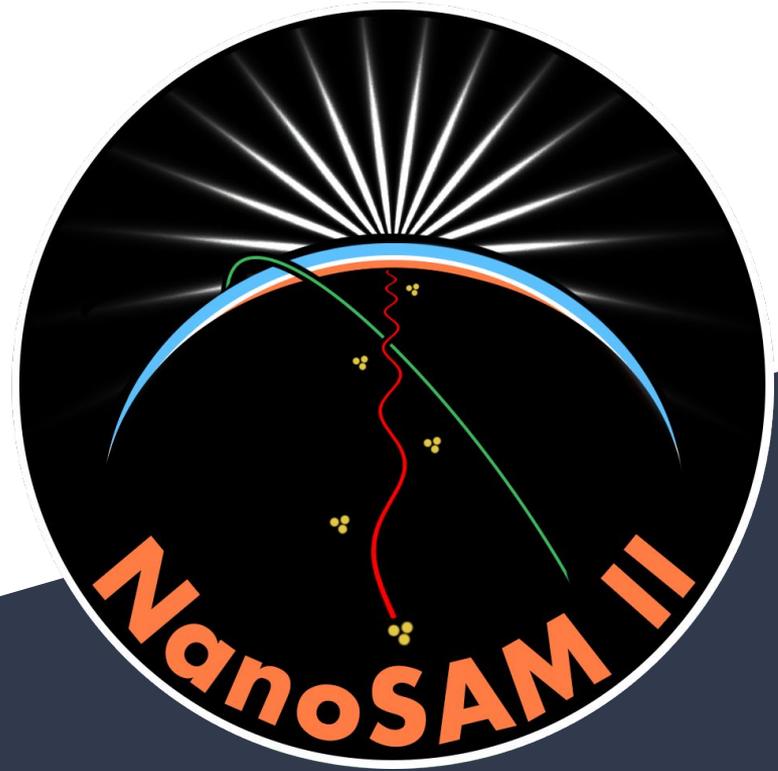


NanoSAM II

Nano-Stratospheric
Aerosol Measurement

Spring Final Review

April 29, 2021



Ball
Aerospace

University of Colorado Boulder
Department of Aerospace Engineering Sciences

Agenda

NanoSAM II
SFR

Overview

Design Description

Test Overview

Test Results

Systems Engineering

Project Management

Project Overview

Jaret Anderson

Project Background & Purpose

SAM/SAGE Instruments

(1979-1984, 2001-2006, 2011-Current)

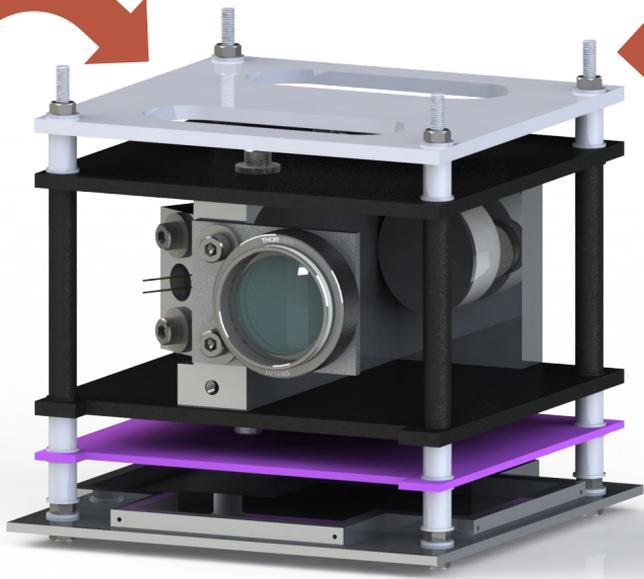
Bulky, High Cost, Low Data Volume



NanoSAM I

(2019-2020)

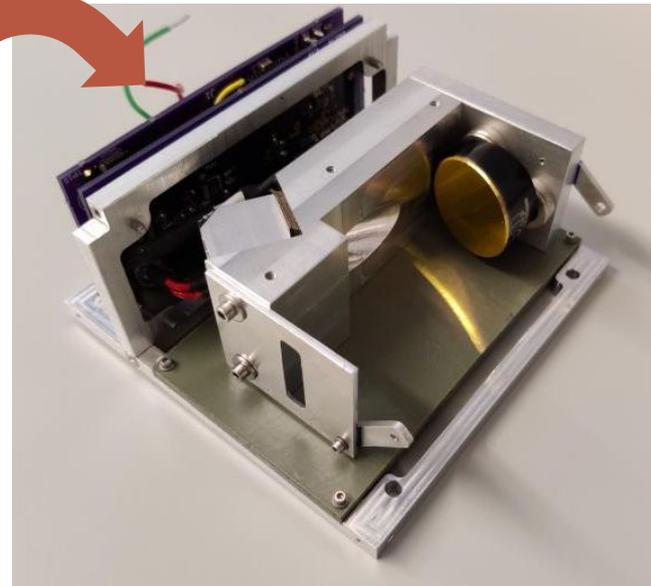
Optical Instrument for
CubeSat Footprint



NanoSAM II

(2020-Current)

Integrated 0.5U
CubeSat Payload



NanoSAM Mission CONOPS



Levels of Success

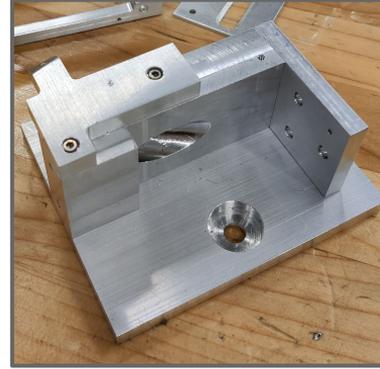
| | Level 1 (solar tracking test) | Level 2 (Improved Ground Performance) | Level 3 (Flight Capability) |
|-----------------------|---|---|--|
| Payload Housing | The payload housing contains the integrated electronics board and optics bench inside a 0.5U enclosure. | The payload housing structural interface is compatible with an industry standard bus. | The payload housing functions within the operating temperature range of -20°C to 50°C and its lowest vibrational natural frequency is greater than 100Hz. |
| Data Capture | Software and electronics acquires, digitizes, packetizes, and downloads raw data from a photodetector to a computer at a rate of at least 50Hz within the mission specific measurement schedule detailed in the CONOPS. | Error checking measures are implemented in the ground software to detect data corruption occurring during transmission. | Data is transferred from the payload to a computer emulating an industry standard CubeSat bus communications system. |
| Electronics & Control | The redesigned electronics board successfully controls and powers all on-board operations and has a footprint compatible with the 0.5U payload enclosure. | The redesigned electronics board supports all optical design improvements. | The redesigned electronics board remains within the operating temperature range of -20°C to 50°C and its lowest vibrational natural frequency is greater than 100Hz. |

Critical Project Elements



Structure

0.5U Payload Form
Factor



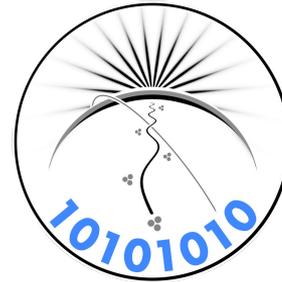
Optics

Match SAM-II
Instrument Legacy
Performance



Electronics

Low-Noise
Signal Processing



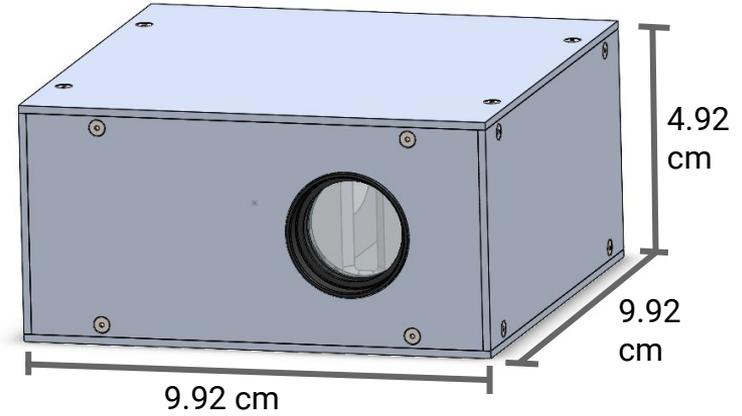
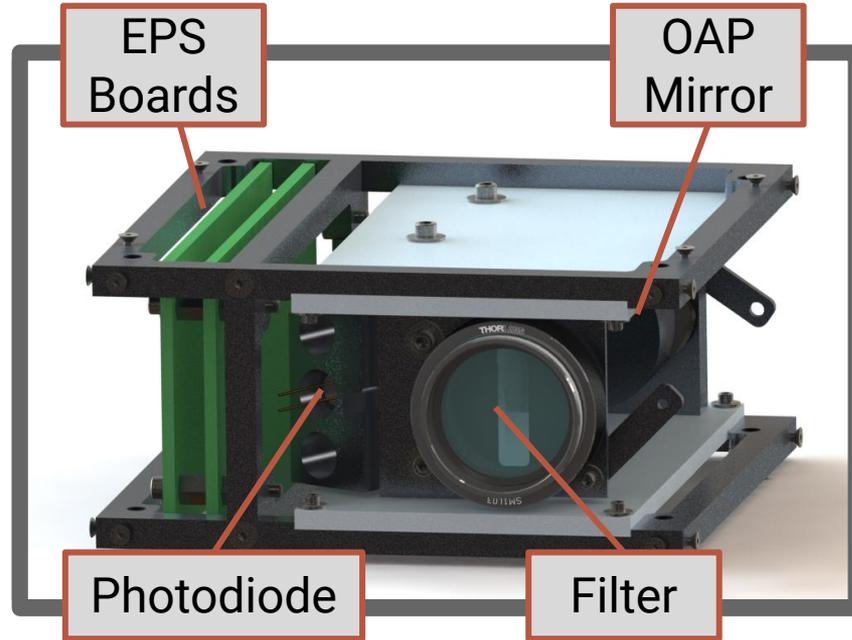
Software

Timely and Reliable
Data Collection

Design Description

Donavon Schroeder

NanoSAM II Payload

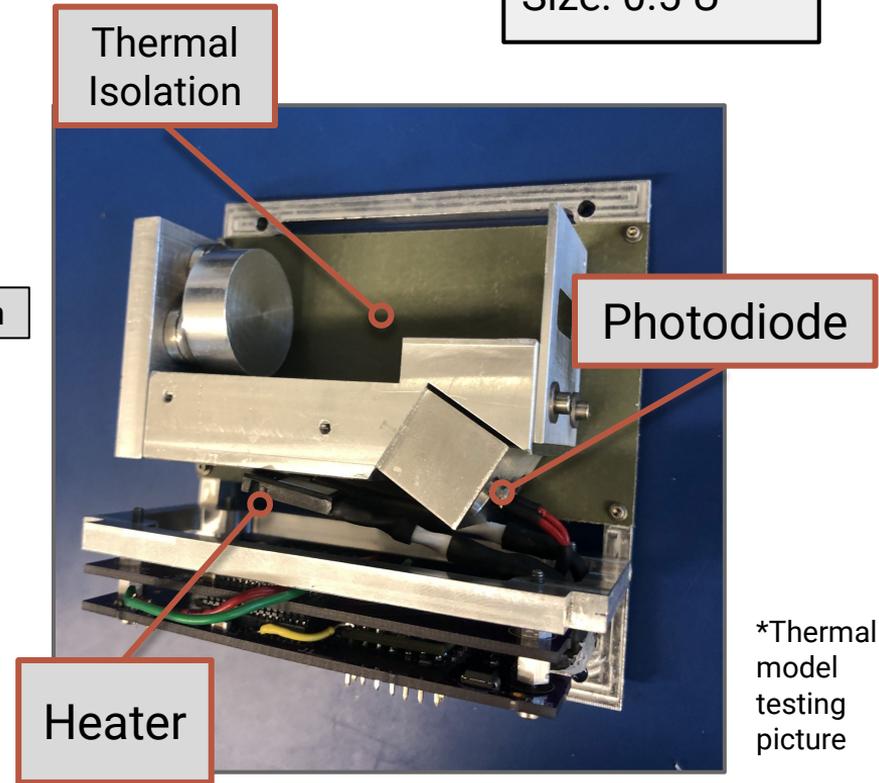
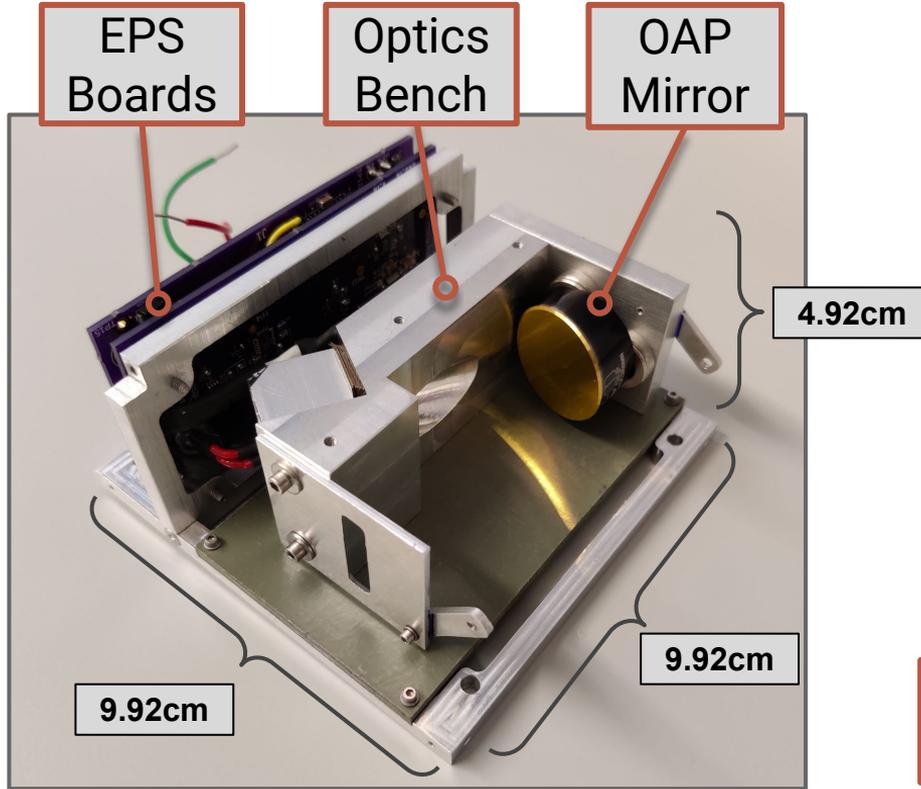


