

# Aspect-ratio Redesign of Eagle owl for Stormchasing

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**CUSTOMER:** Dr. Brian Argrow

**ADVISOR:** Dr. Donna Gerren



# Mission Statement

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**Aspect-ratio Redesign of Eagle-owl for Stormchasing (ARES)** will build upon the previous Eagle Owl project by designing, building, and testing a box-wing unmanned aircraft with a Flush Air Data Sensing (FADS) system to measure relative wind velocity with the objective of creating a high endurance system that can eventually fly into extreme weather conditions.





# Agenda

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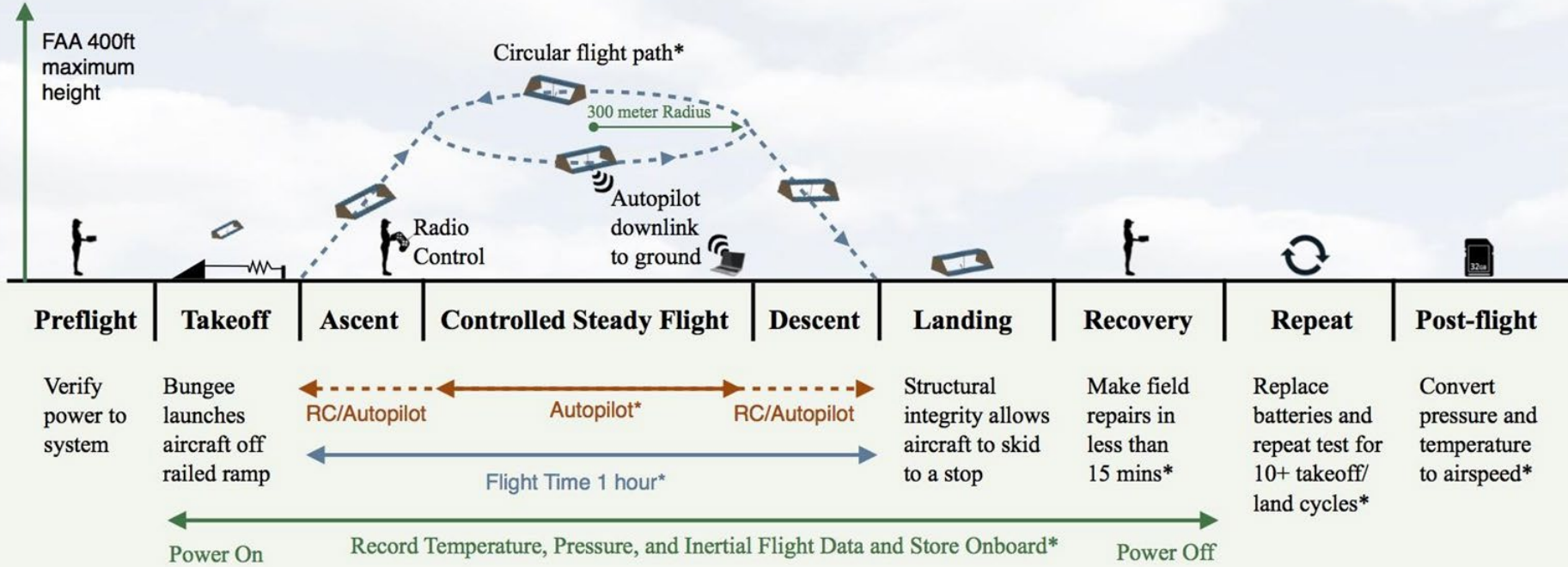
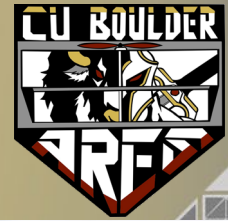
**Project  
Overview**

**Baseline  
Design**

**Feasibility  
Study**

**Summary**

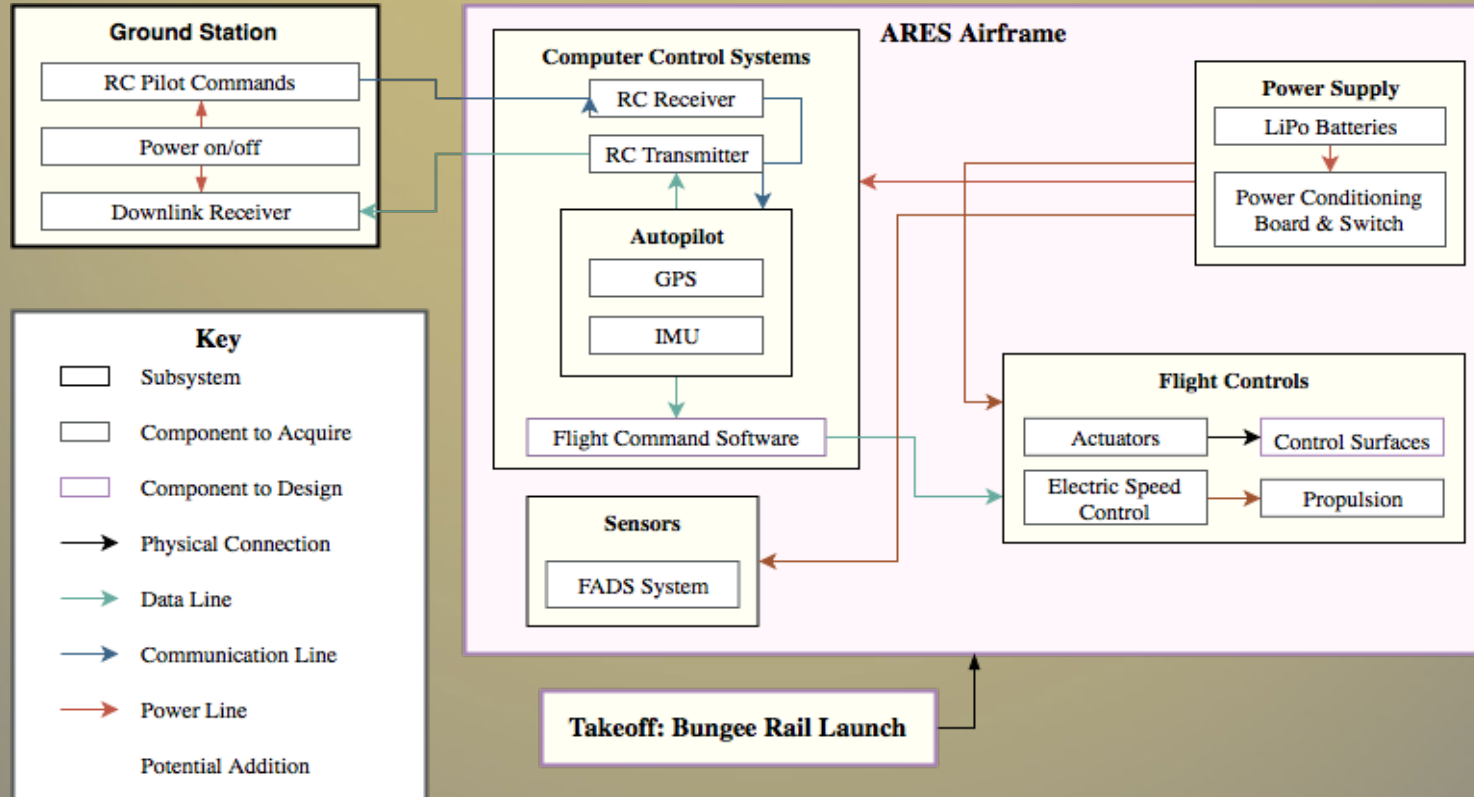
# Concept of Operations



Location: Boulder Aeromodeling Society Airfield or CU Boulder South Campus

\*customer defined

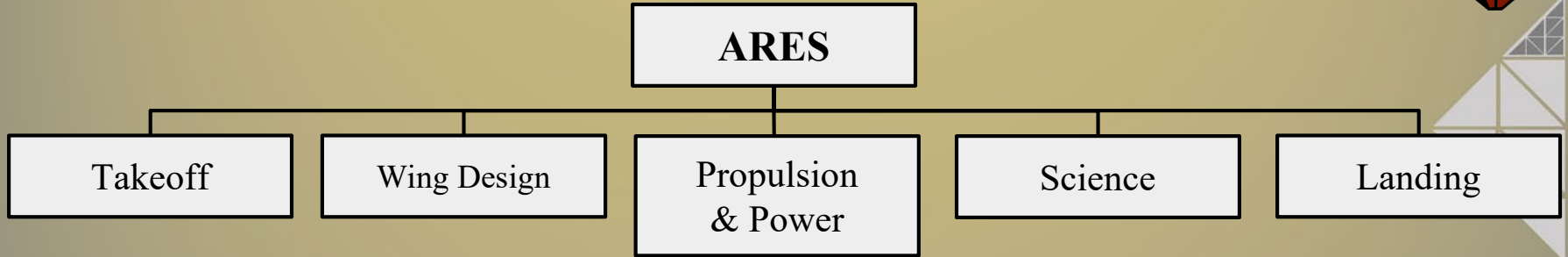
# Functional Block Diagram





# Critical Project Feasibility Elements

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# Baseline Design

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**Project  
Overview**

**Baseline  
Design**

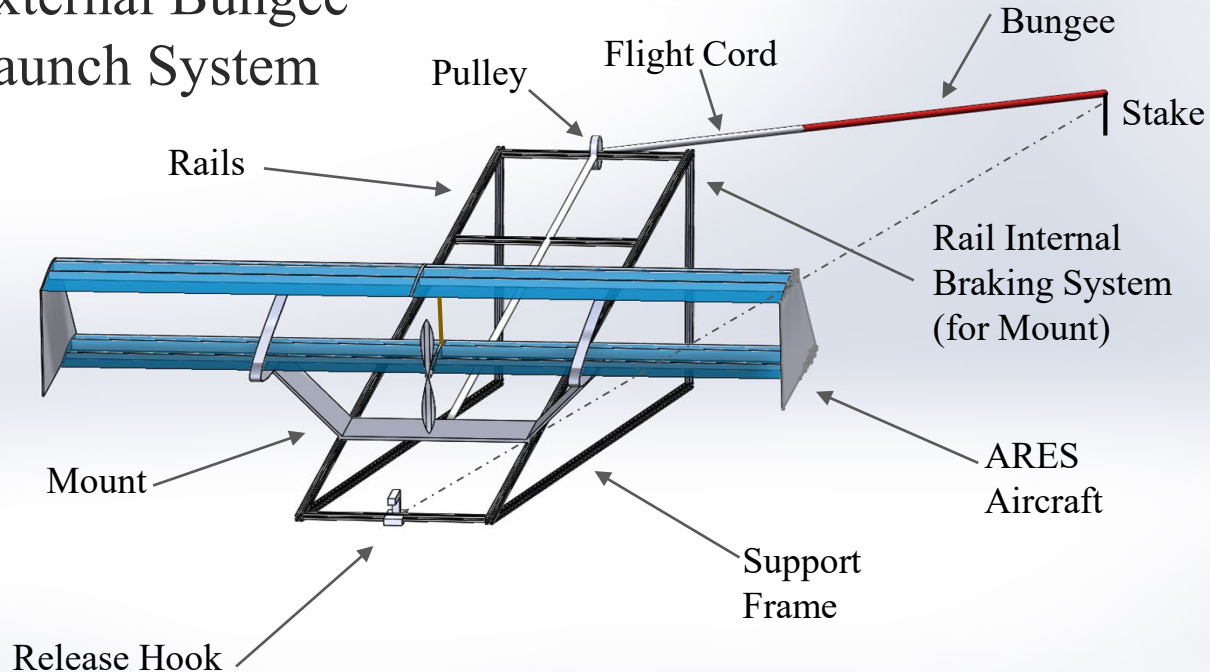
**Feasibility  
Study**

**Summary**

# Takeoff Baseline Design

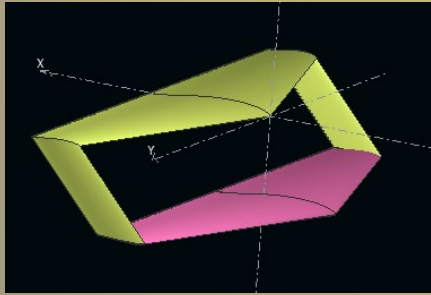
FR 3.0: The aircraft shall demonstrate a controlled takeoff.

## External Bungee Launch System

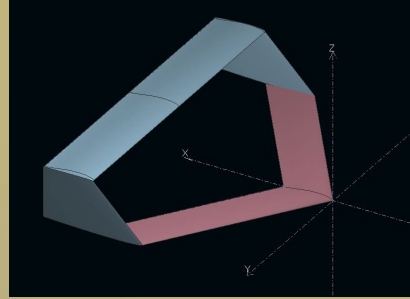




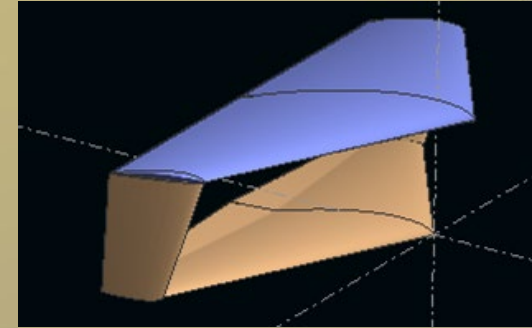
# Baseline Wing Design



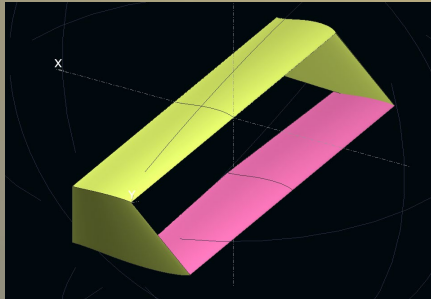
Pentagonal Wing



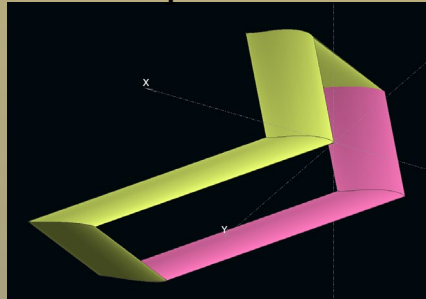
Rectangular Top  
Swept Bottom



Eagle Owl



Rectangular Wing

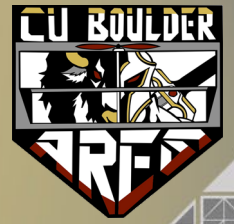


Swept Back Wing

XFLR5 Models

Note: Not to scale, ARES AR = 3, Eagle Owl AR = 1.39

# Baseline Wing Design



	$C_{L,max}$	$L/D_{max}$	$C_{m,\alpha}$ [rad <sup>-1</sup> ]	$V_{stall}$ [m/s]	$V_{cruise}$ [m/s]
<b>Rectangular</b>	<b>0.728</b>	<b>26.3</b>	<b>-0.0393</b>	<b>7.60</b>	<b>11.1</b>
Pentagon	0.708	24.2	-0.0498	7.71	10.2
RTSB	0.709	24.7	-0.0412	7.70	11.9
Swept Back	0.710	25.4	-0.1310	7.69	11.6

Main Takeaway: The rectangular wing combined excellent flight characteristics with simpler manufacturability

# Baseline Wing Design

FR 2.0: The system shall be an aircraft with a box wing configuration with a span no larger than 2 meters.

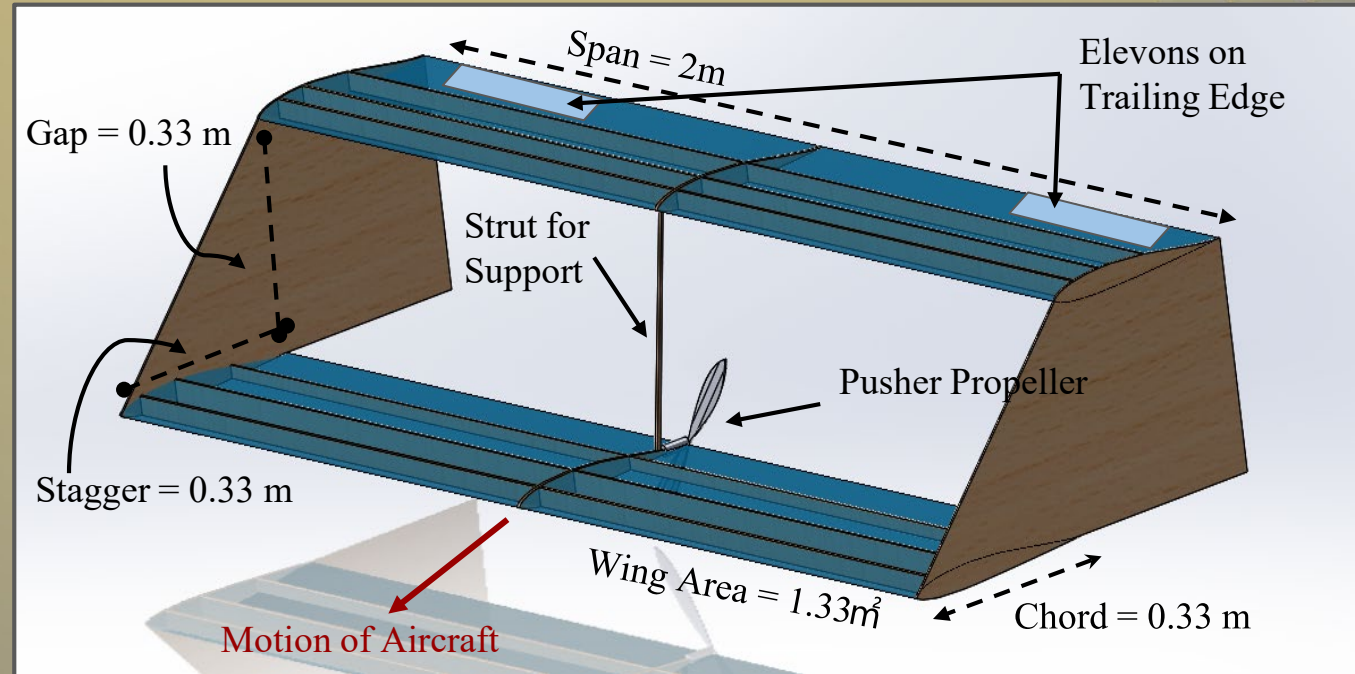
Materials:

Balsa Wood

EPP Foam

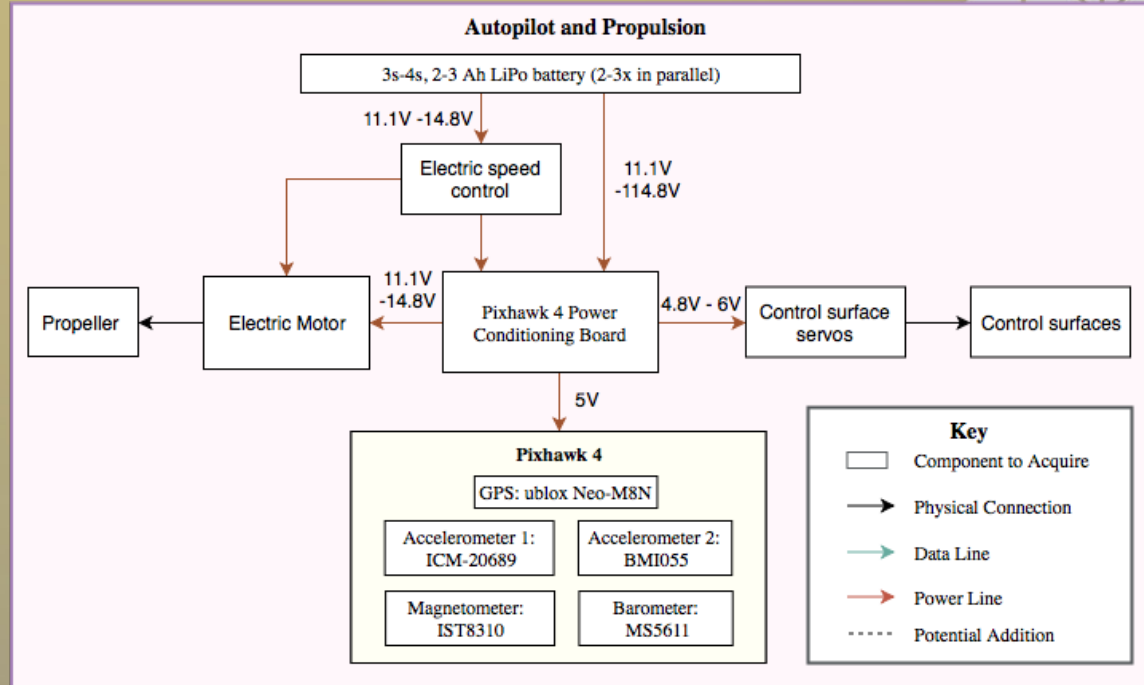
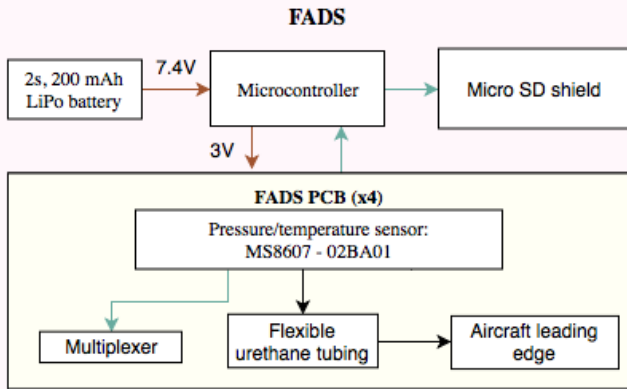
Main Takeaway:

Rectangular planform chosen for aerodynamic efficiency ( $C_L$  vs AoA,  $C_D$  vs AoA)

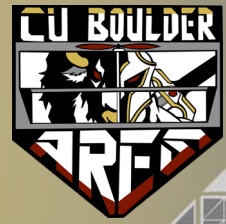


# Power/Avionics Baseline Design

FR 1.0: The aircraft shall have a total flight endurance of at least 1 hour while maintaining visual sight with the operator.

