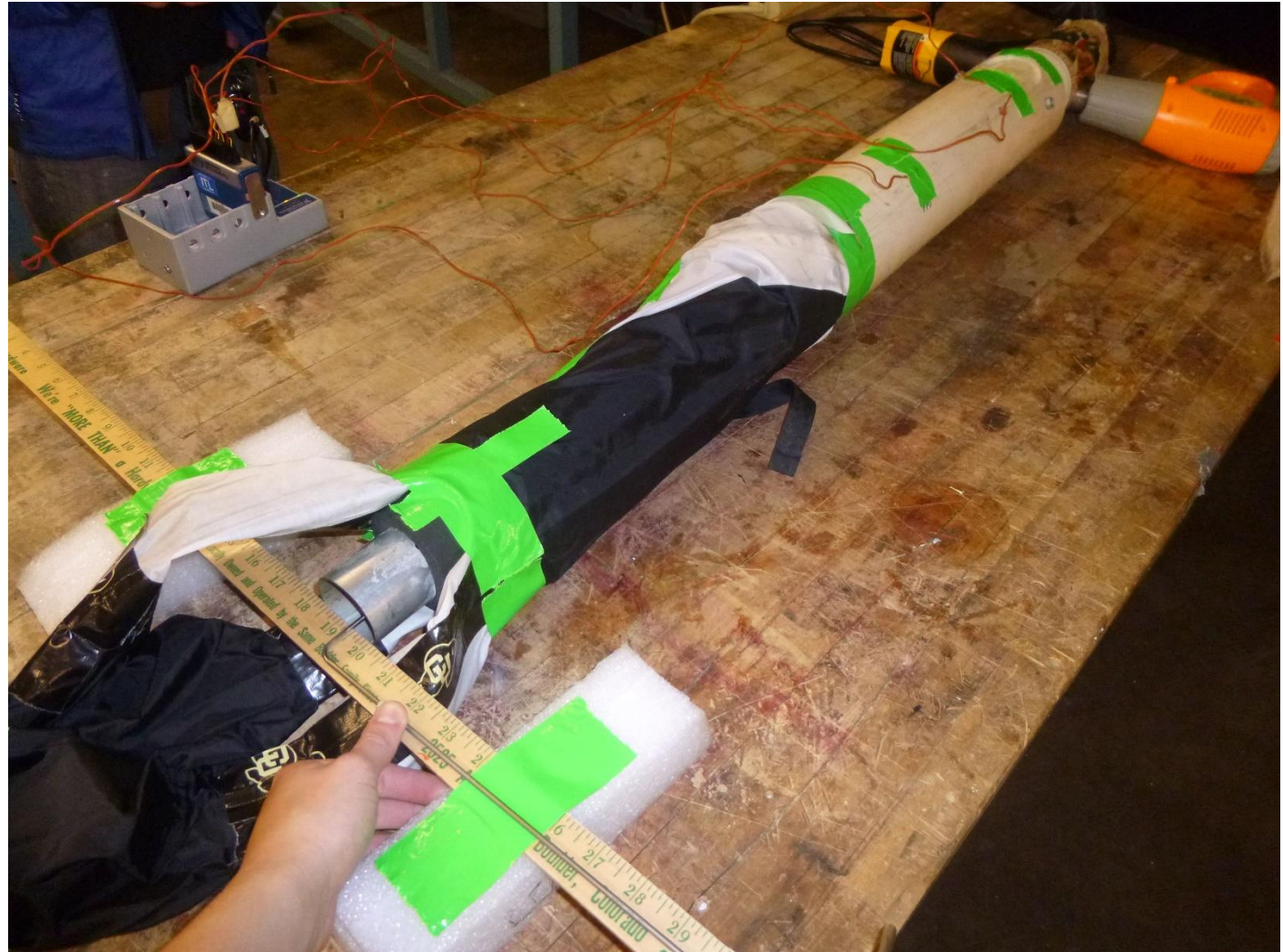
- Description
 - Concentric pipe flow
 - Hot flow from car exhaust
- Lessons Learned
 - Car exhaust is not hot/ fast enough for turbulent flow
 - Not a sustainable test, takes too long to reach steady state
 - Difficult to set up and tear down



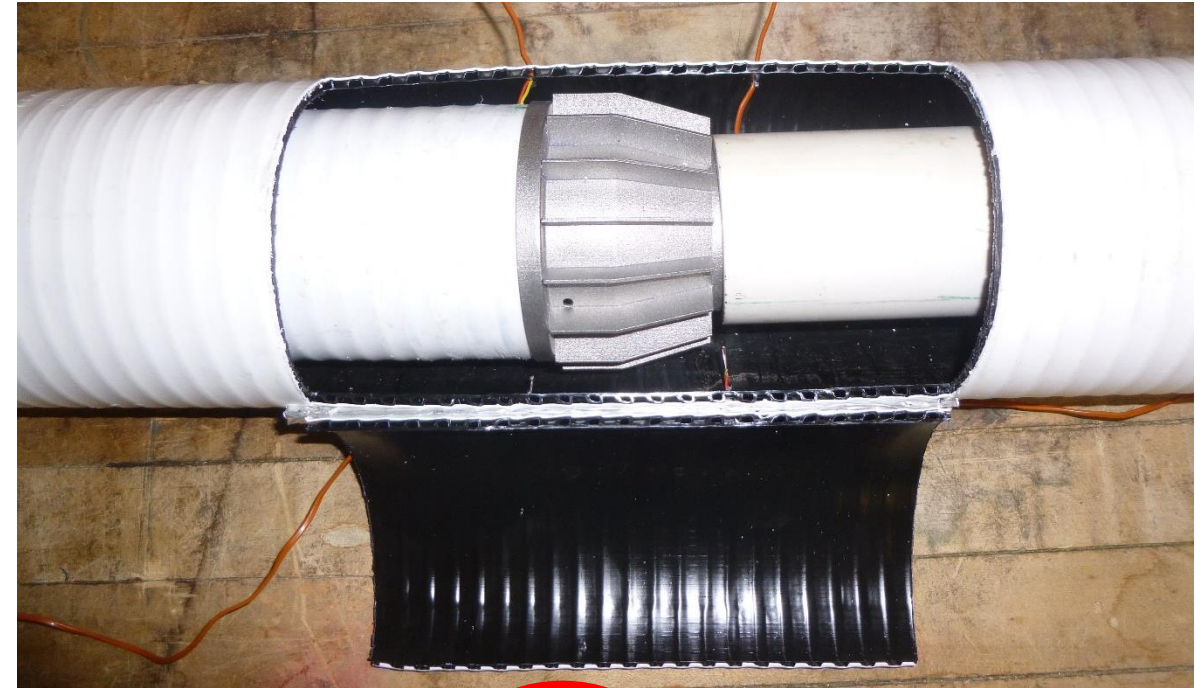
- Description:
 - Concentric pipe flow
 - Single heat gun for hot flow
- Lessons Learned:
 - Flow is uneven in the cold flow since the leaf blower is coming in from the side
 - Test section not long enough for fully developed turbulent flow
 - Results are difficult to quantify since the heat exchange is small. Need more heat



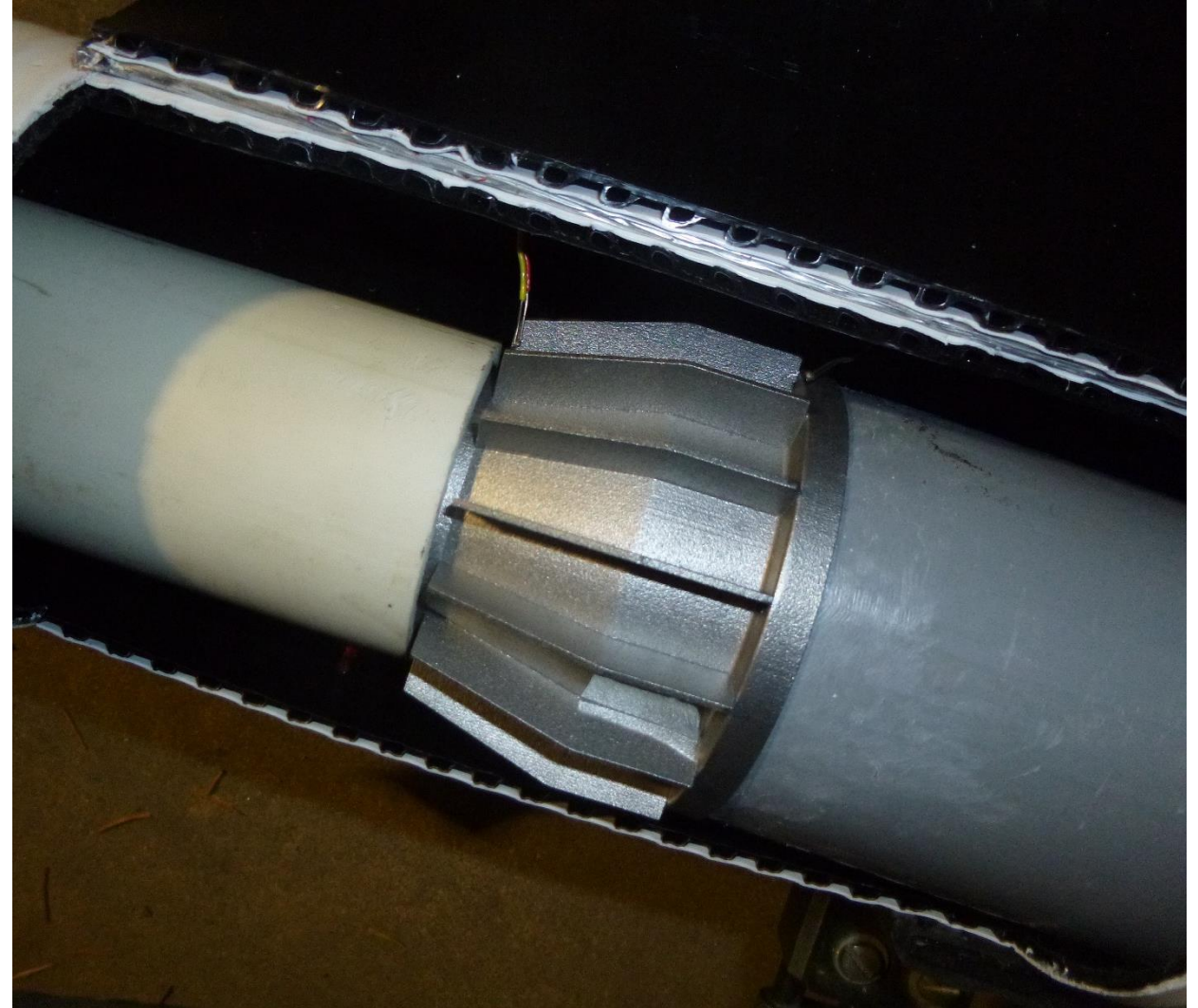
- Description:
 - Concentric pipe flow
 - Cold flow straightened via flow diverter/ shroud
 - Cold flow has longer to develop
 - Two heat guns and additional flow for greater temperature
- Lessons Learned:
 - Heat guns over heated, because hot air was flowing back through them
 - Thermocouples difficult to integrate in flow since the pipe is closed