Mass: 0.48 kg
Size: 0.5 U

Gathers Irradiance
Measurements
at 50 Hz

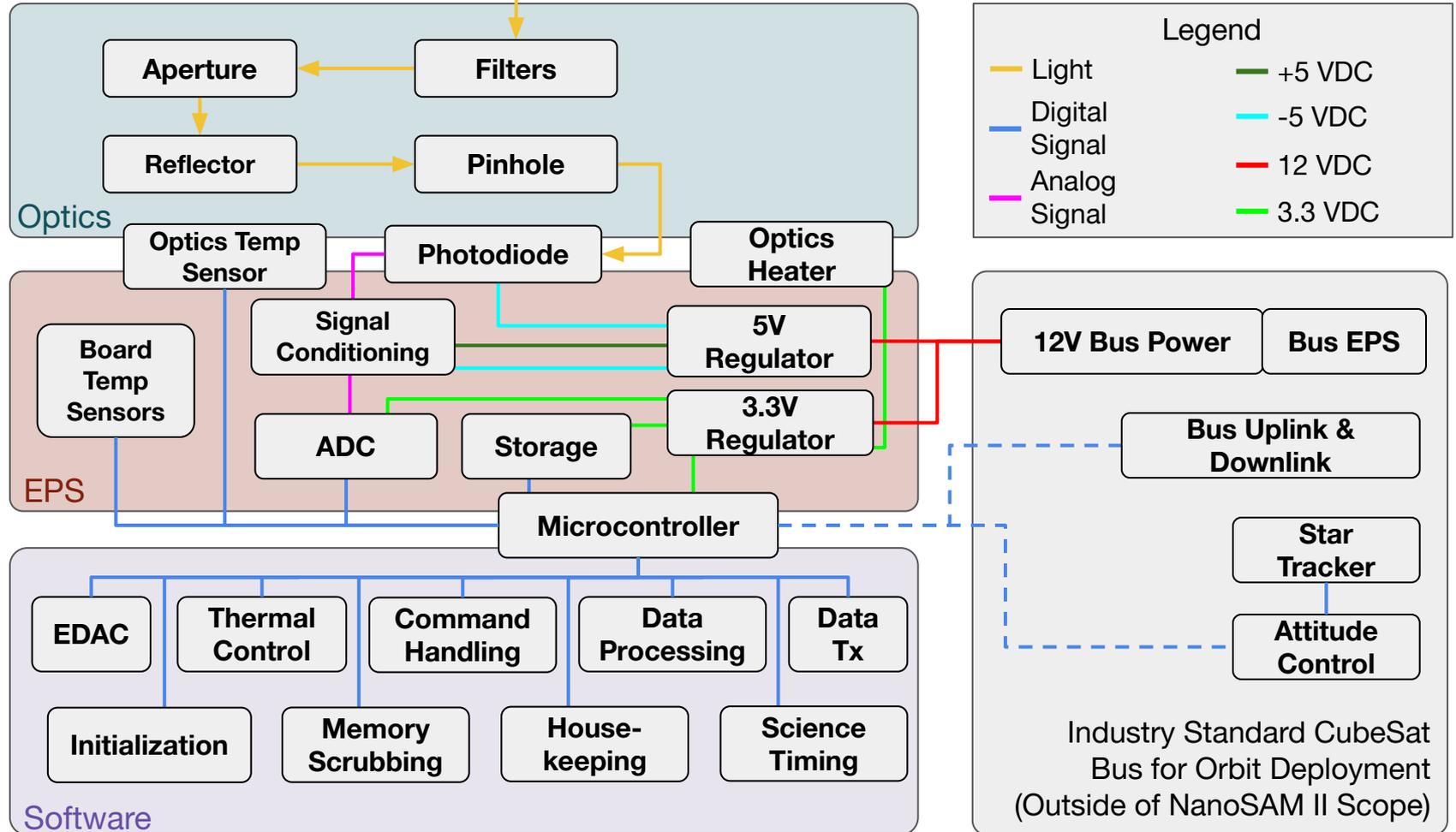
Integrated Payload

Mass: 0.48 kg
Size: 0.5 U



Functional Block Diagram

Updated 11/29/20

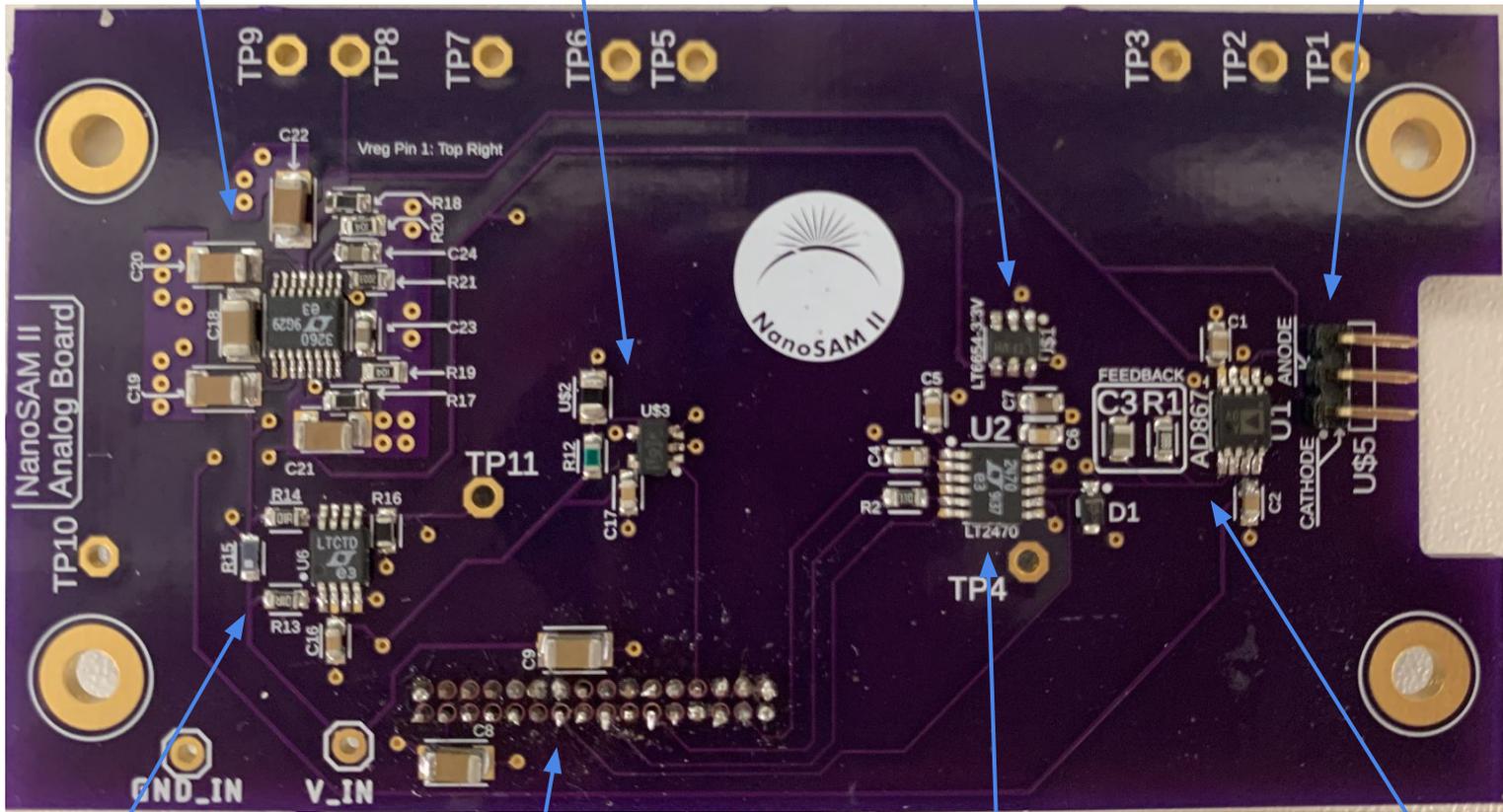


5V Bipolar Regulator

Board Temp Monitoring

3.3V Voltage Reference

Photodiode

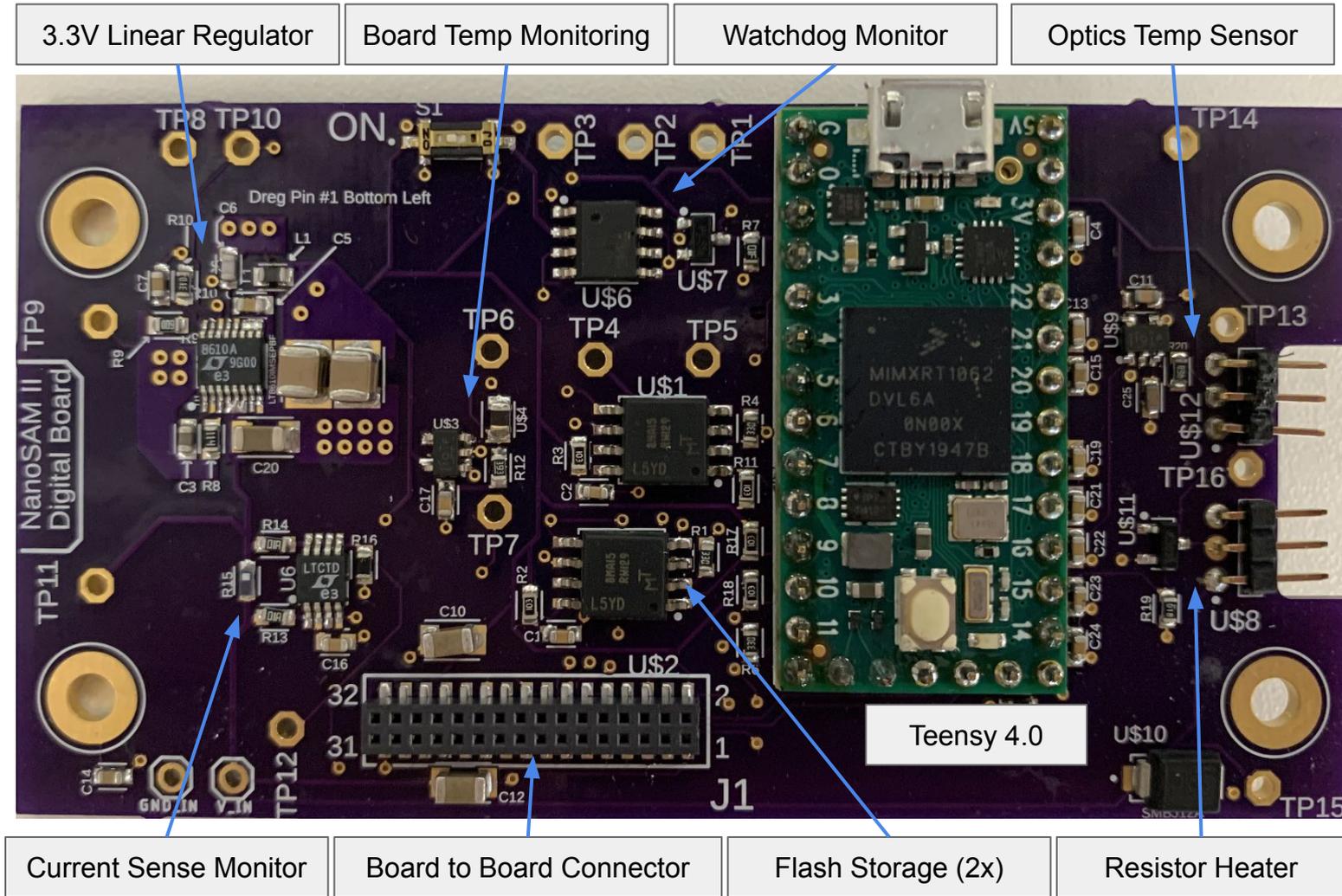


Current Sense Monitor

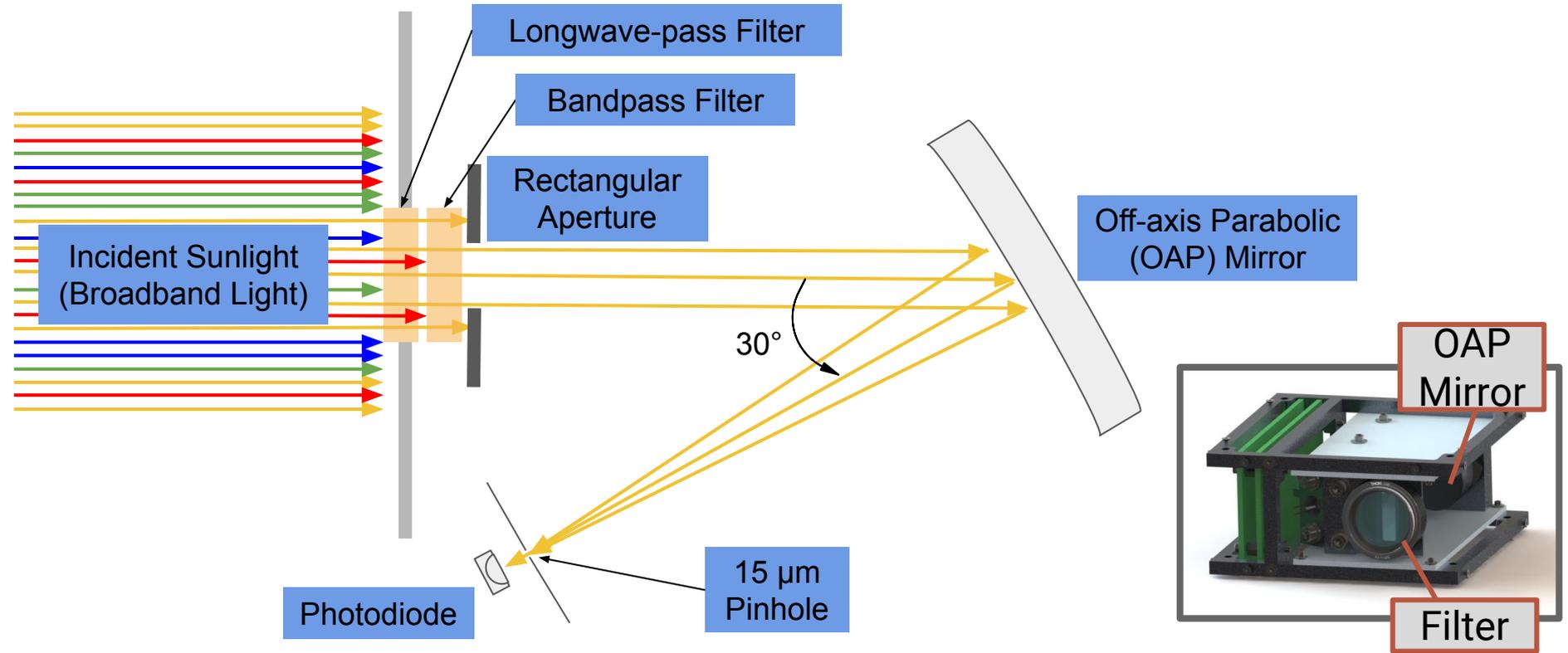
Board to Board Connector

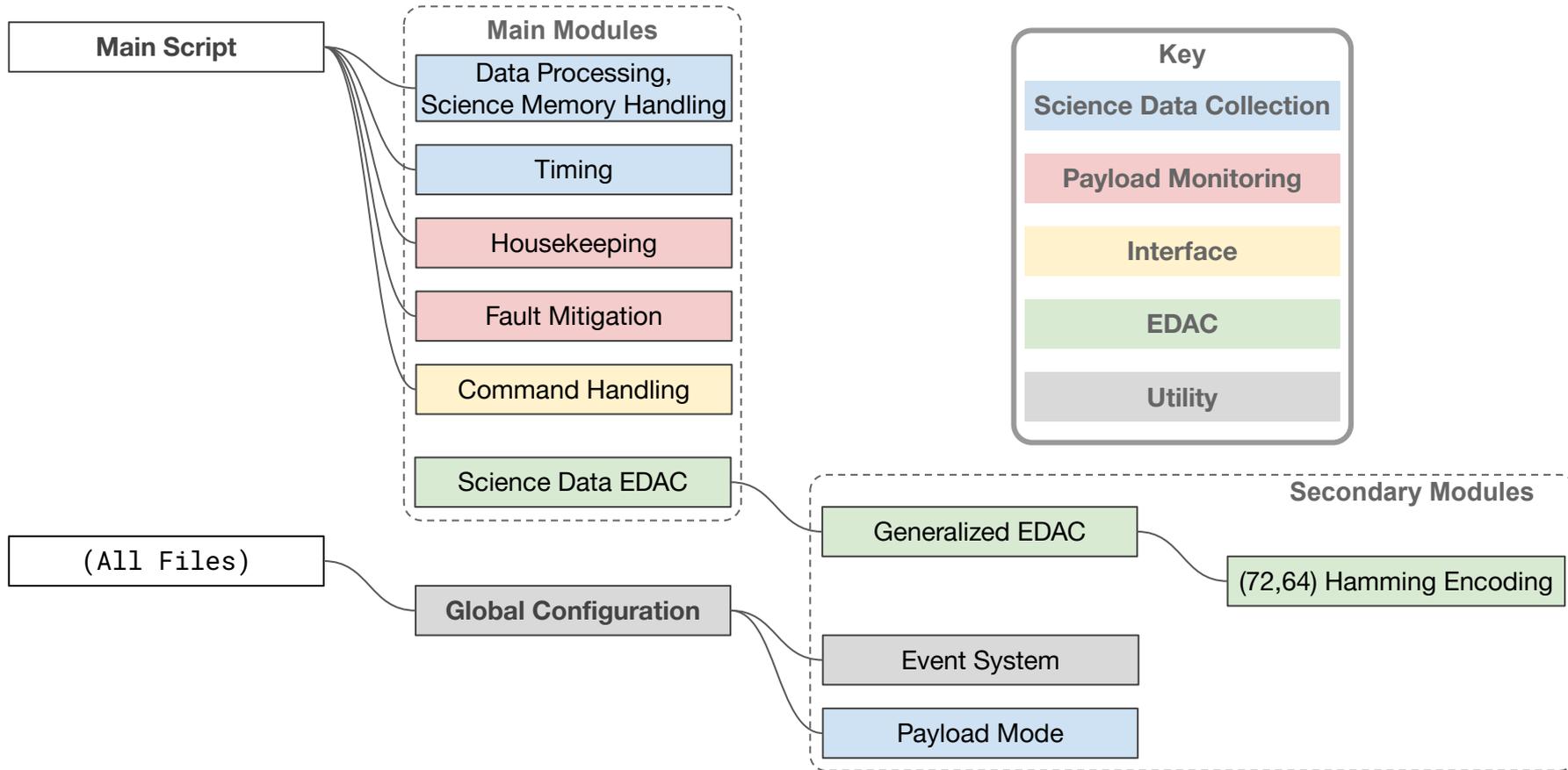
Analogue to Digital Converter

Transimpedance Amp



Optics Final Design





Flight Software Header Tree

Software Data Parameters

Science Data

| | |
|--------------------------------|--------------------|
| Photodiode sample rate: | 50 Hz |
| Sample size (primary ADC): | 16 bits |
| Sample size (backup ADC): | 12 bits |
| Max window duration: | 240 sec |
| Max data per window (encoded): | 27009 Bytes |
| External flash capacity: | 2 x 128 Mb |
| Minimum time to fill flash: | 38 days |

Persistent Payload Data

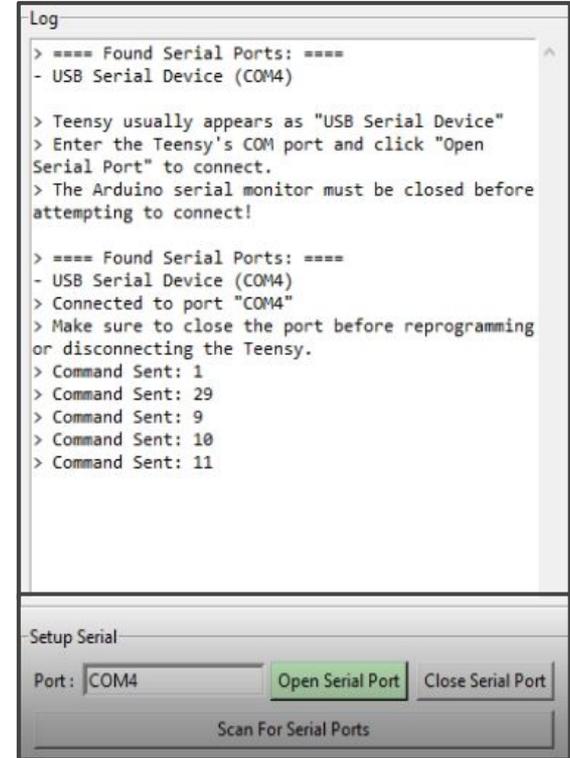
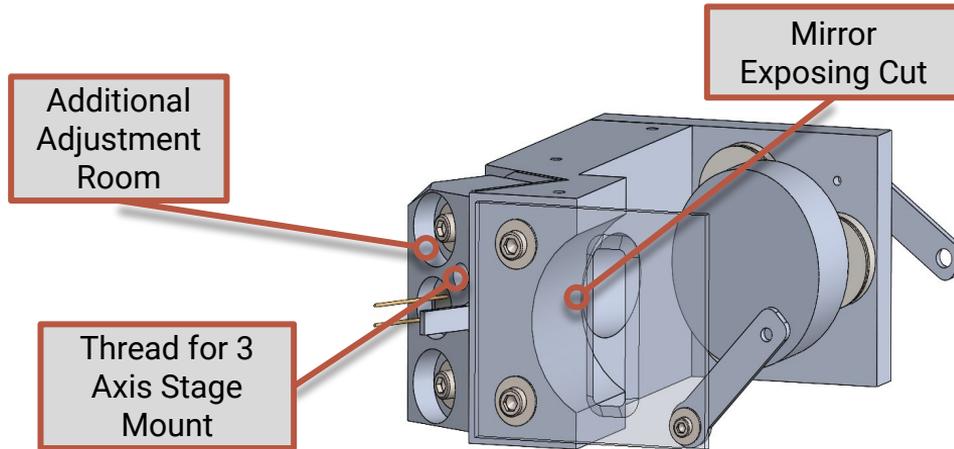
| | |
|-----------------------------------|-------------------|
| Persistent data size (encoded): | 90 Bytes |
| EEPROM size: | 1080 Bytes |
| Max EEPROM writes per address: | 100,000 |
| Max writes with address shifting: | 1,200,000 |

Housekeeping Data

| | |
|------------------------------------|------------------|
| Housekeeping sample rate: | 1 Hz |
| Housekeeping sample size: | 32 Bytes |
| Sample buffer size (5000 samples): | 156.25 kB |

Changes Since TRR

- Software GUI
- Electronics white wire
- Bench drawing modifications
 - Not able to implement in hardware this year, but will be useful for future teams



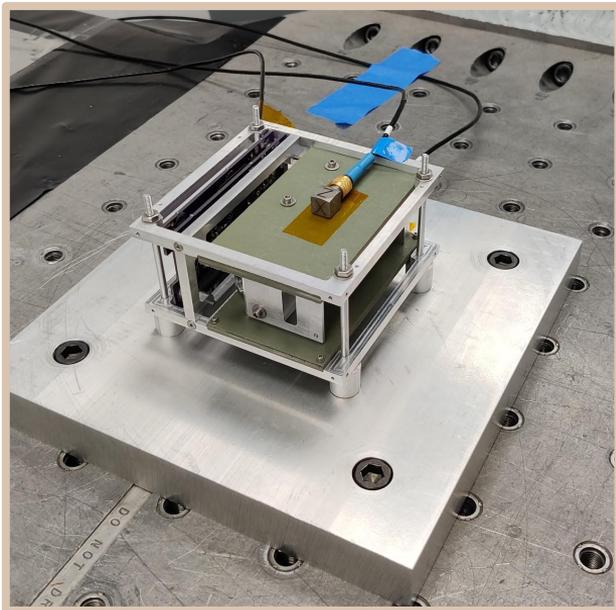
Test Overview

Ryan Smithers

Tests Conducted

| Test | Requirements | Success Level |
|---------------------|--|---|
| Electronics System | Electronics gather 12 bit photodiode samples at 50 Hz | Level 3 (Flight Capable) |
| Data Collection | Payload shall process and store ≥ 10 bit data at 50 Hz for the duration of a data window and communicate this data to a ground computer | Level 3 (Flight Capable) |
| Alignment | NanoSAM II shall have optical performance equivalent to or surpassing those of SAM-II | Level 1 (Solar Tracking Test) |
| Solar Tracking Test | The system shall demonstrate solar tracking accuracy of 1 mRad or finer during ground testing | Level 3 (Flight Capable) |
| Vibration Test | The system shall maintain optics performance following exposure to vibration, Lowest natural frequency shall be > 90 Hz | Level 2 (Improved Ground Performance) |
| Thermal Test | Payload contents shall operate across a temperature range of -20°C to 60°C | Level 1 (Photodiode data not collected as light source could not be used in chamber) |

Vibration Test Objectives

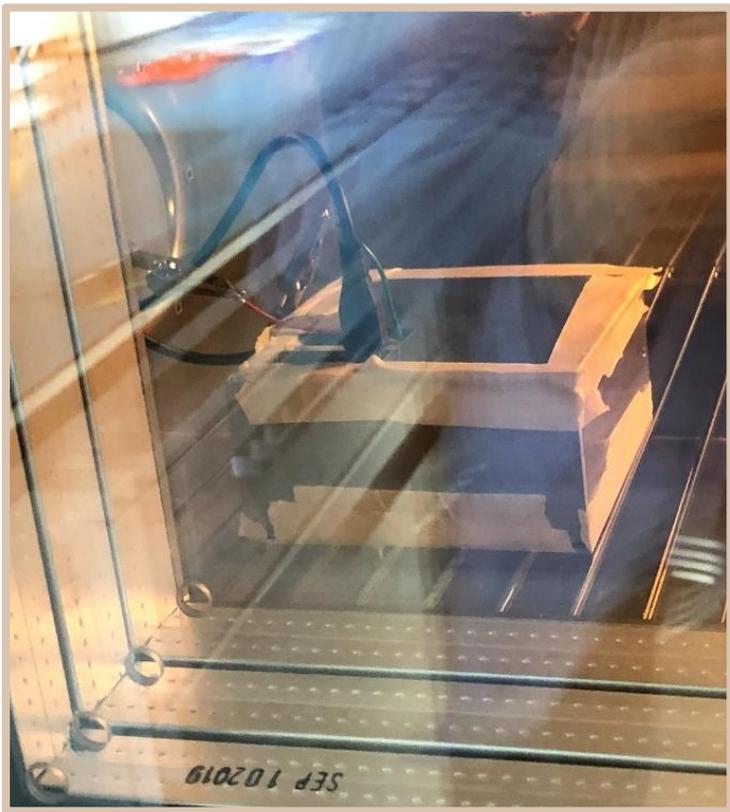


- Determine the resonant frequencies along each payload axis
- Use experimental modes to validate our vibrational model
- Test hardware identical to final hardware, analogous versions of the optics and electronics were used
- Test carried out at Altius Space Machines (Broomfield, CO)

Related Requirements

The system shall maintain optics performance following exposure to vibration - not assessed since optic is not staked
Lowest natural frequency shall be > 90 Hz

Thermal Test Objectives

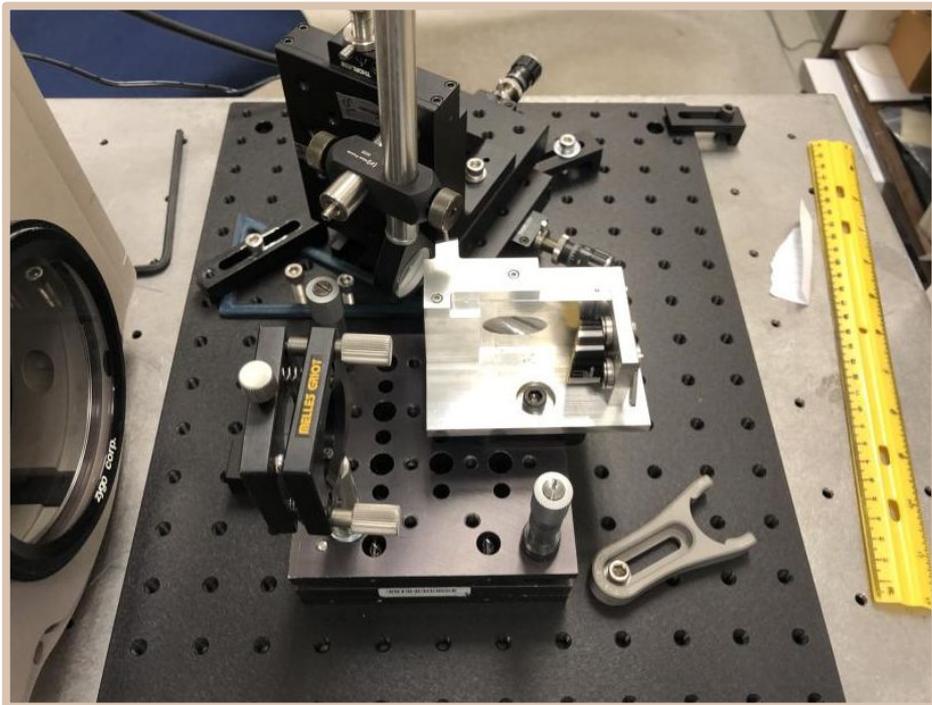


- Gather data: temperature of the optics bench and electronics boards compared to ambient temperature
- Assess the effectiveness of the thermal isolation fiberglass boards used for isolating optics
- Ensure electronics continue to function as the payload reaches the extremes of the temperature requirements
- Test done in a CU thermal chamber

Related Requirements

Payload contents shall operate across a temperature range of -20°C to 60°C

Optics Alignment Objectives

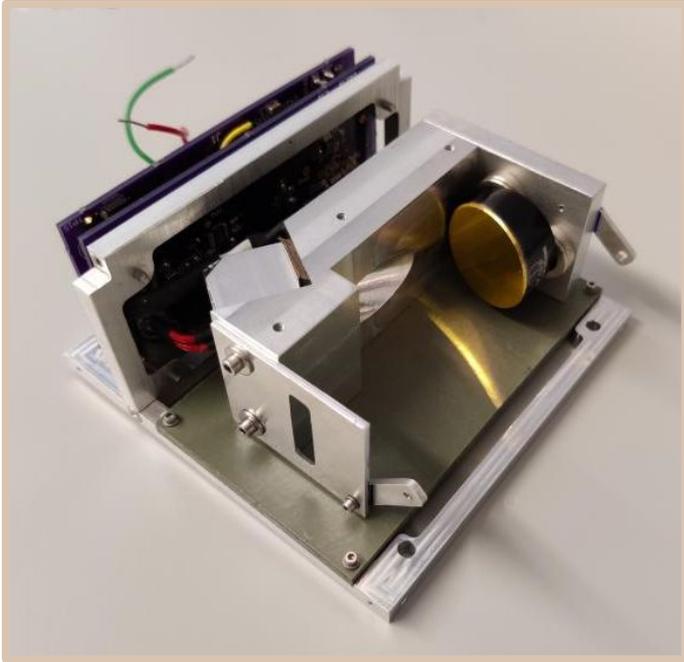


- Use an interferometer to align the optic as best as possible
- Limited timeframe as the interferometer usage has been donated to us by Meadowlark Optics
- Metrics to measure this are modulation transfer function (MTF), defocus, and radial displacement
- Target MTF (derived from SAM-II): 0.74