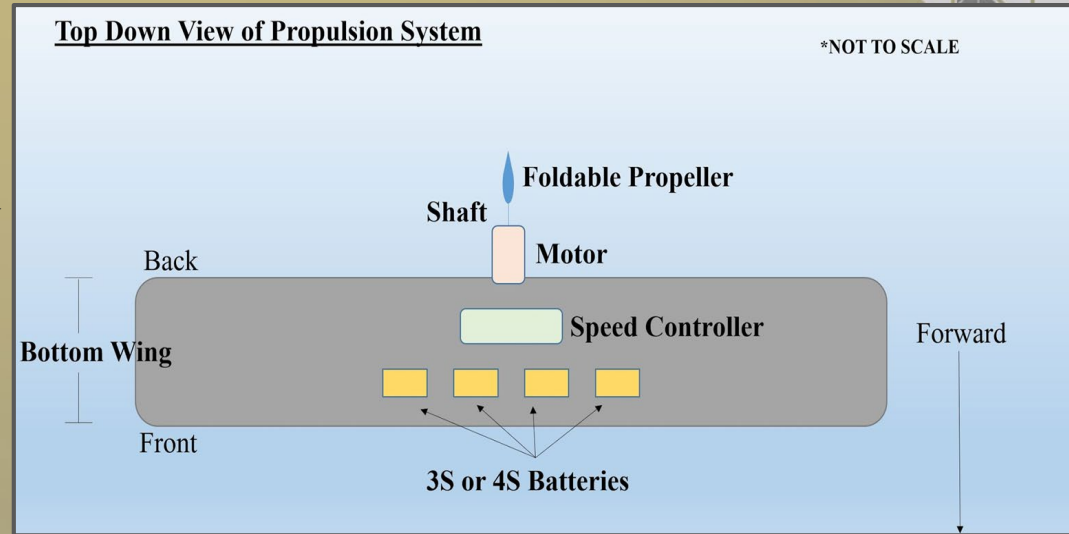


# Propulsion Baseline Design



- Propulsion consists of bottom mounted shimmed pusher
  - Mounted on bottom to lower CG and prevent prop moment
- Electric motor chosen due to reusability, simplicity, heritage, and size
- Components:

- Motor:
  - T/W: 0.2 - 0.25
  - Rating: 500 - 1000 Kv
- Propeller:
  - Able to fold back
  - Diameter: 10" - 12"
  - Pitch: 6" - 10"
- Speed Controller:
  - Castle Phoenix Edge Lite 40-100 A

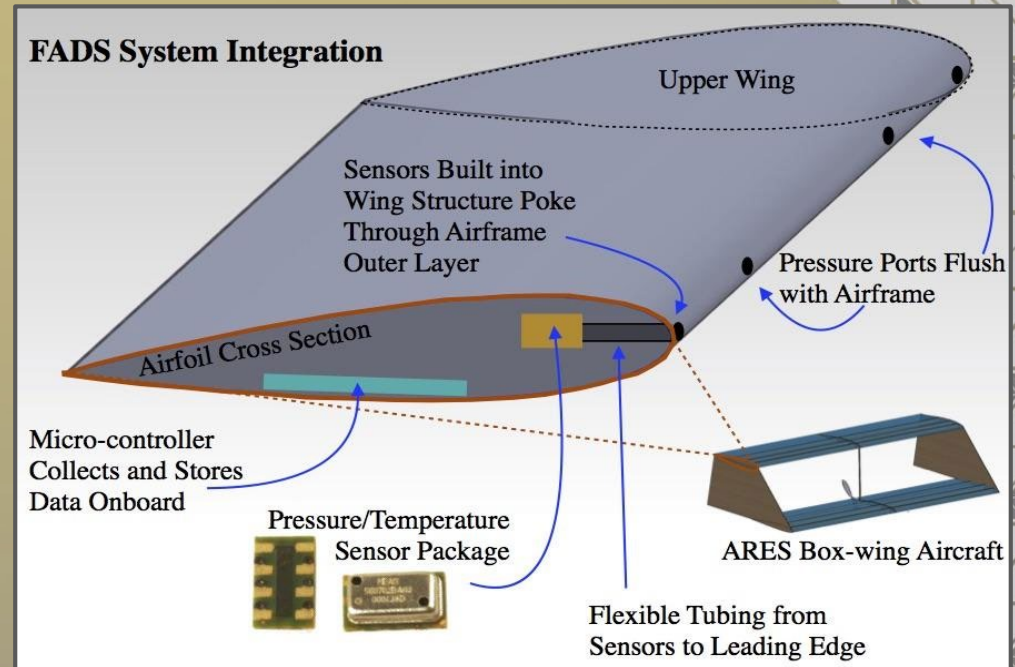


# Science Baseline Design

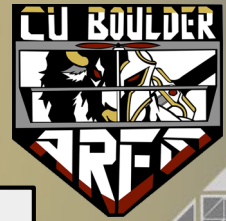
FR 5.0: The aircraft shall simultaneously measure external temperature, inertial flight data, and pressure on the airframe surface at multiple points with a flush airdata sensing (FADS) system. The recorded data shall be stored on-board and converted to relative wind speed after flight.

## Flush Airdata Sensing System

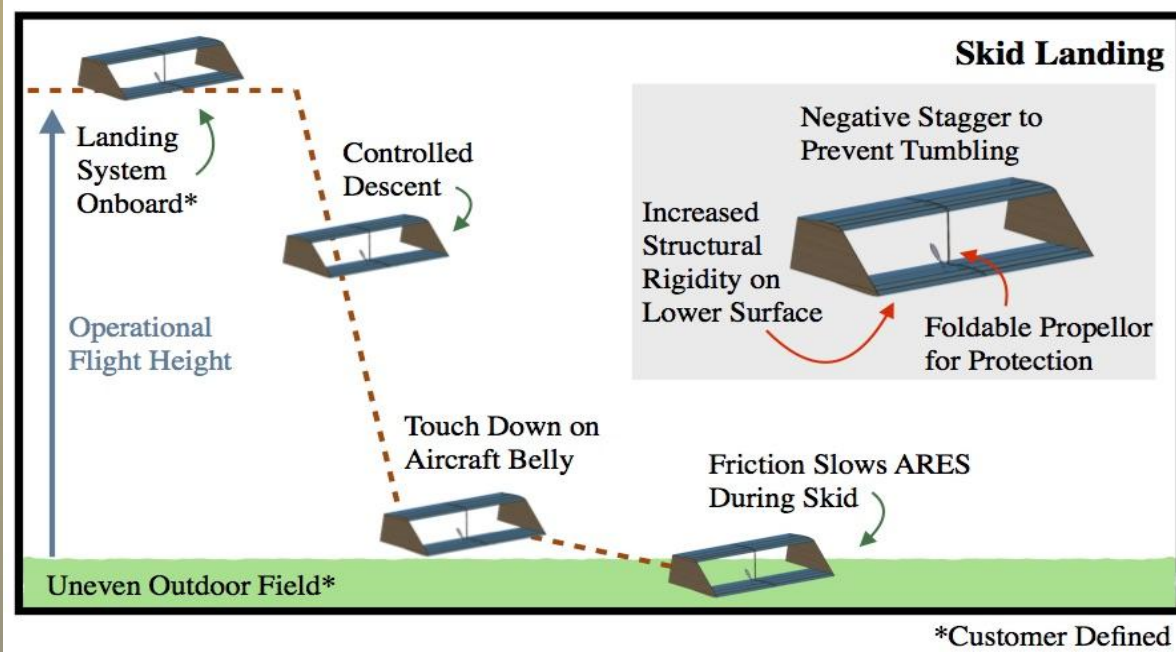
A FADS system measures pressure at multiple points on the aircraft in order to compute angle of attack and sideslip, which can then be combined to get wind velocity.



# Landing Baseline Design



FR 6.0: The aircraft shall land in a manner such that the aircraft is capable of completing at least 10 takeoff and landing cycles with only 15 minutes on the ground between landing and takeoff.

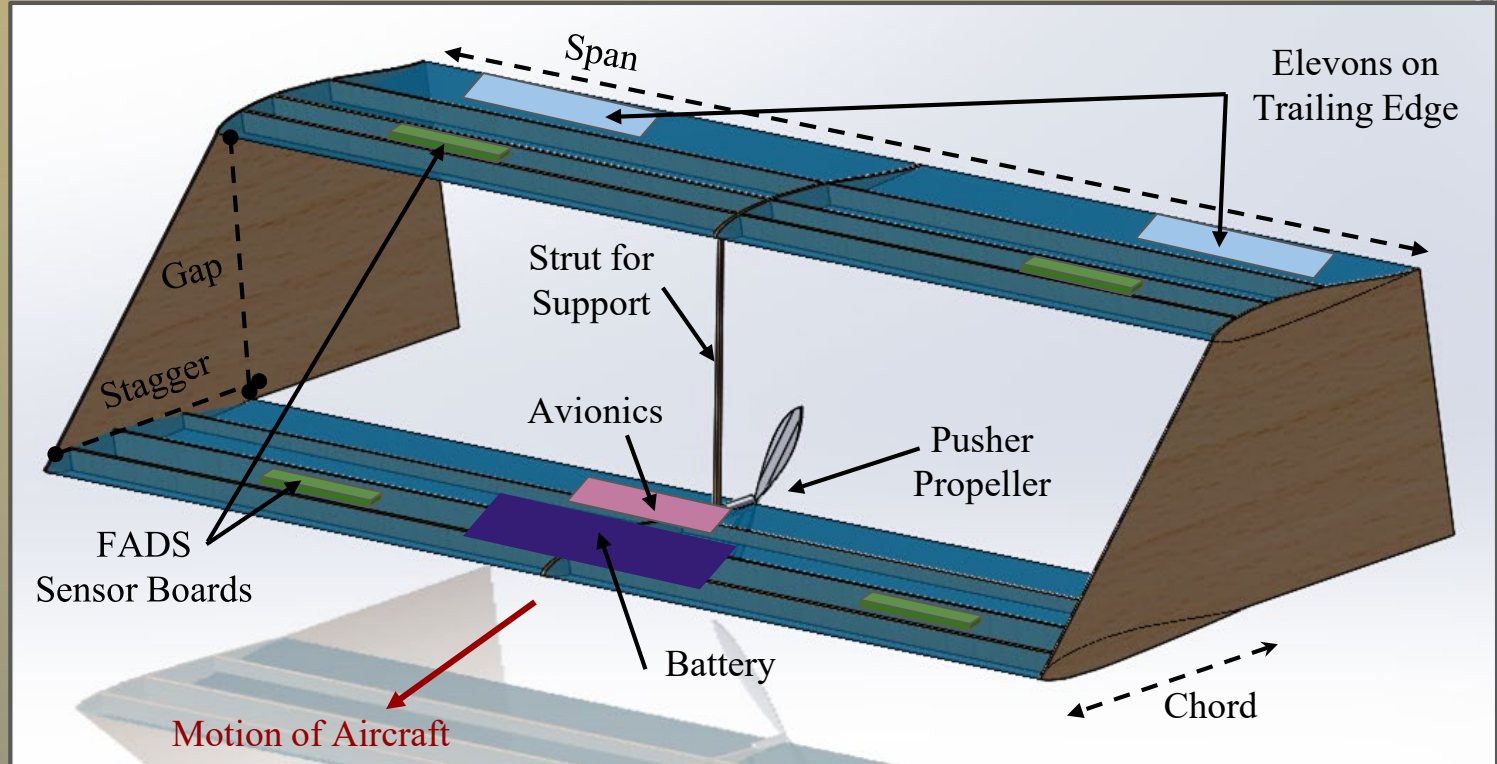


# Integrated Baseline Design

## Avionics:

- autopilot
- FADS
- microcontroller
- power
- management

\*Components  
Not to Scale







# Feasibility Studies

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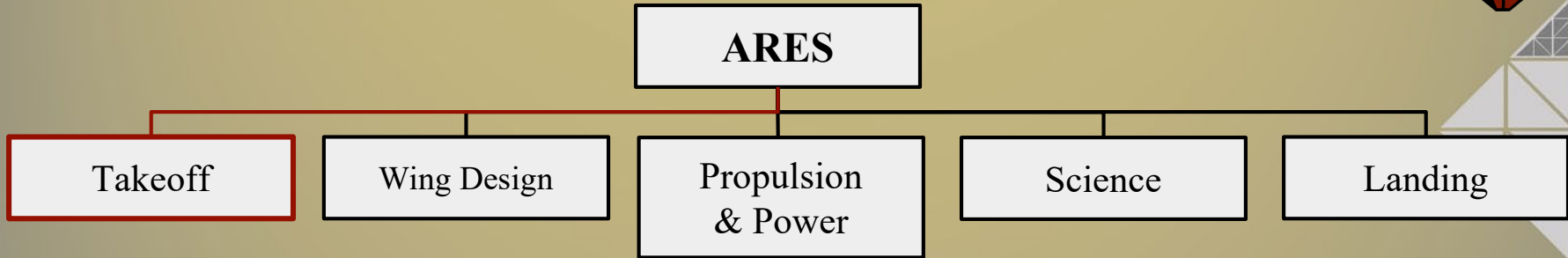
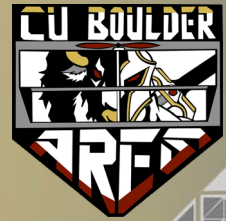
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# Critical Project Feasibility Elements

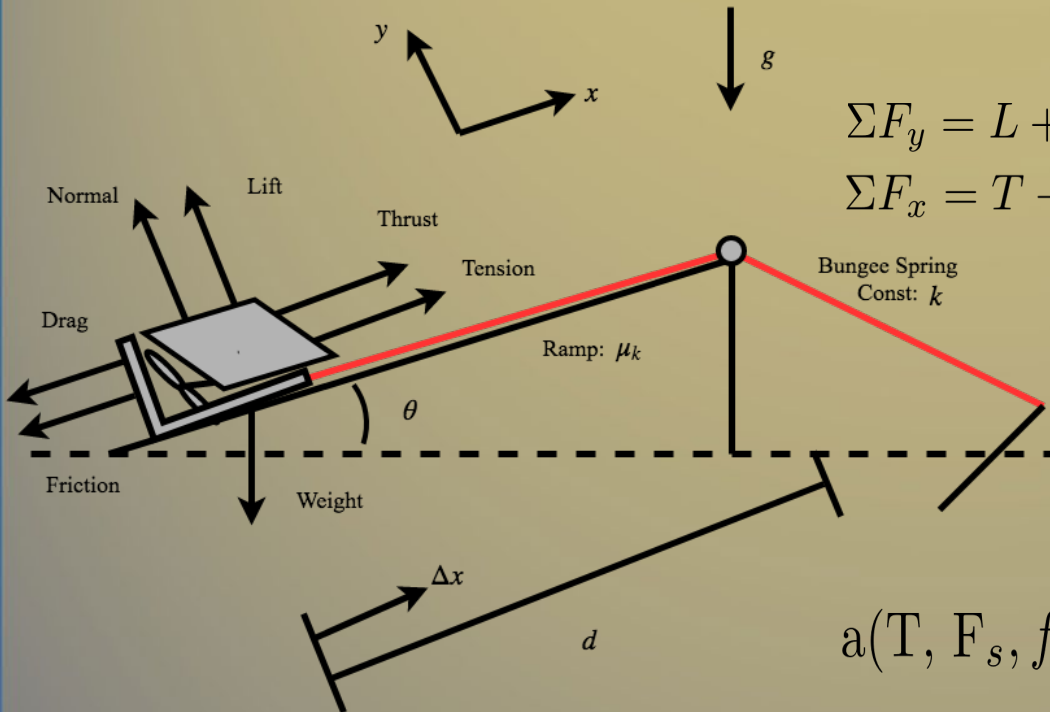


DR 3.2: The takeoff system shall be able to bring the aircraft to its desired initial velocity before it leaves the takeoff system.

DR 3.4: The aircraft shall not require repairs, due to takeoff, that last longer than 15 minutes after a full flight cycle.

# Takeoff System: Model

## Free-Body-Diagram

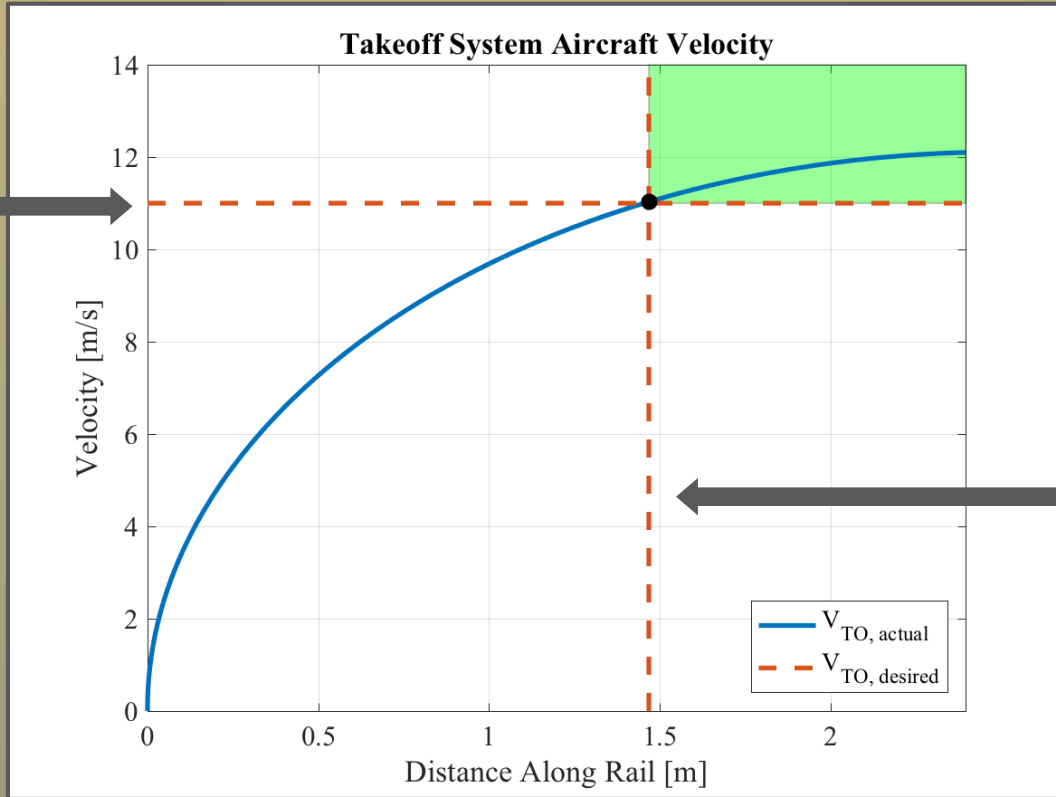


$$\Sigma F_y = L + N - \sin(90 - \theta)W = ma_y$$

$$\Sigma F_x = T + F_s - f_k - D - \cos(90 - \theta)W = ma_x$$


$$a(T, F_s, f_k, D) = \frac{T + F_s - f_k - D - \cos(90 - \theta)W}{m}$$

# Takeoff System: DR 3.2 Feasibility



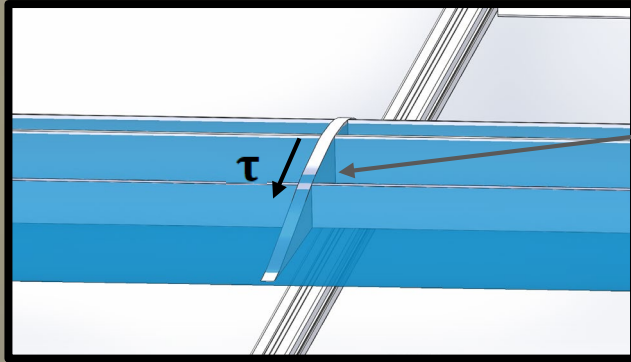
Desired takeoff velocity (cruise velocity) of 11 m/s

Factor of Safety: 1.1

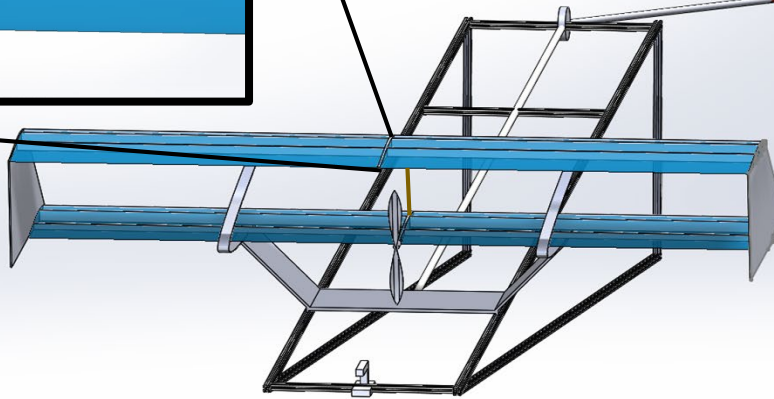
DR 3.2: Bring the aircraft to desired initial velocity 

Minimum rail length of 1.5 m

# Takeoff System: DR 3.4 Feasibility

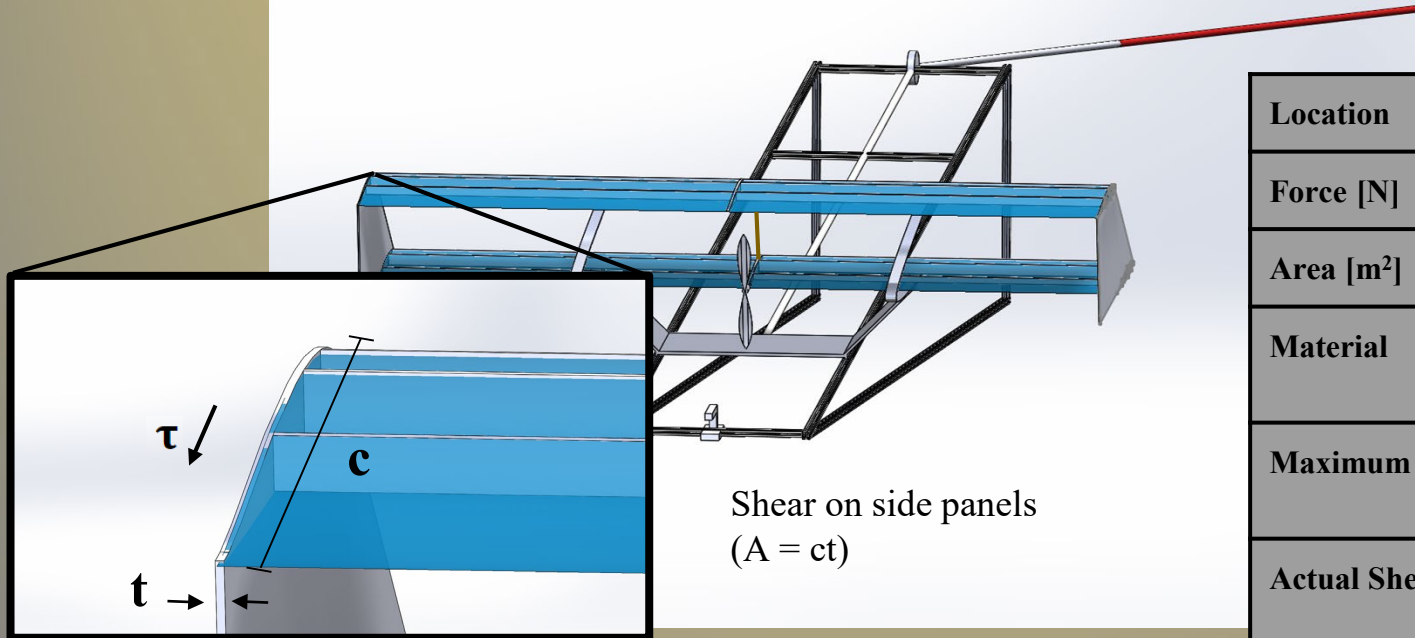


Shear on wing  
(using airfoil area)