- Description:
 - Concentric pipe flow with heat exchanger
 - Longer heat pipes for developed flow
 - Door cut for easier access to heat exchanger and thermocouples
 - Hot flow pulled down the pipe using a sucking fan, allowing for higher Reynolds number, hotter flow, and less risk for the heat guns
- Lessons Learned:
 - Extra heat from heat guns caused severe melting and weird results from unknown melting sections



- Description:
 - Concentric pipe flow with heat exchanger
 - New hot flow entrance pipe, with metal interior and pvc exterior to take the heat better, but still provide insulation to the flow
- Lessons Learned:
 - The new pipe held up, but the heat guns melted the Y-pipe so that it was unusable. Plastic is a bad idea



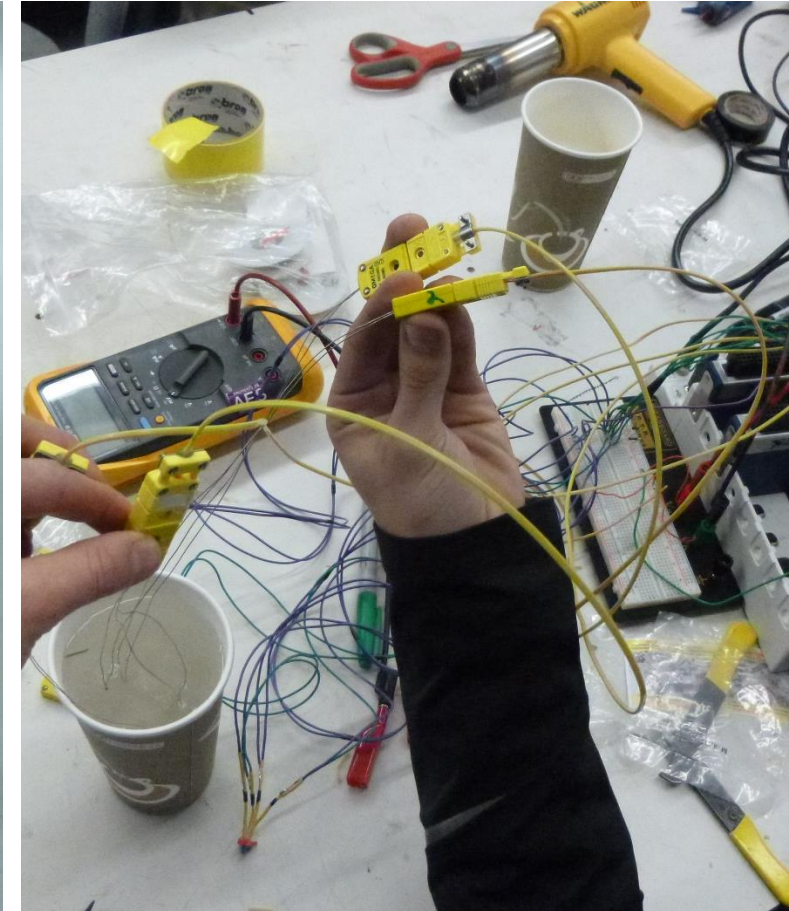
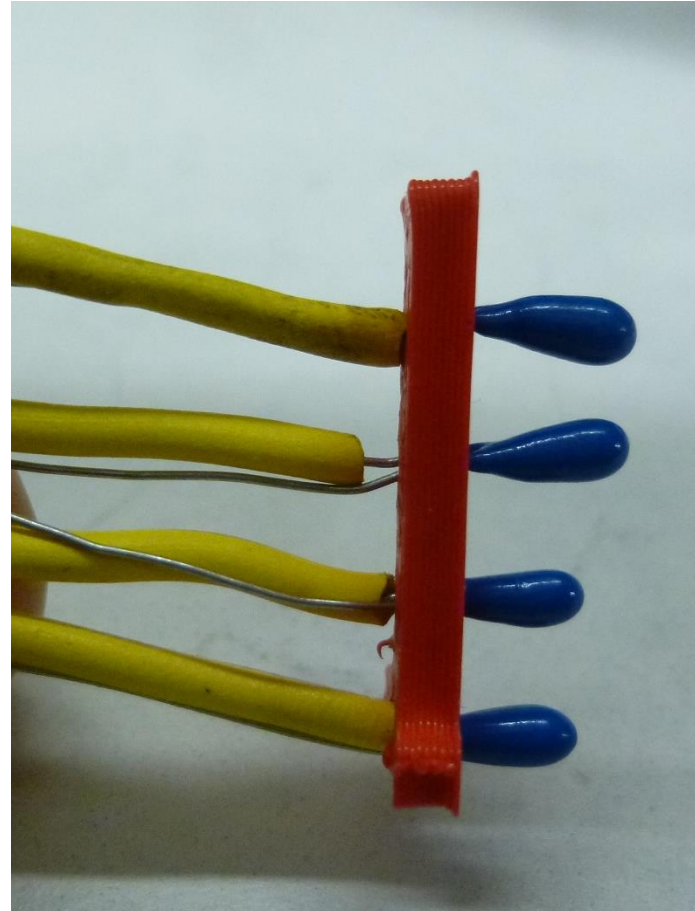
- Description:
 - Concentric pipe flow with heat exchanger
 - Replaced Y-pvc pipe with a Y-car exhaust pipe
- Lessons Learned:
 - A temperature profile is necessary for the cold flow because the thermocouples are very sensitive to placement



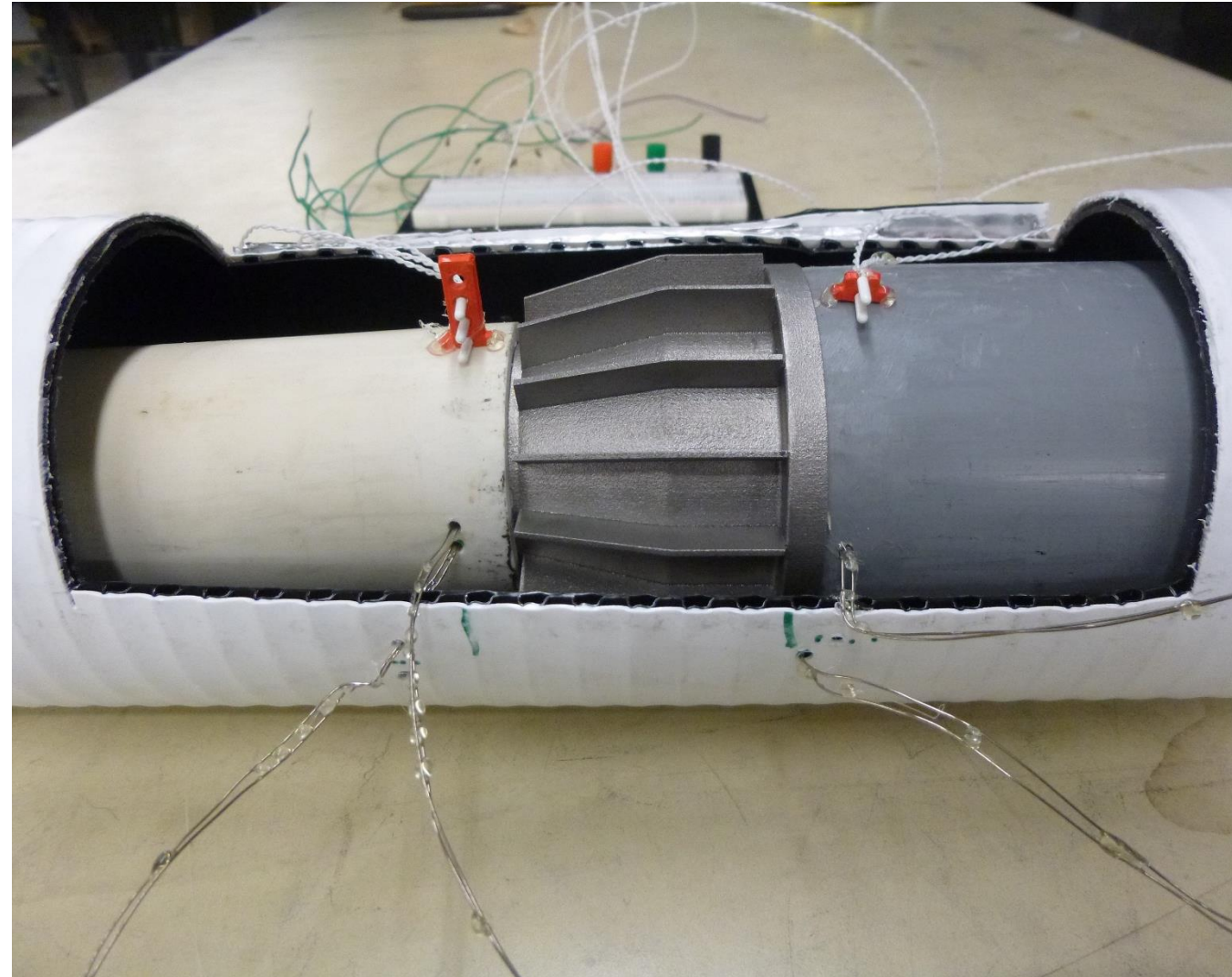
- Description:
 - Used level 0 setup to get a temperature profile in concentric pipe flow
 - Found experimental profile for different leaf blower and sucker speeds
- Lessons Learned:
 - Leaf blower low, sucker low
0.37°/mm (radial)
 - Leaf blower high, sucker low
0.74°/mm (radial)
 - A temperature profile is needed for conclusive results
 - Thermistors should be used instead of thermocouples, because they have less error



- Description:
 - Concentric pipe flow with heat exchanger
 - 3D printed profile insert for thermistors
 - Made in-house thermocouples with bare wire for easier integration and testing with the Daq
- Lessons Learned:
 - Bare wires are difficult to work with and created poor data when test was run since wires kept touching in flow