Related Requirements

NanoSAM II shall have optical performance equivalent to or surpassing those of SAM-II

Regulated Light Test Objectives



- Record photodiode output when receiving optical signal of known source
- Use results to characterize system accuracy by comparing to theoretical irradiance calculations
- Compare the 16-bit and 12-bit ADC results

Related Requirements

Payload shall process and store ≥ 10 bit data at 50 Hz for the duration of a data window and communicate this data to a ground computer

Solar Attenuation Test Objectives



- Full system test, requires all other subsystems to be functional before it can be conducted
- Track the sun as it passes across the horizon and continuously gather irradiance measurements
 - This is as close to our on-orbit operations as we can get with a ground test
- Result of this test is a Langley plot

Related Requirements

Payload shall process and store ≥ 10 bit data at 50 Hz for the duration of a data window and communicate this data to a ground computer

Test Results

Ryan Smithers & Dan Wagner

Validation Status

| Functional Requirement | Tests | Success Level Explanation |
|------------------------------|---|---|
| 0.1 Data Capture | Thermal, Regulated Light, Solar Attenuation | Pending Success, data captured and stored at the proper rate |
| 0.2 Communications | Thermal, Regulated Light, Solar Attenuation | Pending Success, data properly formatted and communicated to ground computer |
| 0.3 SAM II Equivalent Optics | Optics Alignment | MTF req. not met but light passing through system is adequate for testing |
| 0.4 Payload Dimensions | Measurement | Dimensions are within 0.5U CubeSat volume/mass |
| 0.5 Flight Testing | Vibration, Thermal | Vibrational Modes met requirement, Optic was not staked for testing, photodiode measurements were not taken during thermal test |
| 0.6 Cost | Analysis | Project came in \$1000 under budget |

Success Level: Level 3, Level 2, Level 1, Failed, Pending

Vibration Test Results

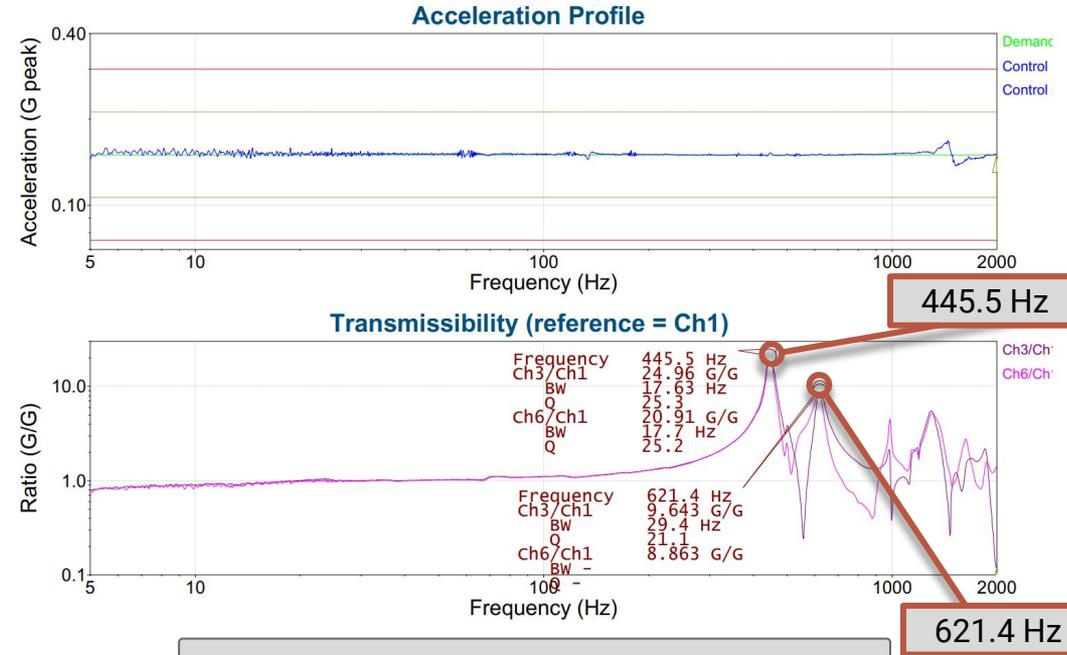
Level 2 Success

Improved Ground Performance



- 0-2000 Hz 3 Axis Resonance Survey Conducted at Altius Space Machines
- Meets requirement as there are no resonant frequencies below 90 Hz
- Lowest frequency from survey was 445 Hz compared to 962 Hz from Model
- Model extremely sensitive to boundary conditions

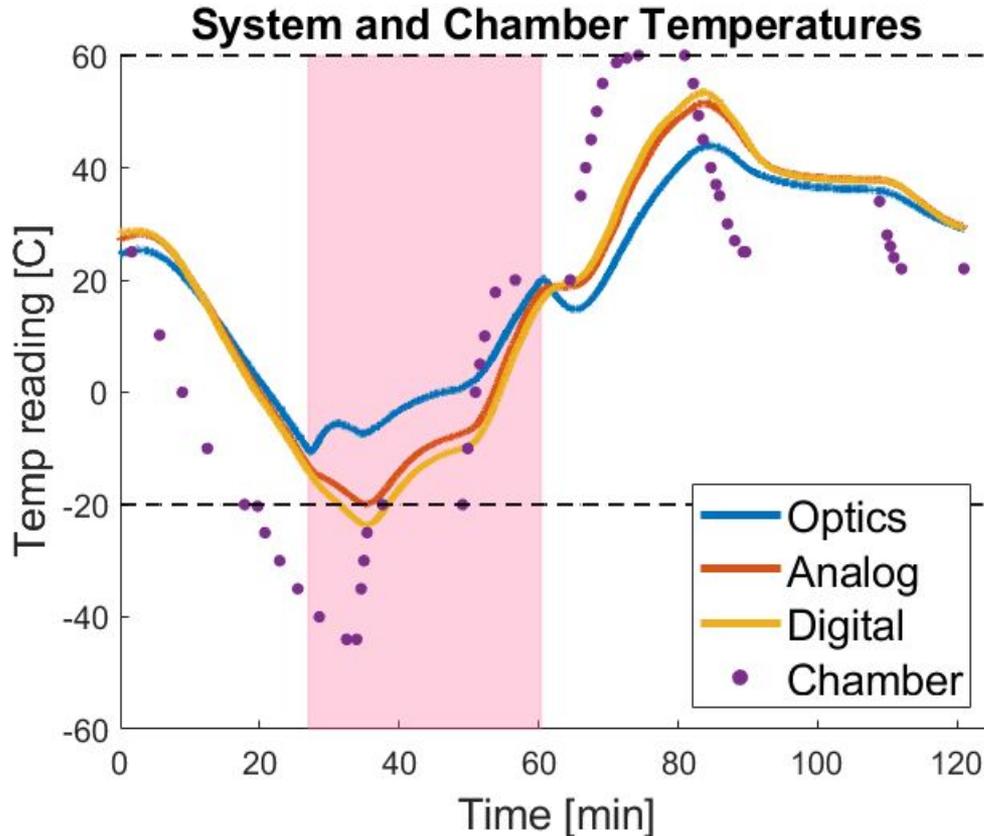
Test Report



Test Results - Y Axis (Normal to Electronics Boards)

Thermal Test Results

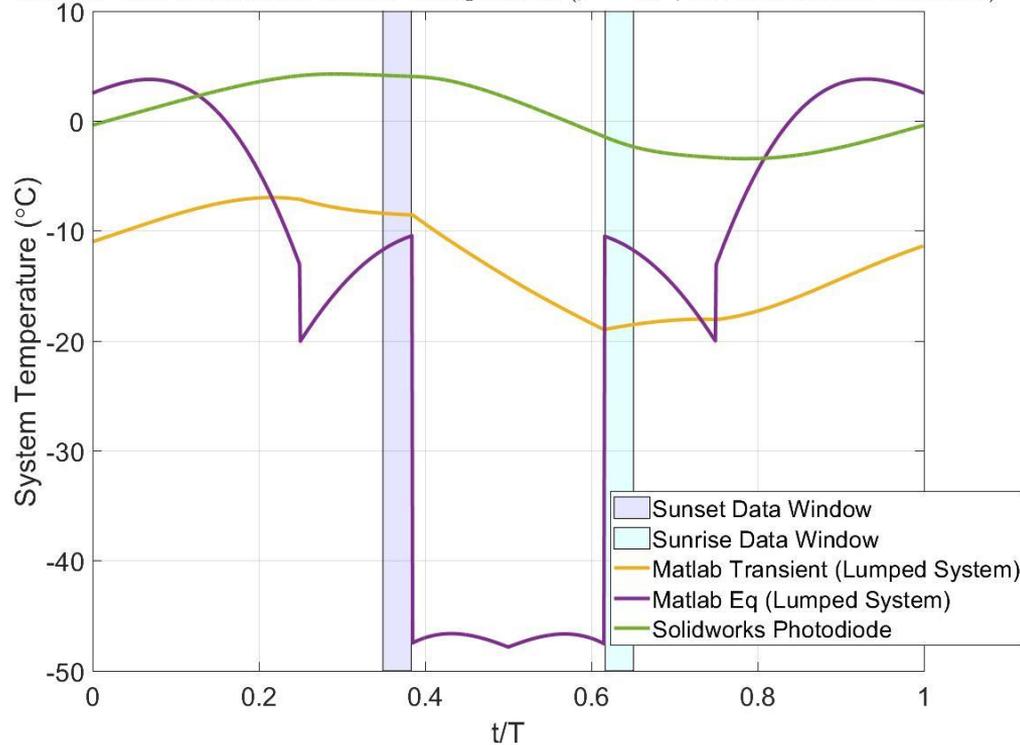
Test results incomplete
No success level satisfied



- Photodiode data was not gathered so thermal requirements could not be fully verified by this test
- Shallower slopes in optics temperature curve compared to electronics temperature curves
 - Suggests thermal isolation efforts were effective
- No vacuum in this test, so it is not representative of spaceflight conditions
- We recommend adding a photodiode temp sensor to create a clearer profile of the entire bench

Thermal Model Validation

Matlab and Solidworks Model Comparison ($\beta = 60^\circ$, Black Anodize Exterior)



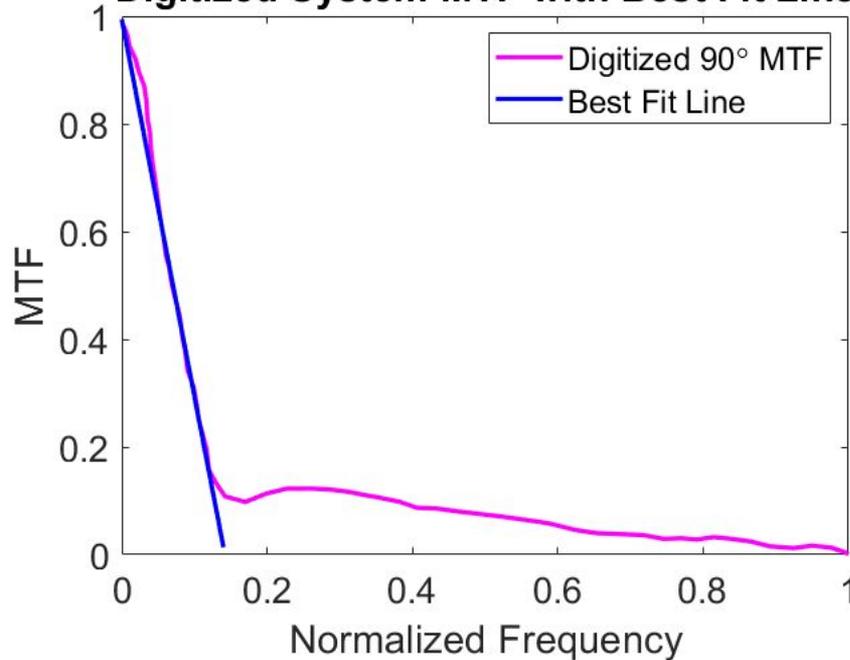
- Heater updated to dissipate 2.4 W (+/- 0.1 W), electronics boards produce negligible heat
- Temperature of the system still stays within the allowable range (-20 °C to 50 °C) with average conditions
- Further analysis needed
 - Equilibrium temperatures were extrapolated from data
 - Still large uncertainty in the power output of the heater and electronics boards due to nature of the test

Optics Alignment Results

Level 1 Success

Solar Attenuation Test Capable

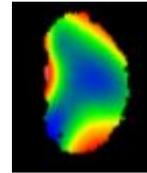
Digitized System MTF with Best Fit Line



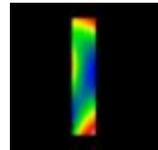
- Mirror MTF at 0.0815 (1 km): 0.4233
- System Target: 0.74
- NSI Mirror MTF: N/A

- System Defocus, ϵ_z : 0.2941 mm
 - Target: 0.045 mm
 - NSI Defocus: 0.735 mm
- Max Radial Displacement, ϵ_r : 0.0676 mm
 - Target: 0.030 mm
 - NSI Radial: 0.159 mm

WFE
Maps:
w/o aperture



With aperture

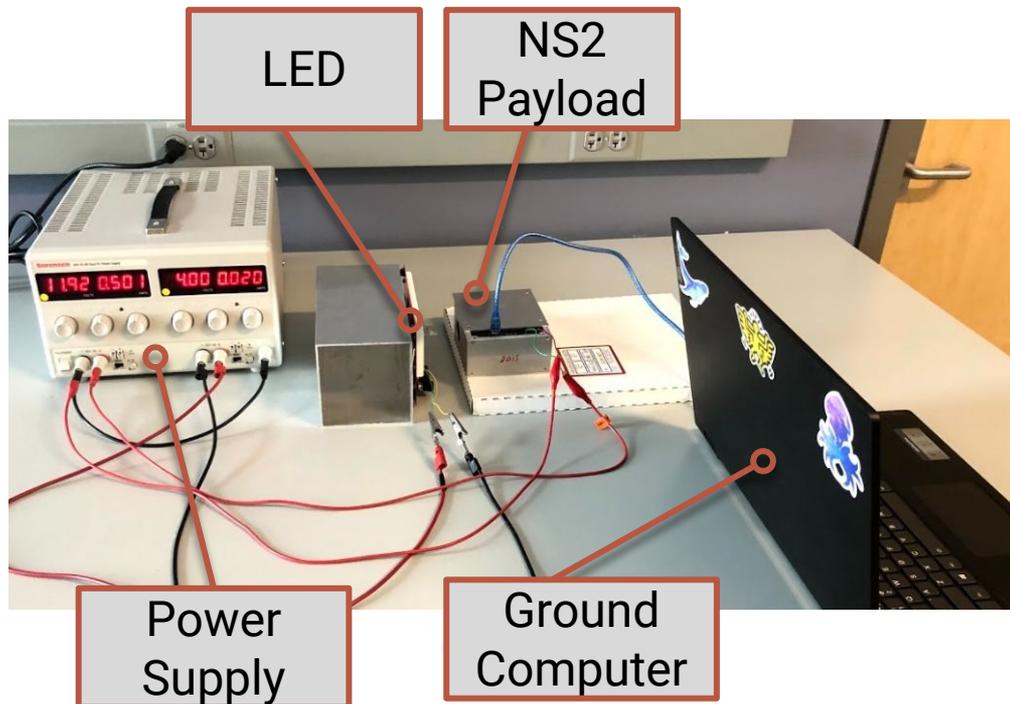


Regulated Light Test

Failed

Due to test design

- Indoor test to quickly validate functionality before solar attenuation
- Test Failed
 - Incoming light rays were not parallel
- But there were positives...
 - Solar Attenuation Test covers remaining unknowns
 - SNR, Error, Measurement Stability
 - Pinhole and Photodiode work independently



Solar Attenuation Test Status

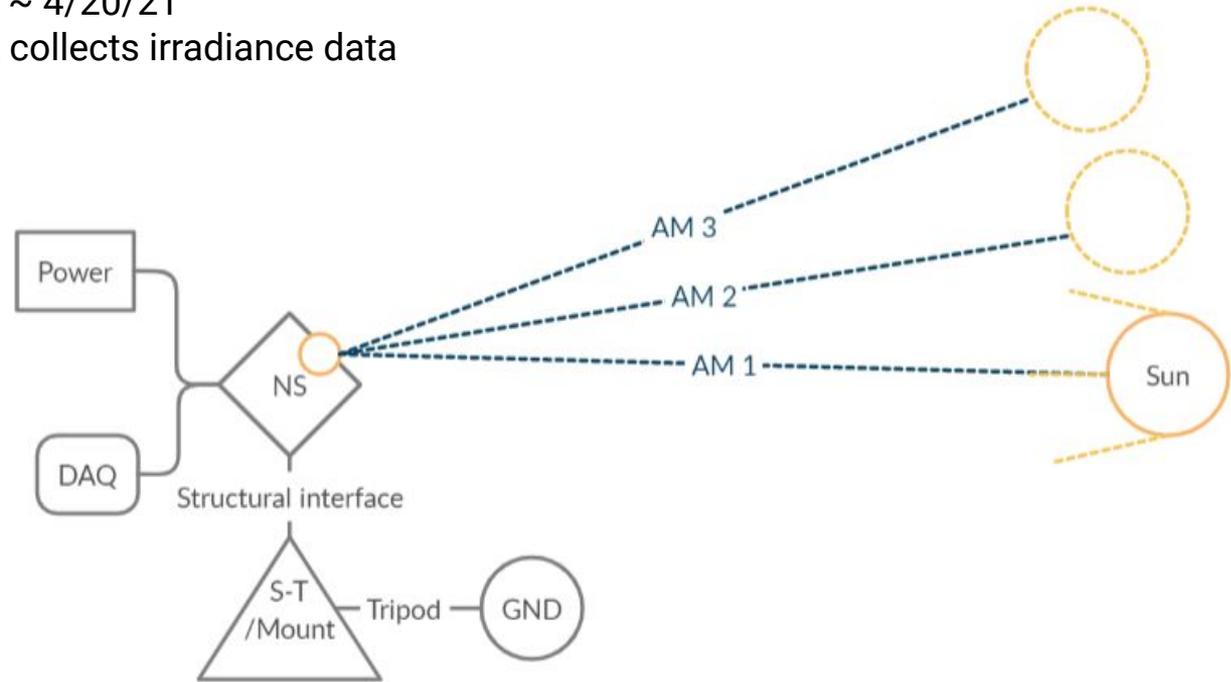
Upcoming

Success level unknown

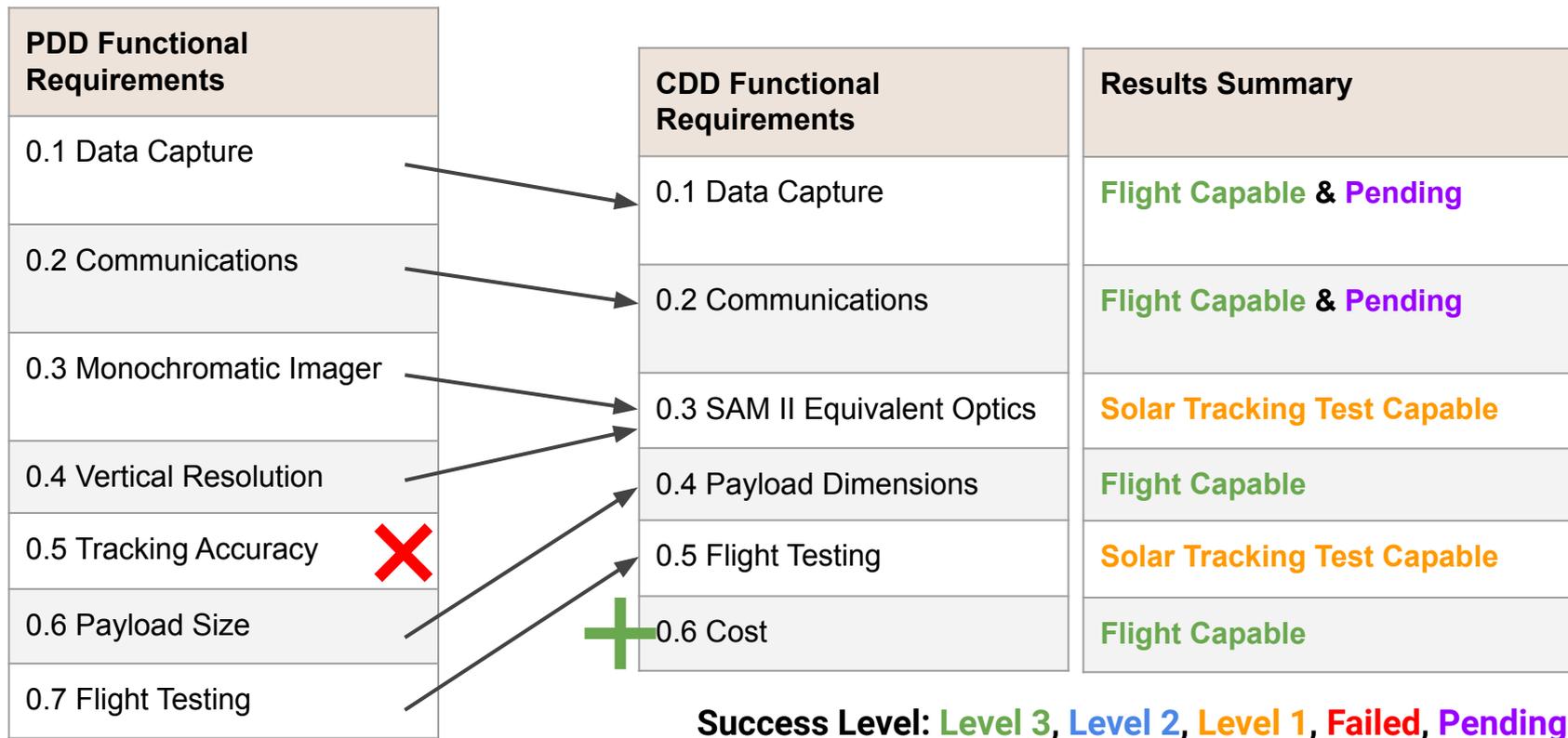
- Test with final assembly of NSII
 - Final assembly competed ~ 4/20/21
- Ground test, using solar tracker, collects irradiance data
- Dependent on weather
- Test data range: 4/(20-30)/21