<b>Location</b>	Wing
<b>Force [N]</b>	515
<b>Area [m<sup>2</sup>]</b>	0.17
<b>Material</b>	Polystyrene Foam
<b>Maximum Shear [Pa]</b>	$0.29 \times 10^6$ (shear)
<b>Actual Shear [Pa]</b>	$3.03 \times 10^3$ (shear)


# Takeoff System: DR 3.4 Feasibility

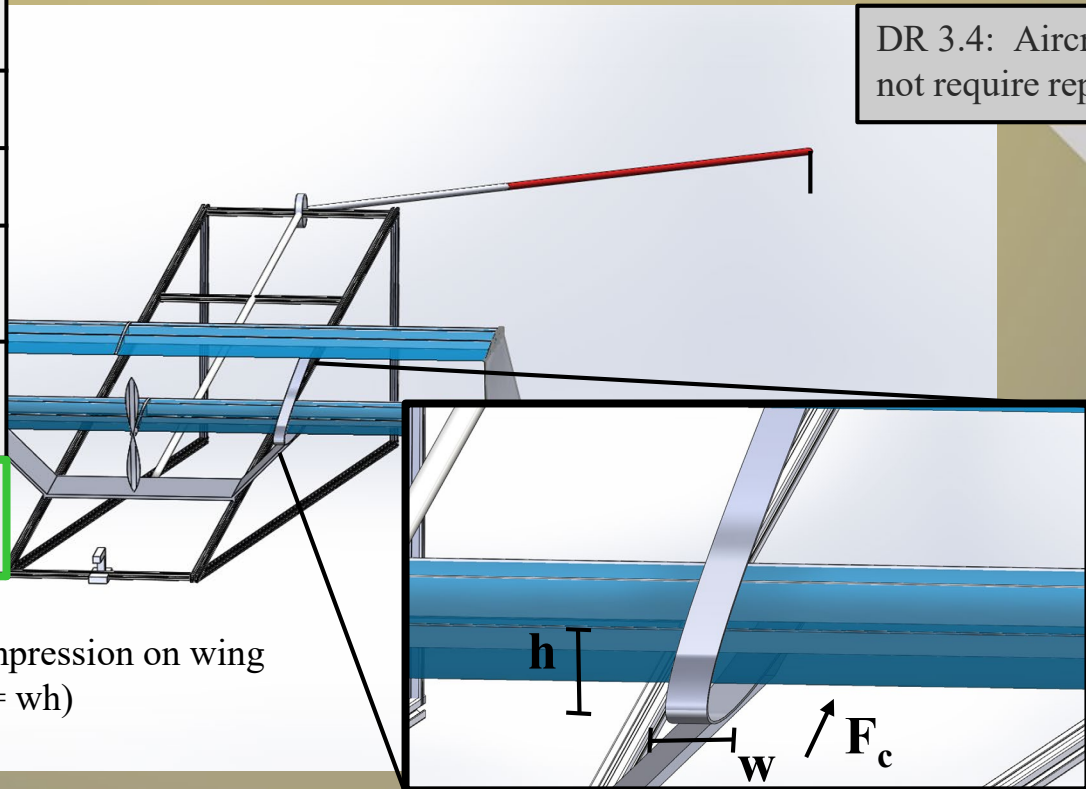


<b>Location</b>	Side Panel
<b>Force [N]</b>	515
<b>Area [m<sup>2</sup>]</b>	$1.2 \times 10^{-3}$
<b>Material</b>	Balsa Wood
<b>Maximum Shear [Pa]</b>	$3.0 \times 10^8$ (shear)
<b>Actual Shear [Pa]</b>	$4.39 \times 10^5$ (shear)

# Takeoff System: DR 3.4 Feasibility

<b>Location</b>	Wing Mount
<b>Force [N]</b>	515
<b>Affected Area [m<sup>2</sup>]</b>	$8.0 \times 10^{-4}$
<b>Material</b>	Polystyrene Foam
<b>Maximum Compression [Pa]</b>	$1.77 \times 10^7$ (compression)
<b>Actual Compression [Pa]</b>	$6.44 \times 10^5$ (compression)

DR 3.4: Aircraft shall not require repairs... 



Compression on wing  
( $A = wh$ )

# Takeoff System: Bungee Feasibility

Target Bungee Design:

$$\Delta x = 5 \text{ m}$$

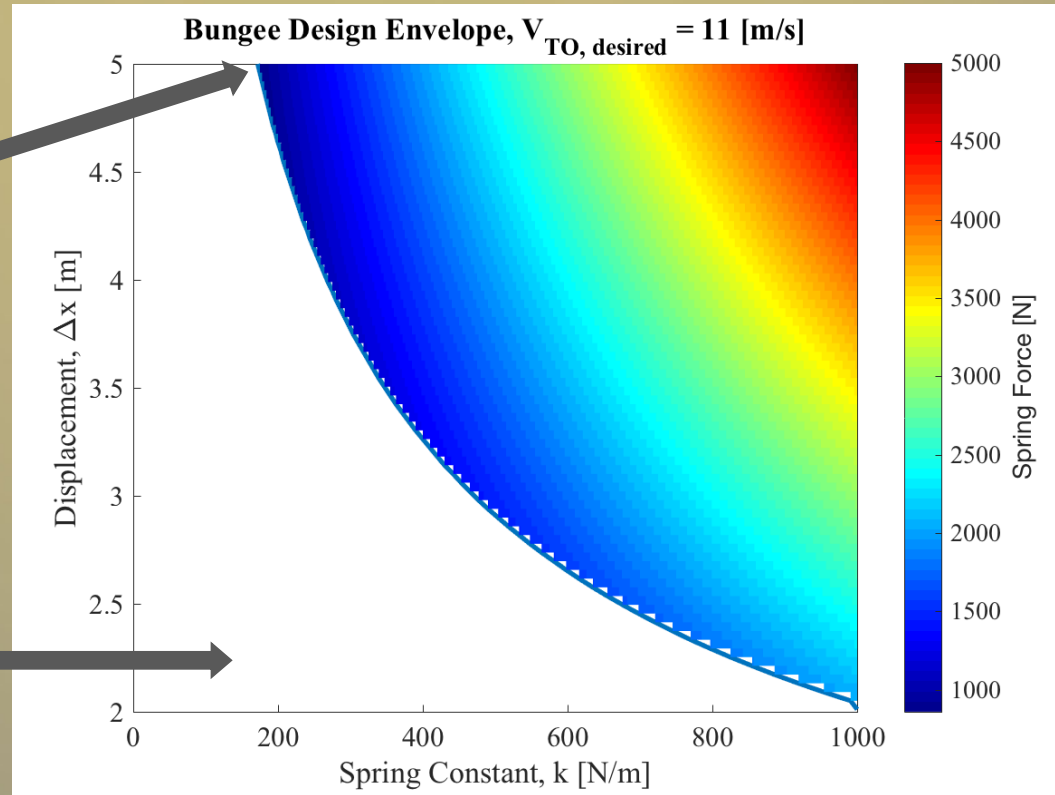
$$k = 172 \text{ N/m}$$

$$F = 860 \text{ N}$$

Divided into 3 bungees:

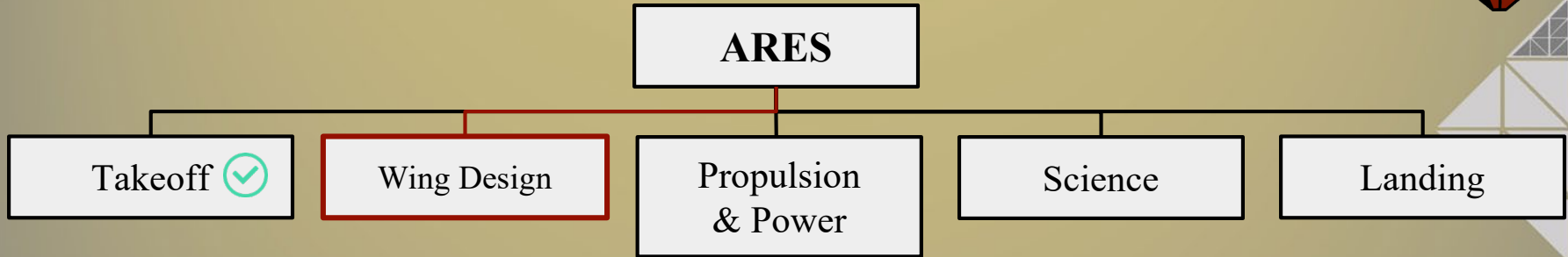
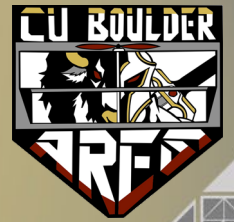
$$F = 287 \text{ N (per bungee)}$$

Infeasible Region: Bungee design does not achieve takeoff velocity





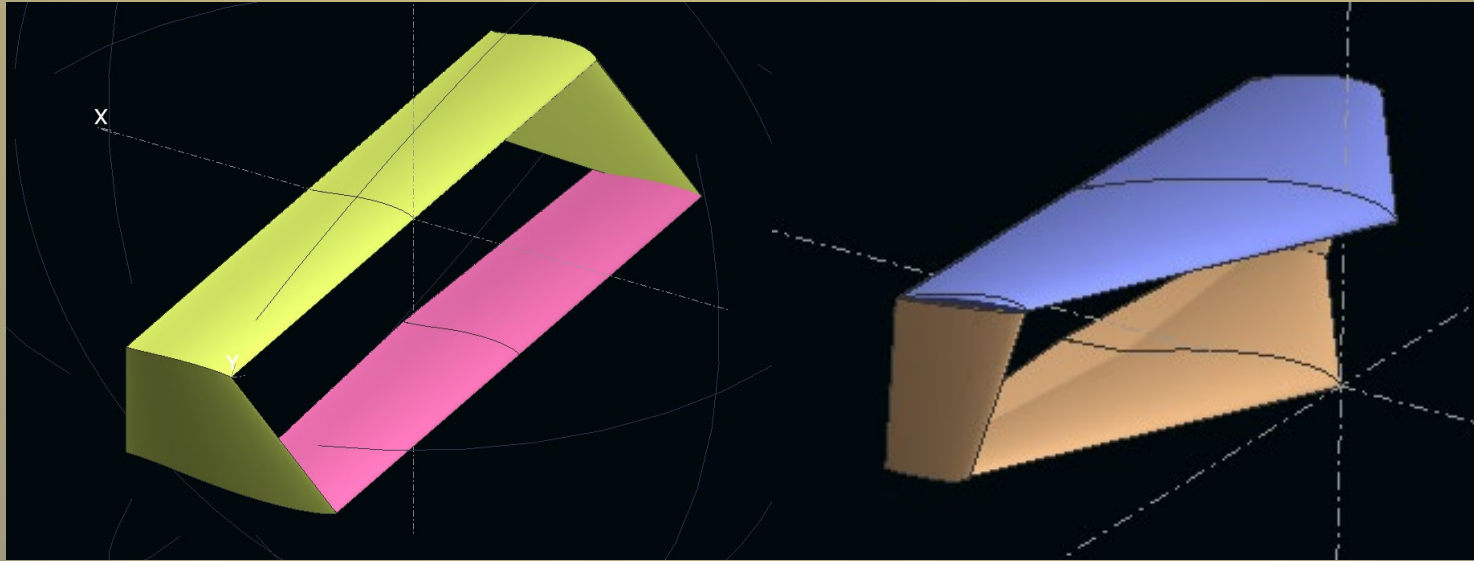
# Critical Project Feasibility Elements



DR 2.1: The aircraft's structure shall only consist of two lifting surfaces connected by struts in the middle and walls on the outside such that it appears in a rectangular "box" shape when viewed from the front and rear.


DR 2.2: The aircraft shall have a Lift-to-Drag ratio greater than that of previous designs from the Eagle Owl lineage.

# Wing Design: Choices



ARES

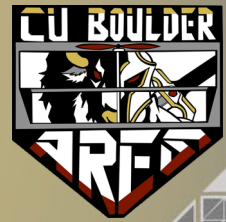
Eagle Owl

DR 2.1: Box shaped  
tailless biplane  
configuration 


XFLR5 Models

Note: Not to scale, ARES has twice the AR of Eagle Owl

# Wing Design: Feasibility Analysis

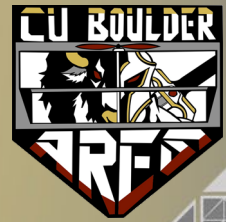


	Span [m]	AR	$C_{L,max}$	$L/D_{max}$	$C_{m,\alpha}$ [rad <sup>-1</sup> ]	$V_{stall}$ [m/s]	$V_{cruise}$ [m/s]
Eagle Owl	0.925	1.39	1.04	12.2	-0.0206	6.36	10.5
<b>ARES</b>	<b>2</b>	<b>3</b>	<b>0.728</b>	<b>26.3</b>	<b>-0.0393</b>	<b>7.60</b>	<b>11.1</b>

DR 2.2: Greater Lift-to-Drag Ratio than Eagle Owl 

Main Takeaway: ARES shows feasibility for flight with similar aerodynamic characteristics to Eagle Owl

# Lateral Static Stability

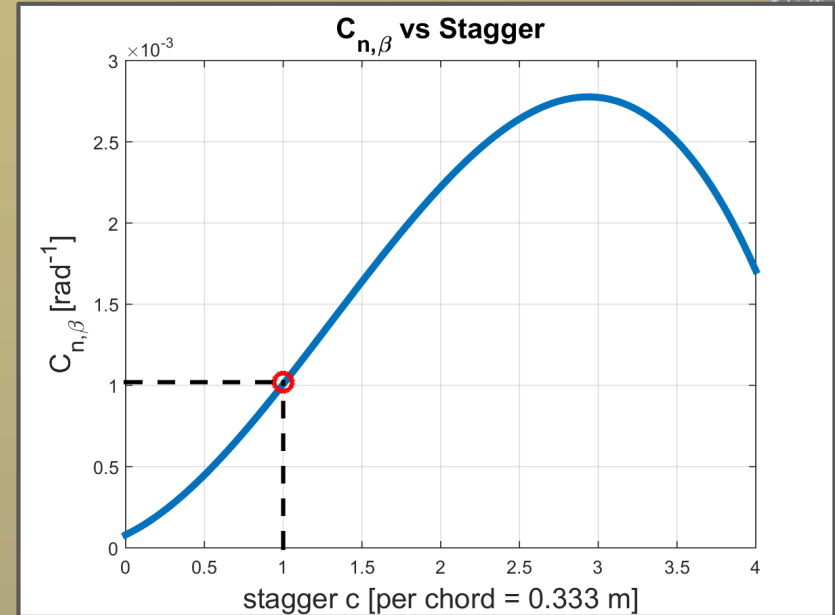


Equation: Yaw Stiffness

$$C_{n\beta} = 2V_V a_F \left( \frac{V_F}{V} \right)^2 \left( 1 - \frac{\partial \sigma}{\partial \beta} \right)$$

BOTE calculation:

	$C_{n,\beta}$ [rad <sup>-1</sup> ]
Eagle Owl	0.001504
ARES	0.001008

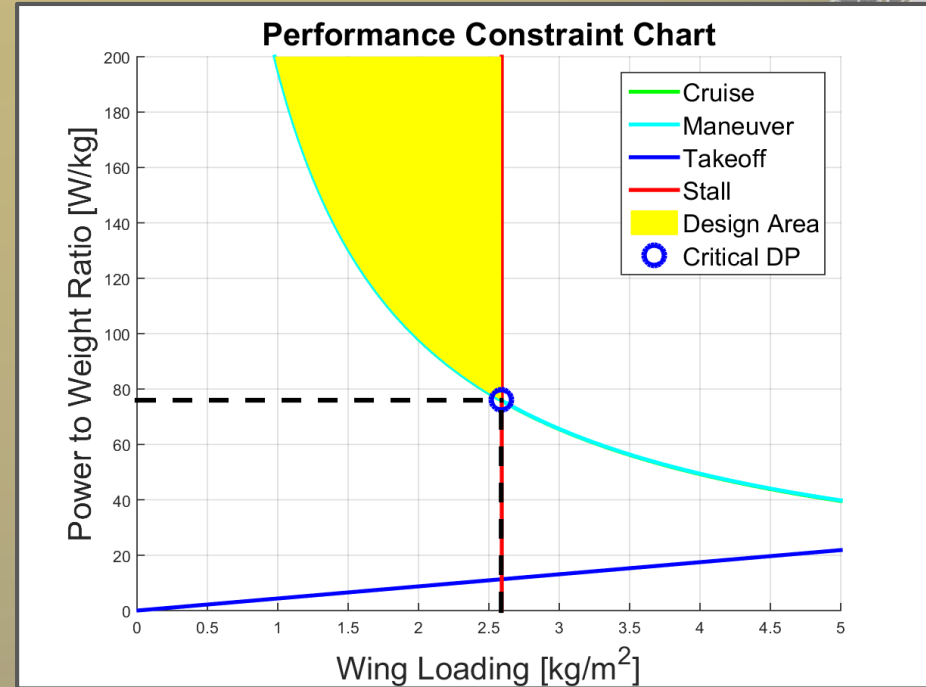


**Main Takeaway:** Positive yaw stiffness proves a laterally stable aircraft design (without rudder)

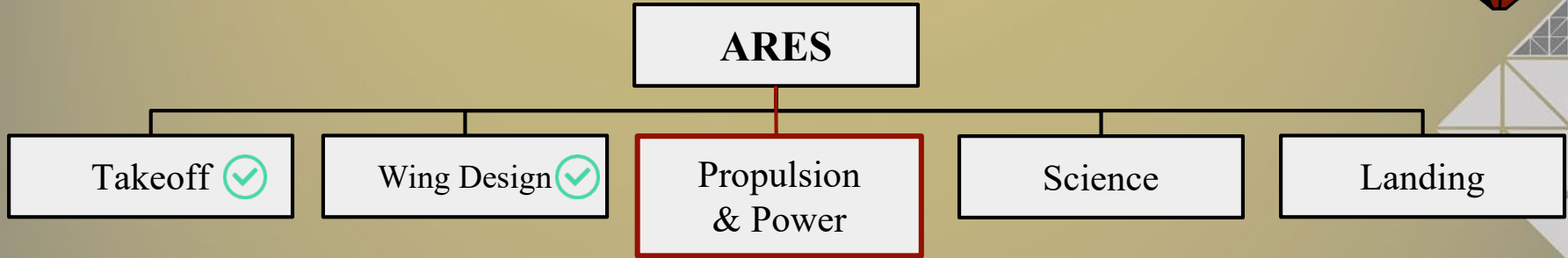
# Performance Constraint Analysis

Generated result:

- Estimated  $S_w$ :  $1.333 \text{ m}^2$
- $W/S = 2.59 \text{ kg/m}^2$ 
  - Estimated Weight =  $3.45 \text{ kg}$
  - 0.5% higher stall speed
- $P/W = 76.0 \text{ W/kg}$  ( $34.5 \text{ W/lb}$ )
  - Assumed 25 % efficiency propulsion system

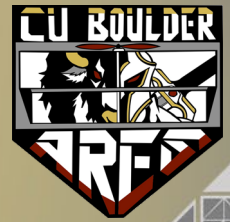


# Critical Project Feasibility Elements



DR 1.2.1: The propulsion system shall be capable of producing enough thrust for the aircraft to reach a flight speeds of 10-30 m/s.