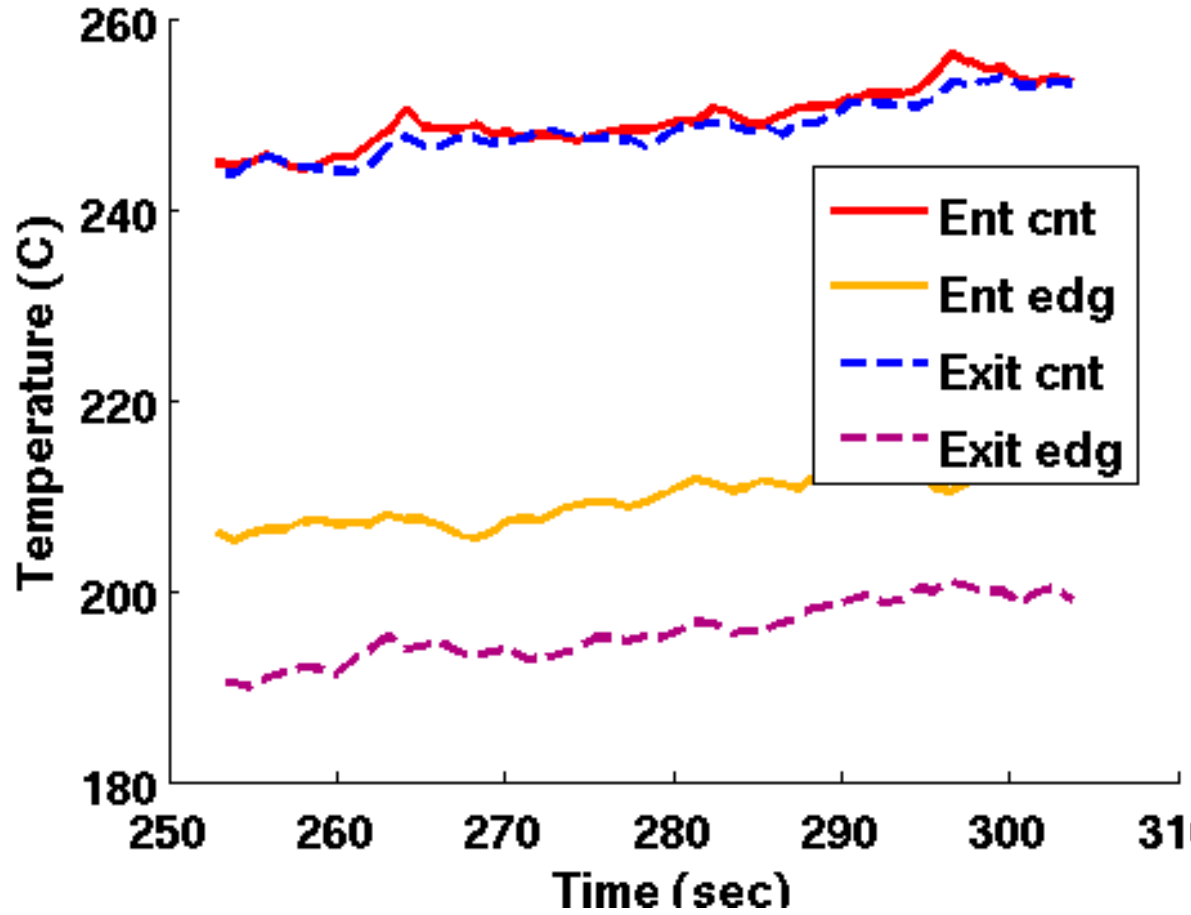
- Description:
 - Concentric pipe flow with heat exchanger
 - Using covered thermistors to prevent wires touching
 - Beaded in-house thermocouples with hot glue to prevent wires touching
- Lessons Learned:
 - Results inconclusive due to: spiraling flow (unexpected stream lines), pressure drops/ unintentional mixing due to leaks, wrongly assumed resistors all have the same resistance
 - Important to take bulk temperatures and velocities in Matlab analysis
 - Need to wait longer between tests to prevent melting