Solar tracker



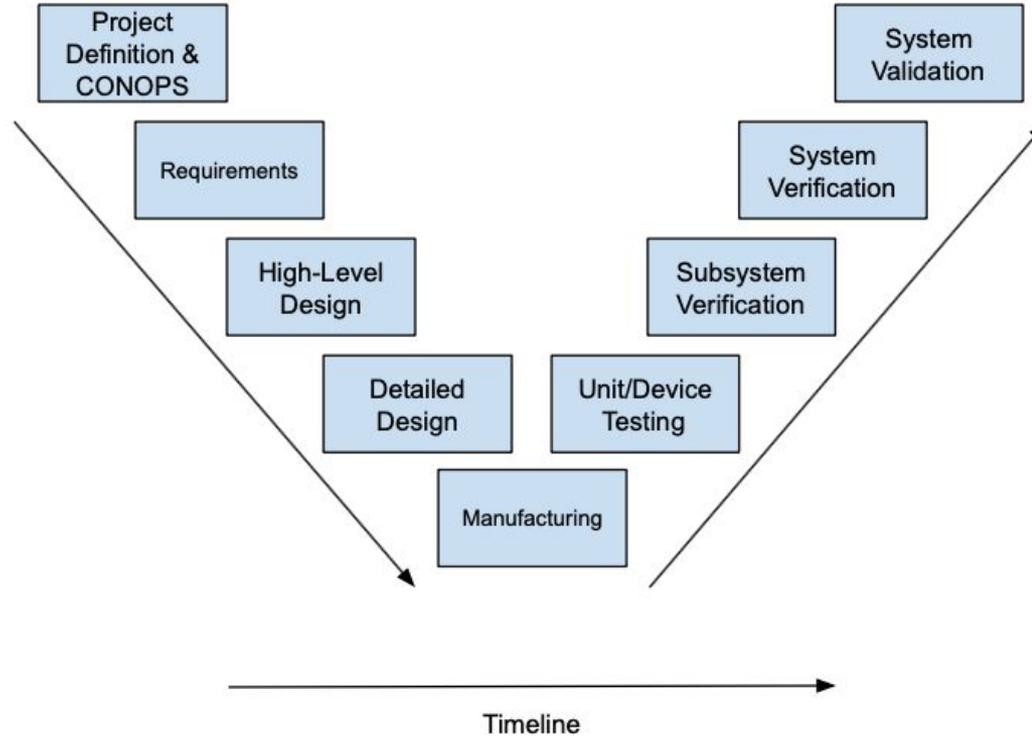
Reflection on PDD Requirements



Systems Engineering

Donavon Schroeder

Systems Engineering Approach



Risks Predicted vs. Issues Encountered

| | Negligible Impact | Low Impact | Moderate Impact | Extreme Impact | Catastrophic Impact |
|------------------------|--------------------|-----------------------------|-----------------------------|--------------------------------|------------------------------|
| Almost Certain | | | | | |
| High Probability | | Short inability to downlink | | | |
| Moderate Probability | | | Photodiode Temp Changes | | |
| Low Probability | Single ADC Failure | Main loop below 50Hz | | Structure fails vibration test | |
| Negligible Probability | | | Unable to get return sphere | Components not manufacturable | No alignment facility access |

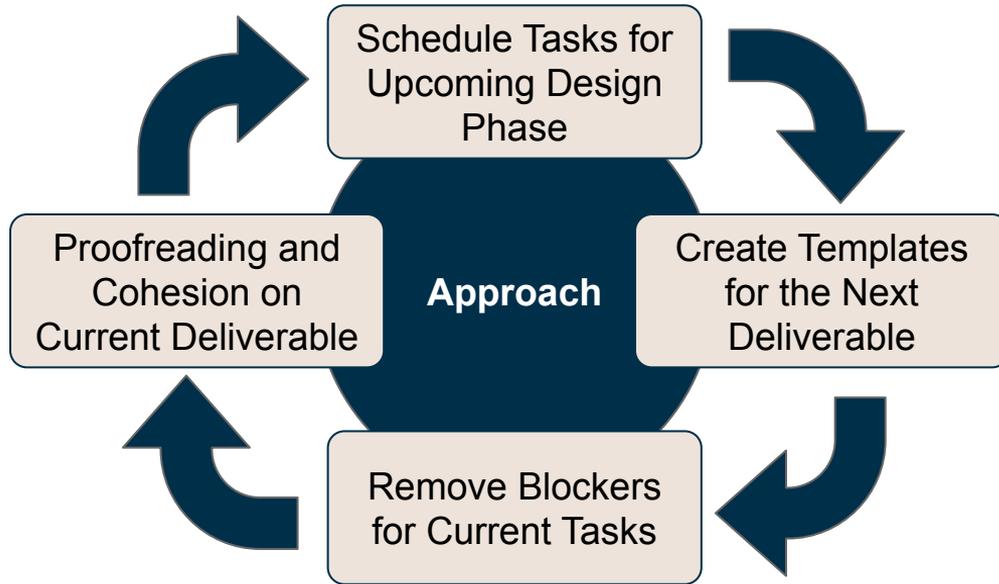
Lessons Learned

- Many of our official tests had overlap
 - Understanding of how the requirements are met
- Integration of subsystems was harder to anticipate than predicted
 - Individual assembly procedures were not continuous during full system integration
 - Heater adhesive
 - Photodiode connectors
- Even though everyone started with same documentation, gaps in knowledge developed
- Impact of subsystem changes to other subsystems
 - Status should include how changes may affect other subsystems

Project Management

Jaret Anderson

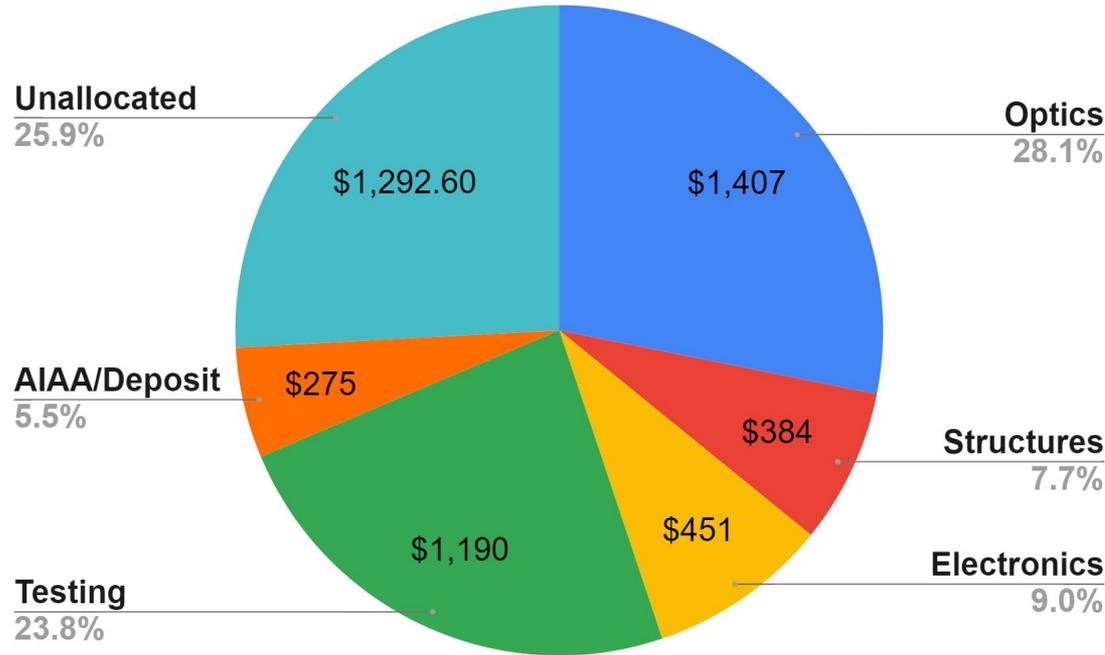
Approach & Lessons Learned



Lessons Learned

- Clear role expectations ensure that tasks are not forgotten, but can lead to uneven work distributions
- We used a peer-review system in software which worked really well
 - Three people all had to sign off on a commit before it was pushed to the main branch
 - Should have used this rigorous review system on our testing procedures as some of our tests ended up not being

Final Budget Summary/Comparison

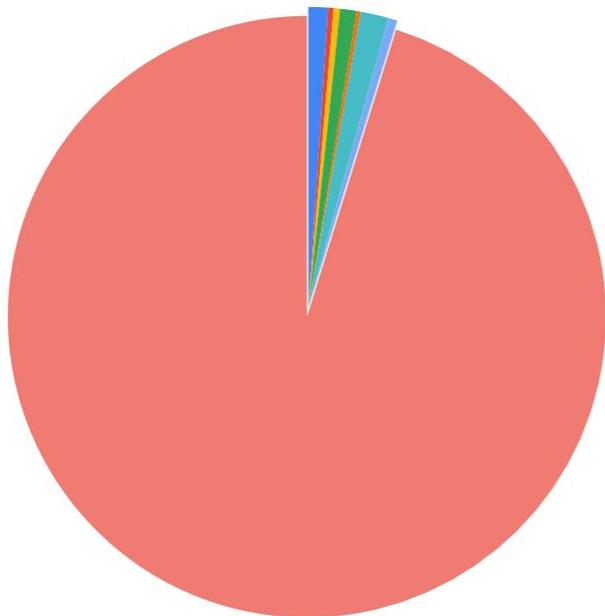


Reasons for changes

- Testing costs allocated
 - Uncertainty in facilities at CDR left margin for testing in the unallocated funds
- New OAP not ordered
- Minor electronics redesign required going over margin slightly

Total Industry Cost

Industry Cost (200% overhead applied)



- Optics
- Structures
- Electronics
- Testing
- AIAA/Deposit
- Meadowlark Alignment
- Thermal Testing
- Labor

| Category | Cost |
|----------------------|-----------|
| Optics | \$2,814 |
| Structures | \$768 |
| Electronics | \$902 |
| Testing | \$2,380 |
| AIAA/Deposit | \$550 |
| Meadowlark Alignment | \$4,000 |
| Thermal Testing | \$1,300 |
| Labor | \$251,532 |
| Total | \$264,277 |

Acknowledgements

Our Customers:

Jim Baer & Jaykob Velasquez
Ball Aerospace

CU Aerospace Department:

Dr. Allison Anderson
The PAB

Our Peer Evaluators:

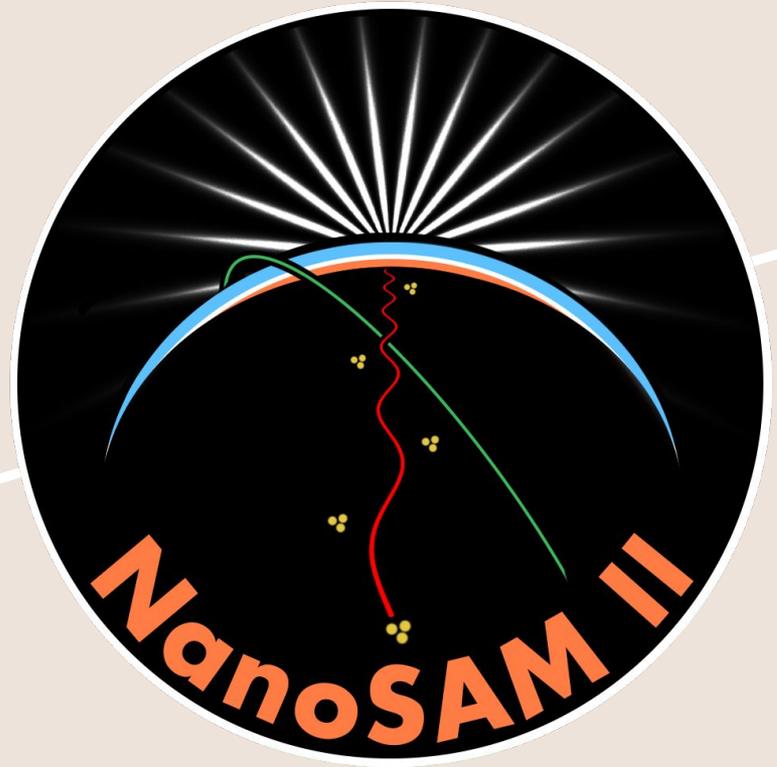
Lara Buri & Colin Claytor

... and all of our personal friends who
should send us a bill for their time
doing engineering review

Our Local Professionals:

Meadowlark Optics Inc
Blue Canyon Technologies
John Ferguson

Questions



References

[1] QB50: System Requirements and Recommendations. Issue 7, Section 1.6 "Thermal Control" and Section 2.2 "Resonance Survey." Published 13 Feb 2015.

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[3] Henninger H. John, "Solar Absorptance and Thermal Emittance of Some Common Spacecraft Thermal-Control Coatings" Goddard Space Flight Center, April 1984.

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[5] Mason, J. & Woods, T. "Miniature X-Ray Solar Spectrometer (MinXSS) – A Science-Oriented, University 3U CubeSat."

<https://arxiv.org/pdf/1508.05354.pdf>

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https://pc104.org/wp-content/uploads/2015/02/PC104_Spec_v2_6.pdf
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<https://www.nrel.gov/grid/solar-resource/spectra-astm-e490.html>
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Version 7.0, 30 Sep 2015, updated 29 March 2019. <https://standards.nasa.gov/standard/gsfc/gsfc-std-7000>
- [11] Kim, Sung-Hwa & Hwangbo, Chang-Kwon. “Temperature Dependence of Transmission Center Wavelength of Narrow Bandpass Filters Prepared by Plasma Ion-Assisted Deposition.” Journal of the Korean Physical Society. Vol. 45, No. 1, July 2004. https://inis.iaea.org/search/search.aspx?orig_q=RN:41100734
- [12] McCormick, M. P. Et. Al. “Satellite Studies of the Stratospheric Aerosol.” Bulletin American Meteorological Society. Vol. 60, No. 9, September 1979.

Backup Slides

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Management

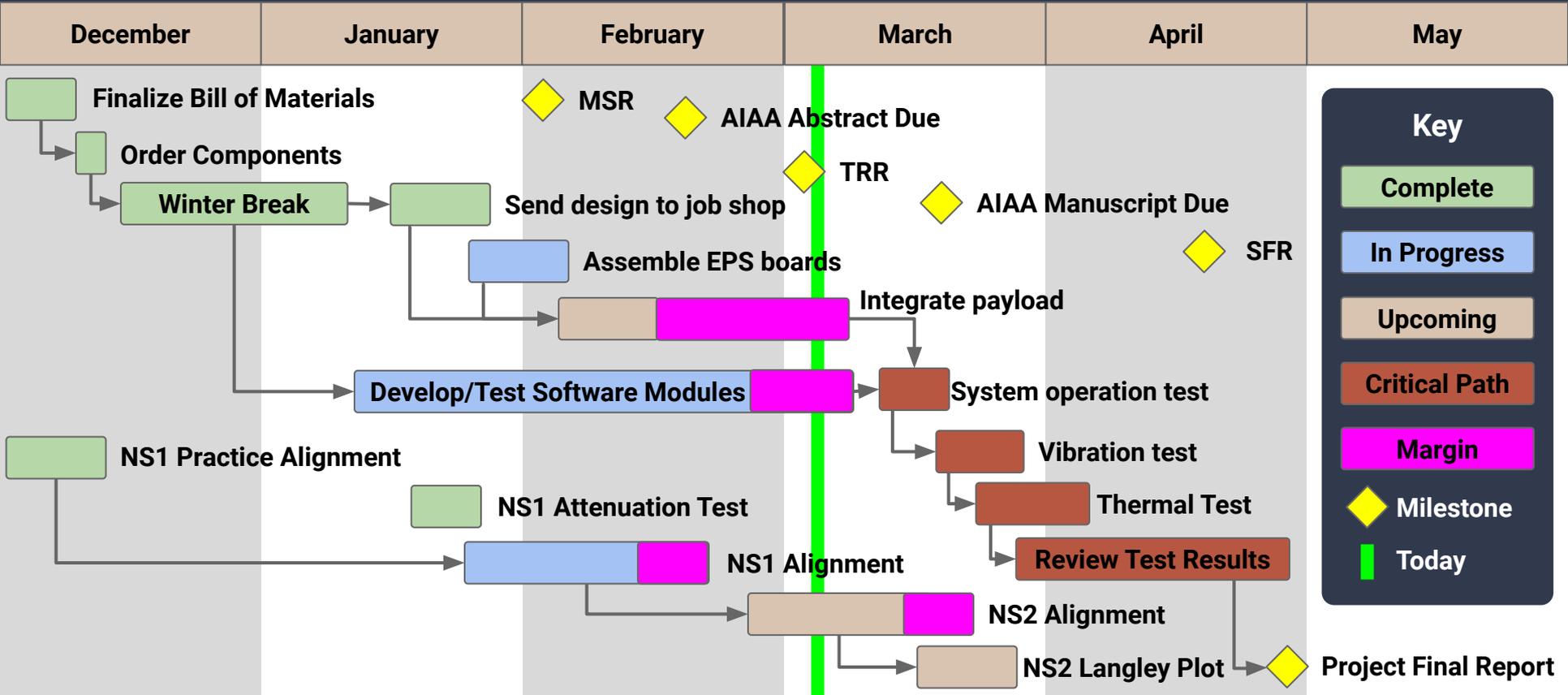
121 - 133

Testing

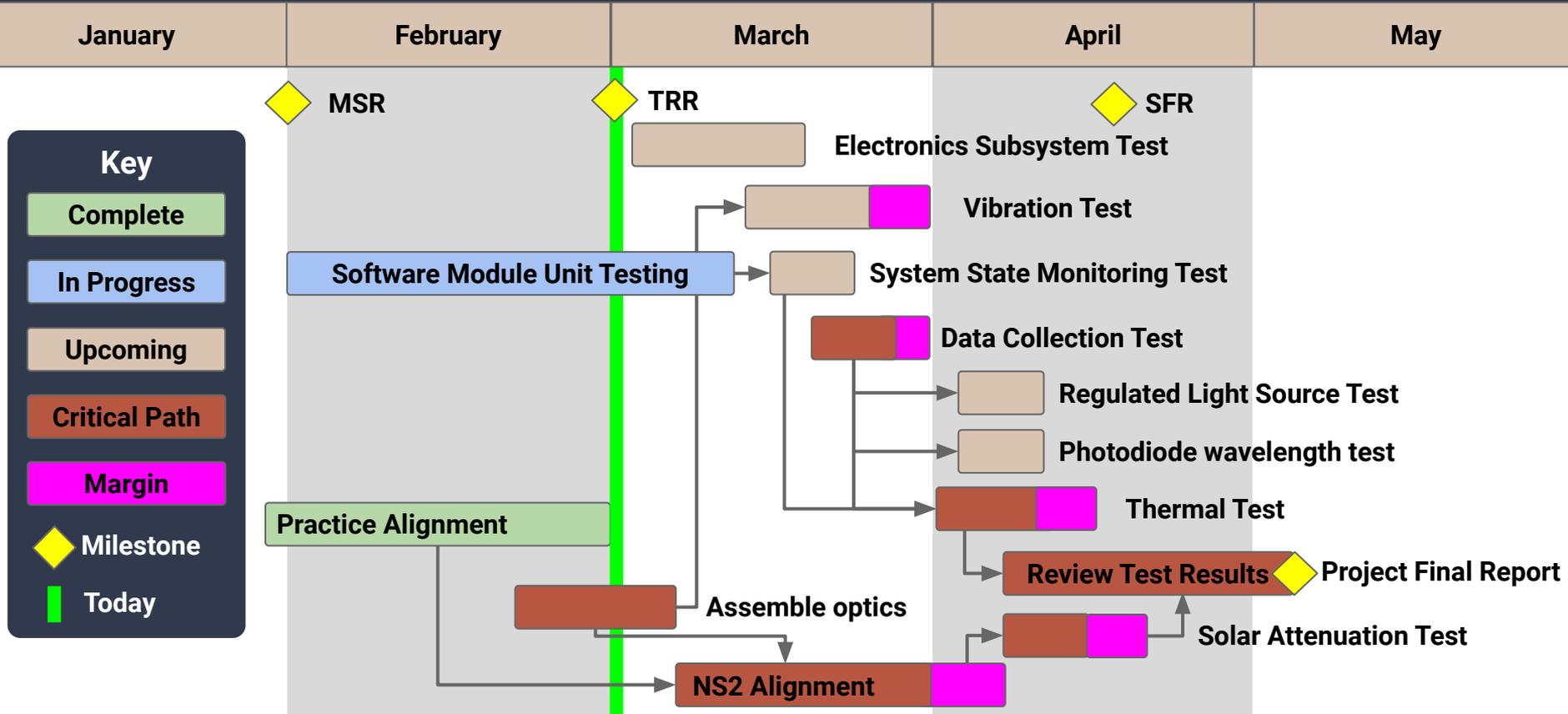
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Backup Slides