# Propulsion: Power Budgeting



- Maximum mass allowed for batteries: 1.29 kg
  - Max mass shown feasible with mathematical modeling - beyond this is too impacting to design

## Assumptions:

$$(L/D)_{\max} = 20$$

$$\rightarrow SF = 1.3$$

$$V_0 = 11.1 \text{ m/s}$$

$$W_{\max} = 33.36 \text{ N}$$

$$\eta_p = 1$$

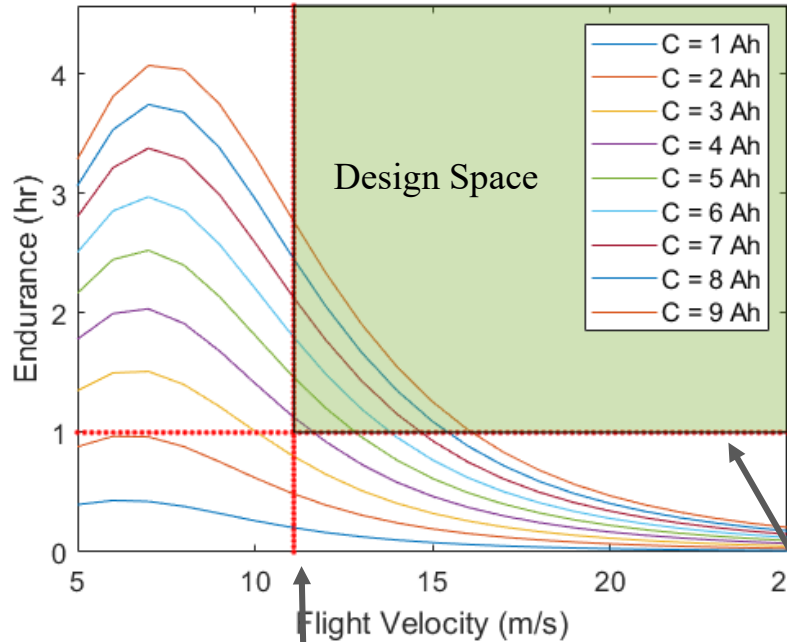
Thrust	Voltage [V]	Current [A]: $I = TV_0/V_{\text{batt}}$	Required Battery Capacity [mAh]	Estimated Battery Weight [kg]
$T_{\min} = W_{\max}(0.2)$	11.1 (3S)	5.132	5132.31	0.3992
	14.8 (4S)	3.849	3849.23	0.4219
$T_{\max} = W_{\max}(0.25)$	11.1 (3S)	6.415	6415.38	0.4990
	14.8 (4S)	4.811	4811.54	0.5273

Best Case

Worst Case

# Propulsion: Power Budgeting

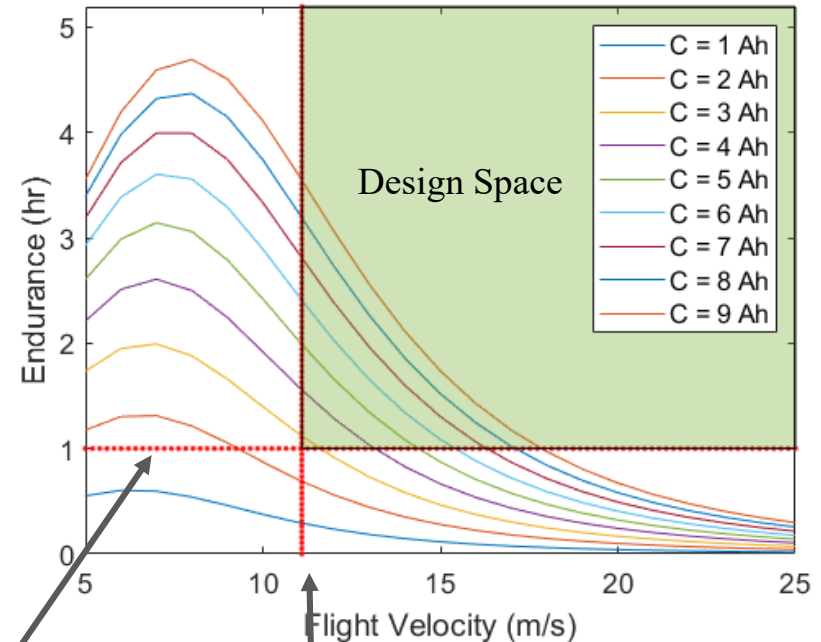
### 3S Battery



Desired cruise velocity (11 m/s)

Desired endurance: 1 hr

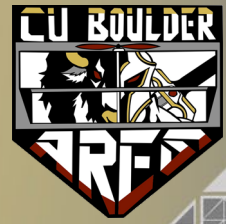
### 4S Battery




Desired cruise velocity (11 m/s)



# Propulsion: Feasibility

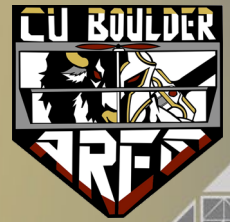


- Proposed ARES propulsion design and strategy is feasible
  - T/W = 0.2-0.25: Comfortable flying with low maneuverability
    - RC Endurance flight Heritage - Mistral, Twister, DataHawk, etc.
    - Mathematical modeling suggests current design can meet design requirements
    - Expert consultation - RC propulsion experts have approved of design
    - Online resources - ECalc, MotoCalc
- Propulsion is easily modifiable during construction and testing stage
  - Evaluate performance using dynamic wind tunnel testing
  - Propeller performance is tunable by changing yoke
    - Helps endurance at consequence of higher propeller stall speed

DR 1.2.1: 1 hour endurance at  
10-30 m/s 

Main Takeaway: Proposed propulsion design can  
provide enough thrust and maintain speed for 1 hr.

# Propulsion/Power: Battery



- Propulsion Requirements:

Battery Voltage	Capacity [mAh]	Endurance [hr]	Mass [g]
11.1V (3S)	3800-9000	1-3	290-695
14.8V (4S)	2900-9000	1-3.5	320-990

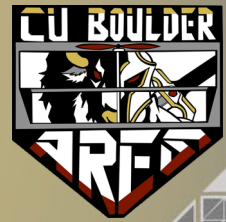
- Science Specifications:

- Voltage: 2S (7.4 V)
- Capacity: 72-102 mAh (200 mAh is smallest possible battery)

- Will be charged under supervision and stored safely


- Assistance and training provided by the Boulder Aeromodeling Society (BAS)


# Propulsion/Power: Summary

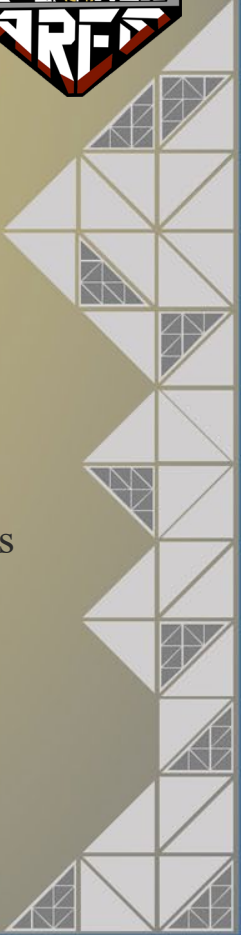


Subsystem	Cost [\$]	Mass [g]	Capacity [mAh]
Propulsion	100-200	290-990	2900-9000
Science	15	20	200

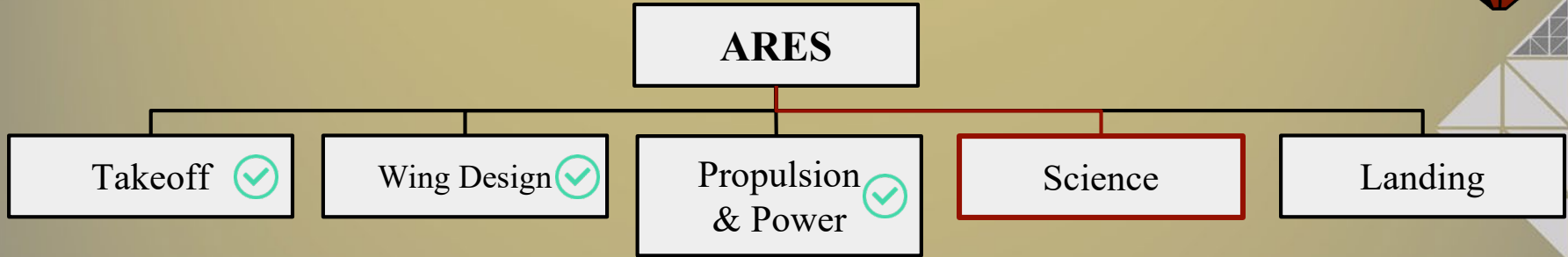
- Batteries can be purchased to achieve 1 hour of flight time.
  - Batteries can be ordered online from E-flite or Venom that are 3-4s with capacities between 200-5000 mAh
- The batteries can provide a flight speed greater than 10 m/s.
- Batteries needed for all subsystems do not weigh more than 1.29 kg

FR 1.0: 1 hour endurance... 

DR 1.2.1: flight speeds 10-30 m/s ... 



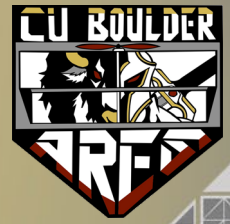
# Critical Project Feasibility Elements



DR 5.1: An array of pressure sensors shall be integrated flush to the exterior of the airframe.


DR 5.5.3: The on-board computer shall be capable of communicating with a minimum of 12 pressure sensors and 1 temperature sensor.

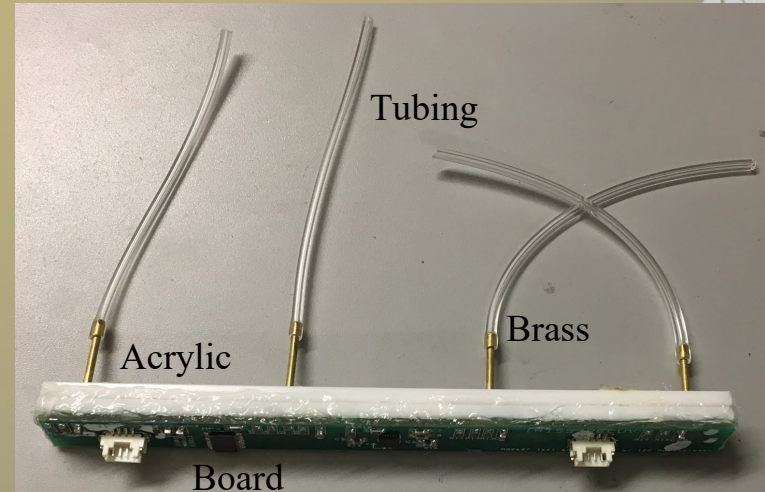
# Science: Pressure Sensors



- MS8607 - 02BA01 Pressure/Temperature Sensors
  - CU FADS expert, Roger Laurence, provided us with custom boards used on Skywalker that house 4 sensors
  - Sensors are housed in acrylic slots that connect to flexible urethane tubing via brass fittings
- Microcontroller
  - Must have 4 ports that accept I2c data

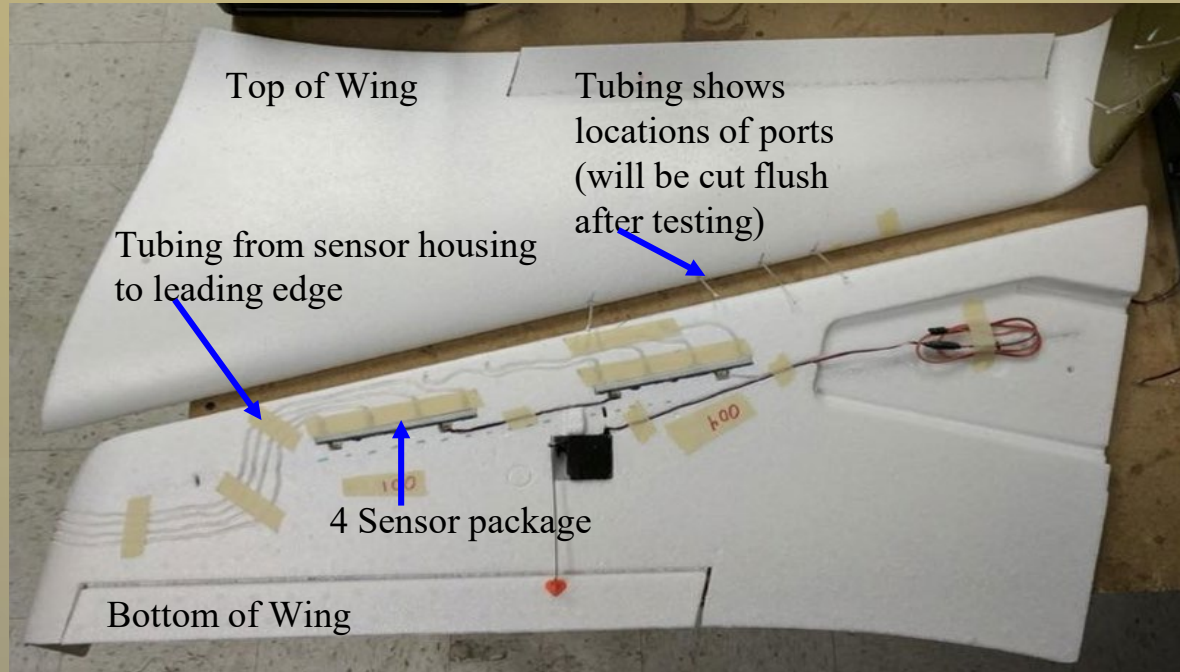
DR 5.1: Pressure Sensors 


DR 5.5.3: Onboard computer capable of communicating with 13 sensors 



# Science: Manufacturing

From CU FADS expert, Roger Laurence on his dissertation work with the Skywalker



DR 5.1: Sensors integrated flush to airframe 

Main Takeaway: FADS have been integrated on aircraft before and we have been given documentation on how to manufacture.


# Science: Calibration of FADS



Our pressure measurements will be imperfect so we will need to calibrate our measurements with some “true” values. All techniques can be conducted without flying the aircraft.

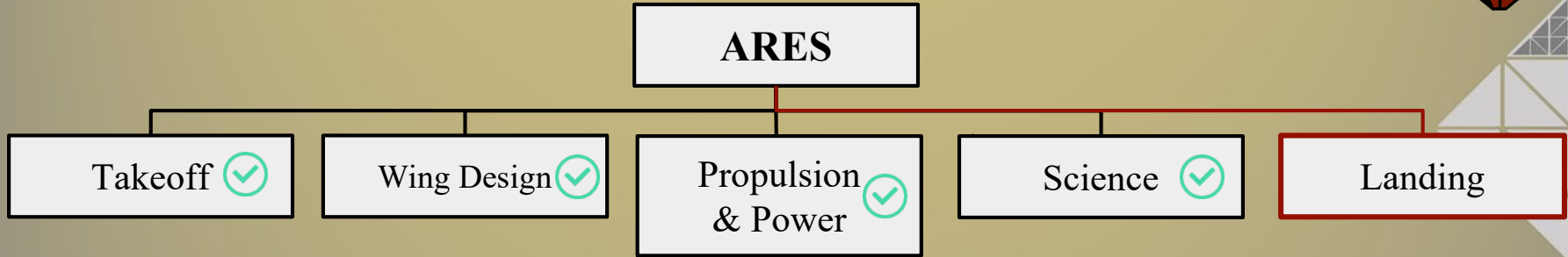
## Technique for Finding “True” Values: **Computational Fluid Dynamics Analysis**

- CFD simulation is capable of determining the pressure felt by the surface of the aircraft
- We will need to:
  - Import a model of our aircraft
  - Determine exactly which grid points correspond to the locations of our our FADS sensors
  - Vary the angle of attack and sideslip
  - Compare the expected pressure from the CFD to the measured FADS pressure using least squares regression

FR 5.0: The data shall be converted to relative wind speed 

**Main Takeaway:** We will calibrate our system using predicted pressure values from CFD analysis instead of flying a multi-hole probe.

# Critical Project Feasibility Elements



DR 6.1: The aircraft shall land such that it can takeoff again within 15 minutes.

DR 6.2: The landing system shall be attached to the aircraft and not rely on an external device.



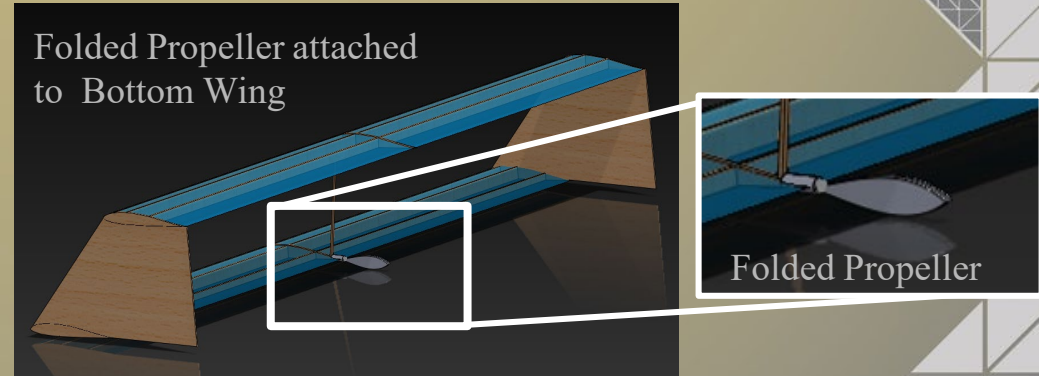
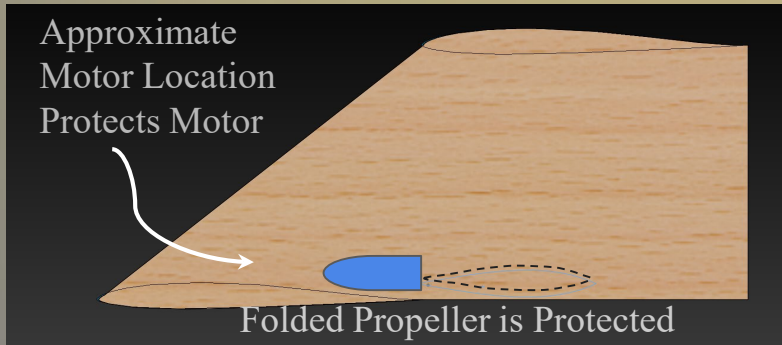
# Landing

## Chosen Solution: Skid Landing

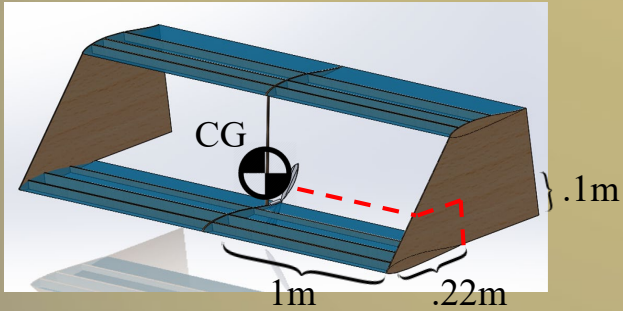
DR 6.2: Attached to aircraft 

### To be feasible:

- The propeller needs to fold to avoid damage
- The CG will be low to decrease the chance of tumbling
  - Preventing tumbling will protect engine shaft and other weak components
- The body needs to withstand the landing forces

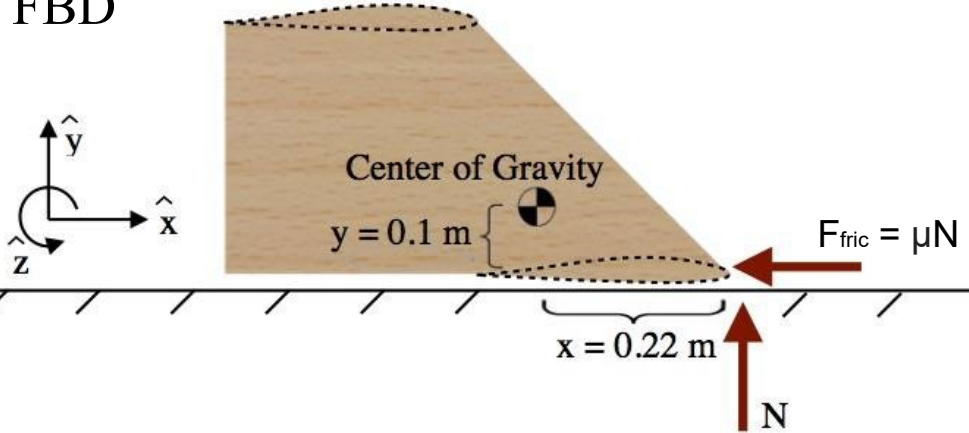


# Landing Feasibility: Sliding



What is the coefficient of friction that will result in sliding rather than flipping?

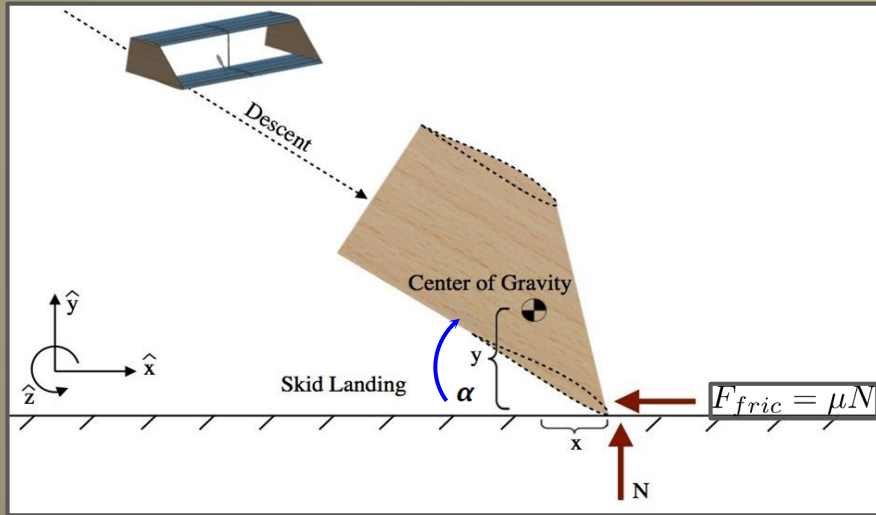
FBD



$$\sum M_{cg} = 0.22N - 0.1\mu N$$

$$0 = N(0.22 - 0.1\mu)$$

# Landing Feasibility: Sliding



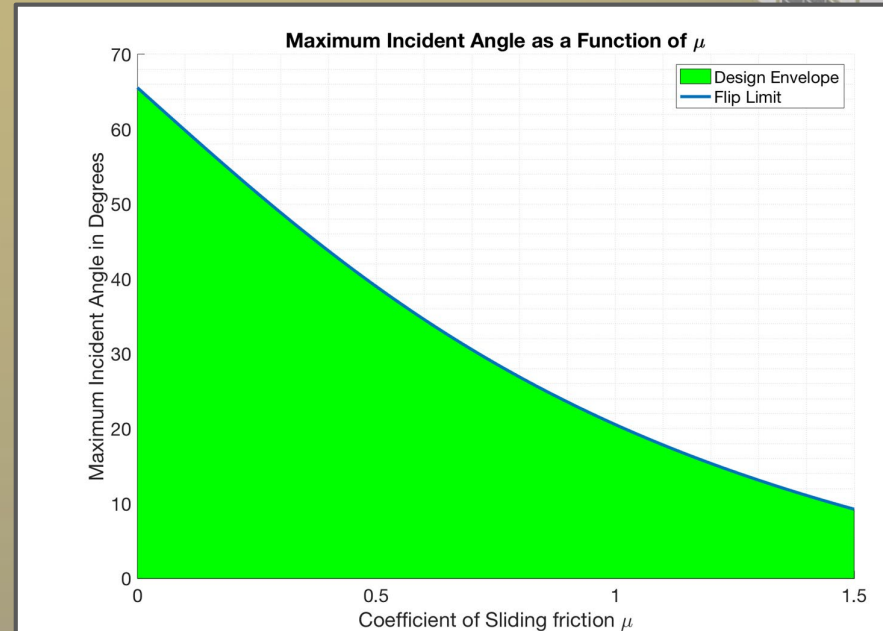
## Variation in Incident Angle Analysis

$$x = -0.1\sin(\alpha) + 0.22\cos(\alpha)$$

$$y = 0.22\sin(\alpha) + 0.1\cos(\alpha)$$

$$0 \leq \sum M_{cg} = xN - y\mu N$$

$$\tan(\alpha) \leq \frac{0.22 - 0.1\mu}{0.1 + \mu 0.22}$$



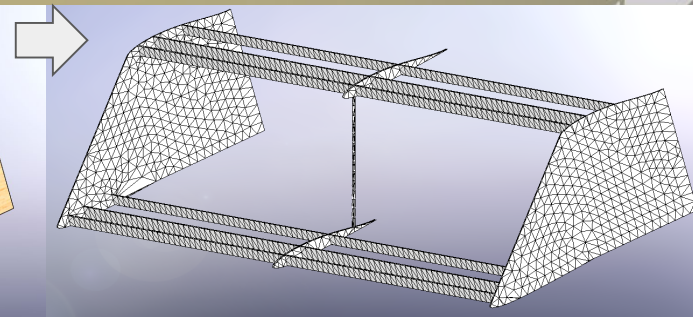
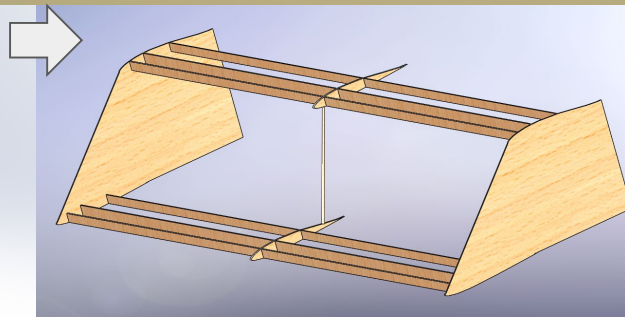
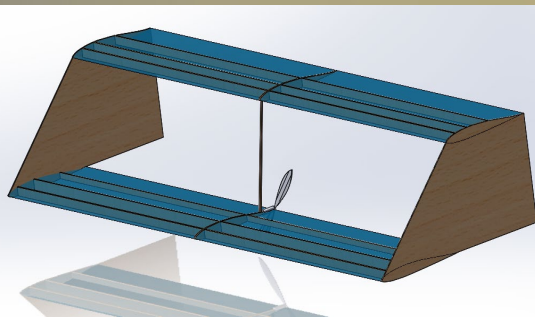
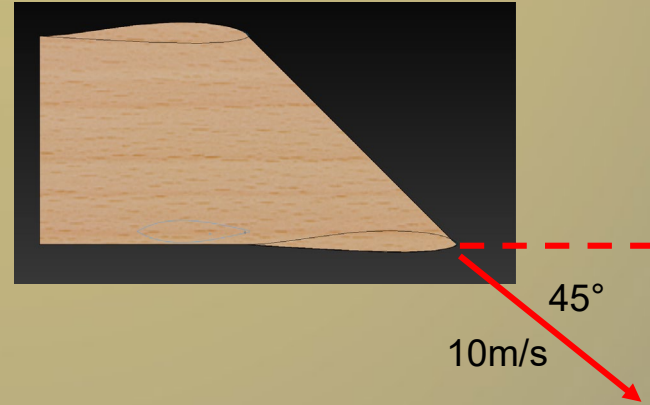
# Landing Feasibility: Simulation