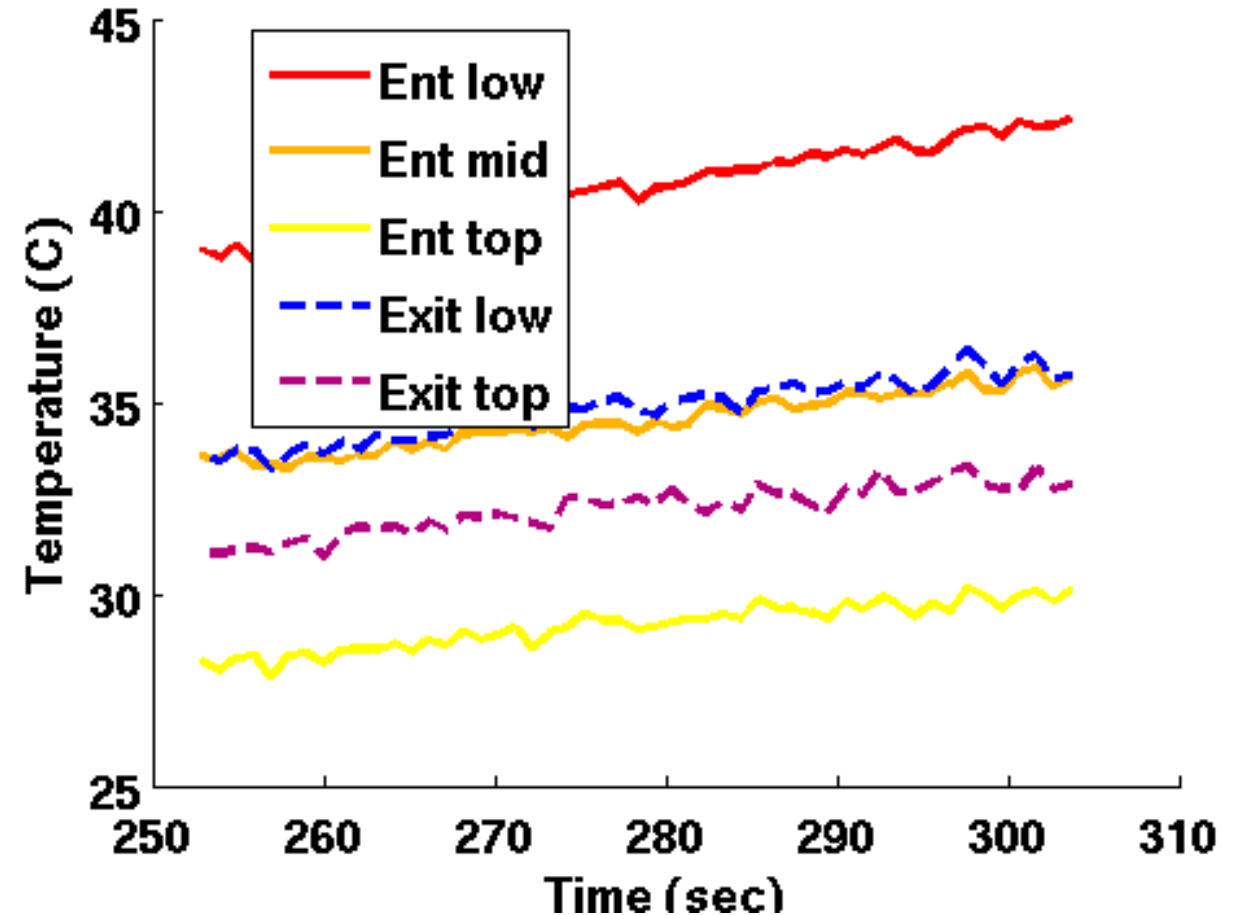
Iterations/ Lessons Learned: Level 1.4

Result: -5 °C across heat exchanger

Hot Flow Temperatures vs Time

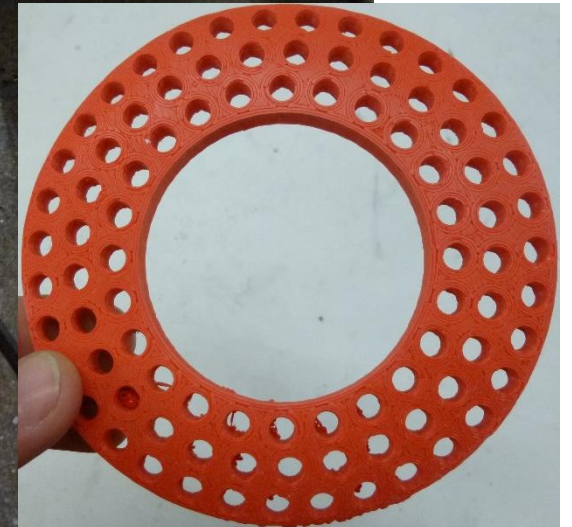


Cold Flow Temperatures vs Time



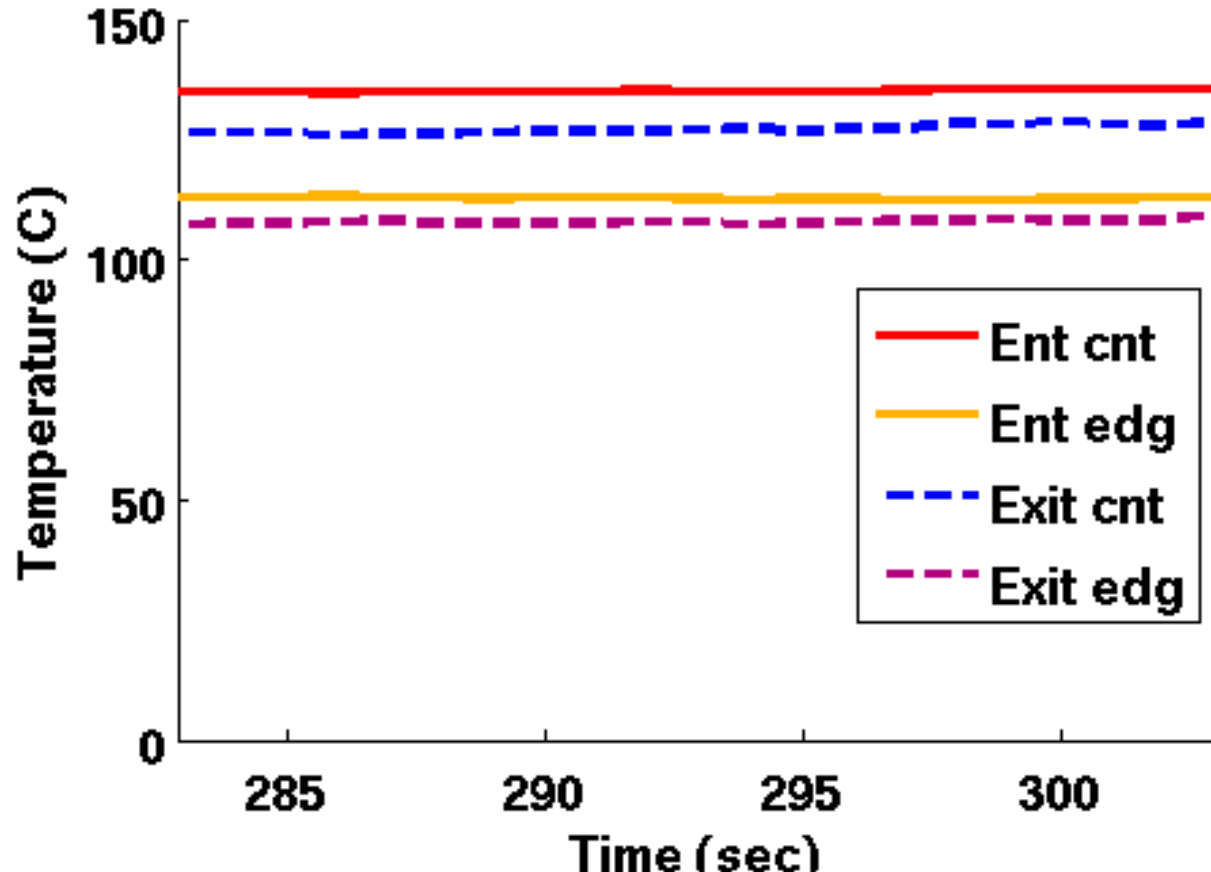
- Description:
 - Concentric pipe flow with heat exchanger
 - Created flow straightener inserts to place in cold incoming flow
 - Secured ducting around the leaf blower to prevent uneven flow and unnecessary pressure drops
 - Place temperature profile inserts with thermistors in different streamlines

- Lessons Learned:
 - Ran 3 tests and found similar data. Need to run more tests for statistical assurance

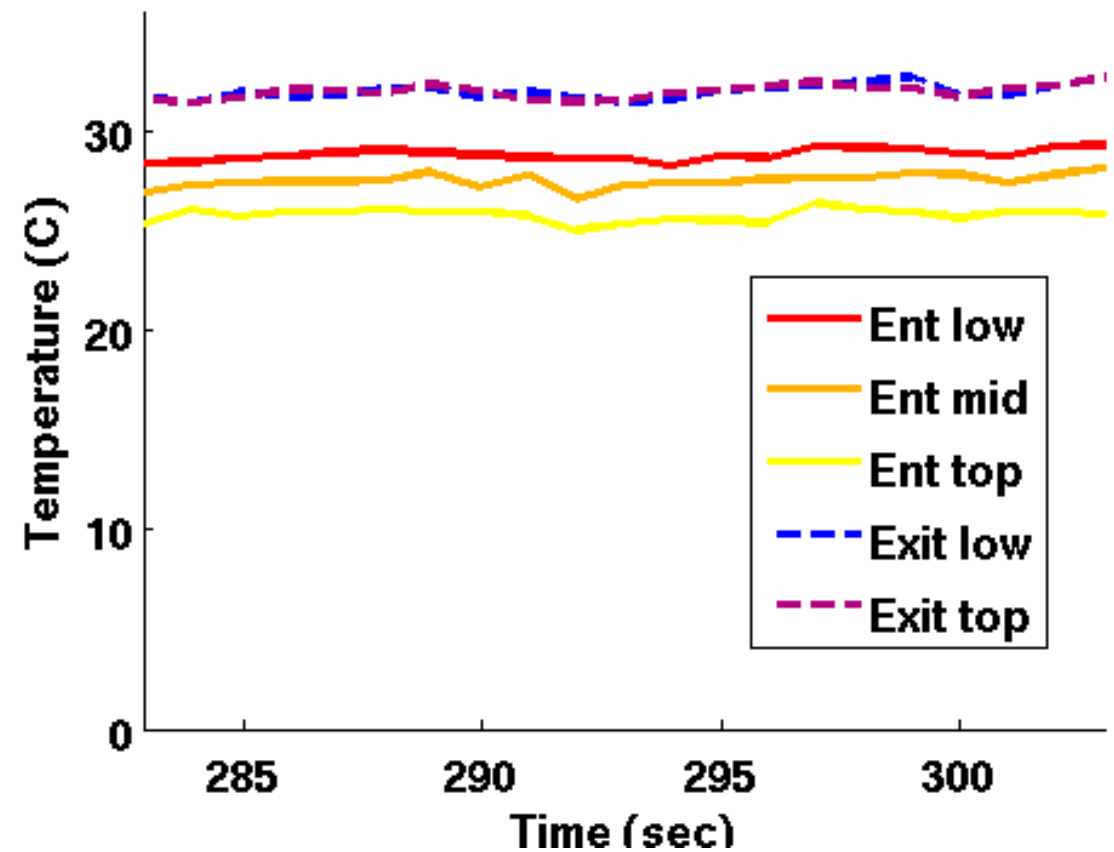


Result: +3.83 °C across heat exchanger

Hot Flow Temperatures vs Time



Cold Flow Temperatures vs Time

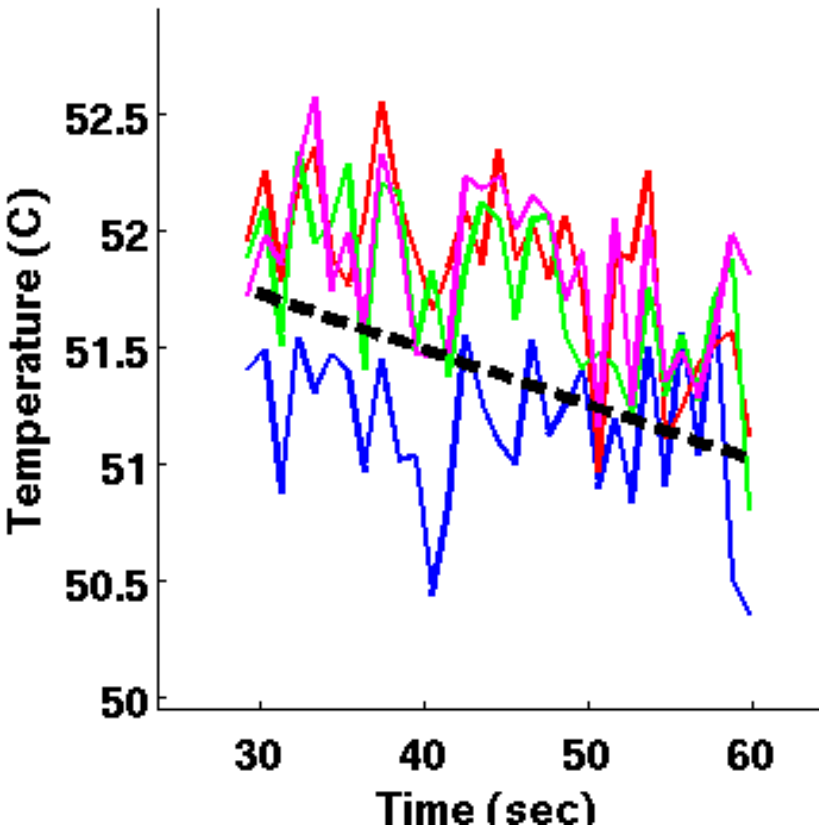


Monte Carlo Simulation Sensitivity Variables

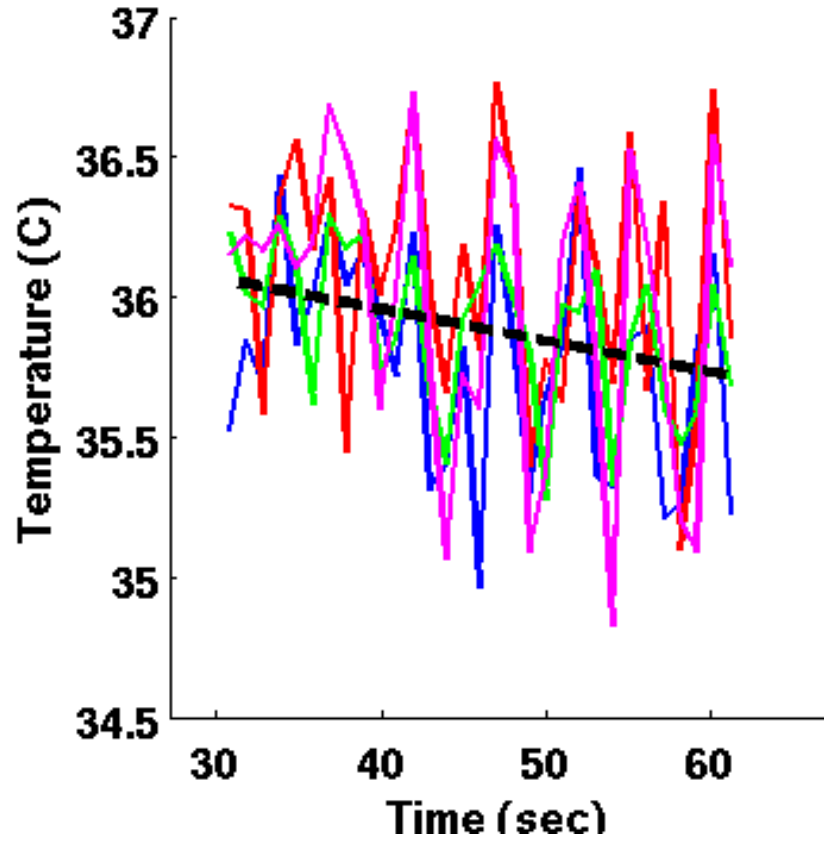
- Temperature
 - Cold flow in
 - Hot flow in
 - Hot flow out
- Velocity
 - Hot
 - Cold

Test	Model	Experimental	Percent Difference
1	1.94±0.2°C	1.29±0.4°C	33.5%
2	2.06±0.2°C	1.59±0.4°C	22.8%
3	1.93±0.2°C	1.72±0.4°C	11.0%
4	2.03±0.2°C	2.37±0.4°C	-17.4%
5	1.99±0.2°C	2.27±0.4°C	-13.9%
6	2.02±0.2°C	2.56±0.4°C	-26.6%
7	1.95±0.2°C	2.16±0.4°C	-10.8%
8	2.17±0.2°C	1.95±0.4°C	10.2%
9	1.09±0.1	0.82±0.4°C	24.4%
10	2.27±0.2°C	1.88±0.4°C	17.0%
Average	1.95±0.2°C	1.86±0.4°C	5.0%