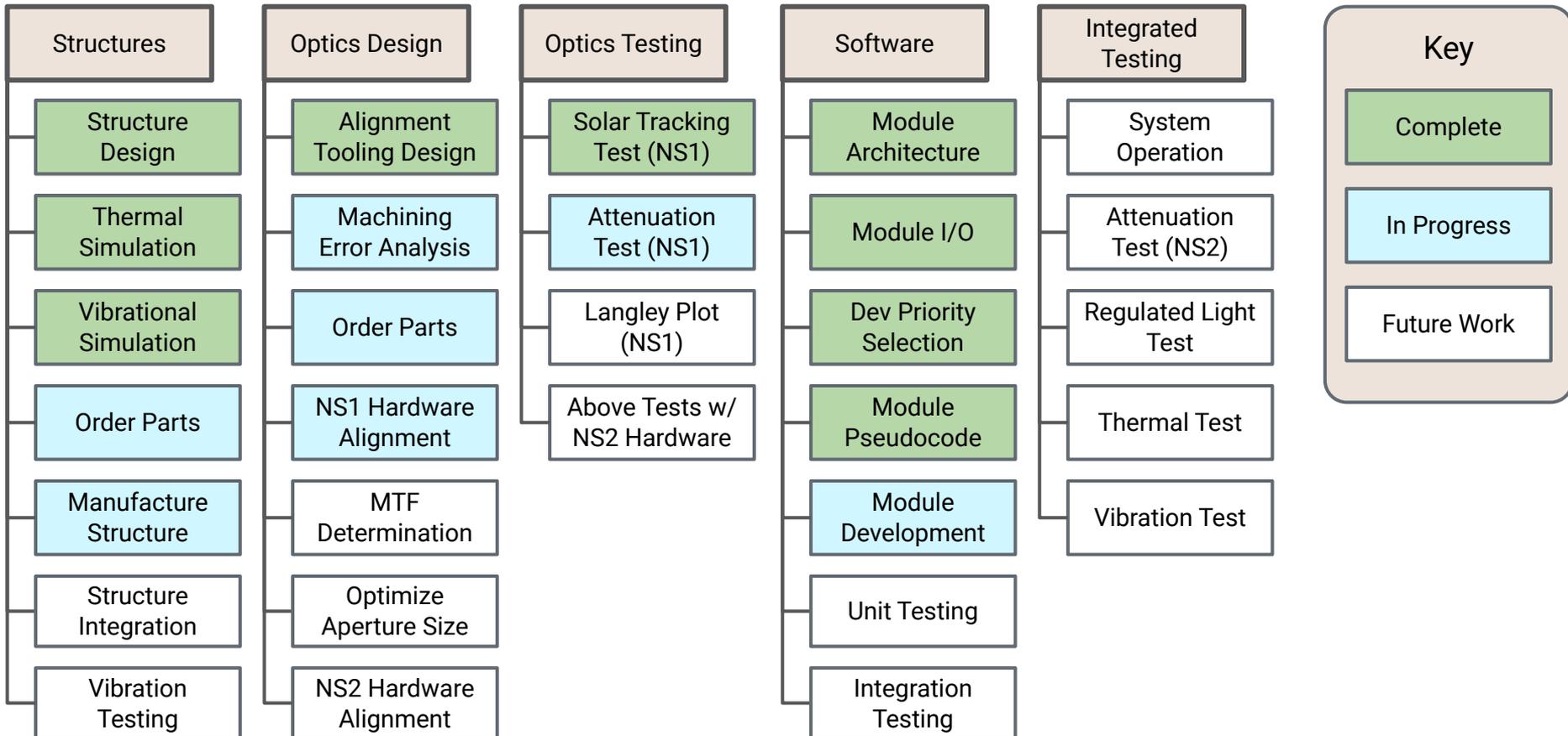
Old Schedule



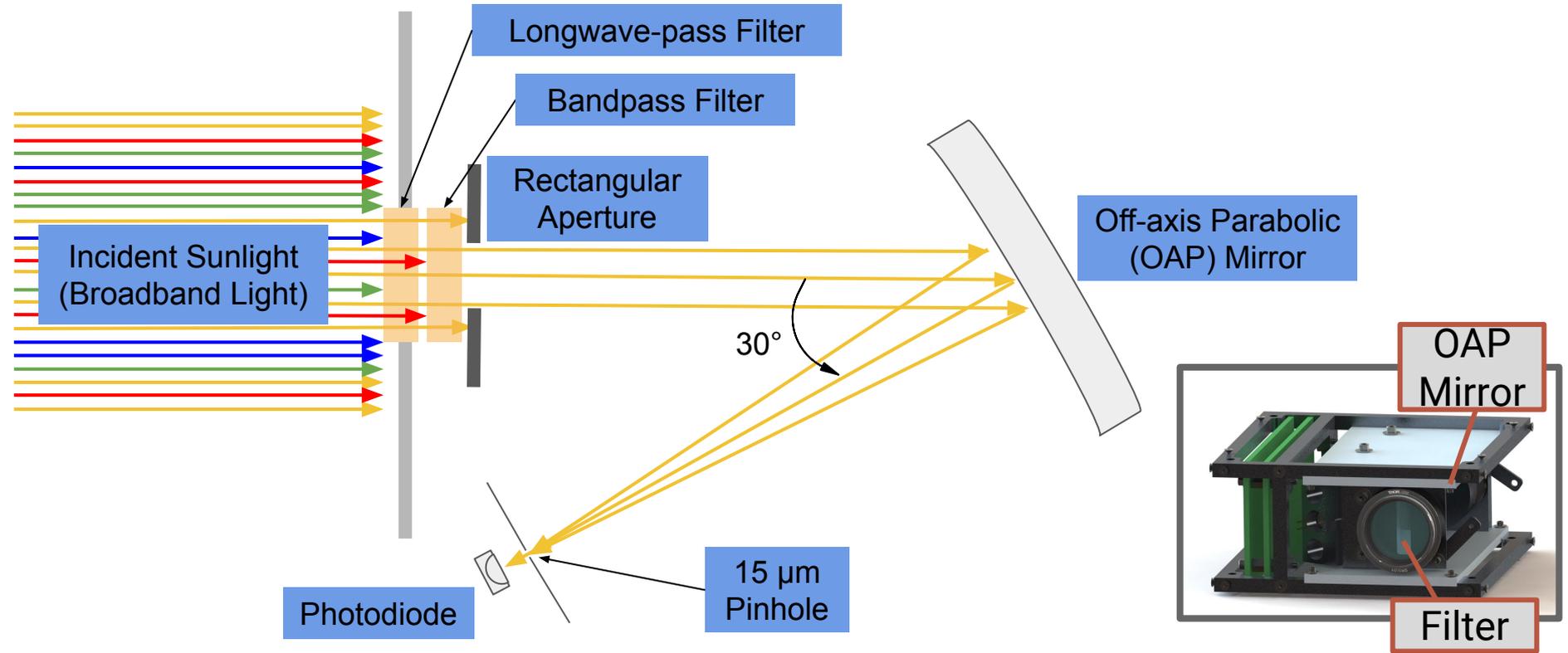
Schedule (Testing Focus)



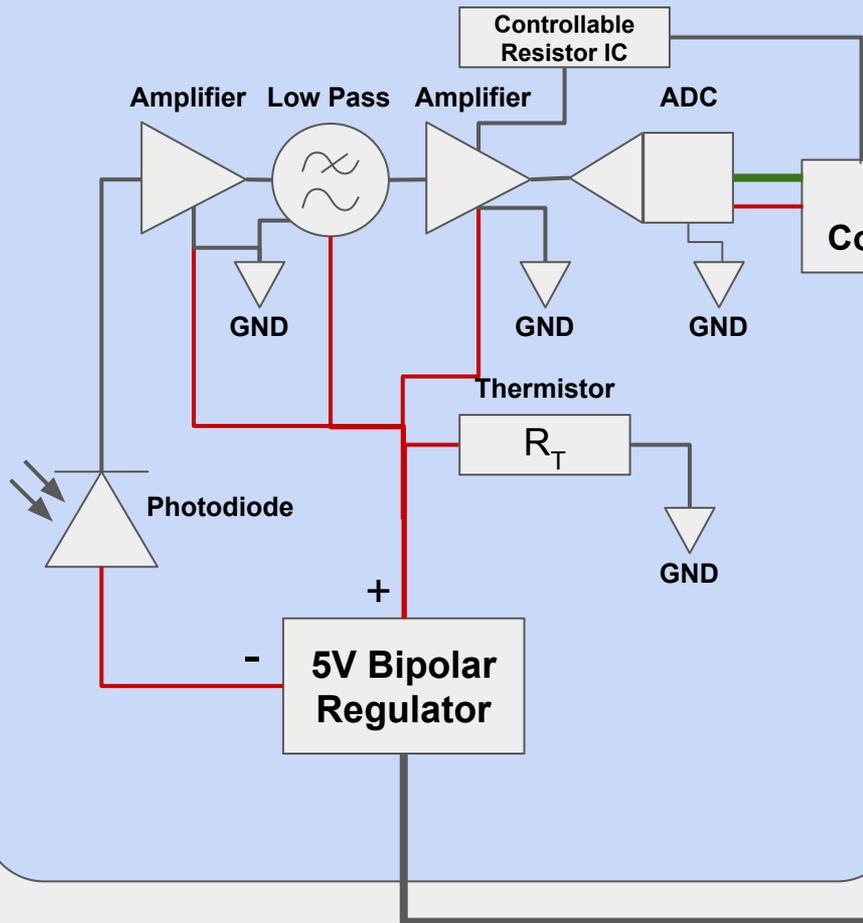
Work Breakdown Structure



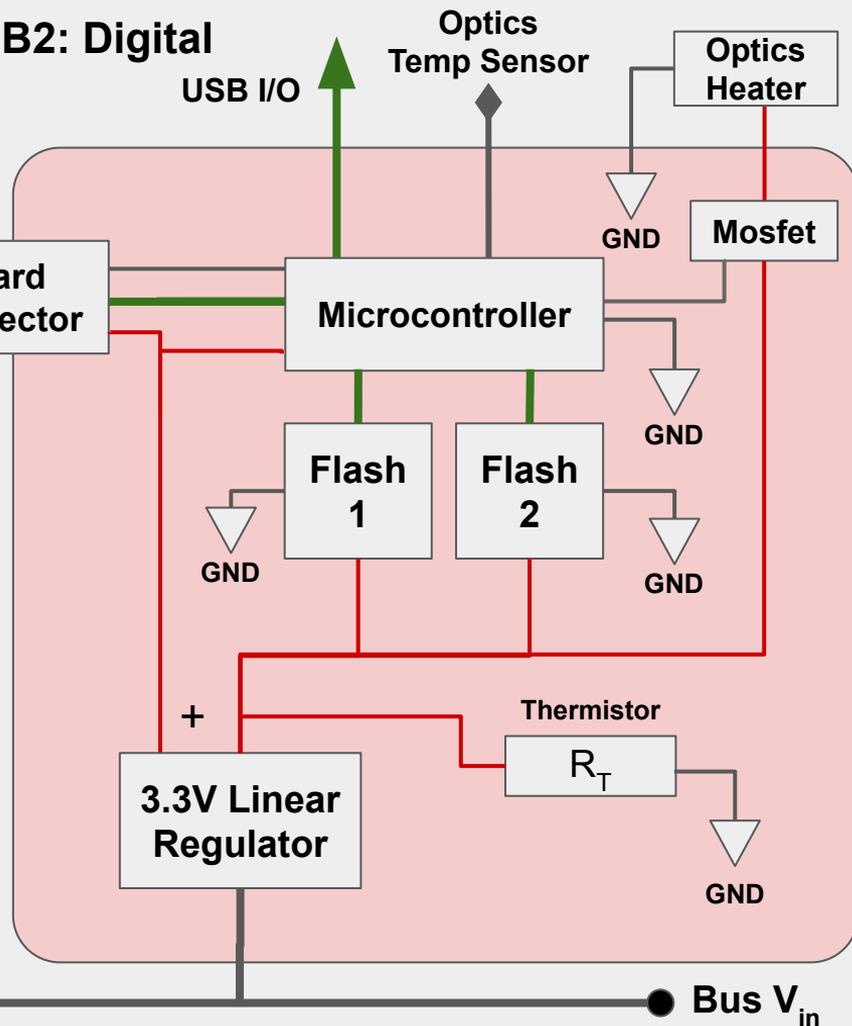
Optics Instrument Overview



B1: Analog



B2: Digital



Bus V_{in}

Power Budget

Power Requirement
8 W

Estimated Power Usage

(worst case scenario)

~7.17 W w/ heater

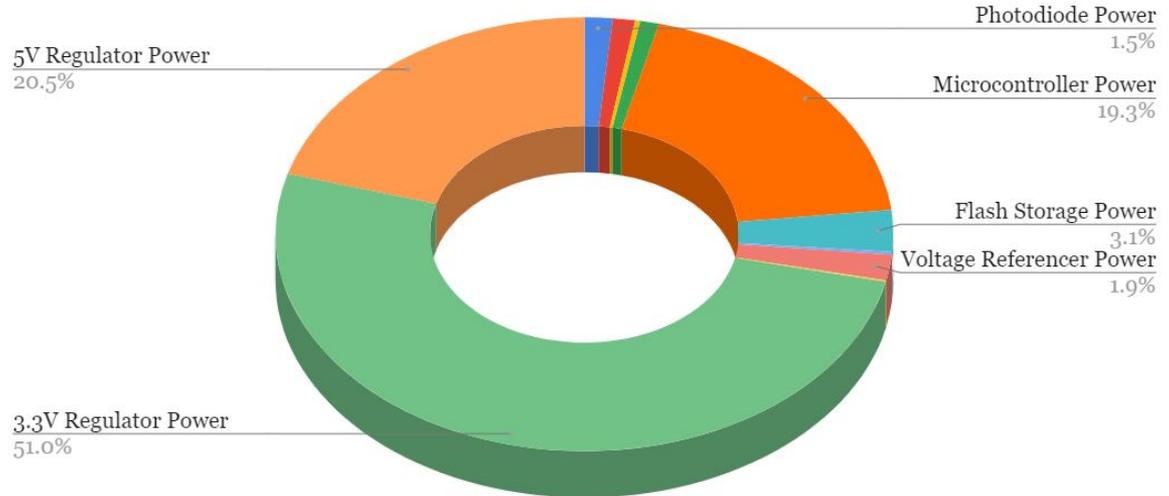
~1.66 W w/o heater

Power Usage Ratio
89.6%

Power estimates for digital I.C's are based off maximum DC characteristics, and are not representative of the typical power draw, merely the maximum possible at any given point

Power Consumption

Percentages are of the 1.66 W board component power usage



- Photodiode Power
- Amplifier Power
- Feedback Resistor Power
- ADC Power
- Microcontroller Power
- Flash Storage Power
- Thermistor Power
- Voltage Referencer Power
- Current Sensor Power
- 3.3V Regulator Power
- 5V Regulator Power



Signal to Noise Ratio (SNR)

Estimated Range

Required SNR
3500

Estimated SNR

10924 (ADC calibrated)
5531 (backup ADC)
1631 (no correction)
656 (worst-case)

SNR Ratio
19% to 312%
(Estimate / Requirement)

Noise Sources [ref. 5]

Photodiode

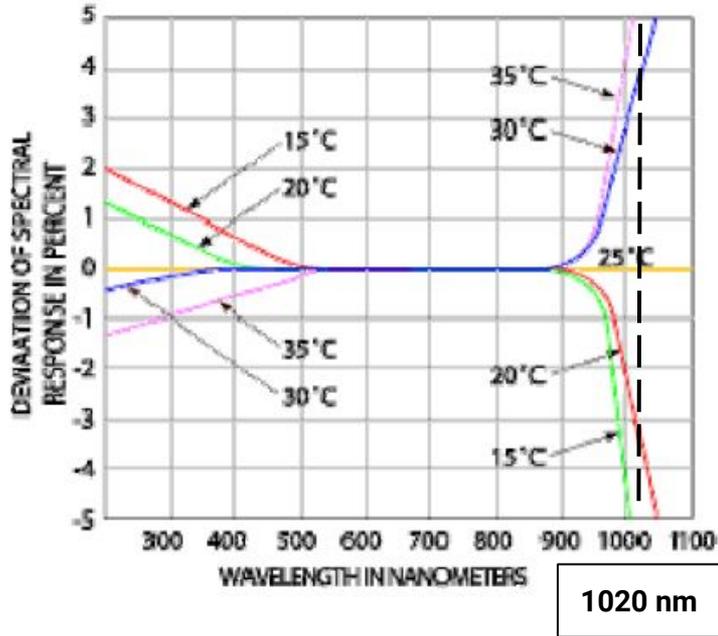
Dark Current
Johnson Noise
Shot Noise
1/f noise

Circuitry / Transmission

Loss in op-amp
5V Regulator Uncertainty
Quantization noise (ADC)
ADC Offset Noise



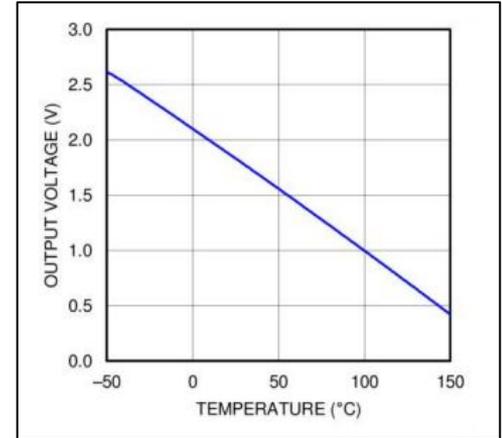
Temperature Monitoring Correction



Texas Instruments LMT86LP

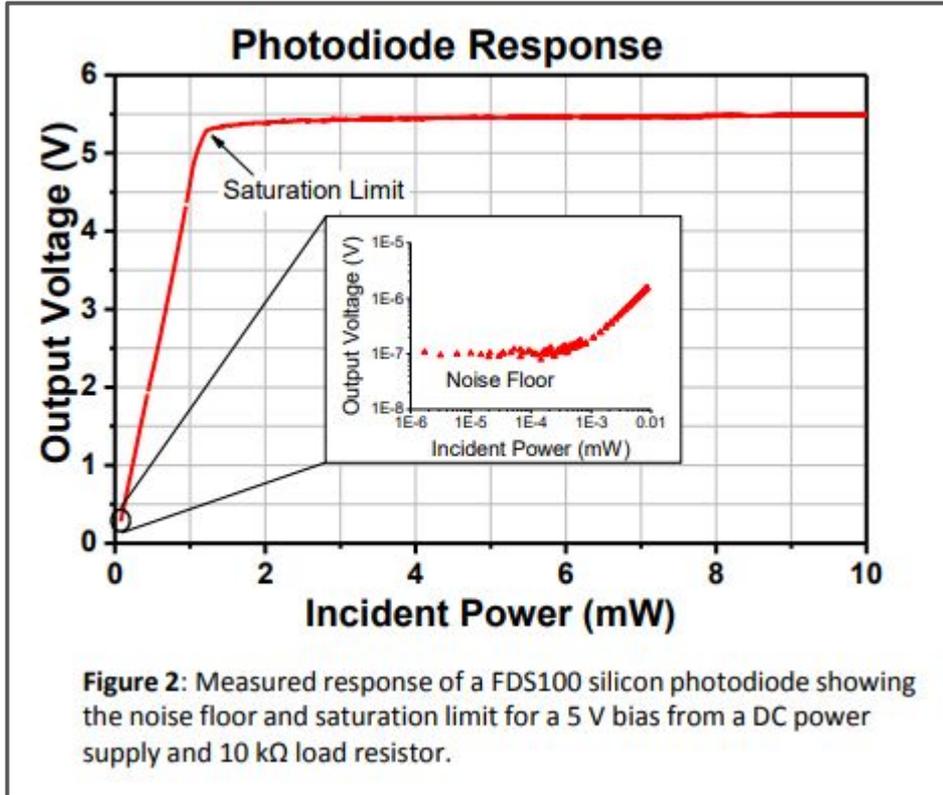
-10.9 mV/°C slope

Sampled w/ 12 bit ADC:
= 0.8mV LSB
= 0.043°C resolution



High precision analog optics bench temperature sensor to track temperature-related errors, correct these errors in software - 0.0198 V/K

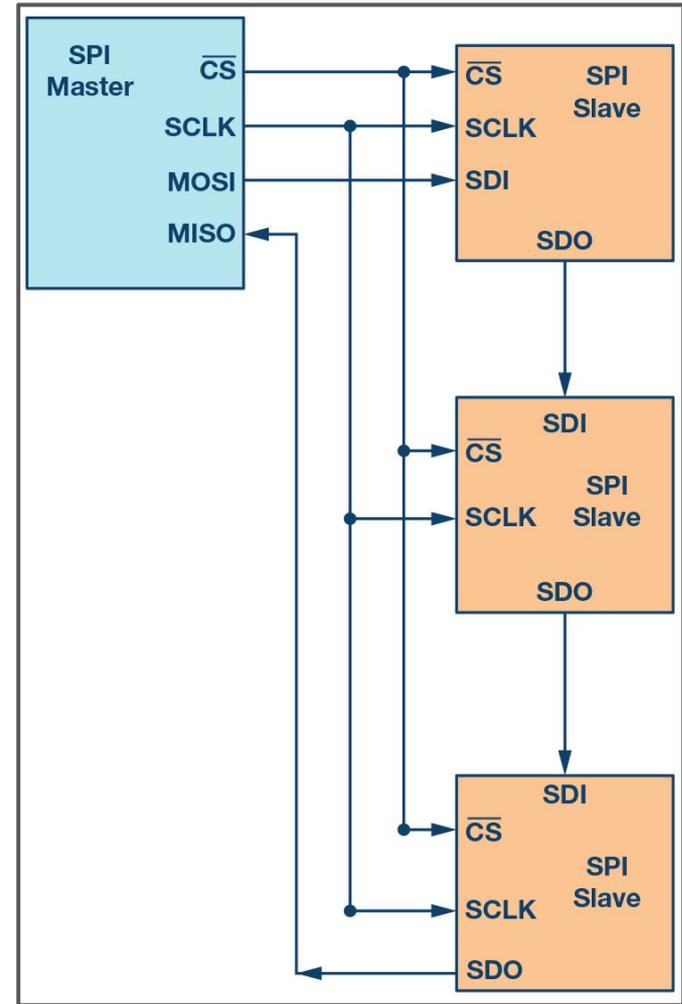
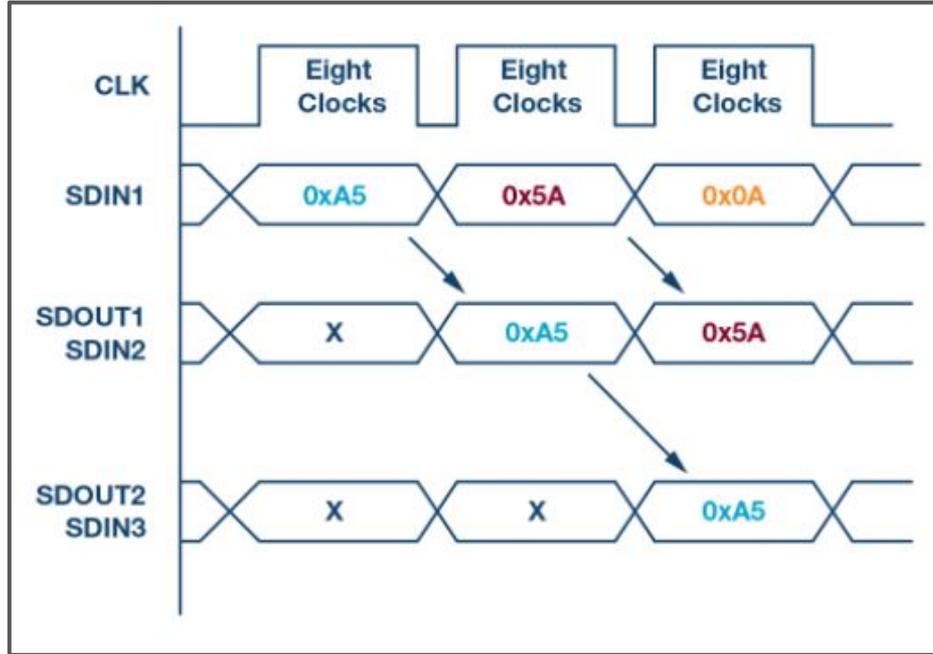
Electronics: Photodiode Saturation



The photodiode output will saturate when the output voltage approaches the reverse bias voltage on the photodiode.

Our reverse bias voltage should be greater than the maximum output voltage, which is 3.3V.