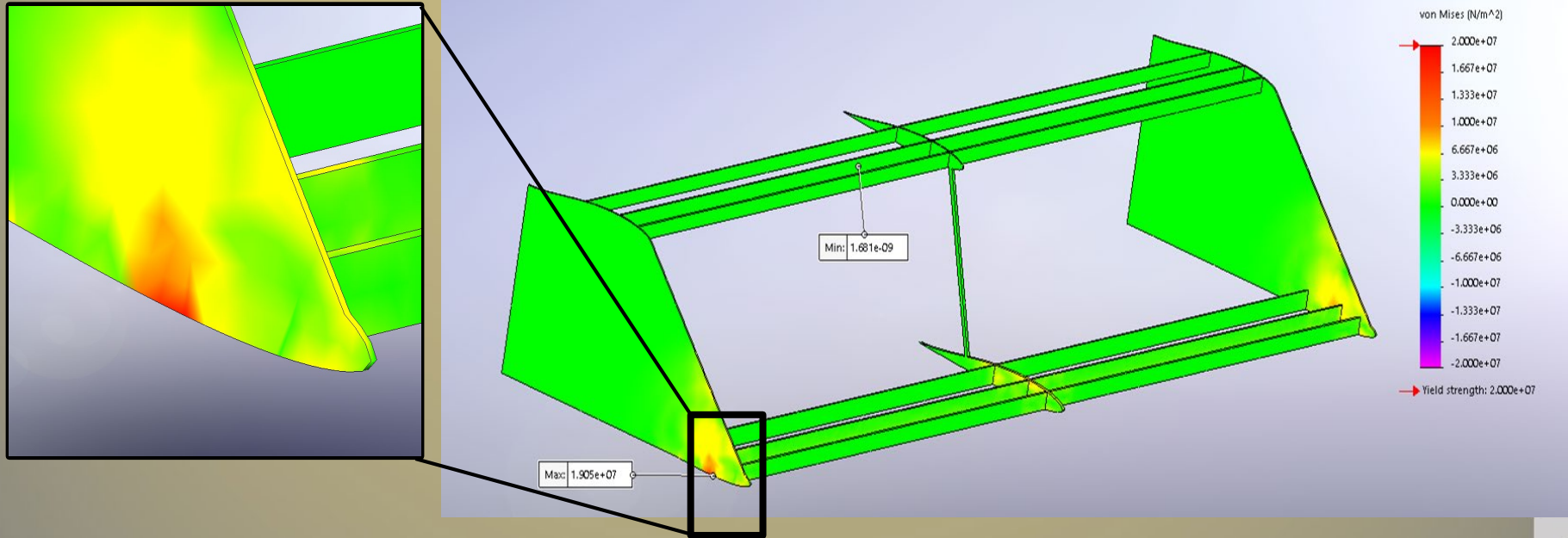
$$V_{\text{stall}} = V_{\text{land}} = 7.60 \text{ m/s}$$

Simulate a “worst case” landing scenario

Simplifications to design for simulation



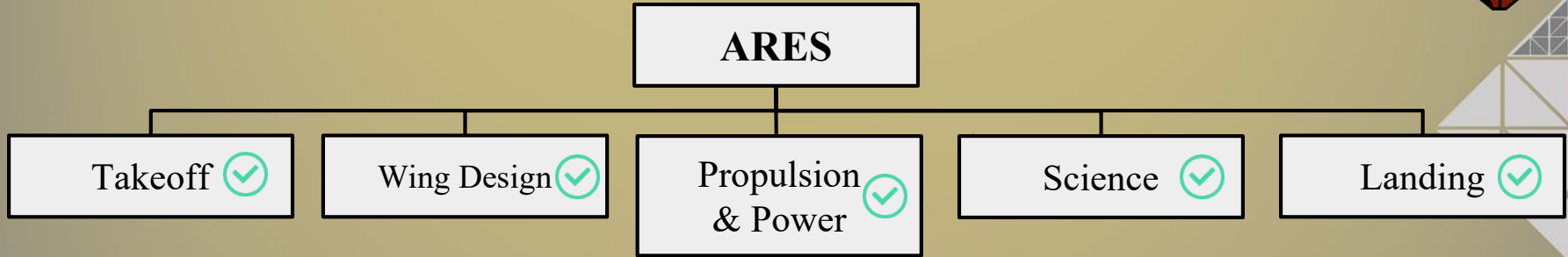
# Landing: Stress



DR 6.1: Land such that it can take-off again

Main Takeaway: Max landing force occurs on back of aircraft. We do not exceed our yield strength.

# Summary



Project  
Overview

Baseline  
Design

Feasibility  
Study

Summary

# Mass Totals



Component	Mass [kg]
Airframe	1.6
Science (Microcontroller, P/T sensors, housing)	(0.010-0.050) + (0.020) + (0.020)
Battery (Propulsion, Science)	(.29-1) + (0.05-0.1)
Autopilot	0.016
Propulsion (Propellers, motors)	(0.05) + (0.3)
Controls (Servos)	0.05
<b>Total</b>	<b>2.36 - 3.14</b>
<b>Lift Constraint</b>	<b>3.5kg at <math>V_{cruise} = 11.1\text{m/s}</math></b>





# Budget Totals

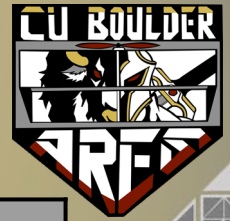


System	Components	Total Cost
Takeoff	Frame, Bungee, Rails, Miscellaneous	\$185
Airframe	Materials	\$300
Propulsion	Motor, Propeller, Yoke	\$60 - \$140
Controls	Servos	\$50
Autopilot	Pixhawk 4	\$180
Science	P/T Sensors, Microcontroller, Housing	\$350 - \$390
Landing	Rails	\$40
Power	Batteries	\$150 - \$200
Miscellaneous	Pilot training, posters, copies, etc.	\$150 - \$200
<b>Total</b>		<b>\$1,465 - 1,685</b>



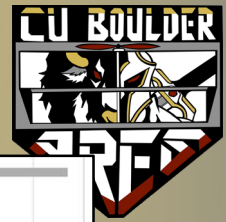


# Power Budget



Subsystem	Component	Power [Wh]	Current [A]	Capacity [mAh]	Voltage [V]
Science	Microcontroller	0.15 - 0.35	0.03 - 0.05	30 - 50	7.4
Science	Pressure transducers	4.2e-3	1.4e-3	1.4	3.0
<b>Science total</b>		<b>0.15-0.35</b>	<b>0.03-0.05</b>	<b>31-51</b>	<b>Peak: 7.4</b>
Propulsion	Propulsion	61-148	6-10	2900-9000	11.1-14.8
Controls	Autopilot	2	0.4	400	5
Controls	Actuators	0.06 - 0.60	0.010 - 0.100	10 - 100	4.8 - 6
<b>Prop/Control total</b>		<b>63-133</b>	<b>6.4-10.5</b>	<b>3310-9500</b>	<b>Peak: 14.8</b>

# Gantt Chart - CDR



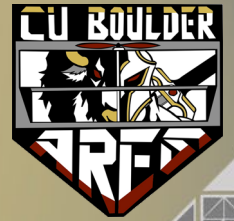
**PDR Presentation**  
10/18/2018

**CDR Presentation**  
FFR



# Moving Forward

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- Most difficult CPEs driving design
  - Battery size/weight impact on endurance
  - Efficiency of propulsion system
  - Structural integrity of airframe on takeoff and landing
- Improvement of models and assumptions to confirm current design
- Details of airframe and control surface design
- Prototype construction
  - Allows for real-life aerodynamic/stability testing
  - Experience gained manufacturing will help during production





# Acknowledgements

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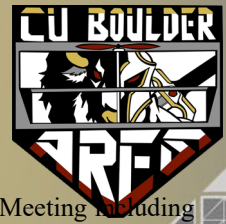


- Dr. Brian Argrow
- Dr. Donna Gerren
- Dr. Dale Lawrence
- Dan Hesselius
- Project Advisory Board
- Dr. Roger Laurence
- Ian Cooke
- Christine Reilly
- Chris Choate
- Boulder Aeromodeling Society





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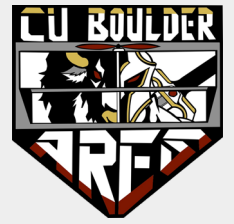
# Thank You

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Are there any questions?

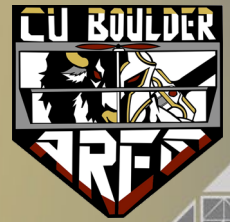




# Backup Slides



# Baseline Design Selection



Takeoff	Flight	Science	Landing	Power/Electronics
External bungee launch system	Rectangular planform, lower wing forward  Autopilot: PX4  Bottom mounted pusher propeller	FADS integration  Calibration  Temperature sensor	Skid landing	Parallel LiPo batteries for propulsion and control  External battery for FADS





# Mission Success Criteria



Level	Data Capture	Landing	Navigation/Control	Flight
1	<p>FADS system integrated/ recording pressure data continuously</p> <p>Record continuous local temperature and inertial measurements to onboard storage while powered</p>	<p>Airframe can survive a simulated landing cycle outside of a flight test</p>	<p>Control surfaces are actuated in response to RC input and autopilot feedback loop</p>	<p>Provide flight models and simulations to show that the design can complete design objectives</p>
2	<p>Same as Level 1</p>	<p>Landing method allows for consecutive takeoff and landing cycles with only power replacement/recharge</p>	<p>Autopilot achieved with ability to maneuver the aircraft in a 600m diameter circle while staying within visual sight</p>	<p>Takeoff with no damage to sensors, structure, or operators</p>
3	<p>Calibrate FADS system such that data is converted to aircraft-relative wind velocity to within 1m/s and 1° of accuracy</p>	<p>Consecutive takeoff and landing cycles occur a minimum of 10 times</p>	<p>Full flight with takeoff and landing achieved with autopilot</p>	<p>Flight endurance is greater than 2 hours with all systems powered</p>

# Motivation

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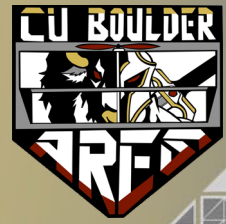
- Obtaining data from inside extreme weather events can be a challenging task
- Getting into a stormcell requires an extremely steady, robust unmanned aircraft
  - Options exist but are expensive
- Implementing a flush airdata sensing system can help eliminate risk of damage to expensive sensors
  - Past renditions used protruding pitot probes but they can break on landing
- Helps to further understand atmospheric patterns





# Functional Requirements

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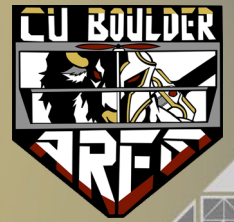


- FR 1.0: The aircraft shall have a total flight endurance of at least 1 hour while maintaining visual sight with the operator.
- FR 2.0: The system shall be an aircraft with a box wing configuration with a span no larger than 72 inches; the effects of increasing aspect ratio from the previous version to increase endurance will be investigated.
- FR 3.0: The aircraft shall demonstrate a controlled takeoff.
- FR 4.0: The aircraft shall be piloted by an autopilot during the steady flight regime of the mission.
- FR 5.0: The aircraft shall simultaneously measure external temperature, inertial flight data, and pressure on the airframe surface at multiple points with a flush airdata sensing (FADS) system. The recorded data shall be stored on-board and converted to relative wind speed after flight.
- FR 6.0: The aircraft shall land in a manner such that the aircraft is capable of completing at least 10 takeoff and landing cycles with only 15 minutes on the ground between landing and takeoff.



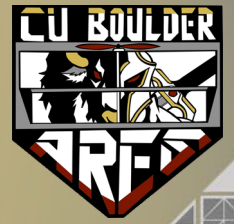


# Schedule



- Important upcoming dates:
  - 10/21/2018 Implement feedback on PDR
  - 10/23/2018 Complete final feasibility analysis (including PAB feedback)
  - 10/23/2018 Complete identification of CPE's most threatening to success
  - 10/23/2018 Final determination of potential off-ramps
- Future milestones:
  - 11/08/2018 Begin prototype aircraft
  - 11/29/2018 Finalized component selection
  - 12/03/2018 Conceptual Design Review
  - 12/17/2018 Fall Final Report due



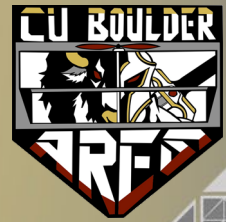


# Take-off Backup Slides





# Takeoff System

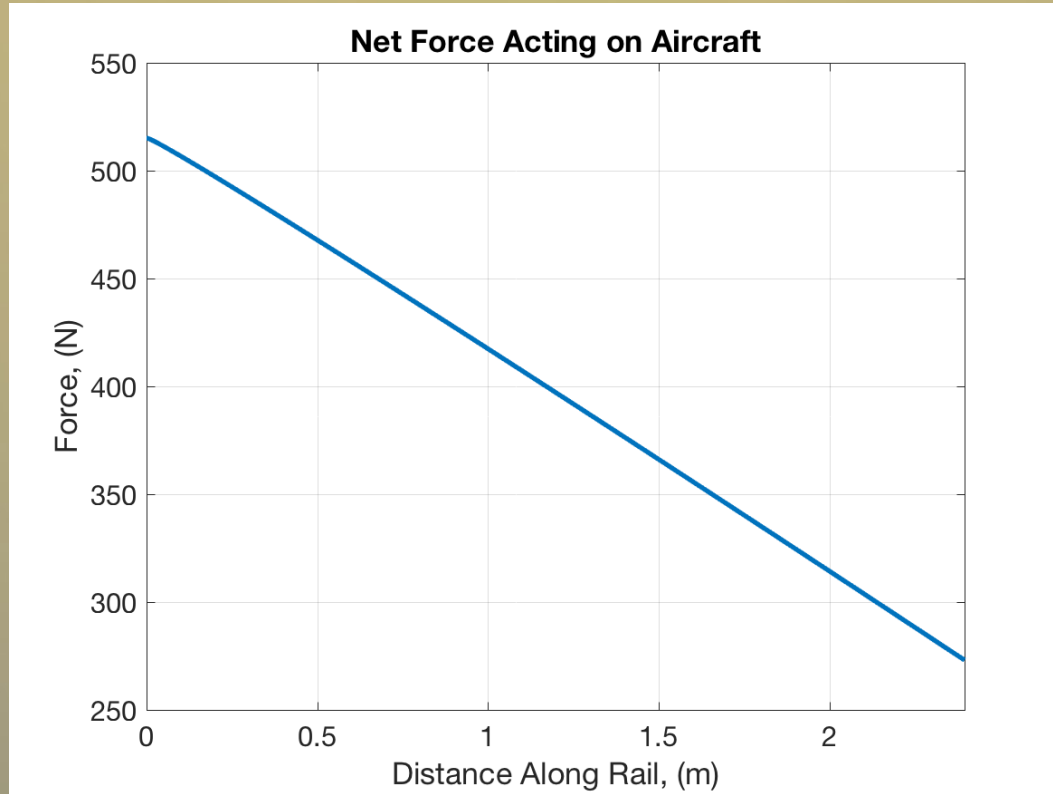


FR 3.0: The aircraft shall demonstrate a controlled takeoff

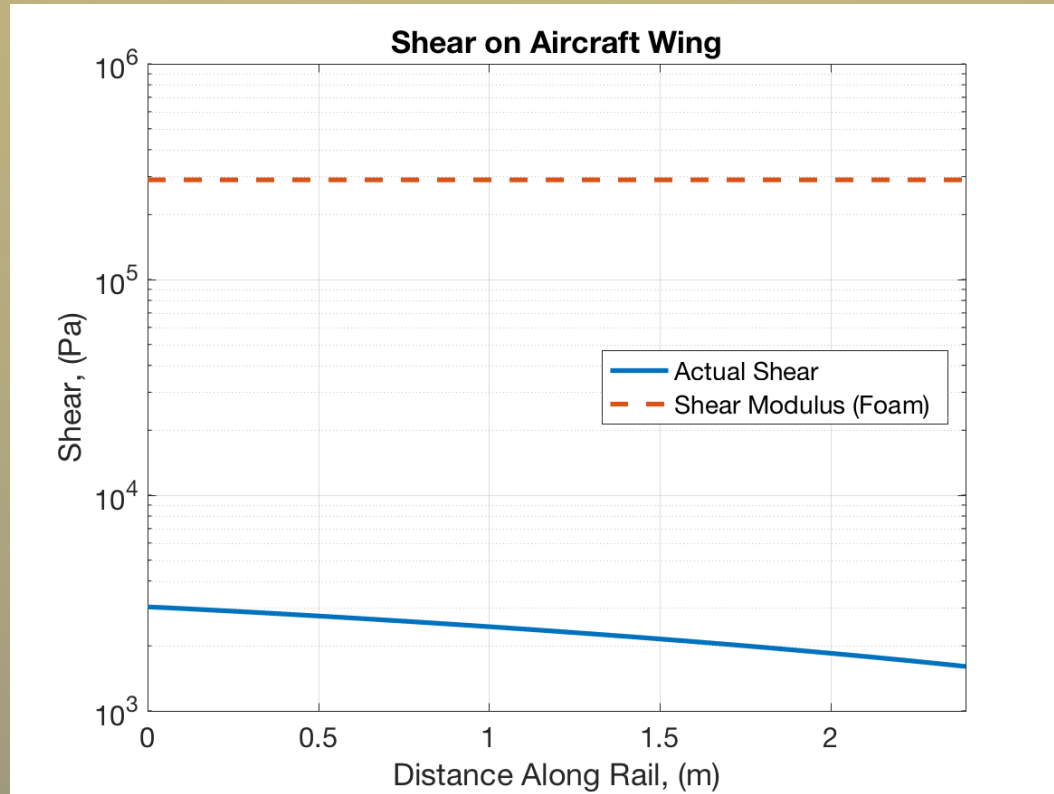
## Chosen: External Bungee Launch System

- Abundance of flight heritage/documentation
- Easy to dictate final takeoff velocity
  - Determined by length of rails, bungee spring constant, bungee displacement
- Simple to manufacture and cost effective
  - 80/20 for rails and other structure, aluminum for other components
  - Many commercial options for bungee
- Mobile
  - Easy to assemble and disassemble

# Takeoff System - Extra

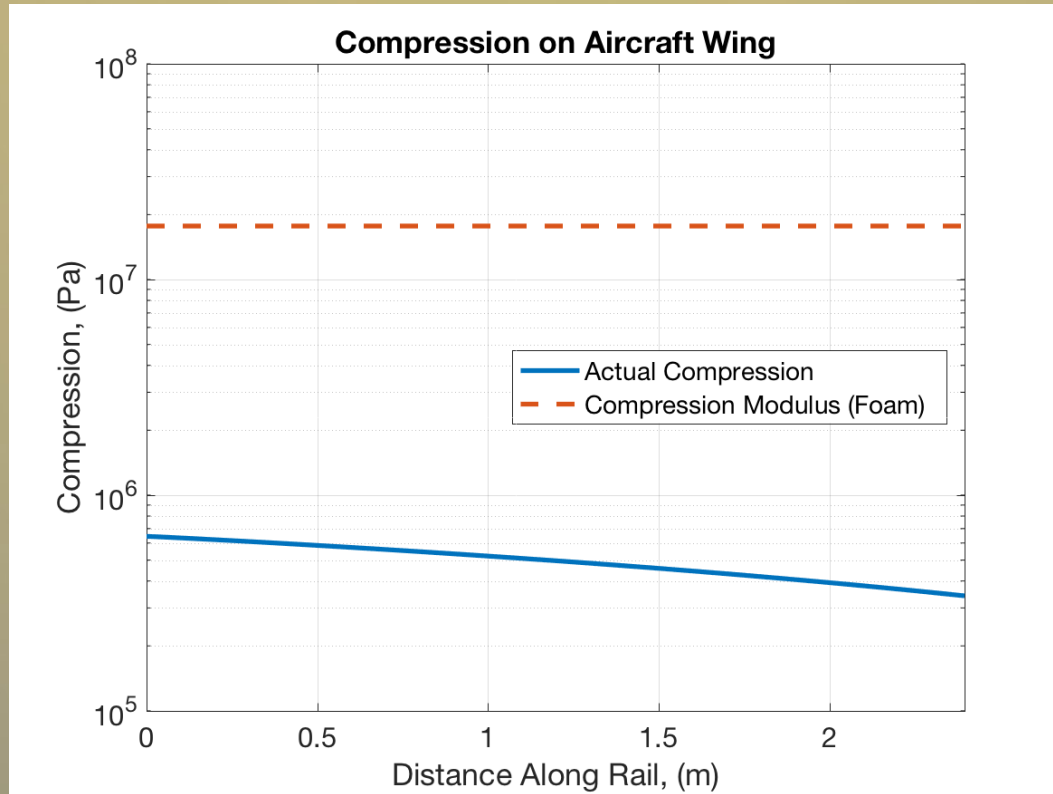
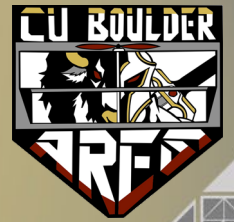