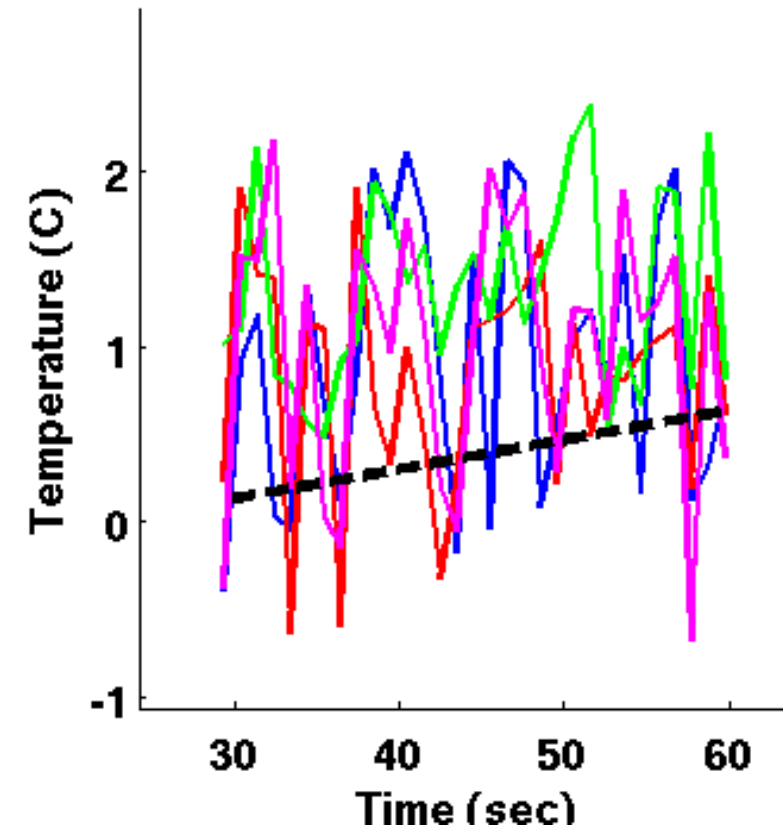
HotWaterComparison



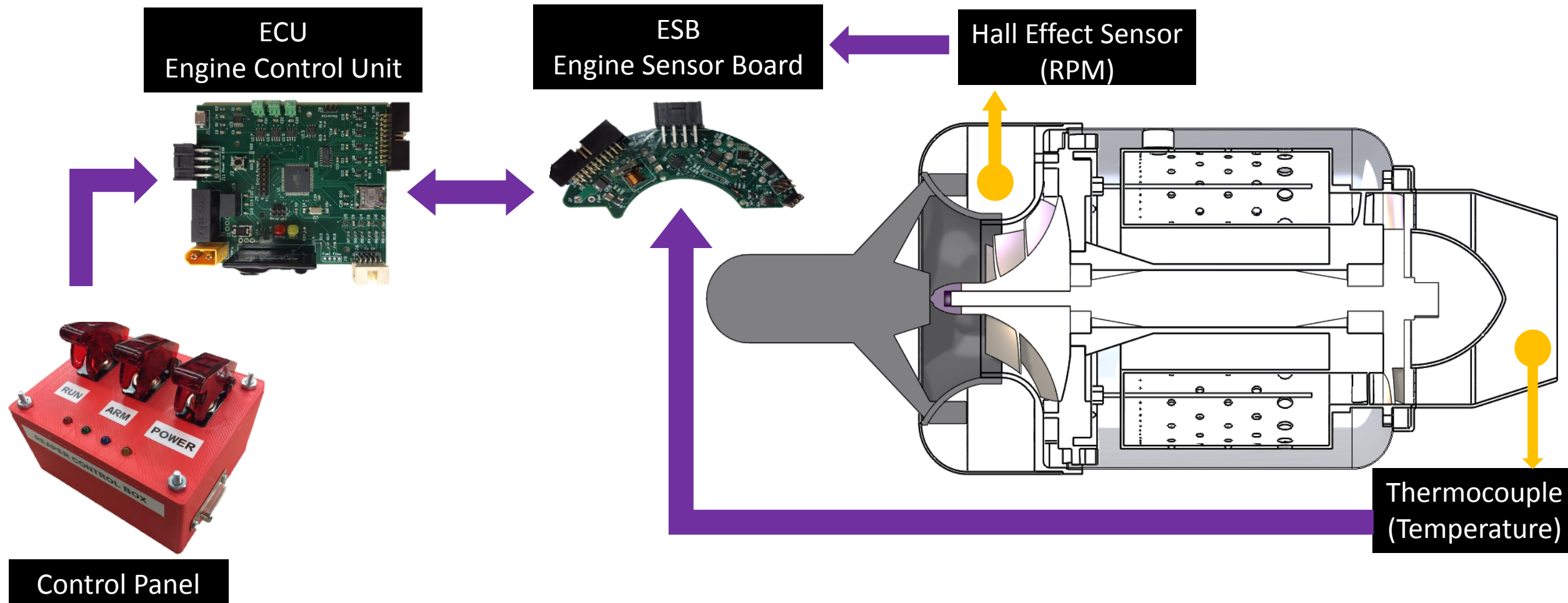
LukeWarmWaterComparison



ColdWaterComparison

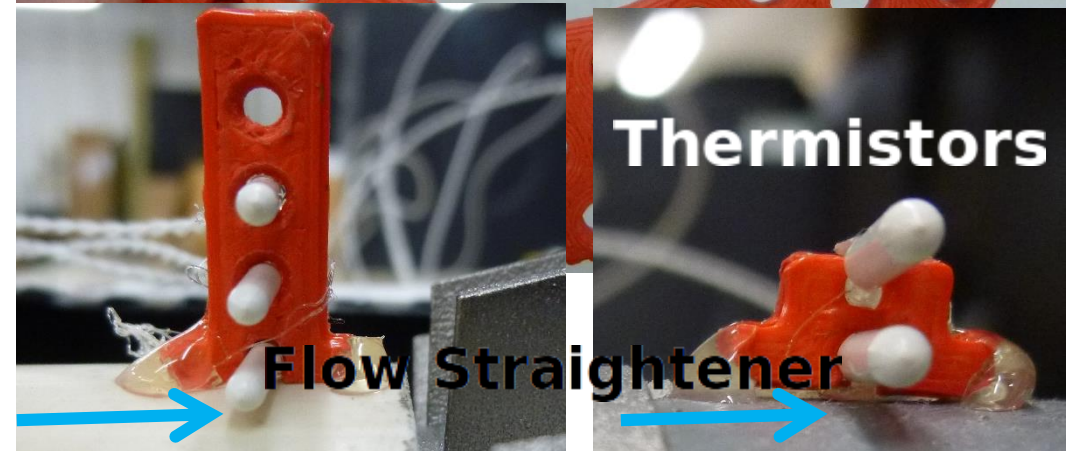
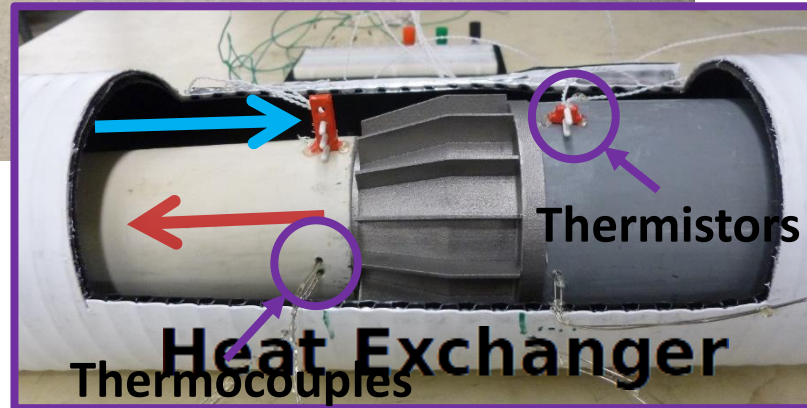
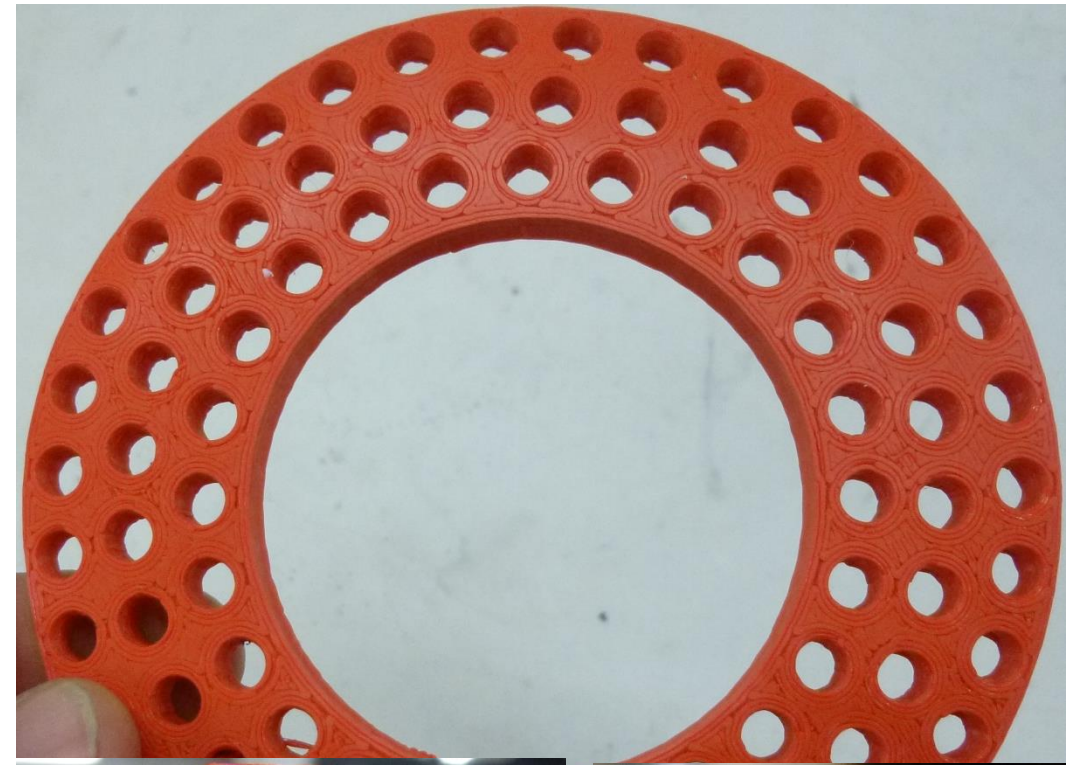
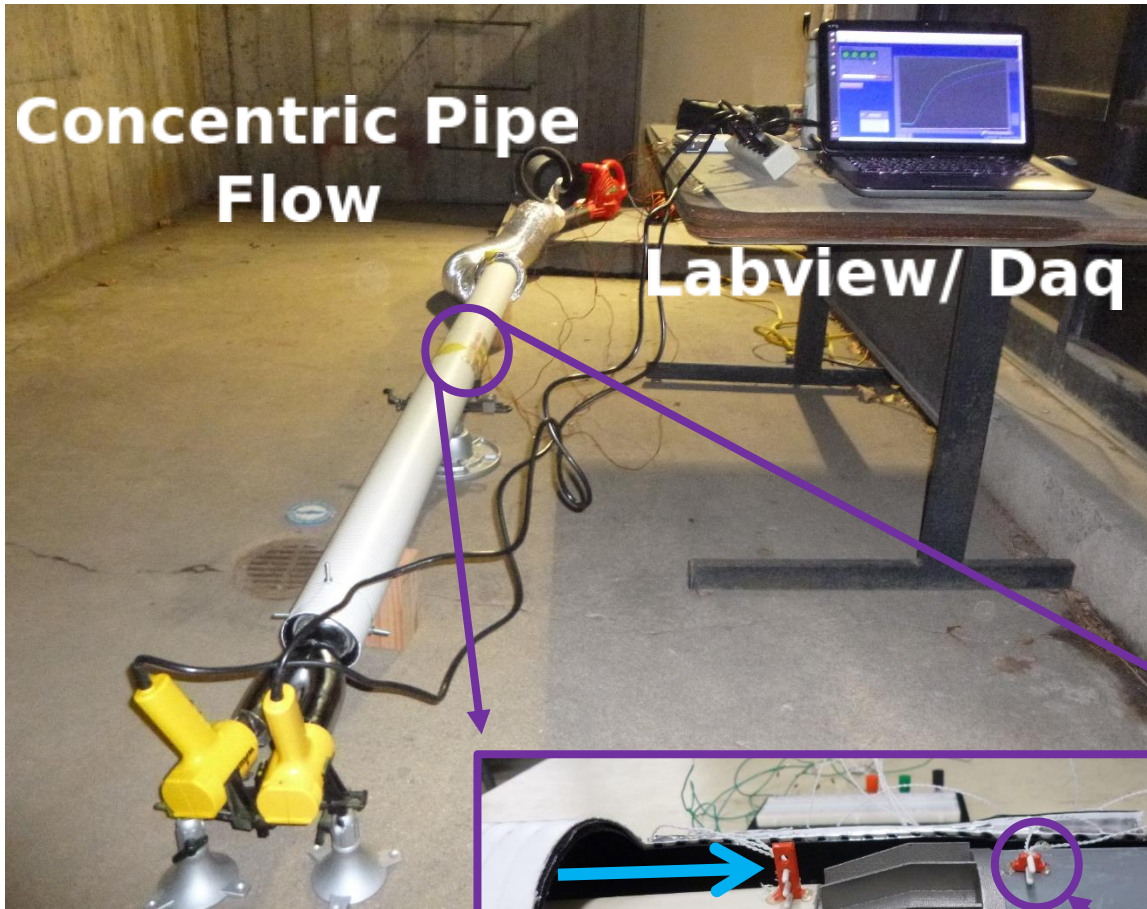