Electronics: SPI Bus Connections

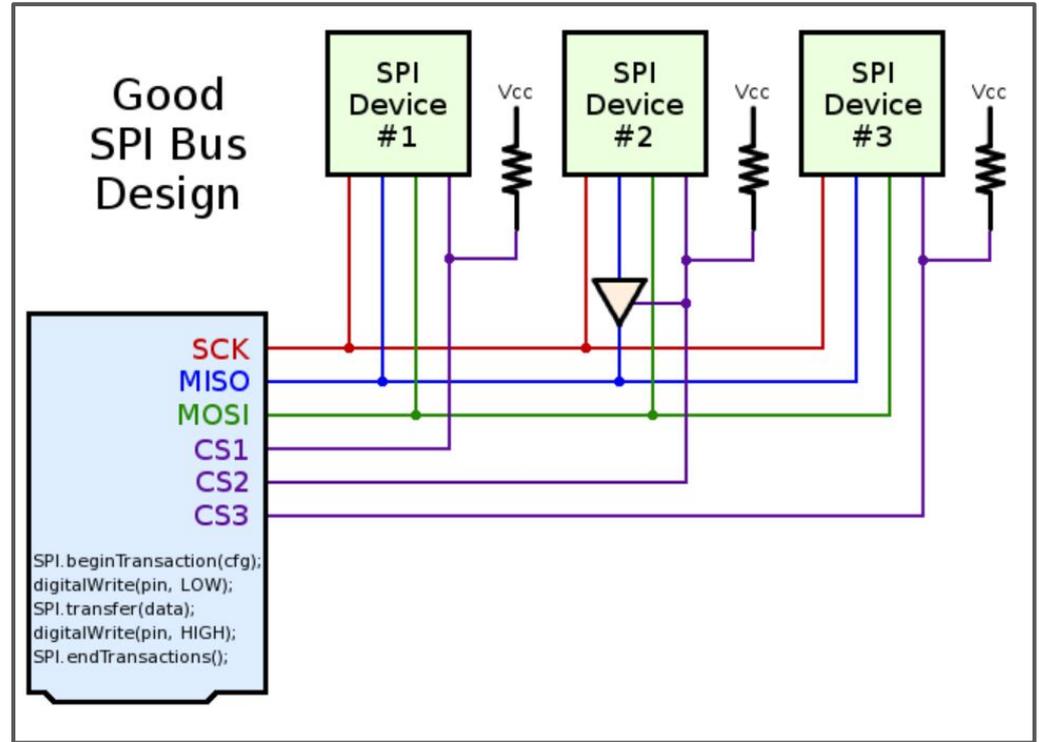


Electronics: SPI Bus Pull Up Resistors

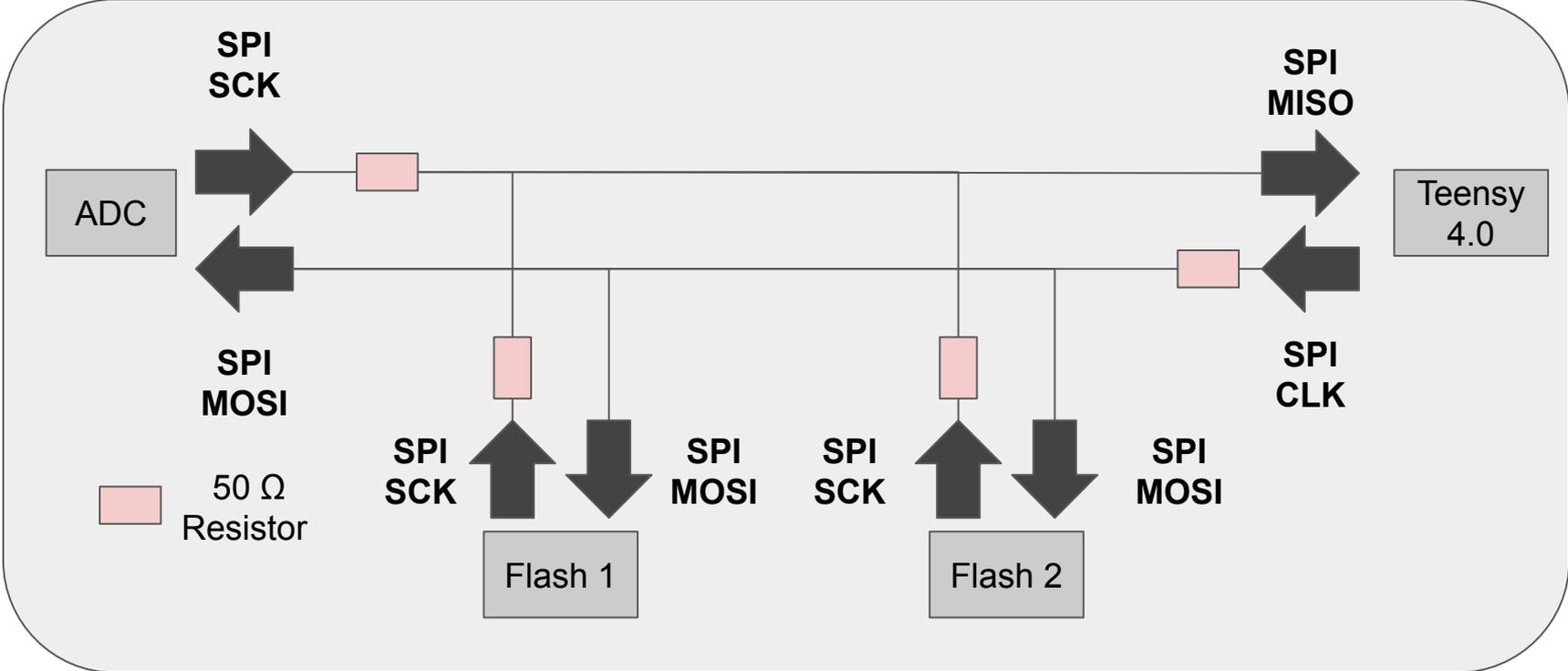
Pull up resistors on the chip select pins ensure that the CS pin is high, thus the MISO/MOSI lines will disengage.

This makes sure a line is only transmitting when absolutely driven low by the microcontroller, reducing potential cross talk.

This can also be corrected in software, but it provides an extra layer of redundancy at little cost.



Electronics SPI Bus Noise Considerations



Electronics: Resistor Heater

3.3V Linear Regulator can supply the needed 1.65 A. This increases the power requirement of the system a lot. We can directly use the 12V input to save power usage, controlling the input with a TVS diode.

MOSFET provides a very low voltage drop, but can be accounted for in resistor sizing.

Microcontroller can supply the activation signal with a PWM output

-20-50°C temp range

N-channel Enhancement MOSFET

"power mosfet"

$P = I_D V_{cc} \rightarrow I_D = \frac{5.46 \text{ W}}{3.3 \text{ V}_{cc}}$
 $I_D = 1.65455 \text{ A}$

$P_{\text{mosfet}} = I_D R_{DS}$
 R_{DS} from datasheet for chosen mosfet

$V_{in} = 3.3\text{V}$ (~ 3.2 ish maybe from the HI microcon signal)

Design constraints:

$V_{in, \text{max}} = 3.3\text{V}$, 10 mA max
 $V_{cc} = 3.3\text{V}$, 3.5 A max
 $P_{\text{req}} = 5.46 \text{ W (across } R_H)$

$P = \frac{V^2}{R} = \frac{3.3^2}{R_H}$
 $R_H = \frac{V^2}{P} = \frac{3.3^2}{5.46 \text{ W}}$
 $R_H = 1.9945 \Omega$

Errors

\rightarrow When off: $V_{GS} = V_{in} < V_{th}$ (from datasheet use $\sim 1-10 \text{ mV}$ (HI signal is $\sim 3.2-3.3\text{V}$))
 $I_D \approx 0$ (extremely low)

\rightarrow When on: $V_{GS} \gg V_{th}$
 $R_{DS} \approx 0.1 \Omega$ [datasheet]
 $V_{DS} = I_D R_{DS} \approx 0.16 \text{ V}$

Incorporating loss: $R_H = \frac{(V_{cc} - V_{DS})^2}{P_{\text{req}}} = \frac{(3.3 - 0.16)^2}{5.46}$

$R_H \approx 1.80579 \Omega$

Electronics: Extended Bill of Materials

| Part | Value | Device | Package | Size (mm^2) | DK Part # | Cost | Temperature Rating |
|-------|------------------|------------------|-------------|-------------|---------------------------|-------|--------------------|
| U\$2 | TEENSY4.0 | TEENSY4.0 | TEENSY4.0 | 814.1 | 1568-DEV-16997-ND | 24.38 | -40°C ~ 85°C |
| U\$3 | AD8671 | AD8671 | SO8 | 31 | AD8671ARMZ-ND | 2.89 | -40°C ~ 125°C |
| U\$4 | LT6105 | LT6105 | MSOP8 | 4.7925 | LT6105HDCB#TRMPBFTR-ND | 3.46 | -40°C ~ 125°C |
| U\$5 | LTC2470 | LTC2470 | MSOP12 | 10.5 | LTC2470IMS#TRPBFTR-ND | 5.01 | -40°C ~ 85°C |
| U\$12 | LT8610A | LT8610A | MSOP16 | 19.79 | LT8610AEMSE#TRPBFTR-ND | 9.5 | -40°C ~ 125°C |
| U\$16 | MT25QL128ABA1ESE | MT25QL128ABA1ESE | SO-08M | 48 | 557-1982-2-ND | 2.29 | -40°C ~ 85°C |
| U\$17 | MT25QL128ABA1ESE | MT25QL128ABA1ESE | SO-08M | 48 | 557-1982-2-ND | 2.29 | -40°C ~ 85°C |
| U\$19 | THERMISTOR | THERMISTOR | M0805 | 2.58064 | BC3395CT-ND | 1.08 | -40°C ~ 150°C |
| U\$26 | LTC2470 | LTC2470 | MSOP12 | 10.5 | LTC2470IMS#TRPBFTR-ND | 5.01 | -40°C ~ 85°C |
| U\$30 | LT6105 | LT6105 | MSOP8 | 4.7925 | LT6105HDCB#TRMPBFTR-ND | 3.46 | -40°C ~ 125°C |
| U\$33 | LT6654-3.3 | LT6654-3.3 | SOT23-6L | 8.12 | LT6654BMPS6-5#TRMPBFTR-ND | 9.76 | -55°C ~ 125°C |
| U1 | LTC3260EMSEPBF | LTC3260EMSEPBF | MSOP-16_MSE | 16 | LTC3260EMSE#PBF | 8.47 | -40°C ~ 125°C |
| U2 | LMV324 | LMV324 | SO14 | 9.15 | LMV324QPW-ND | 0.9 | -40°C ~ 125°C |

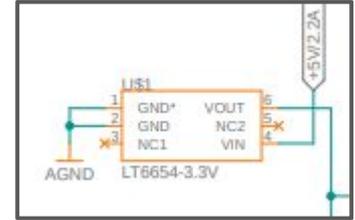
| Total Size (mm^2) | Total Cost (\$) | # Components | Clearance (mm^2) | Traces (mm^2) | Board Cost |
|-------------------|-----------------|--------------|------------------|---------------|------------|
| 5060.264744 | 517 | 129 | 14.5125 | 655.32 | 65 |

Temperature Effects on Components

| Device | Temperature Effects (over -20C to 50C) |
|--------------------------|--|
| Transimpedance Amplifier | Output voltage high and low remain within our necessary bounds, supply current delta around 0.5mA, and slight increase in input offset voltage with temperature, overall negligible. |
| ADC | Gain error and offset error change by ~6-10 LSB, unavoidable but quite small. Calibrating for median temperature will help. Negligible change in conversion time. |
| Voltage Reference | ~0.1mV change maximum, will not affect a significant amount of LSB. |
| 5V Bipolar Regulator | ~100mV change maximum, could introduce AD8671 op-amp noise, but we use decoupling capacitors. Does not veer outside of required operating range. |
| 3.3V Linear Regulator | ~5mV change in voltage output, not enough to affect digital component operation |
| Current Sense Monitors | 0.01% gain error change, no concern |

Electronics: Voltage Regulator Output Noise

Reference voltage for ADC



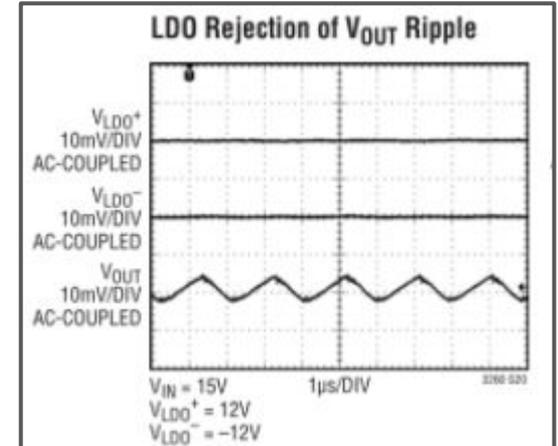
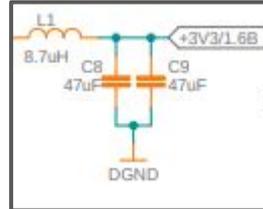
| | | |
|----------------------|----------|--------------|
| 5V Bipolar Regulator | | |
| Output Voltage Noise | 100e-6 V | 2 bins noise |

+ Decoupling capacitors on transimpedance amplifier Vcc

3.3V Linear Regulator

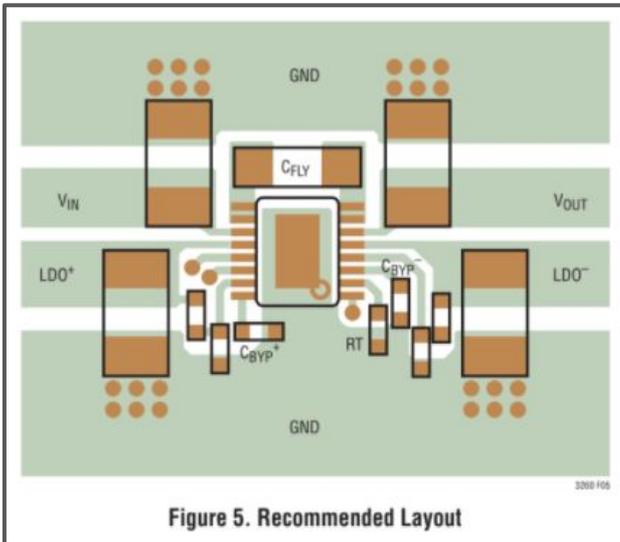
Table 1. Output Voltage Ripple vs Output Capacitance for LT8610AB when $V_{IN} = 12V$, $V_{OUT} = 3.3V$, and $L = 4.7\mu H$

| OUTPUT CAPACITANCE | OUTPUT RIPPLE |
|---------------------|---------------|
| 47 μF | 40mV |
| 47 $\mu F \times 2$ | 20mV |
| 47 $\mu F \times 4$ | 10mV |

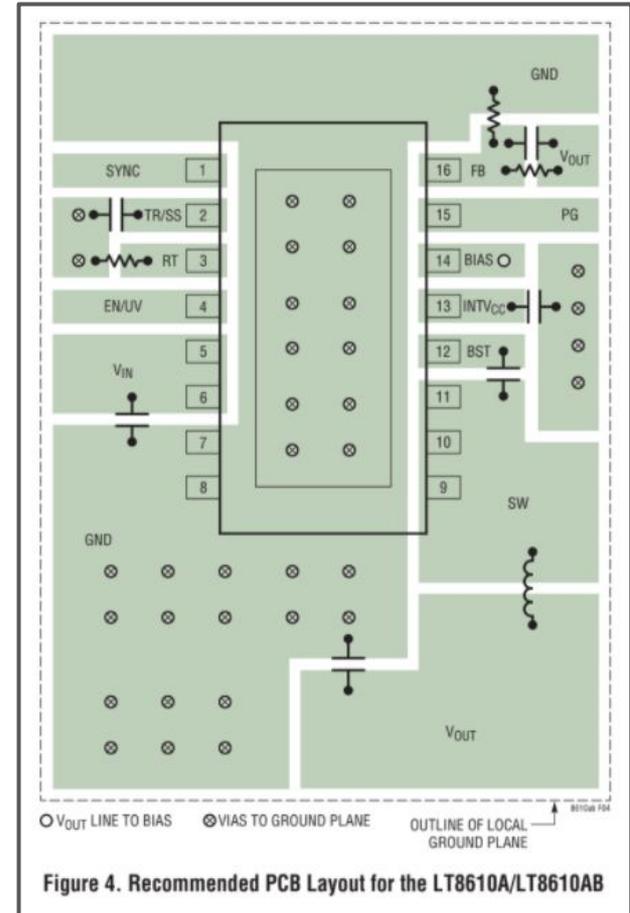


Electronics: Recommended Voltage Regulator Routing

Analog Voltage Regulator



Digital Voltage Regulator



Electronics: ADC Saturation

Maximum temperature (during data collection):

30 deg C

Responsivity at maximum temperature:

0.405 A/W

Maximum incident power:

0.006 W

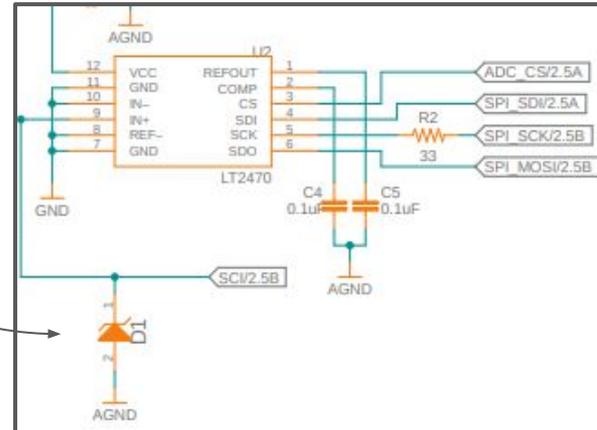
Maximum output current:

0.00247 A

Feedback resistor for 3.3V

1268 Ohms

We also use a 3.3V zener diode on the ADC input to prevent overvoltage. The ADC COMP can only accept 3V to 3.6V (at 3.3V Vcc).



Electronics: SNR Detailed Calculations

All noises are converted to an equivalent voltage, and compared to the expected voltage signal to the ADC. For a worst case scenario, we assuming the typical signal will be 50% of our dynamic range, or 1.65V.

$$V_{shot} = R_f * \sqrt{2q(I_s + I_d)f}$$

$$V_{johnson} = R_f * \sqrt{\frac{4k_B T f}{R_{shunt}}}$$

$$V_{dark} = R_f * I_{dark}$$

$$V_{lowpass} = \frac{28nV}{\sqrt{f}}$$

$$V_{regulator} = 0.1mV$$

$$V_{quantization} = \frac{LSB}{\sqrt{12}}$$

$$SNR = \frac{0.5 * I_s R_f}{\sqrt{V_{quantization}^2 + 2V_{regulator}^2 + V_{lowpass}^2 + V_{dark}^2 + V_{johnson}^2 + V_{shot}^2}}$$

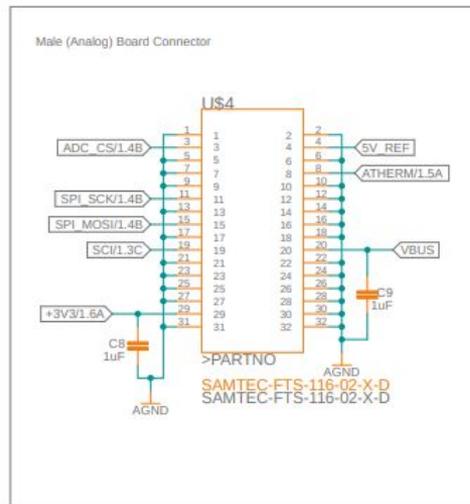
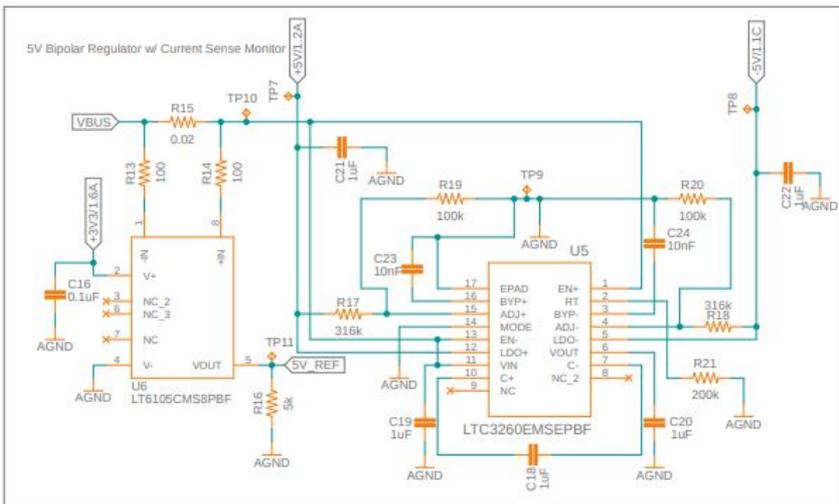
Electronics Risks

| Risk | Mitigation |
|---------------------------|--|
| Voltage regulator noise | Low noise components, voltage reference for ADC, recommended routing patterns |
| Pin overvoltages | TVS diode on heating resistor, zener diode on ADC input, voltage regulators |
| ADC failure | Backup 12 bit ADC on Teensy meets SNR requirements |
| ESD component destruction | Test plan recommendations, ESD safety in test procedures |
| Signal integrity | Signal-ground connector layout, low frequency signals, off-board wire shielding, robust SPI communication design |

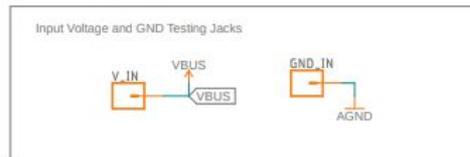
Electronics Risks

| Risk | Mitigation |
|--|---|
| ESD damage or component issues go undetected | Abundant test points to check all input/outputs to each IC |
| Photodiode saturation | Reverse bias voltage applied on pin >3.3V |
| Photodiode responsivity changes | Software correction via high sensitivity optical temp sensor IC |
| ADC Dynamic Range | Feedback resistor sized for maximum expected output current with margin of error |
| Radiation triggers Teensy 4.0 latch up | External watchdog monitoring circuit and backup watchdog implementation in software (using microprocessor built in) |

Analogue Board (2/2)