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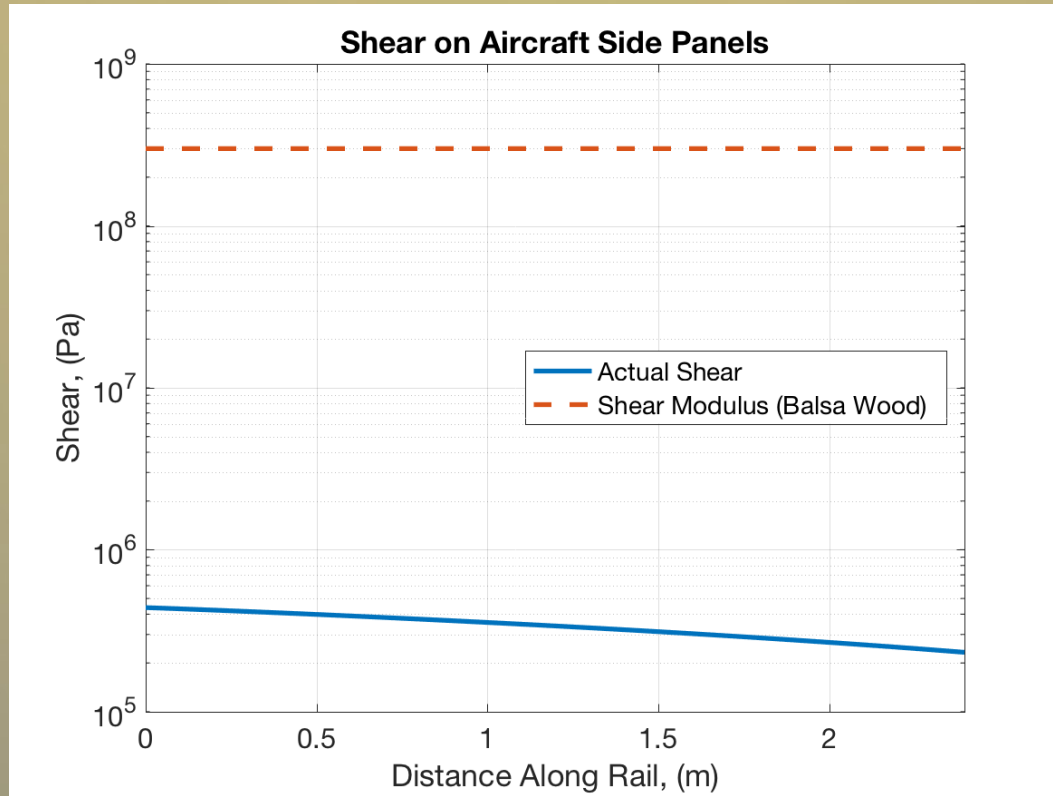
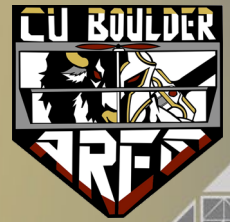




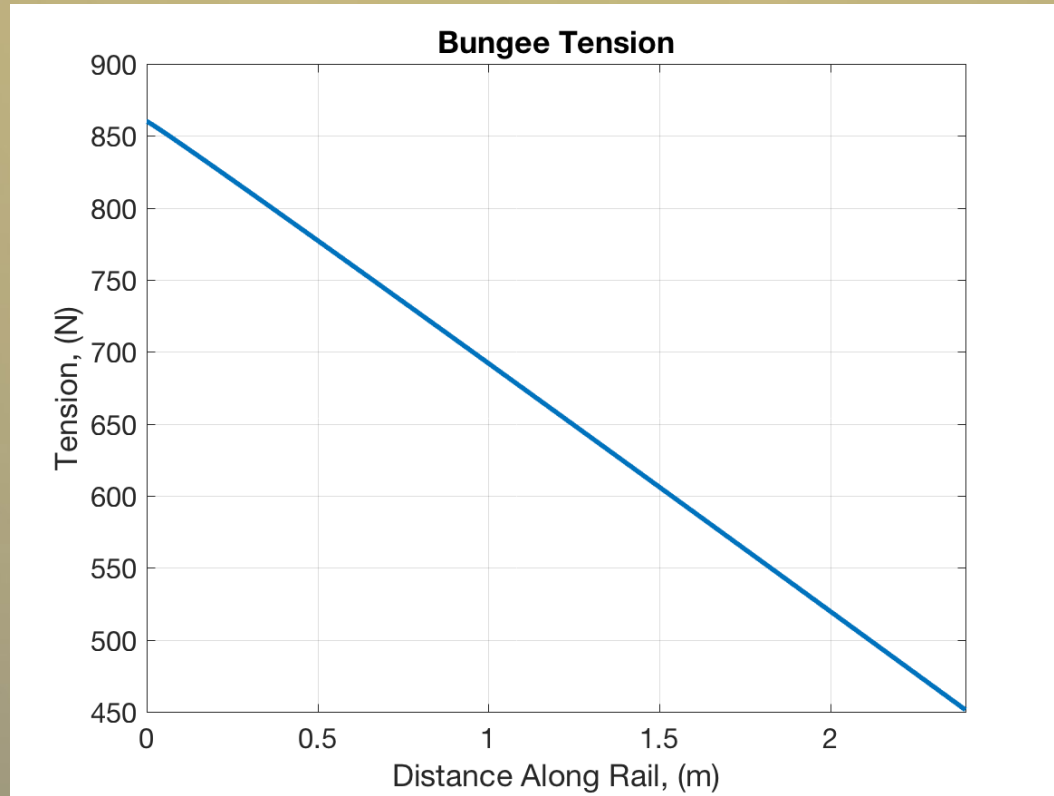
# Takeoff System - Extra



# Takeoff System - Extra



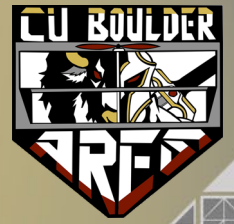
# Takeoff System - Extra





# Takeoff System - Extra

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## Manufacturing Feasibility

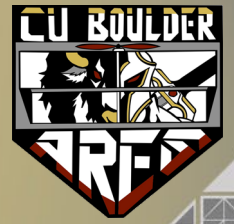
- Very few machined parts
  - Base plate to hold aircraft
  - Release mechanism
  - All other components will be purchased
- Material: Aluminum
- Nothing machined should exceed capabilities of Lathe, Drill Press, Mill.
- Techniques: facing, turning, milling, drilling, tapping, deburring, grinding.





# Takeoff System - Extra

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## Cost Feasibility (approximate)

- Bungee ~ \$25 (KBand Training)
- Rails ~ \$30 (80/20 Inc.)
- Stock Aluminum ~ \$100 (Online Metals)
- Ground Stake ~ \$ 5 (Home Depot)
- Misc: Screws, Hooks, Pulley, etc. ~ \$25 (Home Depot)

Total = \$185



# Takeoff System - Calculations



## Model

### General Forces

$$f_k(N) = \mu_k N$$

$$N(L) = (\sin 90 - \theta)W - L$$

$$F_s = k(d - \Delta x)$$

### Kinematics

$$x(t) = vt + \frac{1}{2}at^2 + x_0$$

$$v(t) = at + v_0$$

### Aerodynamic Forces

$$D(v) = \frac{1}{2}\rho v^2 C_D S$$

$$L(v) = \frac{1}{2}\rho v^2 C_L S$$



# Takeoff System - Calculations

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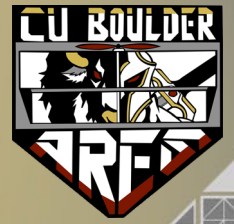
Model (cont.)

$$\Sigma F_x = T + F_s - f_k - D - \cos(90 - \theta)W = ma_x$$

$$\Sigma F_y = L + N - \sin(90 - \theta)W = ma_y$$

$$a(T, F_s, f_k, D) = \frac{T + F_s - f_k - D - \cos(90 - \theta)W}{m}$$



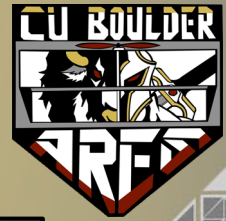


# Wing Design Backup Slides





# Wing Baseline Design



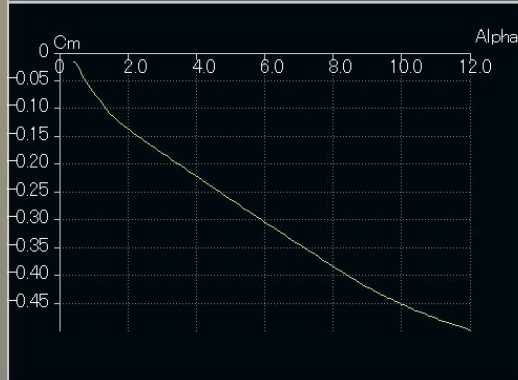
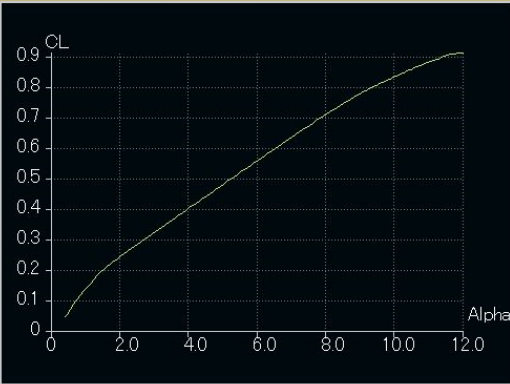
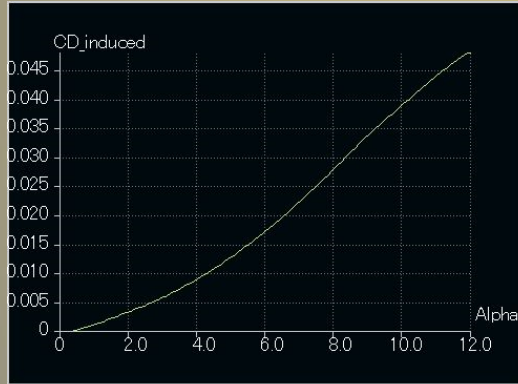
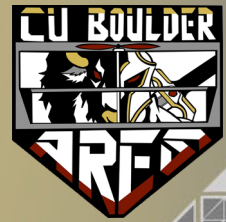
FR 2.0: The system shall be an aircraft with a box wing configuration with a span no larger than 2 meters.

Chosen: Rectangular planform

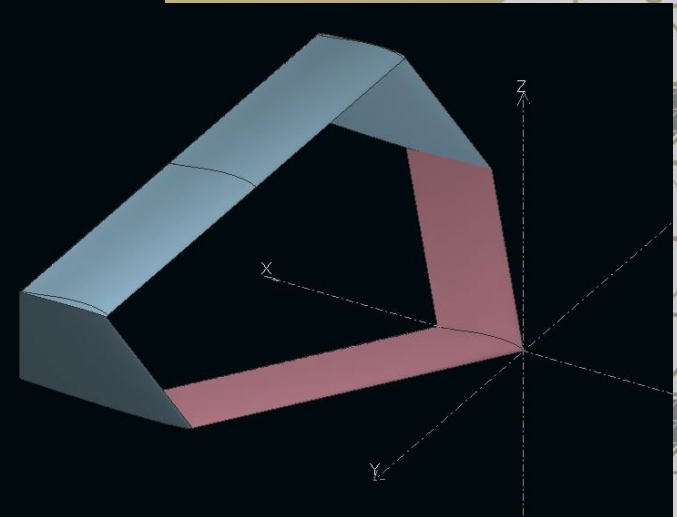
- $AR = 3$ ,
- $S = 1.333 \text{ m}^2$ ,
- $b = 2 \text{ m}$
- $c = 0.333 \text{ m}$
- $0.333 \text{ m}$  stagger (bottom wing forward)
- $0.333 \text{ m}$  vertical separation
- Mass:  $1.6 \text{ kg}$
- Airfoil: MH61 -
  - Used for feasibility analysis
  - Commonly used reflex airfoil for RC flying wings

Main Takeaway: Rectangular planform chosen for aerodynamic efficiency ( $C_l$  vs  $AoA$ ,  $C_d$  vs  $AoA$ )

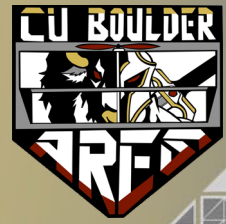
# Baseline Wing Design: XFLR5



RTSB  
— RTSBLLTfixL02



# Wing Design: $C_{L,max}$ loss



$C_{L,max}$  is lower than Eagle Owl due to Negative Stagger

According to “Gap and Stagger Effects on Biplanes with End Plates”,

- Negative stagger lowers the  $C_{L,max}$  by 22.2%. This is an experimental data not shown in XFLR5
- The presented  $C_{L,max}$  takes this loss into account

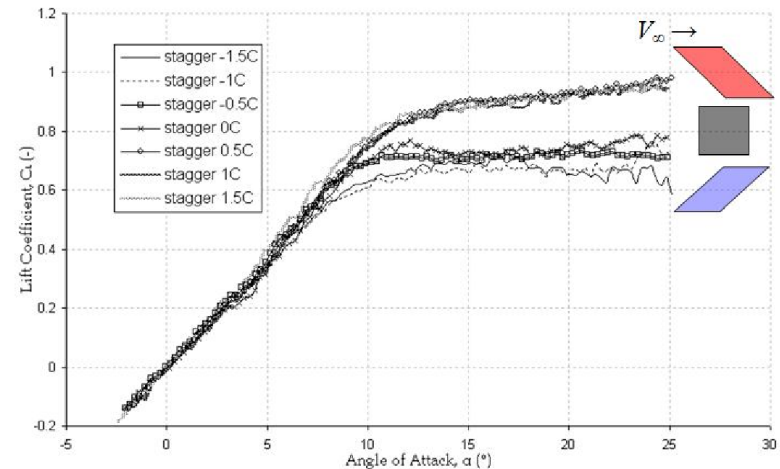


Figure 9 shows dependence of lift on stagger at constant gap with decreasing effect at a higher gap.  $G = 1c$ ,  $Re = 60,000$ .

# Wing Design - Extra

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$$V_{Stall} = \sqrt{\frac{2W}{\rho S C_{L,Max}}}$$

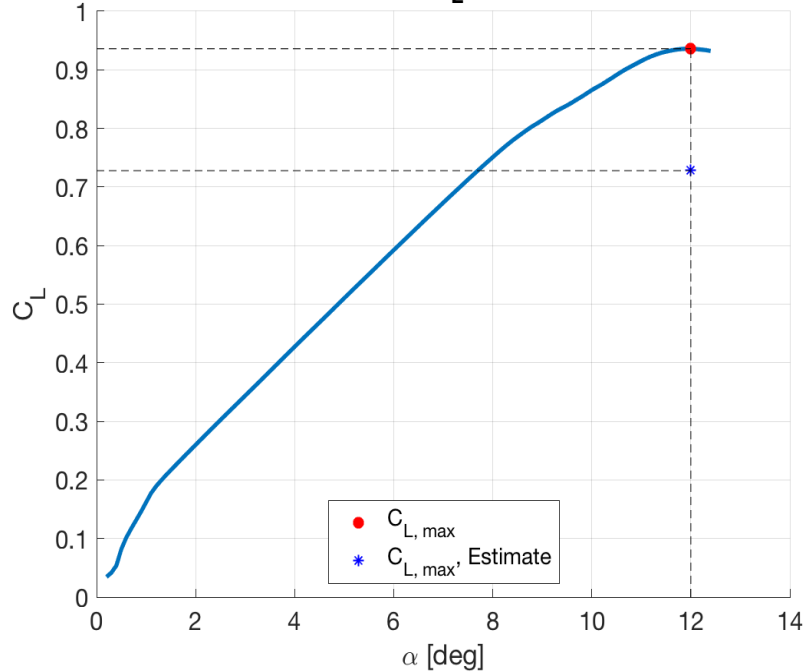
$$V_{cruise} = \sqrt{\frac{2W}{\rho S C_{L,cruise}}}$$