ECU and ESB Stock Engine Test



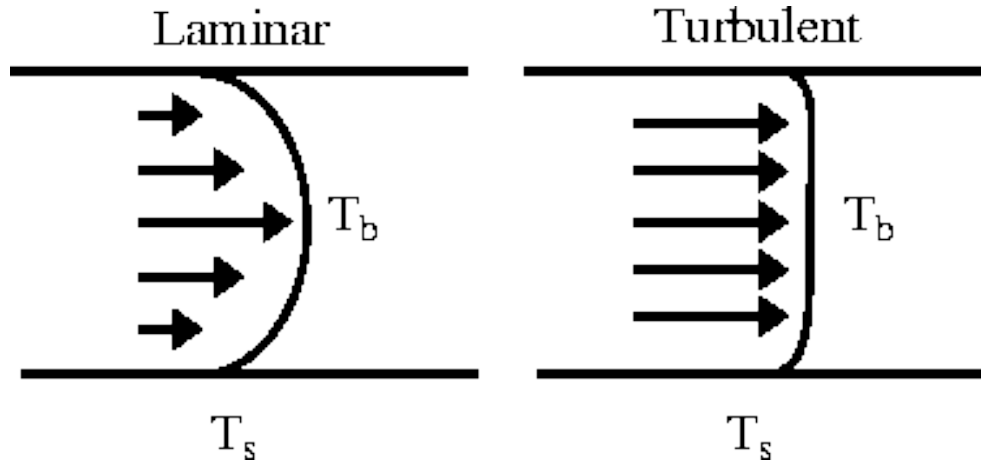
Sensor List	Sensor Error	Expected Range	Minimum Sample Rate
Thermocouple	± 3 °C	0-900 °C	113 Hz
Hall Effect	$\pm 0.5\%$	0- 130,000 rpm	31 Hz

Heat Exchanger Verification



- Expected Results and Considerations:

- Velocity Profiles

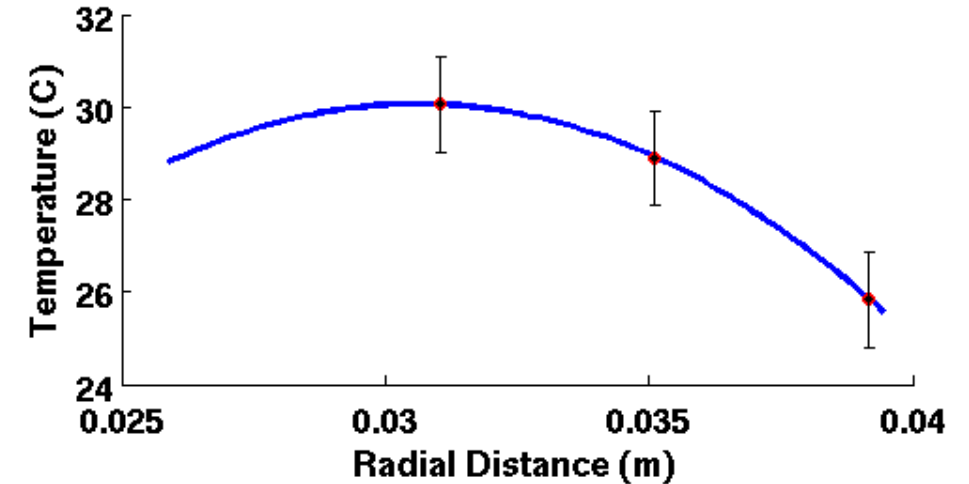


- Take bulk velocity and temperature

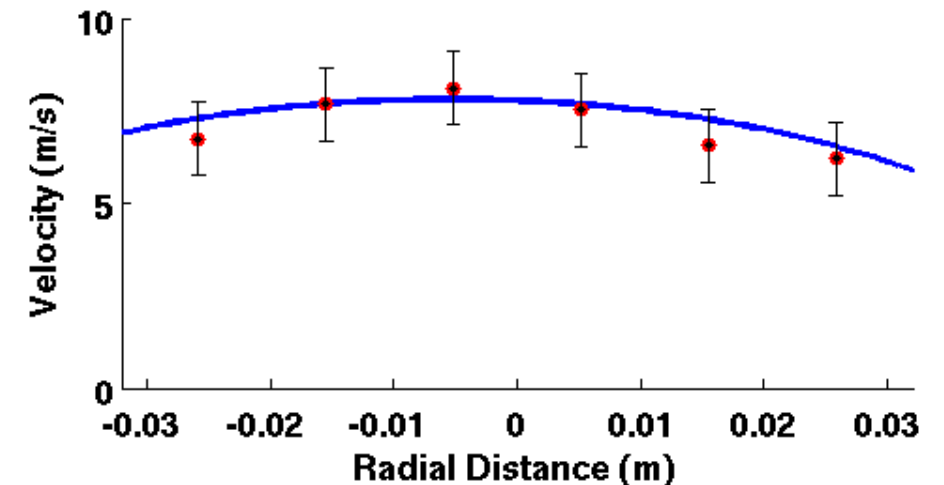
$$T_b = \frac{2}{U_m r_o^2} \int_0^{r_o} u T r dr$$