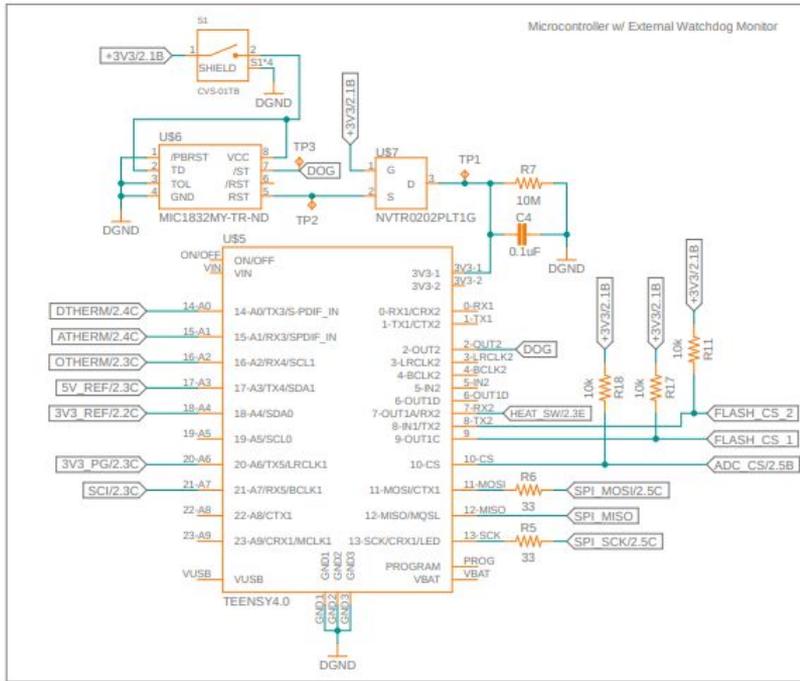


Testing Notes

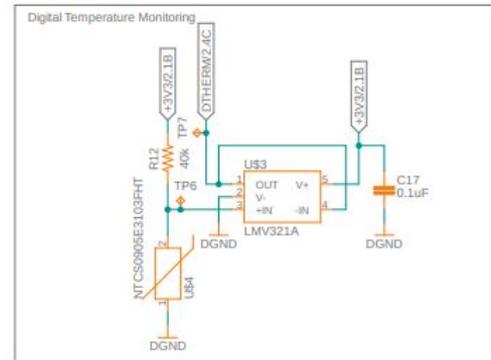
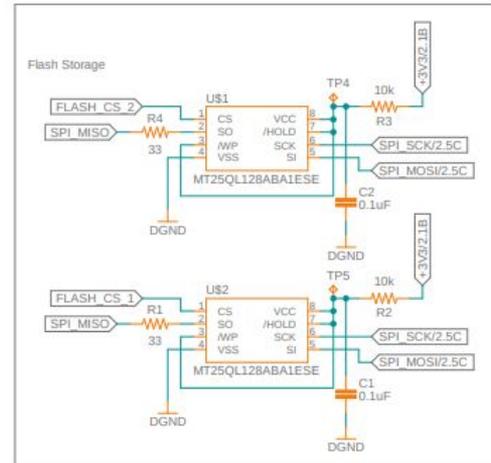


| | |
|------------------------------------|------------|
| TITLE: NanoSAM II Analog Schematic | |
| Author: Jashan Chopra | REV: |
| Date: 2/18/2021 8:21 PM | Sheet: 2/2 |

Digital Board (1/2)

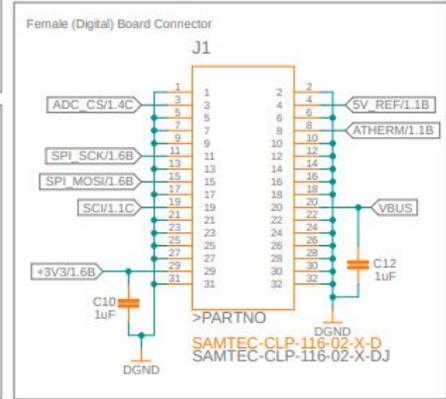
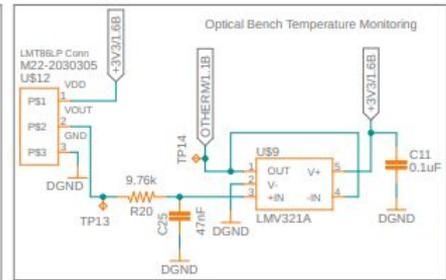
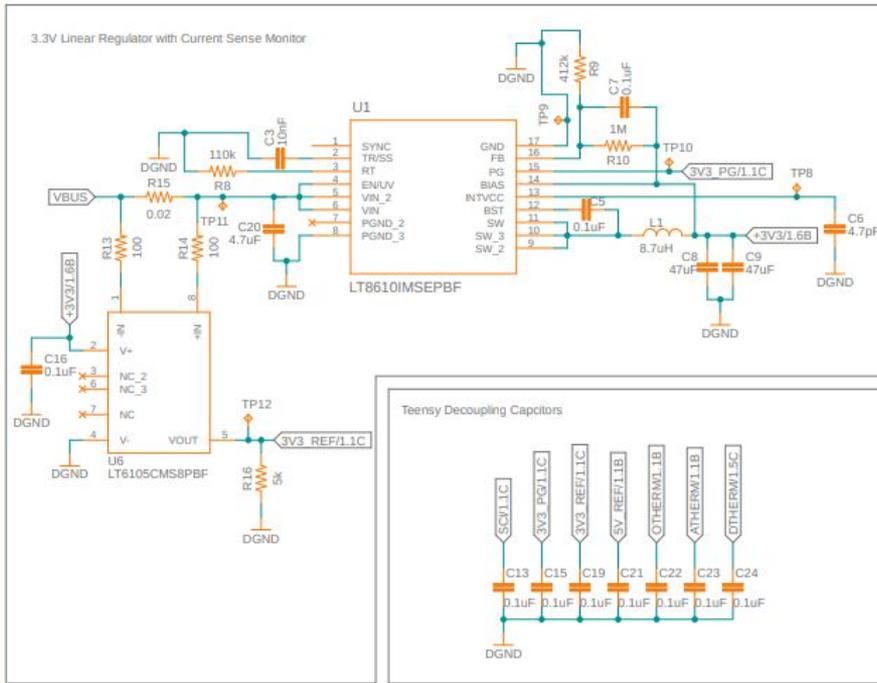


Testing Notes

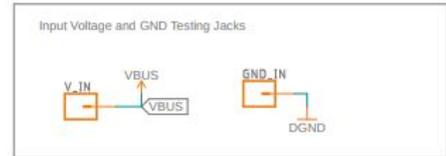
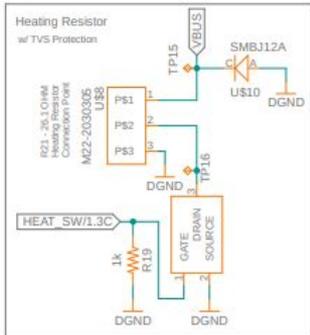


| | |
|-------------------------------------|------------|
| TITLE: NanoSAM II Digital Schematic | |
| Author: Jashan Chopra | REV: |
| Date: 2/18/2021 8:25 PM | Sheet: 1/2 |

Digital Board (2/2)

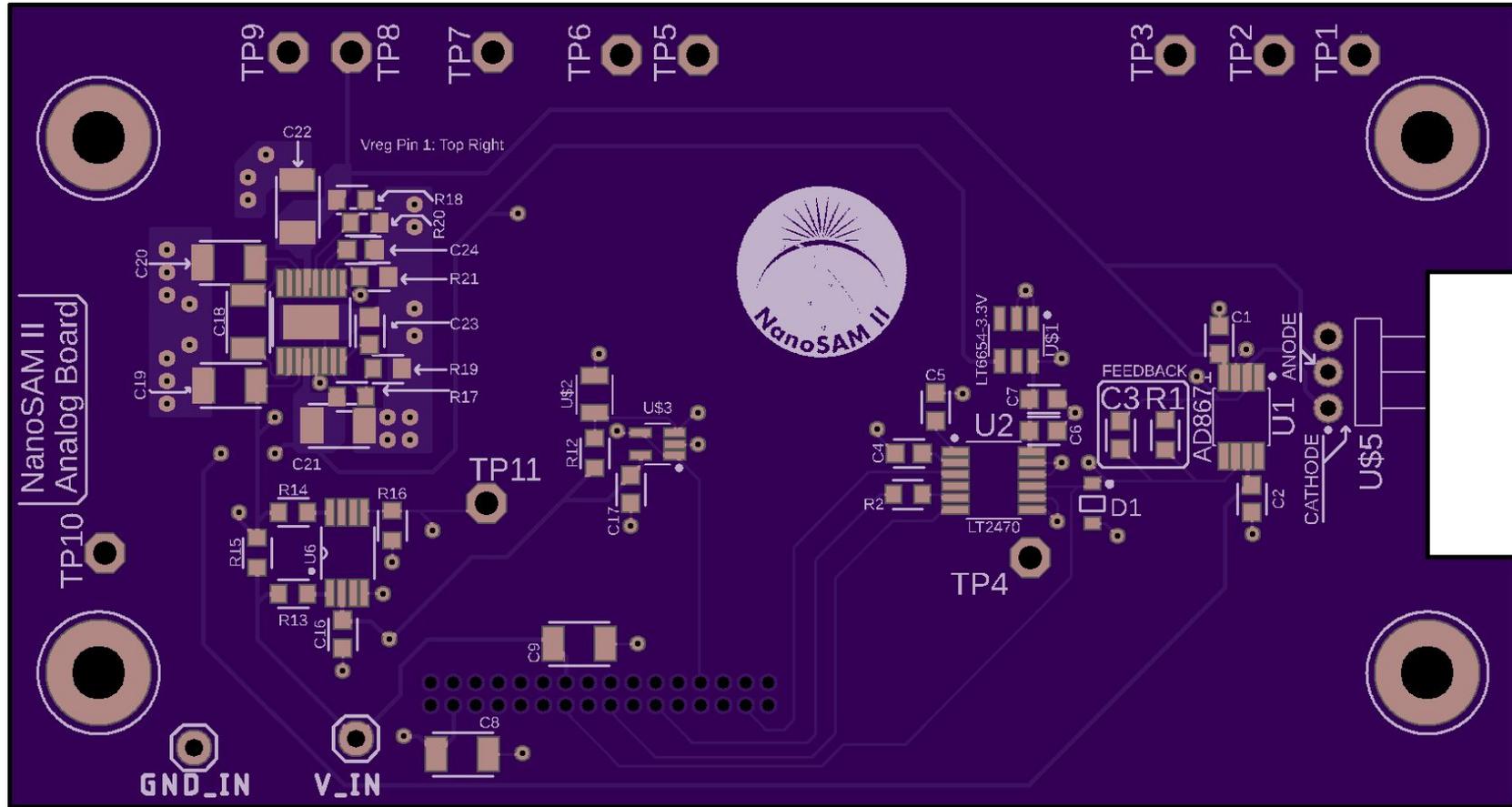


Testing Notes

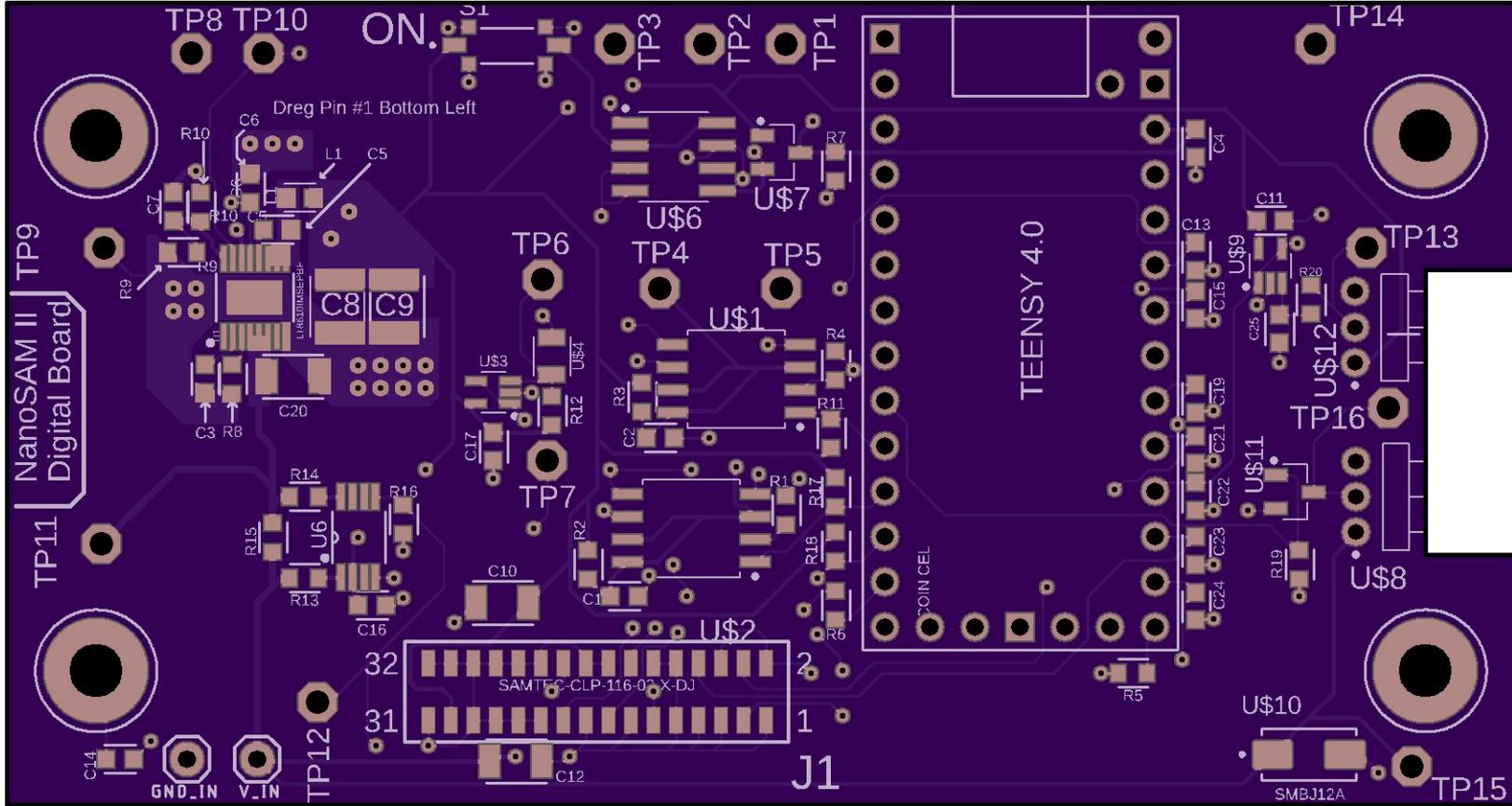


| | |
|-------------------------------------|------------|
| TITLE: NanoSAM II Digital Schematic | |
| Author: Jashan Chopra | REV: |
| Date: 2/18/2021 8:25 PM | Sheet: 2/2 |

OSHPark CAM Job Render [Analog]

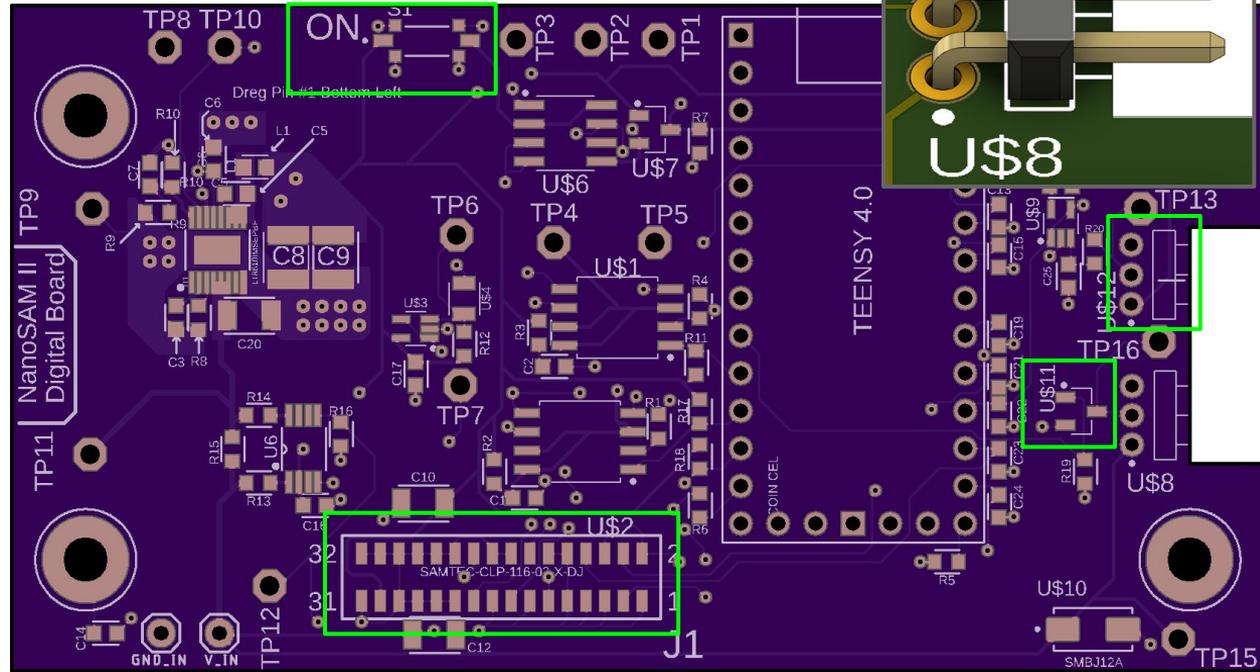


OSHPark CAM Job Render [Digital]



Electronics Design V2

- Manufacturing tolerance on B2B copper pads
- New digital B2B layout with surface mount
- Larger resistor heater MOSFET
- Watchdog hardware switch
- Clip Connectors for ease
- Increased isolation of the ground planes



Electronics System Tests

Requirements V&V

1.0: Data Capture

- The supporting electronics and software shall digitize, packetize, and store housekeeping data and information collected from the photodiode
- The system uses less than 7.3W with the heater running.

2.0: Communications

- Communicates with laptop for ground testing

3/4 - 3/9

Individual Analog Board Test

Individual Digital Board Test

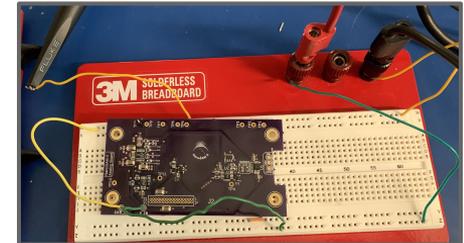
3/11 - 3/16

Basic Integration and Teensy Test

Electronics External Devices Test

3/16 - 3/19

Create Test Setup for Software Integration Tests



Electronics Subsystem Test Results

| Test Point | Actual Value | Expected Value |
|------------|----------------|----------------|
| 1 | 3-4mV floating | 0V |
| 2 | 2-3mV floating | 0V |
| 3 | 3.3V | 3.3V |
| 4 | 2-4mV floating | 0V |
| 5 | 2-4mV floating | 0V |
| 6 | 2-4mV floating | 0V |
| 7 | 4.99V | 5V |
| 8 | -4.99V | -5V |
| 9 | 2-4mV floating | 0V |
| 10 | 11.95V | 12V |
| 11 | 2-4mV floating | 0V |

Table 9 Analog Board Individual Test Results

| Test Point | Actual Value | Expected Value |
|------------------------|-----------------------------|--------------------|
| Analog 2 | 50-70mV [iPhone Flashlight] | [Depends on Light] |
| Board Connector Pin 19 | 2mV less than Analog 2 | N/A |
| Digital 13 | 1.85V | 1.77V at 30 deg C |
| Digital 14 | 1.85V | 1.77V at 30 deg C |
| T14/T13 Low Pass Ratio | 1 | 0.989775 |
| Digital 15 | 12V | 12V |
| Digital 16 | 6mV | 0V |

Table 12 External Connector Test Results

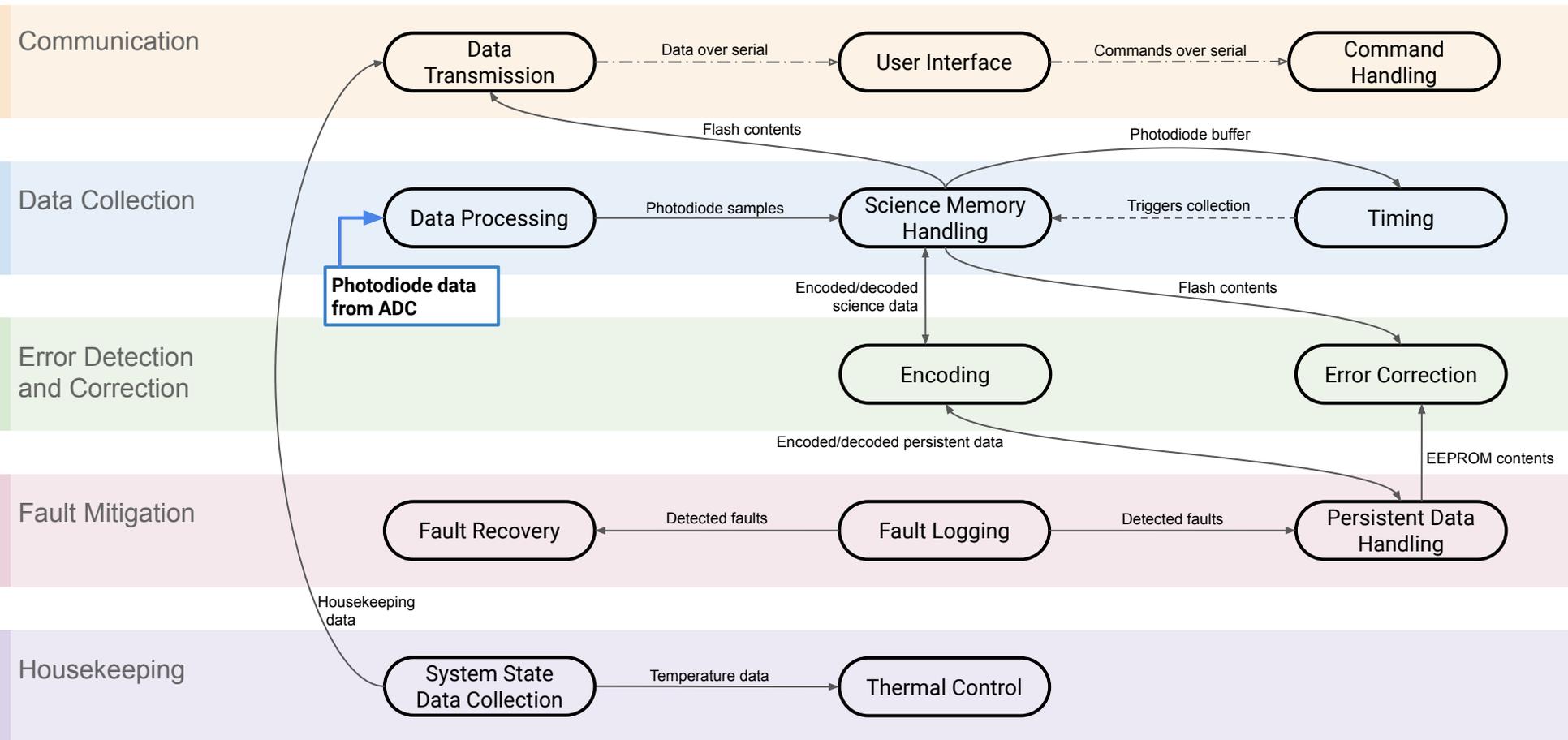
| Test Point | Actual Value | Expected Value |
|------------|----------------------|-------------------------|
| 1 | Floating, 0.6V, 3.3V | 0V [Teensy not on] |
| 2 | 2-3mV floating | 0V |
| 3 | 2-3mV floating | 0V |
| 4 | 3.3V | 3.3V |
| 5 | 3.3V | 3.3V |
| 6 | 3.3V | 0.6V |
| 7 | 3.3V | 0.6V |
| 8 | 3.0V | 3.3V |
| 9 | 0.3mV floating | 0V |
| 10 | 0.35mV | 3.3V |
| 11 | 12V | 12V |
| 12 | 0.31V | Input Current, Variable |
| 13 | 2-3mV floating | 0V |
| 14 | 47mV | 0V |
| 15 | 12V | 12V |
| 16 | 2-3mV floating | 0V |