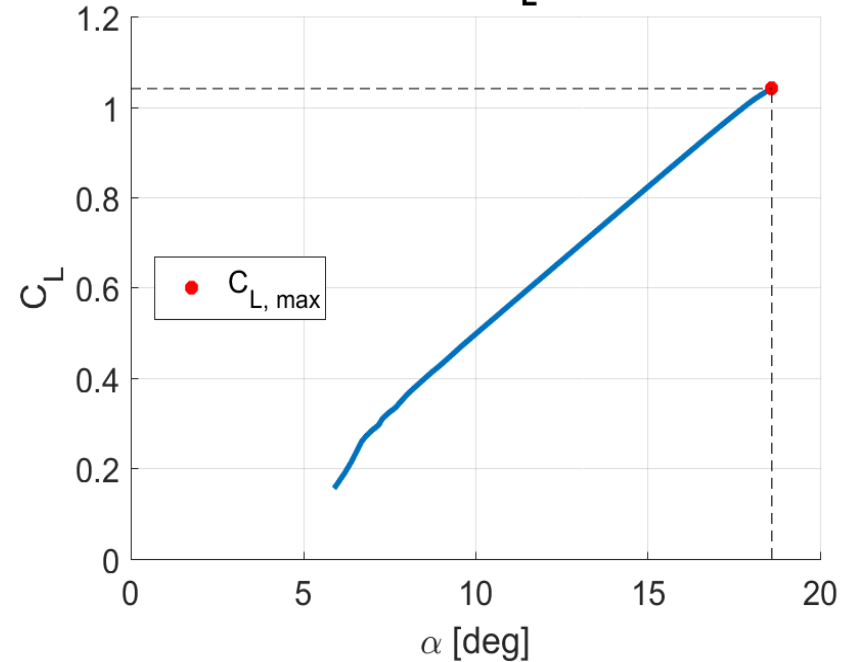
# Wing Design: $C_L$ - Extra



ARES  $C_L$  vs.  $\alpha$

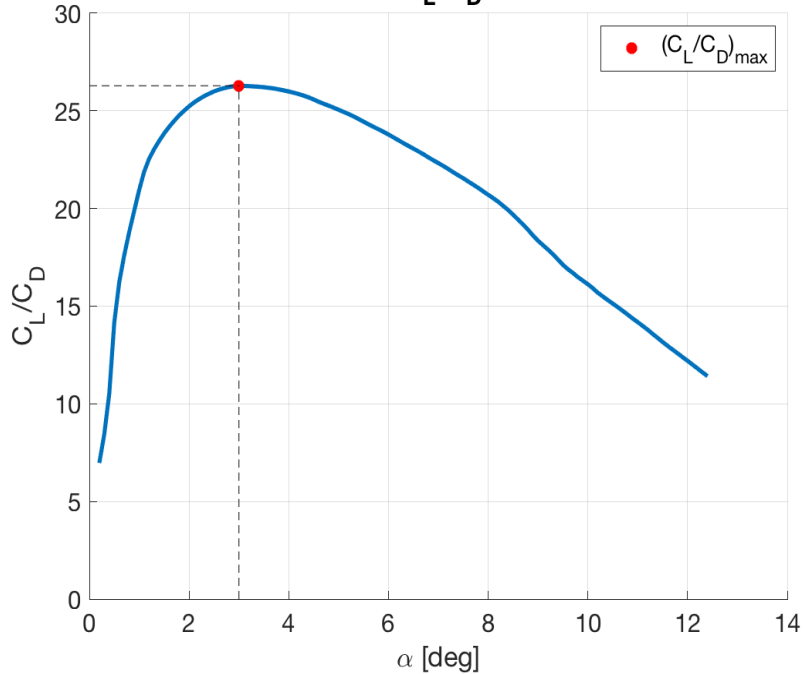


Eagle Owl  $C_L$  vs.  $\alpha$

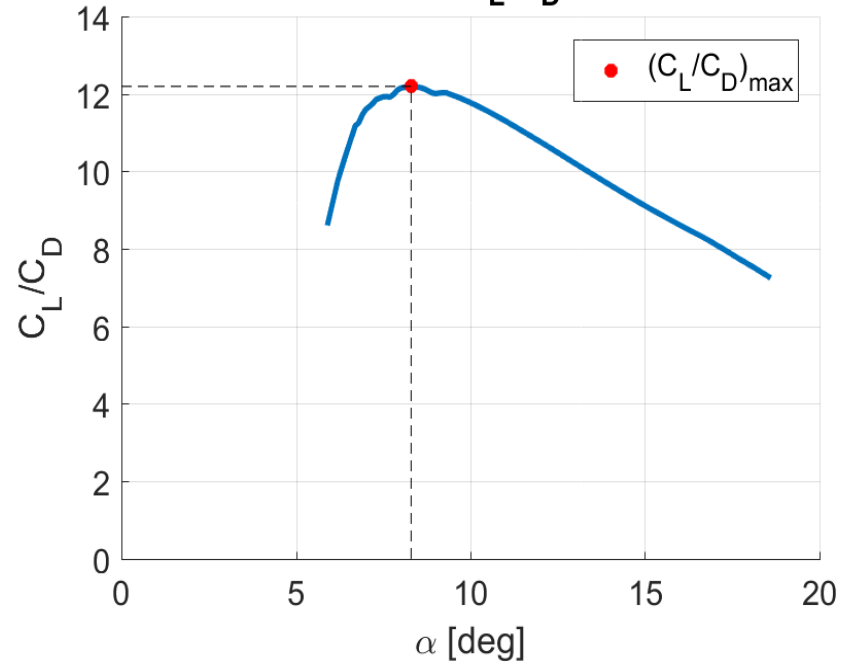


# Wing Design: $C_L/C_D$ - Extra

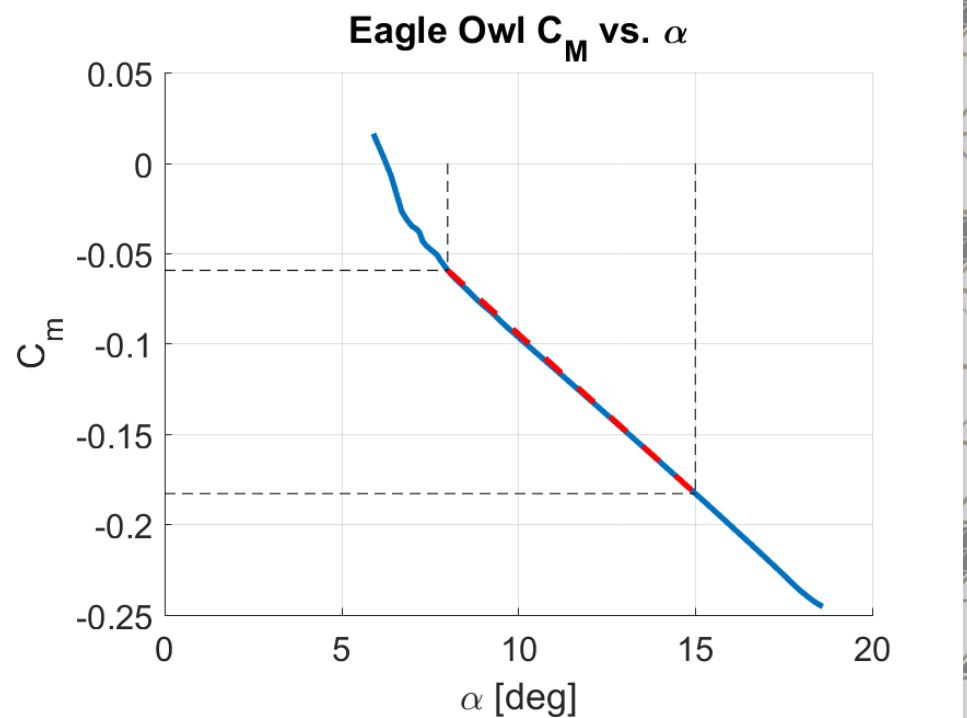
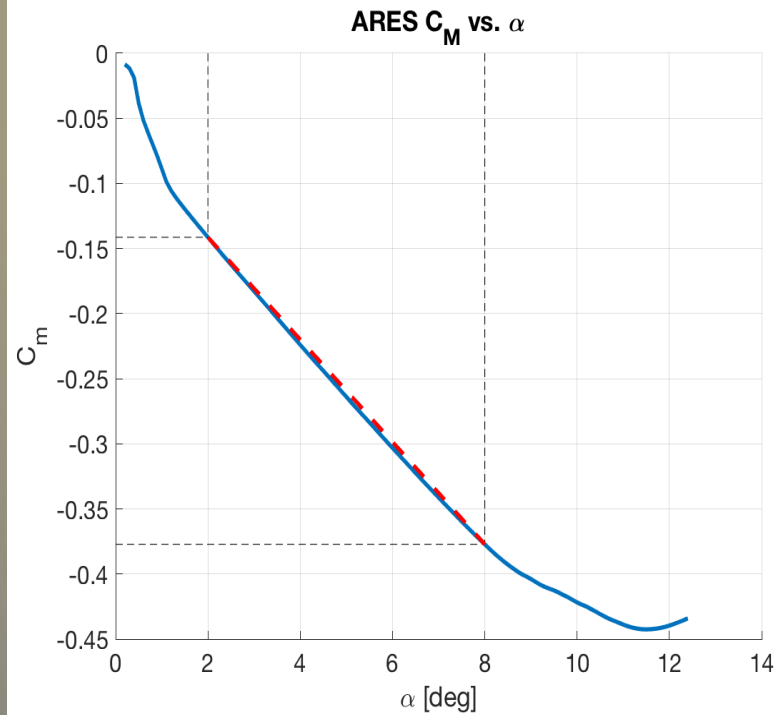
ARES  $C_L/C_D$  vs.  $\alpha$



Eagle Owl  $C_L/C_D$  vs.  $\alpha$



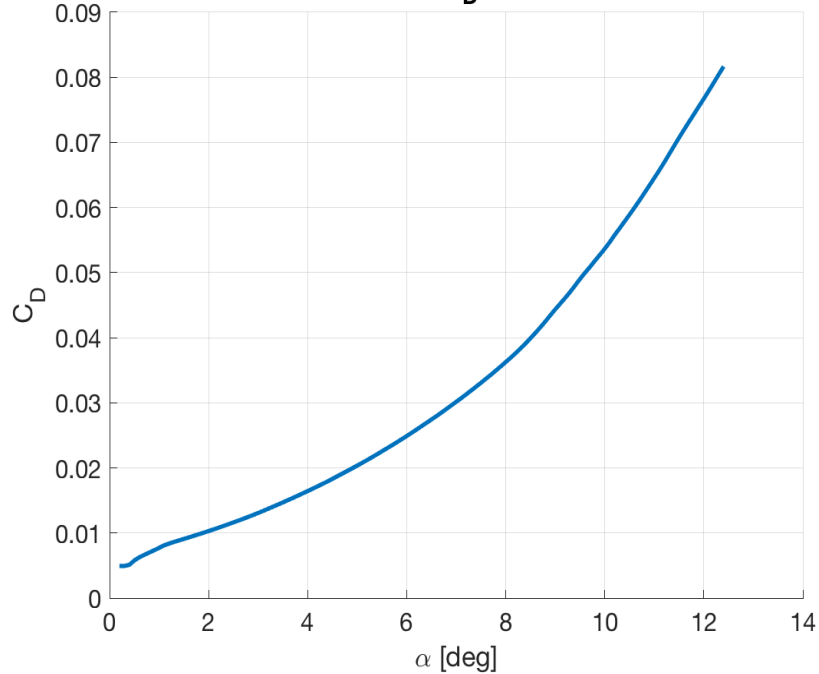
# Wing Design: $C_M$ - Extra



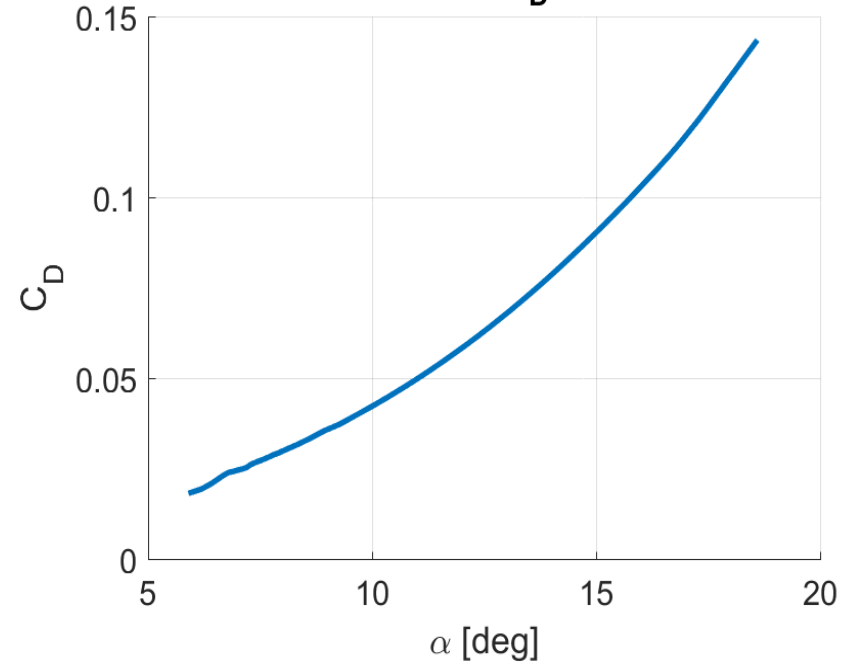
# Wing Design: $C_D$ - Extra



ARES  $C_D$  vs.  $\alpha$

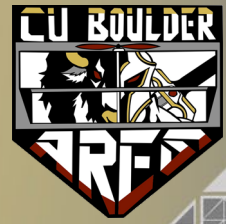


Eagle Owl  $C_D$  vs.  $\alpha$





# Wing Design - Extra



Yaw Stiffness Equation:

$$C_{n_\beta} = 2V_V a_F \left( \frac{V_F}{V} \right)^2 \left( 1 - \frac{\partial \sigma}{\partial \beta} \right)$$

Sidewash derivative approximation:

$$\frac{\partial \sigma}{\partial \beta} = -0.276 + 3.06 \frac{S_F}{S} \frac{1}{1 + \cos(\Lambda_{c/4})} + 0.4 \frac{Z_W}{d} + 0.009 AR$$

## Performance Plot Equations

- Maximum wing loading for given stall velocity:

$$\frac{W}{S} = \frac{\rho V_{stall}^2 C_{L_{max}}}{2}$$

- Maneuvering Constraint Equation:

$$\frac{P}{W_{maneu}} = \left[ \frac{1}{2} \rho V_c^2 \frac{C_{D0}}{W/S} + \frac{1}{\pi A R e} \left( \frac{n^2}{1/2 \rho V_c^2} W/S \right) \right] V_{cruise}$$

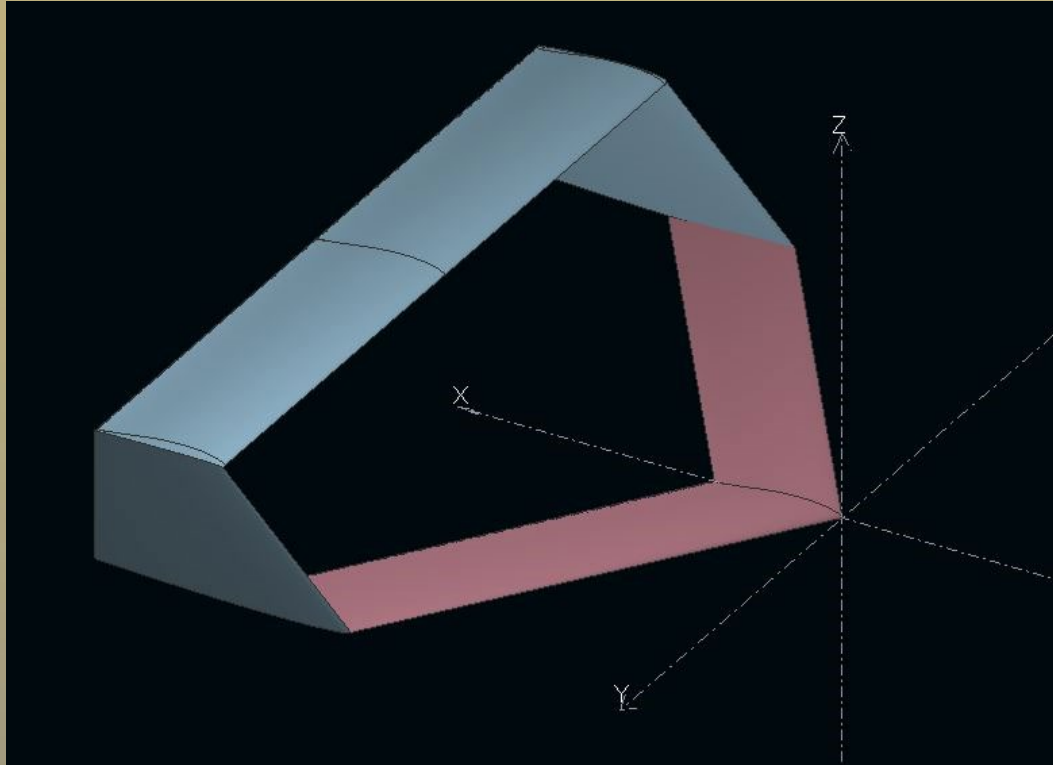
where  $n = G$  load factor



# Wing Design - Extra



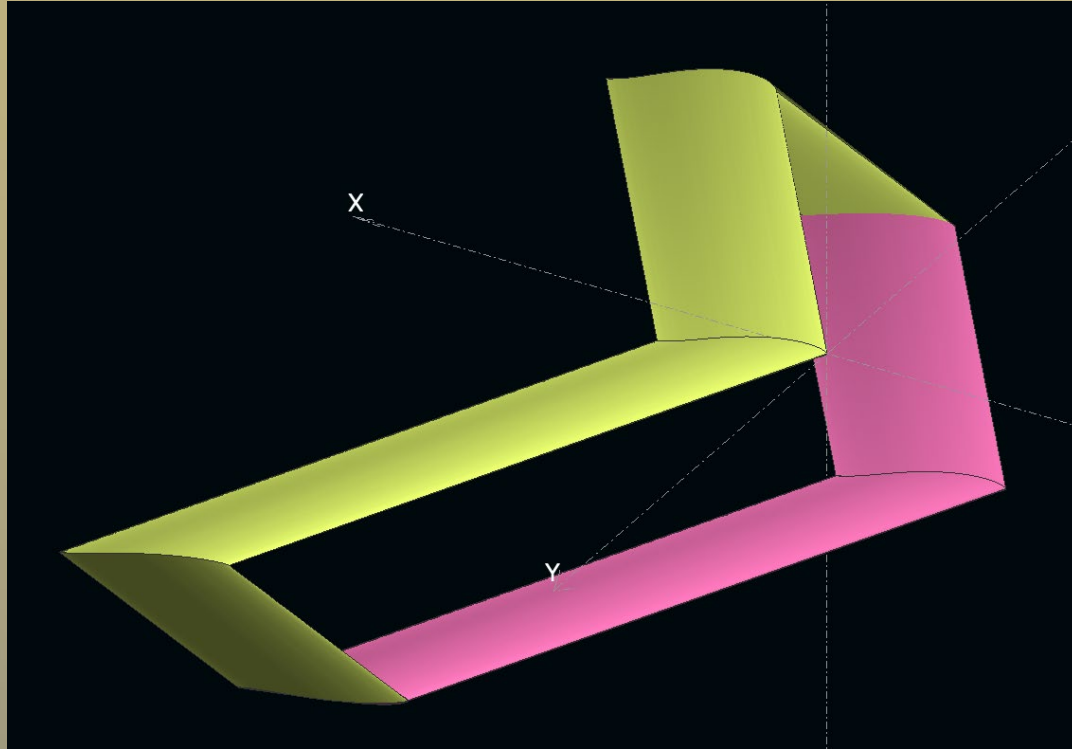
Rectangular  
top, swept  
bottom  
(RTSB)



# Wing Design - Extra



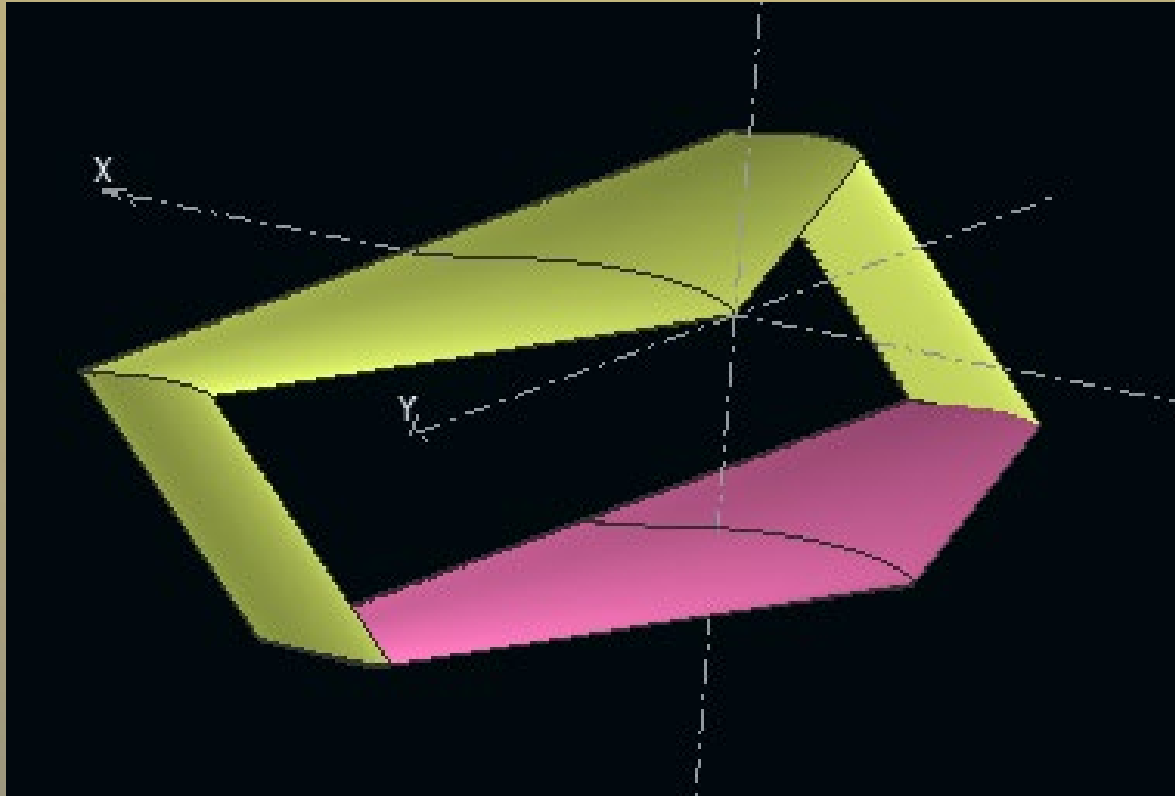
Swept wing



# Wing Design - Extra



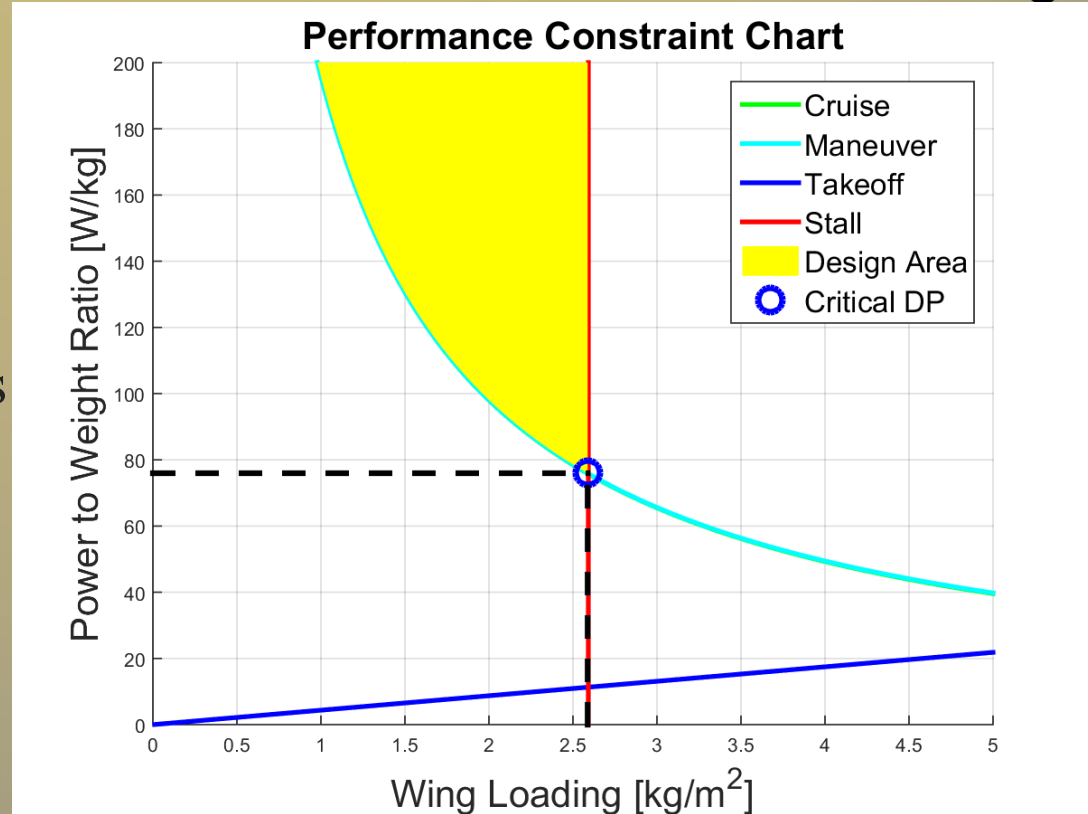
Pentagonal  
Wing

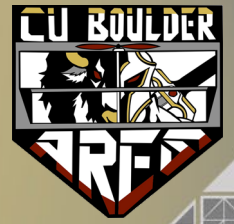


# Performance Constraint Analysis

## Input:

- Airfoil: MH-61
- $C_{L, \text{cruise}} = 0.35$
- $C_{L, \text{max}} = 0.728$
- $V_{\text{cruise}} = 11.1 \text{ m/s}$
- $V_{\text{stall}} = 7.6 \text{ m/s}$





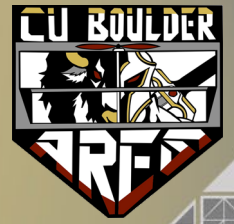
# Propulsion Backup Slides





# Propulsion - Table Explanation

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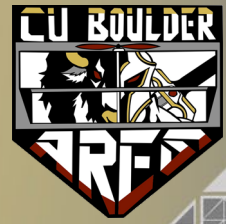


- Flight Speed:  $V_0 = 11.1 \text{ m/s}$
- Thrust:  $T = W(T/W)$
- Battery type determined by type of motor used and size of batteries:
  - Dictated by weight - want a lighter motor
  - Lighter motors have higher Kv - 4S and 3S allow for desired thrust when matched correctly
  - 3S and 4S batteries tend to be relatively small and easy to implement





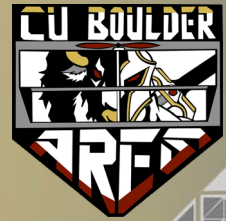
# Propulsion: T/W Justification



- T/W is qualitatively determined based on how you want your aircraft to behave:
  - High T/W (>0.45) - Higher ROC and maneuverability, more power draw
    - Fighter jet like characteristics
  - Low T/W (0.05-0.3) - Lower ROC and maneuverability, less power draw
    - Airliner or glider like characteristics
  - To minimize fuel consumption and based on low maneuverability missions, we want our aircraft to behave like a glider (T/W<0.55)<sup>1</sup>
    - Chose range based on heritage:
      - Eagle Owl - T/W = 0.1\*<sup>2</sup>
      - Twister = 0.35, Mistral T/W = 0.4\*<sup>3</sup>
    - Eagle Owl did not fly well enough, Twister/Mistral reportedly had too much T/W (in the works to lower) - we compromised: 0.22-0.3
      - Will decide exact value for CDR using heavier analysis