$$U_m = \frac{2}{r_o^2} \int_0^{r_o} u r dr$$

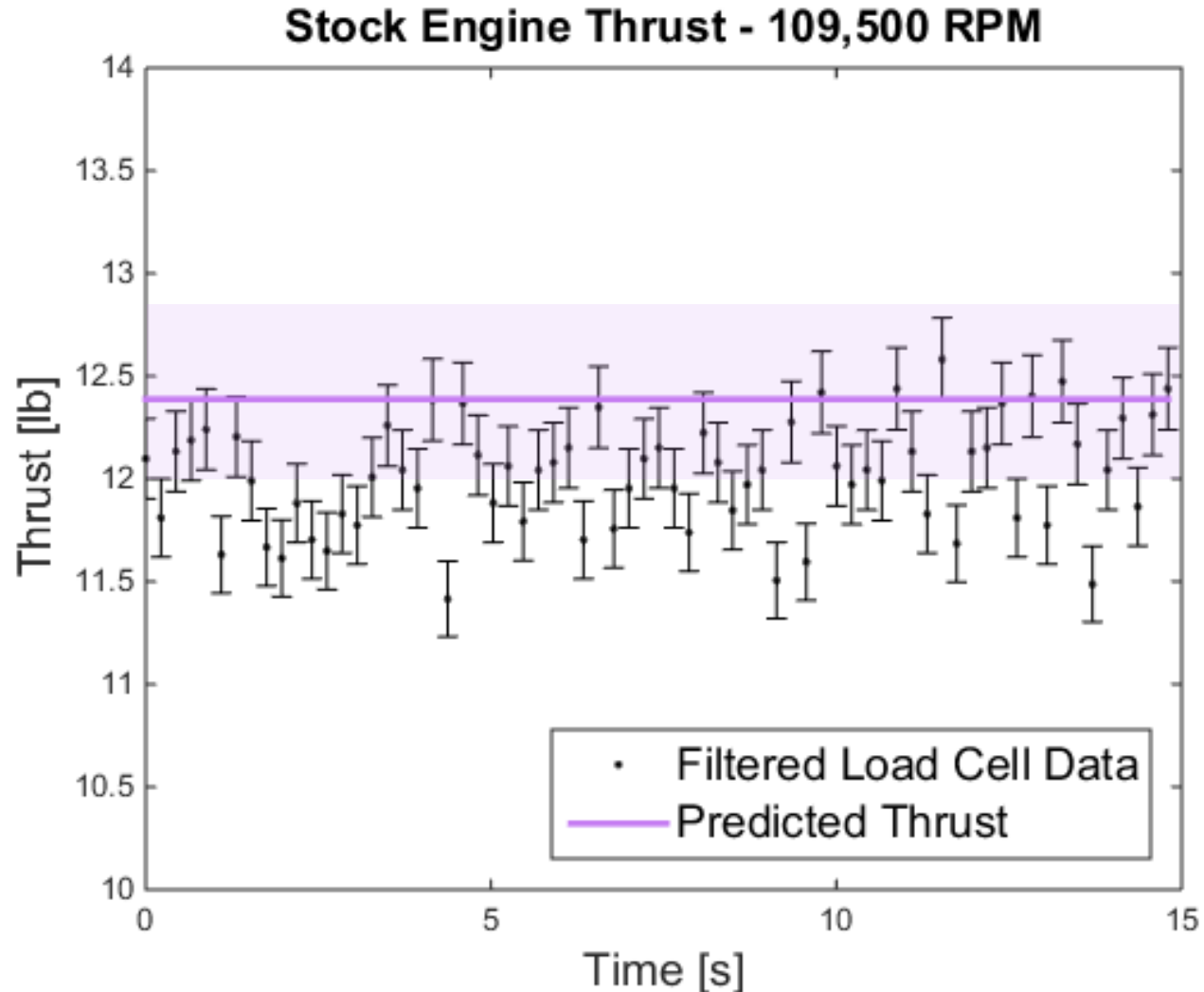
Experimental Radial Temperature Profile
Cold Flow In



Experimental Radial Velocity Profile
Hot Flow Out



Control Volume Model Validation: Thrust



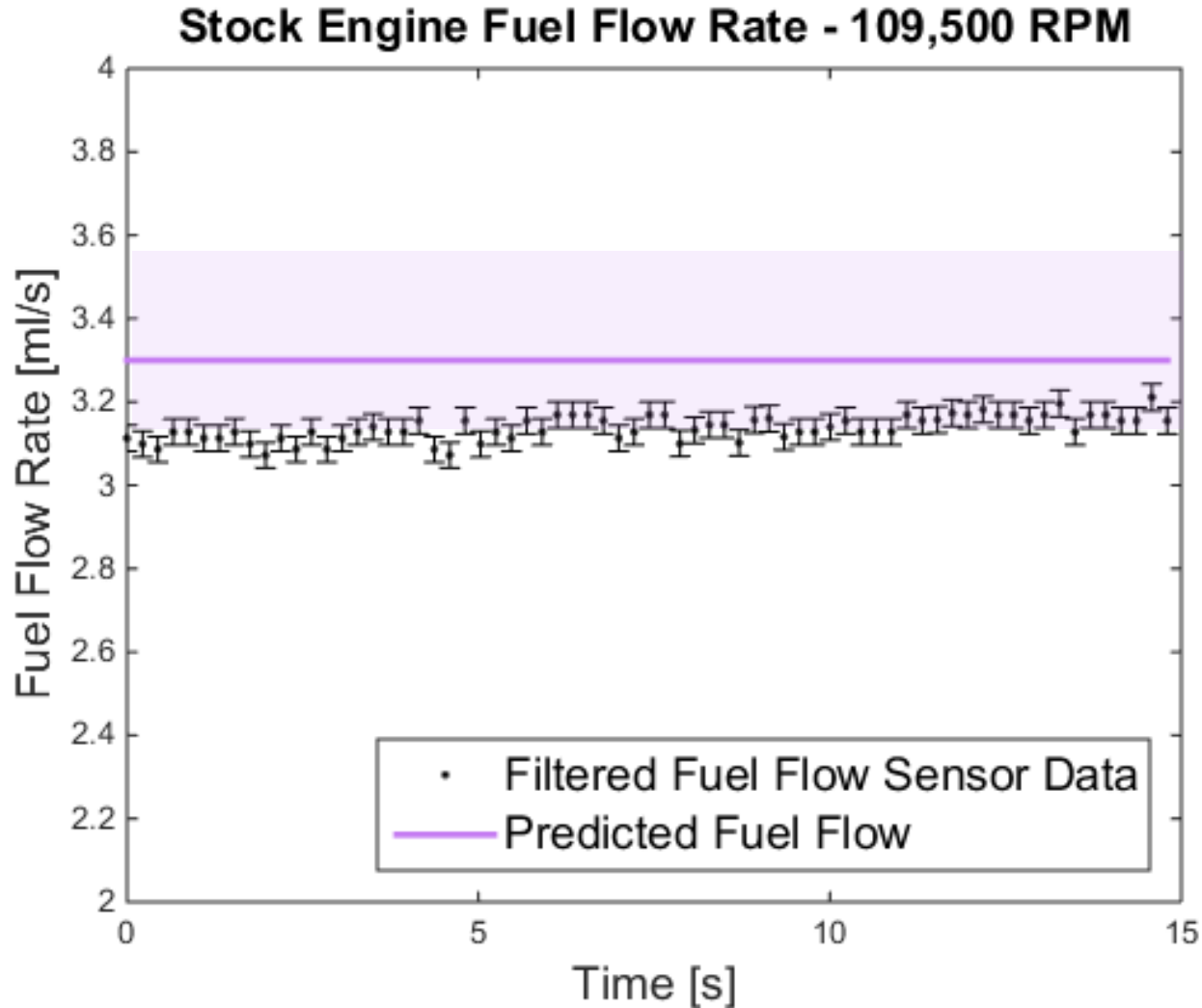
Predicted Thrust: 12.4 ± 0.4 lbs

Measured Average Thrust: 12.0 ± 0.2 lbs

Percent Difference: 3.3%

Conclusions:

- Model can predict P-90RXi thrust (DR 3.1)
- Model can predict losses in engine (DR 3.3)



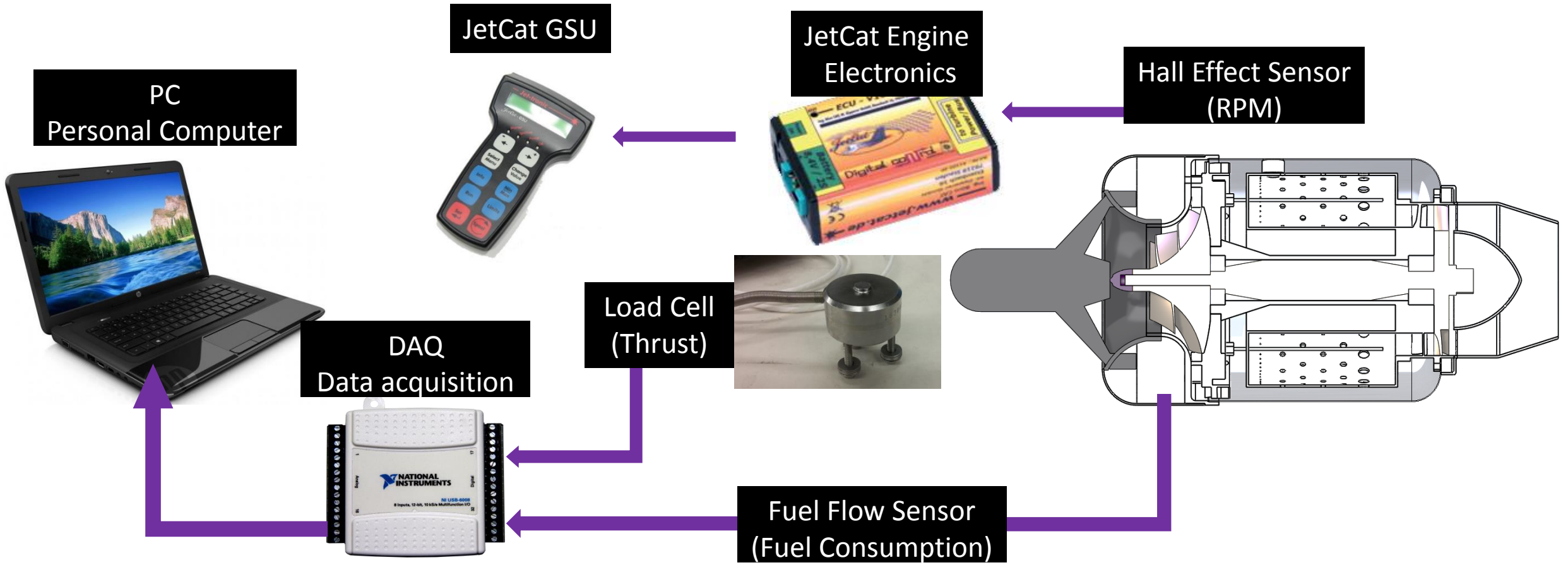
Predicted Fuel Rate: $3.3 \pm 0.2 \text{ ml/s}$

Measured Average Fuel Consumption: $3.13 \pm 0.03 \text{ ml/s}$

Percent Difference: 6.5%

Conclusion:

- Model can predict P-90RXi fuel consumption rate (DR 3.2)



Sensor List	Error	Expected Range	Sample Rate
Fuel Flow Sensor	±1.2%	0-5 mL/s	1 Hz
25lb Load Cell	±1.9%	0- 22 lbs	1 Hz
Hall Effect	±100 RPM	0- 130,000 RPM	31 Hz



Project Management/Systems Engineering Backup Slides

FR 1: Engine control electronics **command the modified engine**

FR 2: Thrust specific fuel consumption **decreases at least 10% at full throttle**

FR 3: Thermal-fluid simulation **models the changes in engine performance**

Defining Scope:

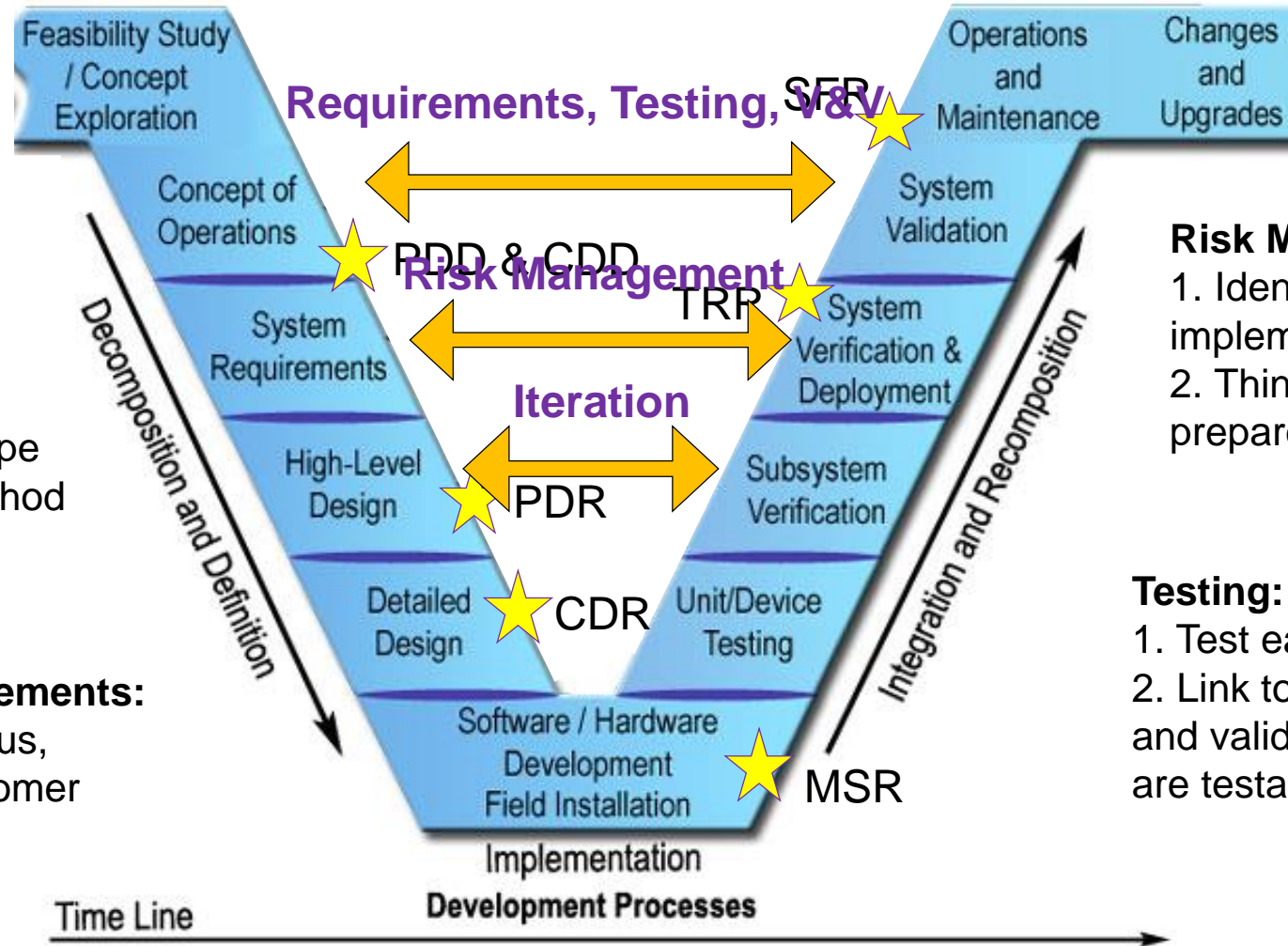
1. Proof of concept
2. Not for flight

Trade Studies:

1. Heat Exchanger Type
2. Engine Control Method

Functional Requirements:

Clear & unambiguous, testable, meet customer requests



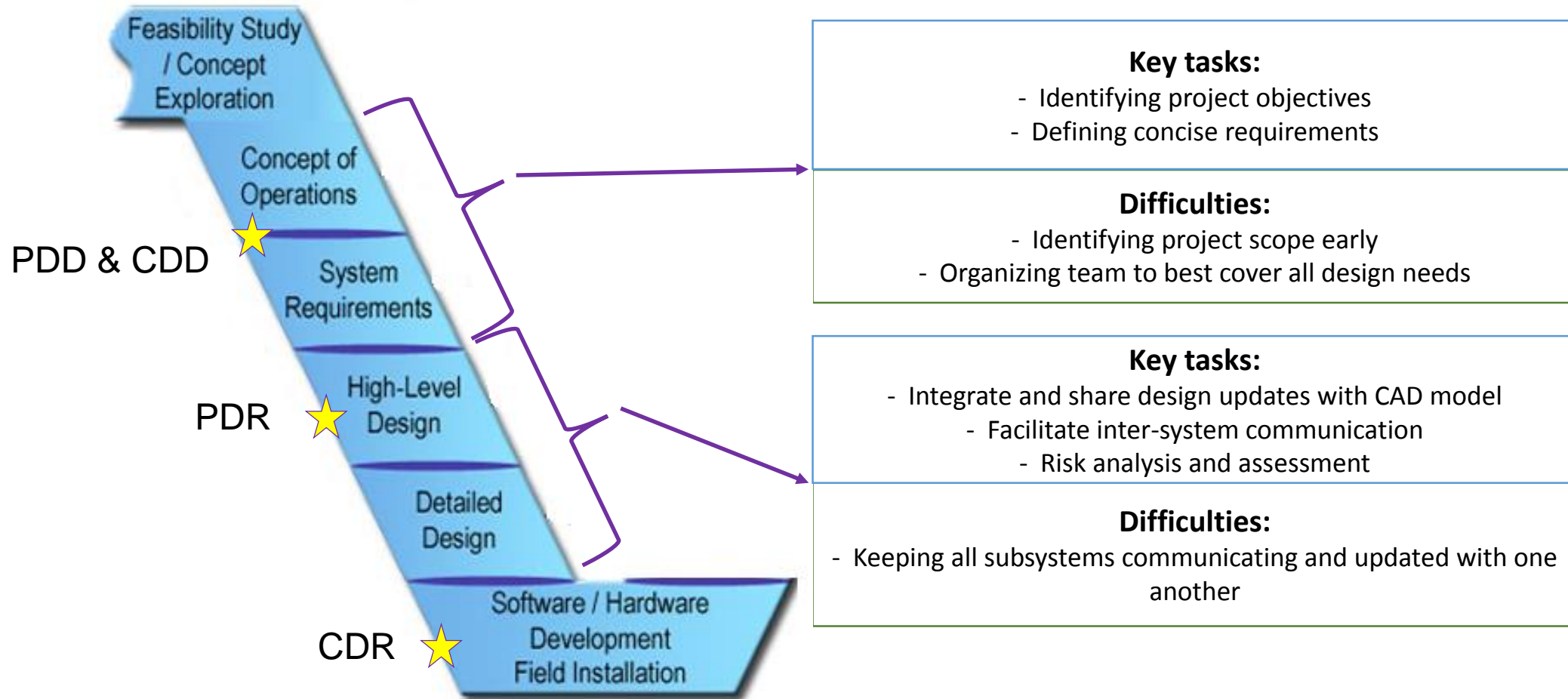
Risk Management:

1. Identify potential threats and implement mitigation plans **early**
2. Things will go wrong so be prepared

Testing:

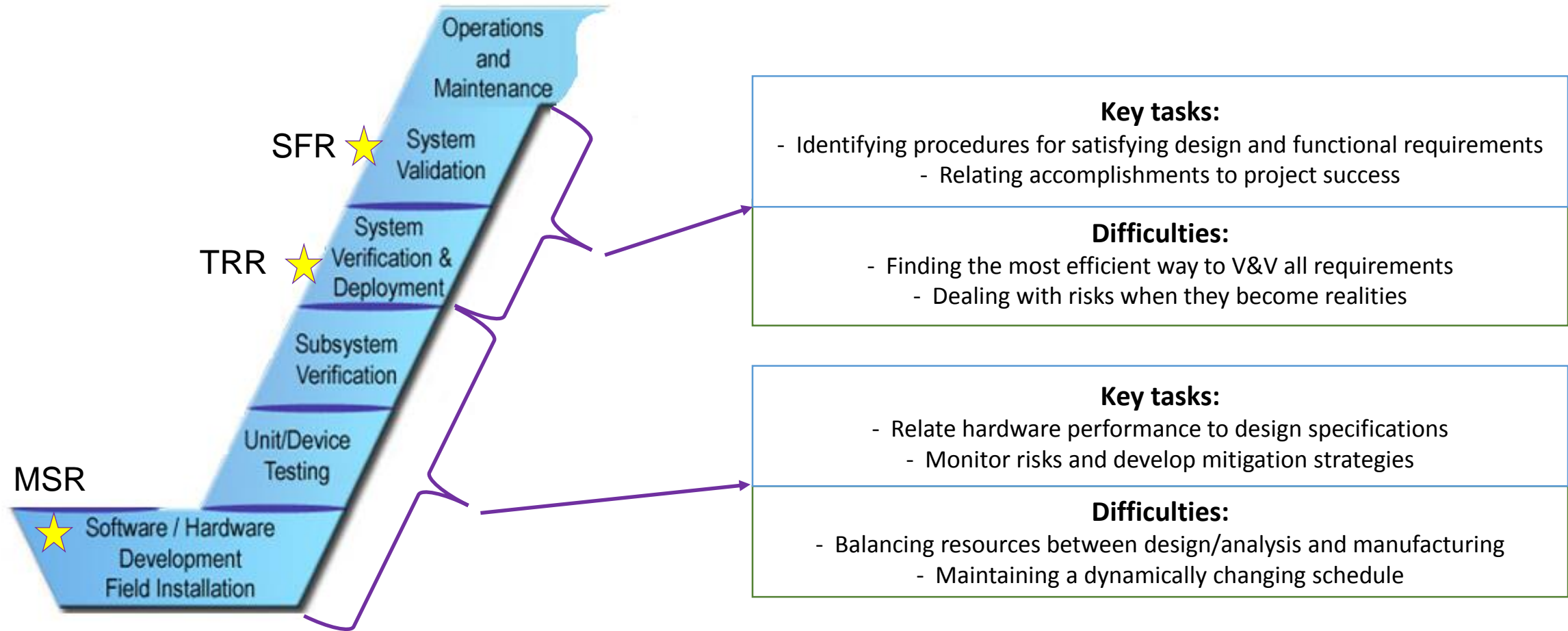
1. Test early and often
2. Link to requirements for verification and validation – make sure requirements are testable!

Systems - Fall Semester



- Lessons Learned:**
- Identify design milestones early
 - Set design limits

Systems - Spring Semester



Lessons Learned:

- Make requirements and levels of success the purpose of actions
- Communication is **essential**

Work Breakdown Structure

REAPER