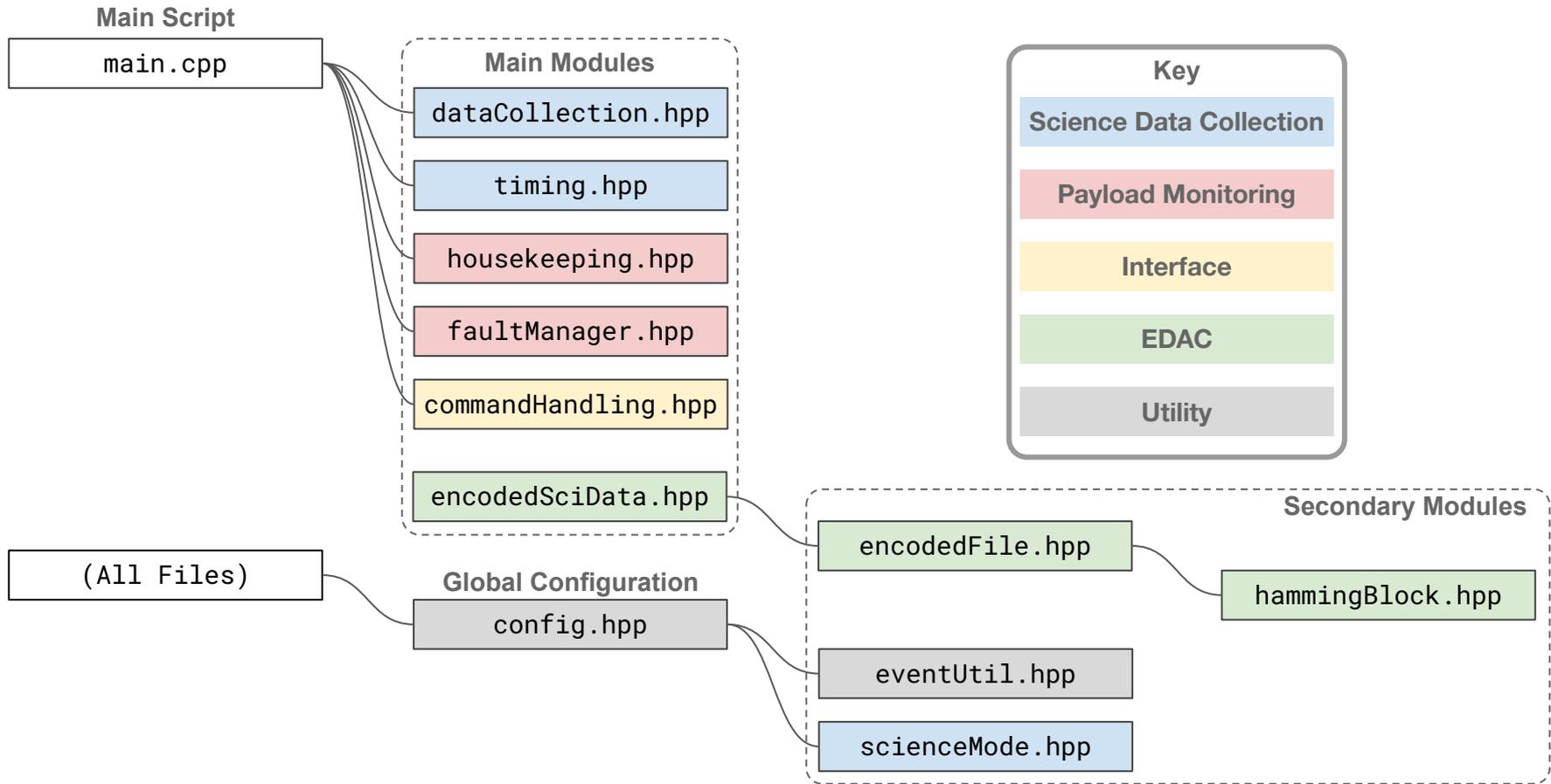
Table 10 Digital Board Individual Test Results

| Test Point | Actual Value | Expected Value |
|------------|------------------|-------------------------|
| Analog 1 | 3-4mV floating | 0V |
| Analog 2 | 2-3mV floating | 0V |
| Analog 3 | 3.3V | 3.3V |
| Analog 4 | 3.7mV | 0V |
| Analog 5 | 0.65V floating | 0.6V [Room Temp] |
| Analog 6 | 0.61V floating | 0.6V [Room Temp] |
| Analog 7 | 5.0V | 5V |
| Analog 8 | -4.97V | -5V |
| Analog 9 | 3.8mV | 0V |
| Analog 10 | 12.01V | 12V |
| Analog 11 | 3.8mV floating | 0V |
| Digital 1 | 2.02V, 0.8V | 3.3V [Teensy on] |
| Digital 2 | N/A [Not Tested] | 0V |
| Digital 3 | N/A [Not Tested] | 0V |
| Digital 4 | 3.3V | 3.3V |
| Digital 5 | 3.3V | 3.3V |
| Digital 6 | 0.367V | 0.6V |
| Digital 7 | 0.367V | 0.6V |
| Digital 8 | 3.3V | 3.3V |
| Digital 9 | 4.6mV | 0V |
| Digital 10 | 0.35mV floating | 3.3V |
| Digital 11 | 12V | 12V |
| Digital 12 | 5.6mV | Input Current, Variable |
| Digital 13 | N/A [Not Tested] | 0V |
| Digital 14 | N/A [Not Tested] | 0V |
| Digital 15 | 12V | 12V |
| Digital 16 | 10mV | 0V |

Table 11 Board Integration Test Results

Software Conceptual FBD

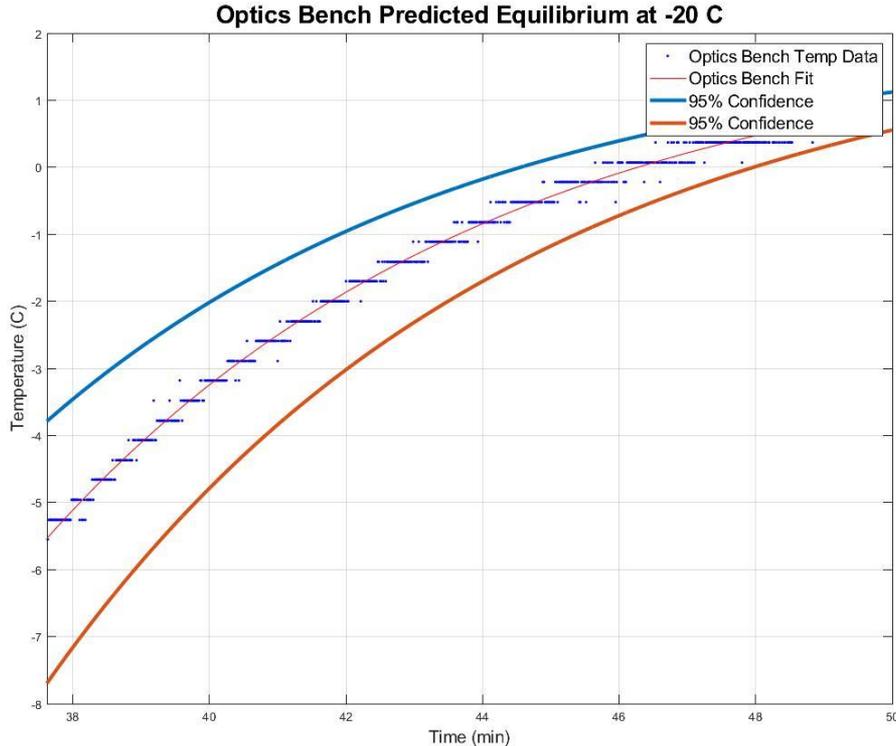




Flight Software Header Tree

Thermal Updates

Determining Heater Output Error Bounds



- Using MATLAB fit toolkit
 - Assuming high stability
 - Imperfect because of resolution inaccuracies that can be seen in the data
- Results from using Eq temperatures in Matlab model:
 - Heater output = 2.4 +/- 0.1 W
 - Electronics outputs below chamber equilibrium
 - Negligible output

$$T(t) = T_{\text{env}} + (T(0) - T_{\text{env}}) e^{-t/\tau}.$$

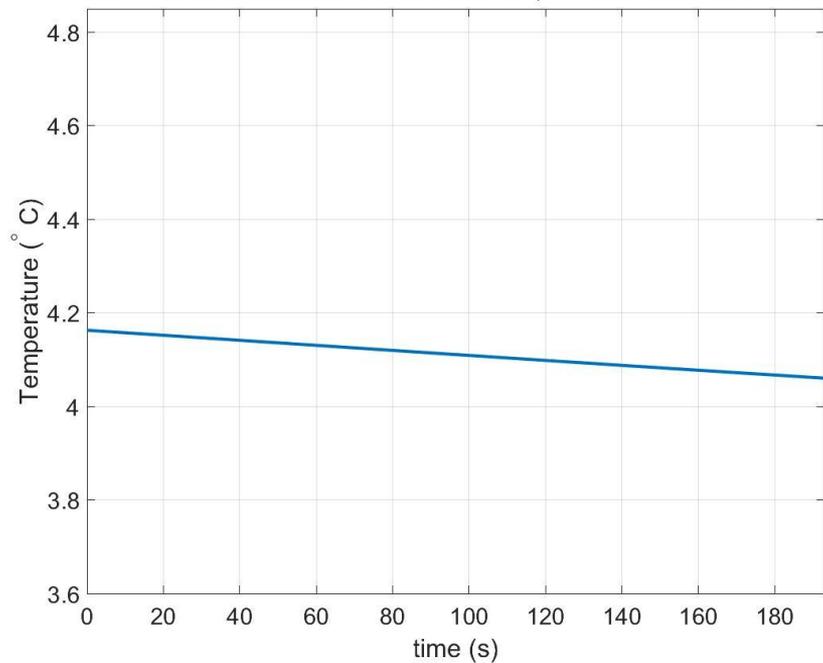
Temperature Change on the Photodiode Block

| Data Window | Max ΔT (K) | Time (s) |
|-------------|--------------------|----------|
| Sunset | ~0.1 | 192.6 |
| Sunrise | ~0.9 | 192.6 |

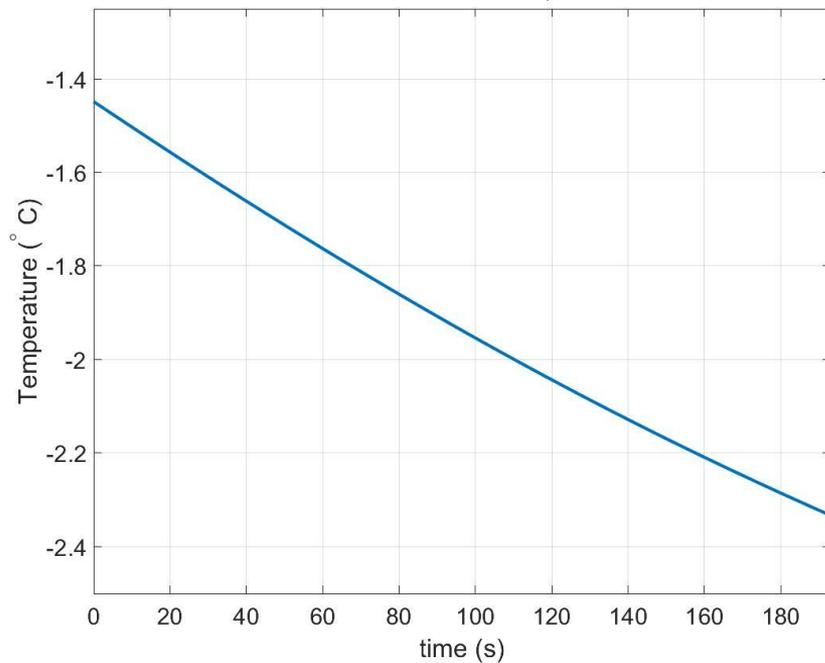
- Calculated for $\beta = 60^\circ$ (orbital parameters corresponding to maximum length data window)
- Average values used for albedo, IR, and solar radiation [2]
- Negligible electronics board power dissipation used in model alongside a 2.4 W heater
- Black anodize exterior coating [3]
- No longer lumped system analysis (done through Solidworks + MATLAB modeling)
 - Threads and screws removed along with small holes

Temperature Change on the Photodiode Block

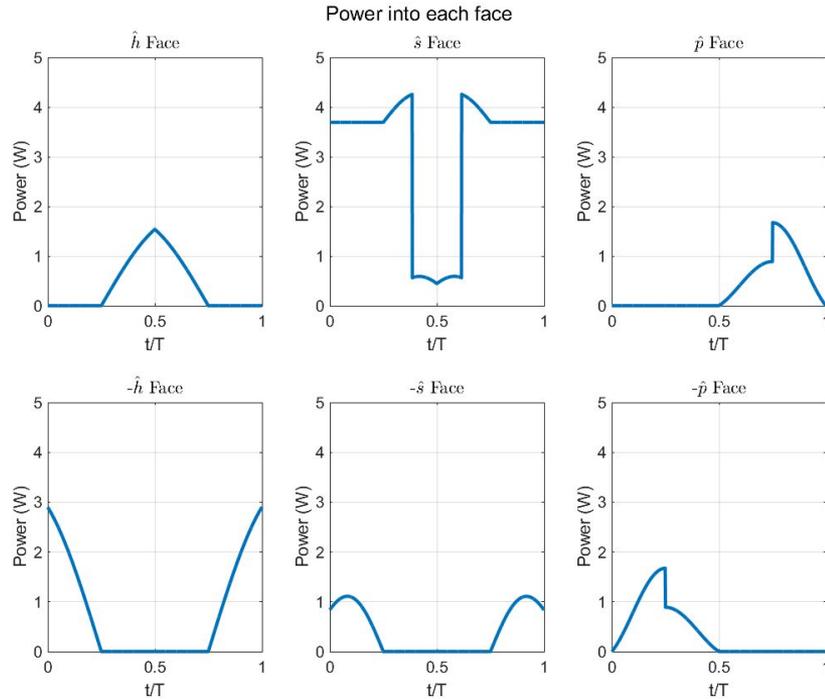
Sunset Data Window Temperature Differential ($\beta = 60^\circ$, Black Anodize Exterior)



Sunrise Data Window Temperature Differential ($\beta = 60^\circ$, Black Anodize Exterior)

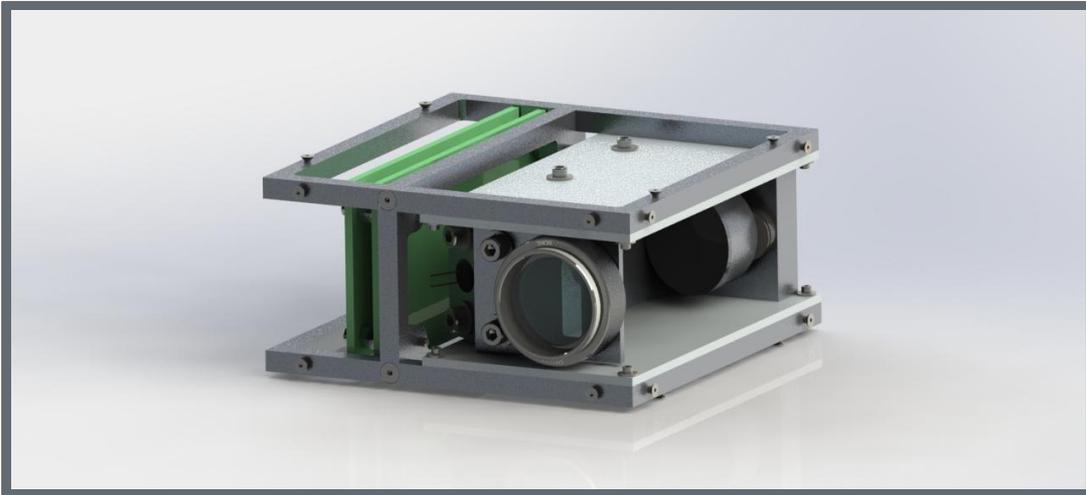


Temperature Change on the Photodiode Block



- Input into SolidWorks in order to account radiation from the Earth
 - Neither SolidWorks or ANSYS has this ability built in
- Still uses **area** factor analysis
- Modeled as surface sources alongside the heater and the EPS board power dissipation

Thermal Isolation of the Optics Bench



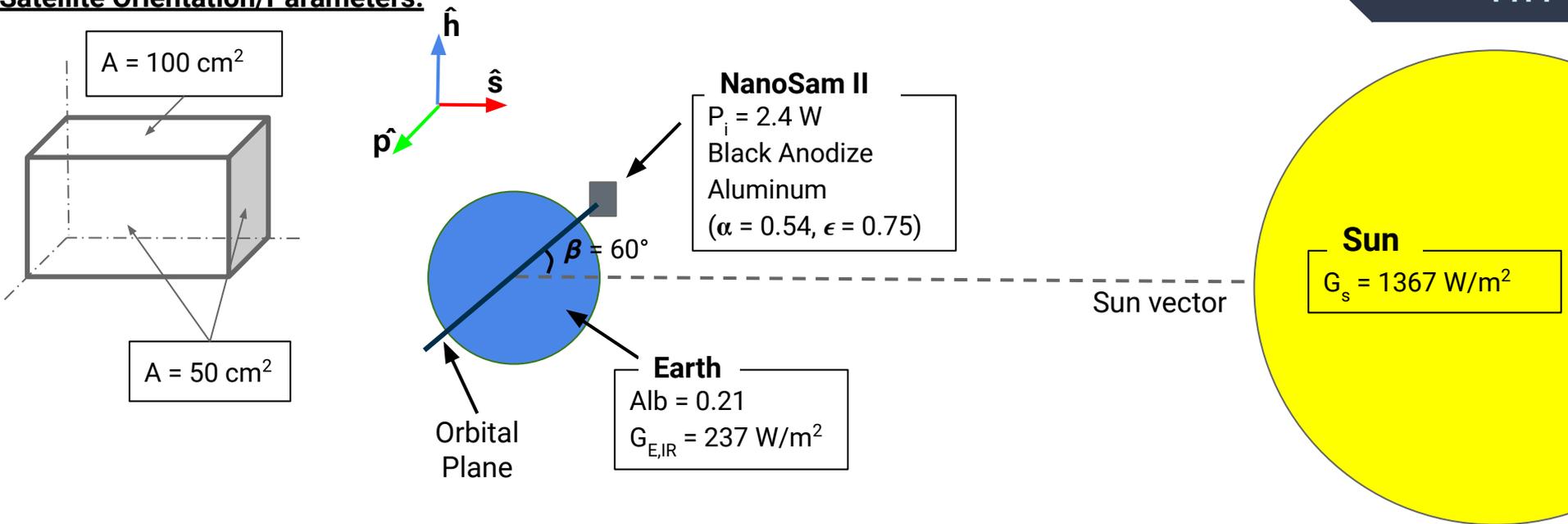
- Introduction of structural fiberglass on either side of the optics bench (S-Glass)

| S-Glass Properties | |
|-----------------------------|------------|
| Density | 2.49 g/cc |
| Thermal Conductivity | 1.28 W/m-K |
| Specific Heat | 738 J/kg-K |

Thermal Model Diagram

Sources : [3] [4]

Satellite Orientation/Parameters:



Thermal Model Details

Key Assumptions:

- Bodies other than the Earth/Sun don't produce significant incident radiation
- Kirchoff's law ($\epsilon_\lambda(T) = \alpha_\lambda(T)$)
- Satellite surfaces are gray, diffuse, surfaces
- Radiation to deep space (0 K)

Key Equations:

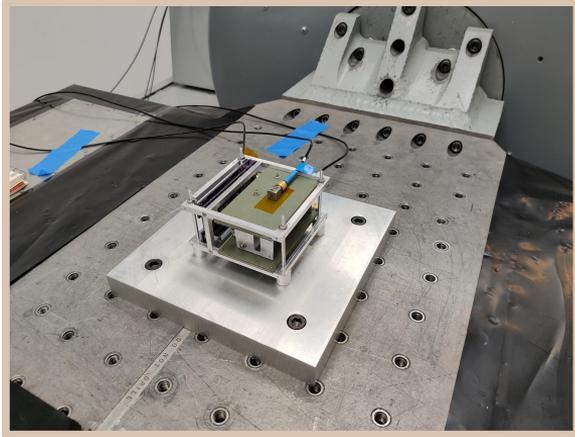
$$T_{sys,eq} = \left[\frac{\dot{Q}_{in,sun} + \dot{Q}_{in,A} + \dot{Q}_{in,IR} + P_i}{2\sigma\epsilon(2A_s + A_p)} \right]^{(1/4)}$$

$$\dot{Q}_{tot} = \dot{Q}_{in,A} + \dot{Q}_{in,IR} + \dot{Q}_{in,sun} + P_i - \dot{Q}_{out}$$

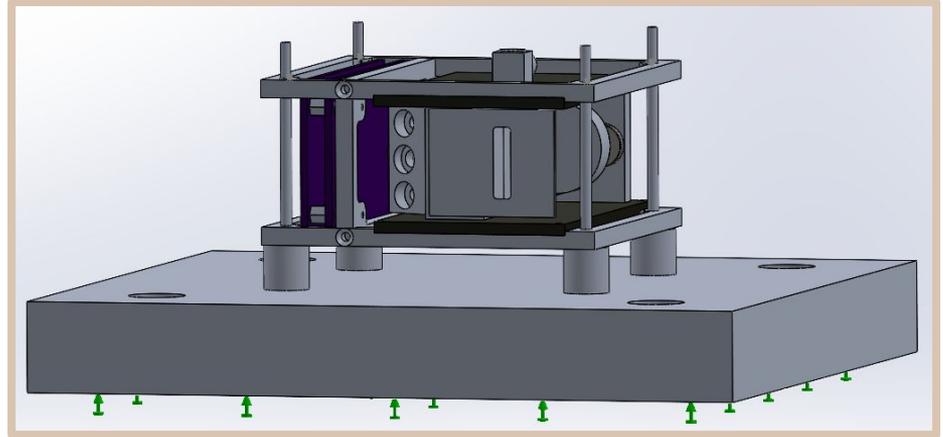
$$T_i = \frac{\dot{Q}_{tot}\Delta t}{mc_p} + T_{i-1}$$

Vibrational Updates

Vibration Test Results



Physical Setup



Model

Vibration Test Results

- **0-2000 Hz 3 Axis Resonance Survey Conducted at Altius Space Machines**
- **Requirement was no resonant frequencies below 90 Hz**
- **Lowest frequency from survey was 445 Hz**
- **Model extremely sensitive to boundary conditions**

| | | Closest Solidworks Resonant Frequency (Hz) | |
|-------------|-----------------------|---|----------------------------------|
| Axis | Frequency (Hz) | Solidworks (Fixed Base) | Solidworks (Fixed Optics) |
| x | 493.3 | 982.6 | 416.8 |
| x | 901.1 | 982.6 | 873.9 |
| y | 445.5 | 982.6 | 416.8 |
| y | 621.4 | 982.6 | 636.5 |
| z | 619.5 | 982.6 | 636.5 |