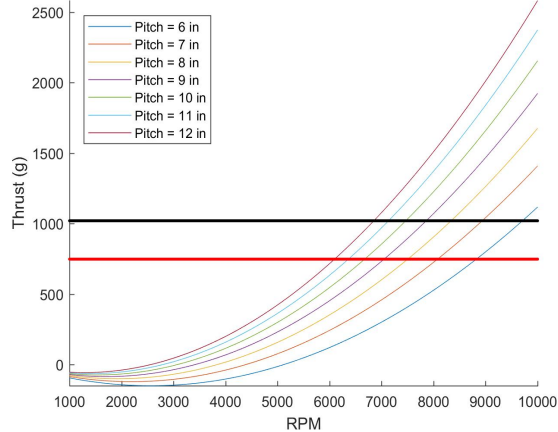
Type of airplane	thrust-to-weight ratio	
Glider /trainer	0.35 to 0.55	
Scale Flight	0.60 to 0.70	
Sport and slow acrobatic	0.70 to 0.80	
Acrobatic fast	0.80 to 1.00	
Jets and 3D	1.00 to 2.5	

# Propulsion: Kv Justification - Extra

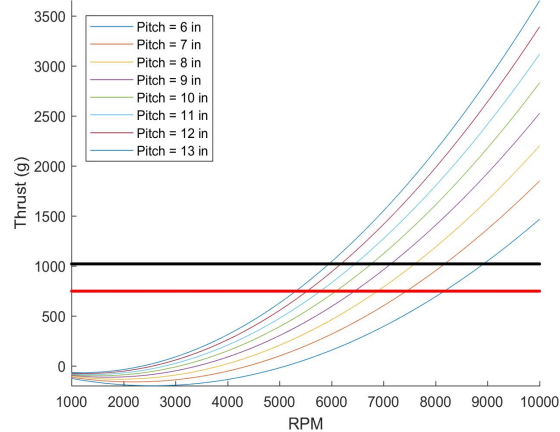


- $K_v$  is dependent on what RPM we want
  - Correlate RPM to thrust (from T/W)
  - Approximate prop size to get range - use design constraints
  - Decide on an RPM based on mission - i.e. aircraft speed
- Once RPM is determined, choose  $K_v$  based on desired output voltage
  - $K_v = \text{RPM}/V$

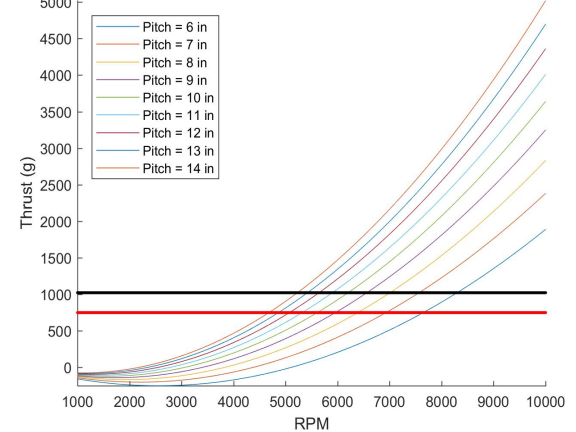
Thrust vs. RPM for Different Propellers at  $V_0 = 13 \text{ m/s}$  and Diameter = 12 in



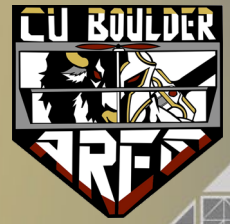
Thrust vs. RPM for Different Propellers at  $V_0 = 13 \text{ m/s}$  and Diameter = 13 in



Thrust vs. RPM for Different Propellers at  $V_0 = 13 \text{ m/s}$  and Diameter = 14 in



# Propulsion



- Battery: 10000-16000 mAh (3-5S=11.1-18.5V)
  - ECalc\* illustrates capability of each of these batteries providing cruise thrust to the motor for 90-120+ minutes
  - Depending on motor and propeller choice, cell requirements and battery capacity will vary
- Speed Controller (ESC): Castle Phoenix Edge Lite 40-100 A
  - The Speed Controller is dependent upon the max amperage draw by the motor
  - Castle is considered an exceptional brand for ESC
- Propeller: Diameter 11-16 in. x Pitch 7-16 in.
  - Propeller will be designed to provide enough thrust at cruise of 13 m/s
  - Dimensions dependent upon final motor choice
  - Foldable prop. due to reduction of damage risk associated with impacts
    - 355kv - 14x9
    - 410kv - 13x8

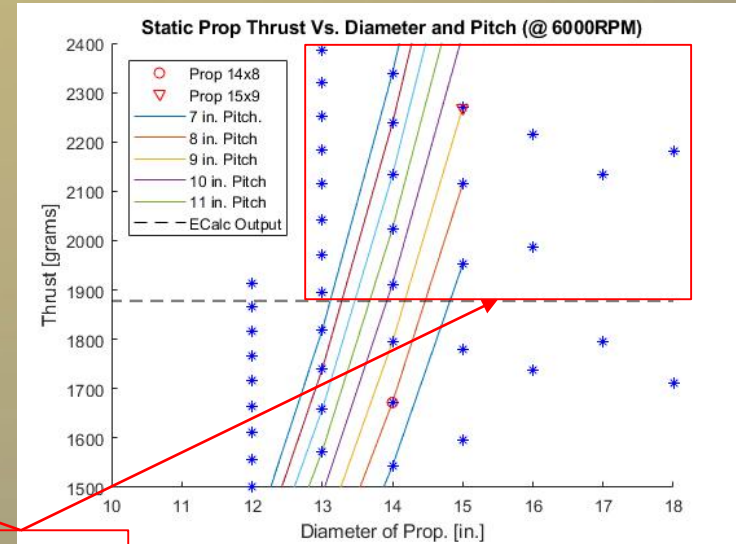
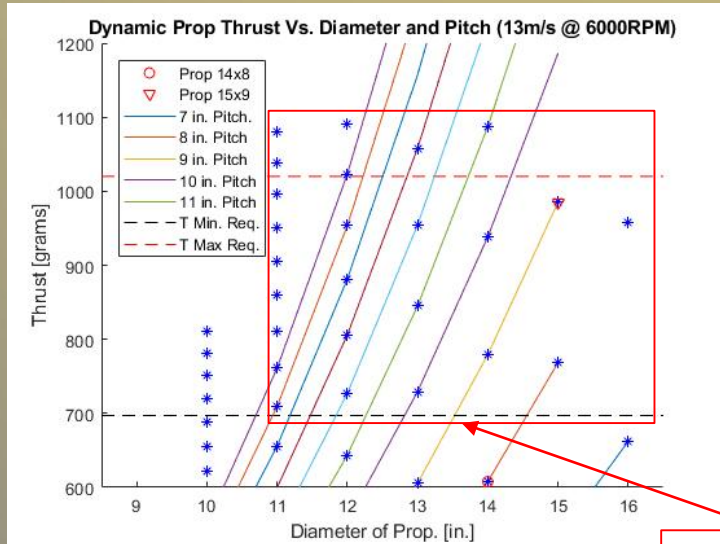


# Propulsion - Propeller Size

- Possible Propellor Combinations

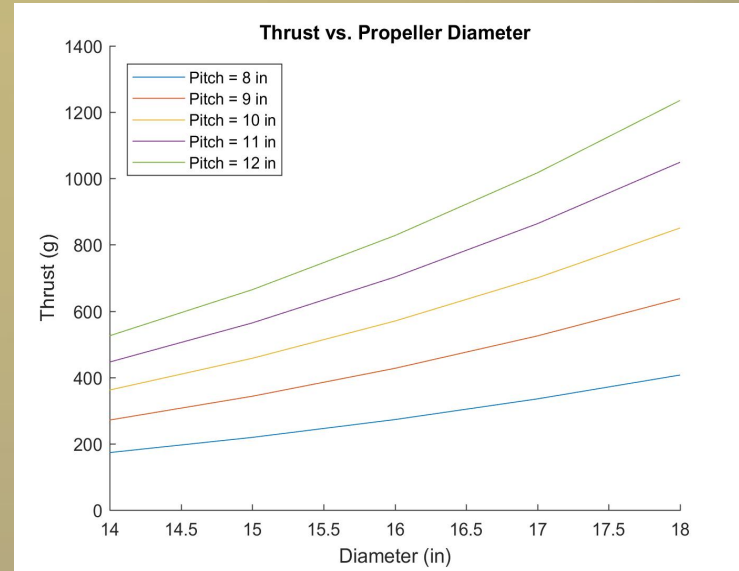
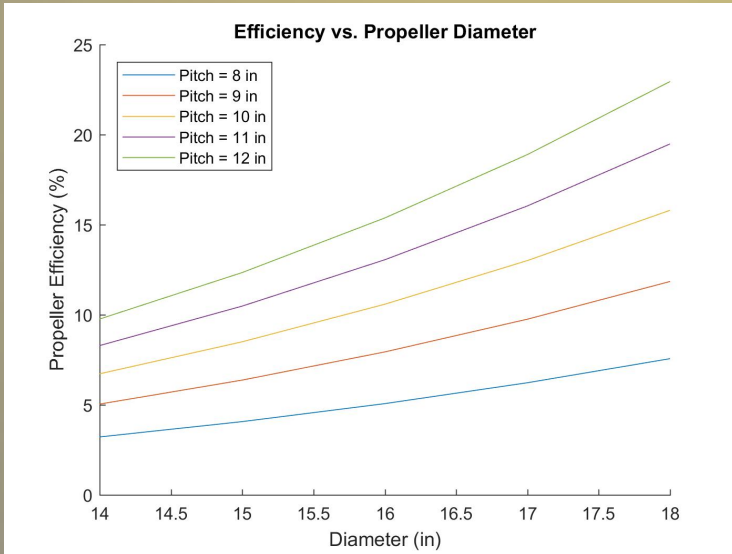
$$F = \rho \left( \frac{\pi(0.0254 \cdot d)^2}{4} \right) \left[ (RPM \cdot 0.0254 \cdot pitch \cdot \frac{1min}{60sec})^2 - (RPM \cdot 0.0254 \cdot pitch \cdot \frac{1min}{60sec}) V_0 \right] \left( \frac{d}{3.29546 \cdot pitch} \right)^{1.4}$$

- Tmin = 680.4 g
- Tmax = 850.5 g



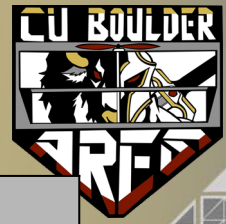
Design Space

# Propulsion: Propeller Size





# Propulsion: ECalc Outputs - Extra



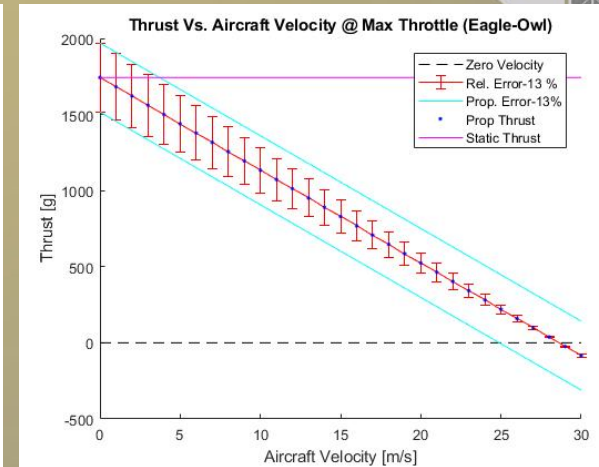
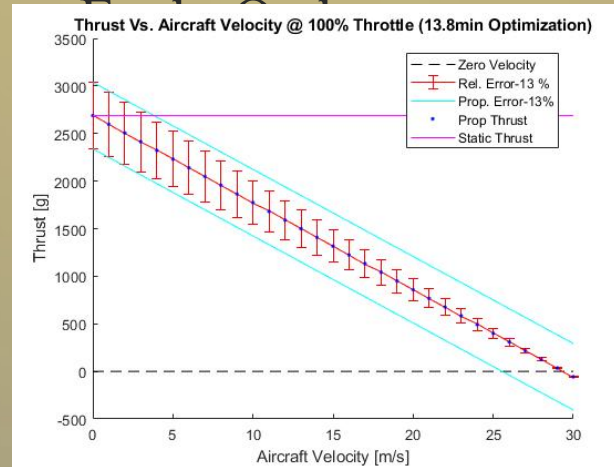
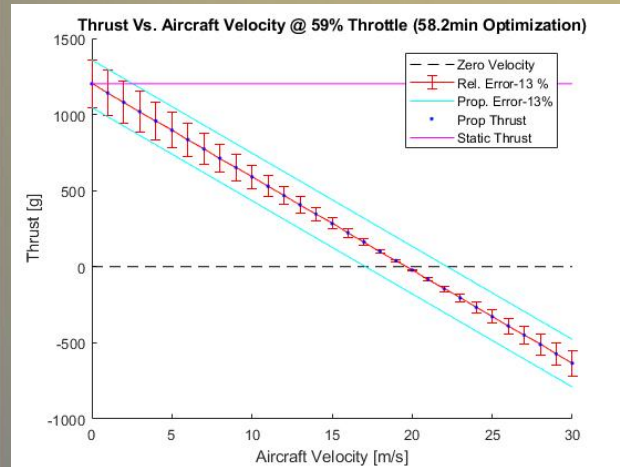
Motor	Kv [RPM/V]	Propellor [in]	Battery [mAh]	RPM	Avail. Thrust at 11m/s [g]	Flight Time at 13m/s [min]
Hacker A-40 12L	410	15x10	10,000 (4S)	4000	1270 (550)	53.2
Hacker A-40 12L	410	15x10	12,000 (4S)	4000	1270 (550)	63.8
Hacker A-40 12L	410	15x10	14,000 (4S)	4000	1270 (550)	74.5
Hacker A-40 14L	355	14x9	10,000 (4S)	3900	1189 (469)	50.6
Hacker A-40 14L	355	14x9	12,000 (4S)	4000	1189 (469)	60.8
Hacker A-40 14L	355	14x9	14,000 (4S)	4000	1189 (469)	71.0
<u>Hacker A-30 12XL</u>	<u>700</u>	<u>13x8</u>	<u>5x2,500 (4S)</u>	<u>5400</u>	<u>1205 (528)</u>	<u>58.2</u>

Main Takeaway: Best motors at  $Kv > 700$  and 4S

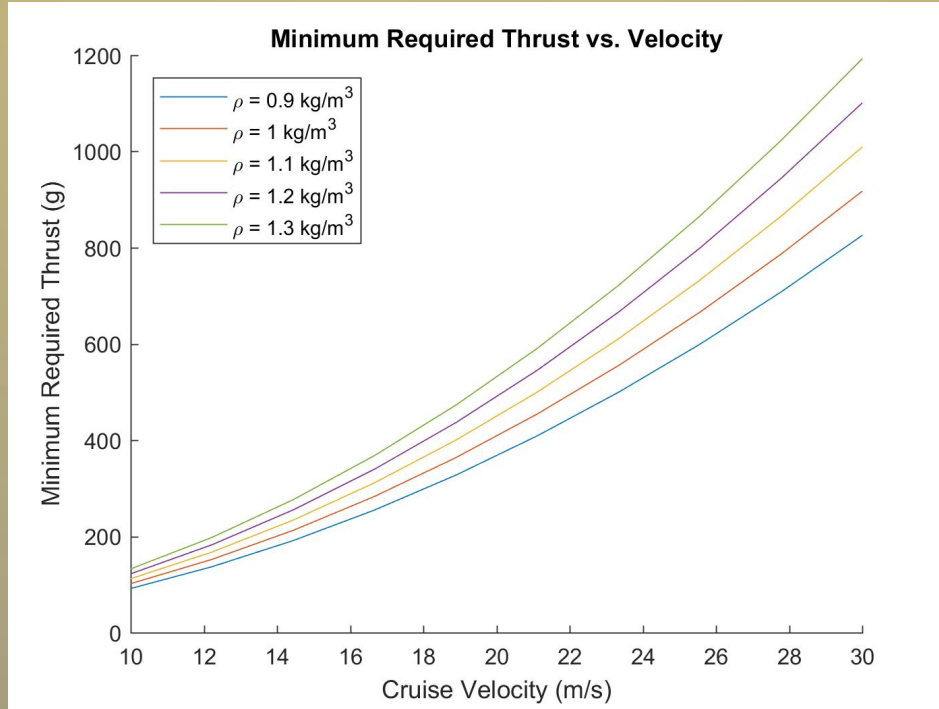
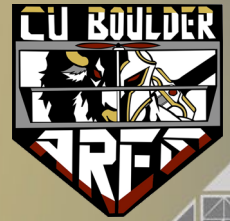
## Dynamic and Static Thrust Vs Airspeed

ARES

ARES



# Propulsion: T vs V - Extra





# Propulsion - Power Budgeting



- Using  $T/W = 0.2-0.25$ , the following parameters could be determined:
  - Range Minimum max thrust -  $T_{\max} = 0.2 * 120 \text{ oz} = 24 \text{ oz} = 680.4\text{g} = 1.5 \text{ lbs}$
  - Range Maximum\* max thrust -  $T_{\max} = 0.25 * 120 \text{ oz} = 30 \text{ oz} = 850.5\text{g} = 1.88 \text{ lbs}$
  - Maximum  $P_r > 255 \text{ W}$  (Upper weight limit = 8.5 lbs)
    - General rule of thumb is 50 W/lb to fly<sup>1</sup>
    - Weight limit decided as team - governed by wing design

## Motor:

- T/W range of 0.20-0.25\*
  - Minimum T/W  $\sim 0.05^1$  (want to fly at 4-5 times that)
    - Computed from  $(L/D)^{-1}_{\max} = (T/W)_{\min}$
  - T/W generally determines the performance of the the aircraft
    - Based on CONOPS: need slow maneuvering, efficient design - low T/W
    - Could define range based on heritage (Eagle Owl, Mistral, Twister) and how those craft performed
    - Shimming negates motor torque on airframe
    - Kv (RPM/V) range of 500-1000
      - Low Kv (100 - 500) = high torque, low RPM\*\*
        - Heavy - requires more coils for more torque
      - High Kv (>1500) = low torque, high RPM\*\*
        - Lighter - Doesn't need as many coils
    - Mission calls for lightweight motor with low power consumption

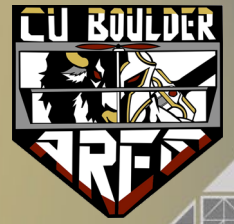


\*from RCGroups.com 1 Mistral plane uses this

\*from [HobbyWarehouse.com](http://HobbyWarehouse.com)



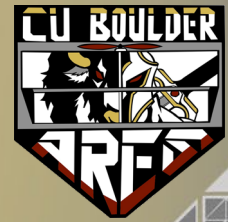
# Propulsion: Motor Selection - Extra



1. Characterize your aircraft:
  - a. Heavy, slow - Low Kv, big prop
  - b. Light, fast - High Kv, small prop
2. Determine  $(T/W)_{\min}$  based on design  $(L/D)_{\max}$
3. Determine functional T/W range using:
  - a.  $(T/W)_{\text{Lower}} = 4(T/W)_{\min}$
  - b.  $(T/W)_{\text{Upper}} = 5(T/W)_{\min}$
4. Decide if we want a fast or a slow plane to choose Kv (RPM/V) Value:
  - a. Higher Kv = Low torque, high speed - Lighter loads at higher speeds; smaller props
  - b. Lower Kv = High torque, low speed - Heavier loads at slower speed; larger props
5. Use mathematical models with CONOPS/aircraft parameters in mind to identify propeller size range
  - a. Matlab function: TvRPMplotter
  - b. Verify with resources like eCalc and MotoCalc
6. Find motor current with  $I = TV_0/V_{\text{battery}}$ 
  - a. Use this to calculate power demand
7. Use current to find speed controller



# Propulsion - Extra



Trade study of pusher vs puller

Metric Characteristics		Configuration					
		Pusher		Puller/Tractor		Push/Pull	
Metric	Metric Weight	Score	Value	Score	Value	Score	Value
Weight	25%	3.5	0.875	4	1	2.5	0.625
Cost	15%	5	0.75	5	0.75	3	0.45
Prop/Motor Protection	20%	3	0.6	3	0.6	3	0.6
Flight Heritage	15%	5	0.75	1	0.15	1	0.15
Motor Efficiency	25%	3	0.75	5	1.25	1	0.25
<b>TOTAL</b>	<b>100%</b>		<b>3.725</b>		<b>3.75</b>		<b>2.075</b>

# Propulsion: 2hr Time - Extra



## WebOCalc Example

### Webocalc 1.7.6 - Imperial Units

*Airframe Details*

All Up Weight (oz)

Number Of Wings

Wingspan (in)

Total Wing Area (sq in)

Number of Propellers

Maximum Prop. Size (inches)  [Run Prop Size Wizard](#)

*Performance Details*

Flight Mission

Desired Top Speed (mph)  [Suggest Top Speed](#)

Desired Thrust (oz)  [Suggest Thrust](#)

Desired Flight Duration (minutes)  [Get More Information](#)

*Powertrain Details*

Motor Efficiency (%)

Select battery chemistry & cell count below  Or  [Run Battery Wizard](#)

Battery Voltage (V)

Desired current per motor (A)

Motor Kv (rpm/volt)  [Run Kv Wizard](#)

### Estimated Model Performance

*WebOCalc Results:*

Flies Like: Indoor flyer.

Power Level: Medium/Mild aerobatics.  
*(with white highlighted prop)* 40 degree climbouts.

Minimum Pilot Skill Needed: Easy Beginner level.

Minimum Flying Field Size: 710 x 510 feet.

Minimum Battery Size: 6S, 15000 mAh, 1 C, lithium polymer.

**Estimated Flight Duration: 120 to 200 minutes depending on pilot. Will vary with throttle usage.**

Suggested ESC Rating: 15 A to 17 A.

Power Into / Out of Motor: 243.0 watts in / 194.4 watts out.

Power To Weight Ratio: 43.20 watts/pound.

Estimated Stall Speed: 14.2 mph.

Wing Loading: 8.36 oz/square foot.

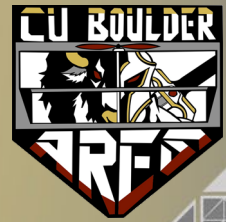
Cubic Wing Loading: 2.62 oz/cubic foot.

**Suggested Prop Sizes (approx):**  
For direct-drive, use props with gear ratio 1.00.  
Adjust current and/or pitch speed if necessary to obtain this ratio.

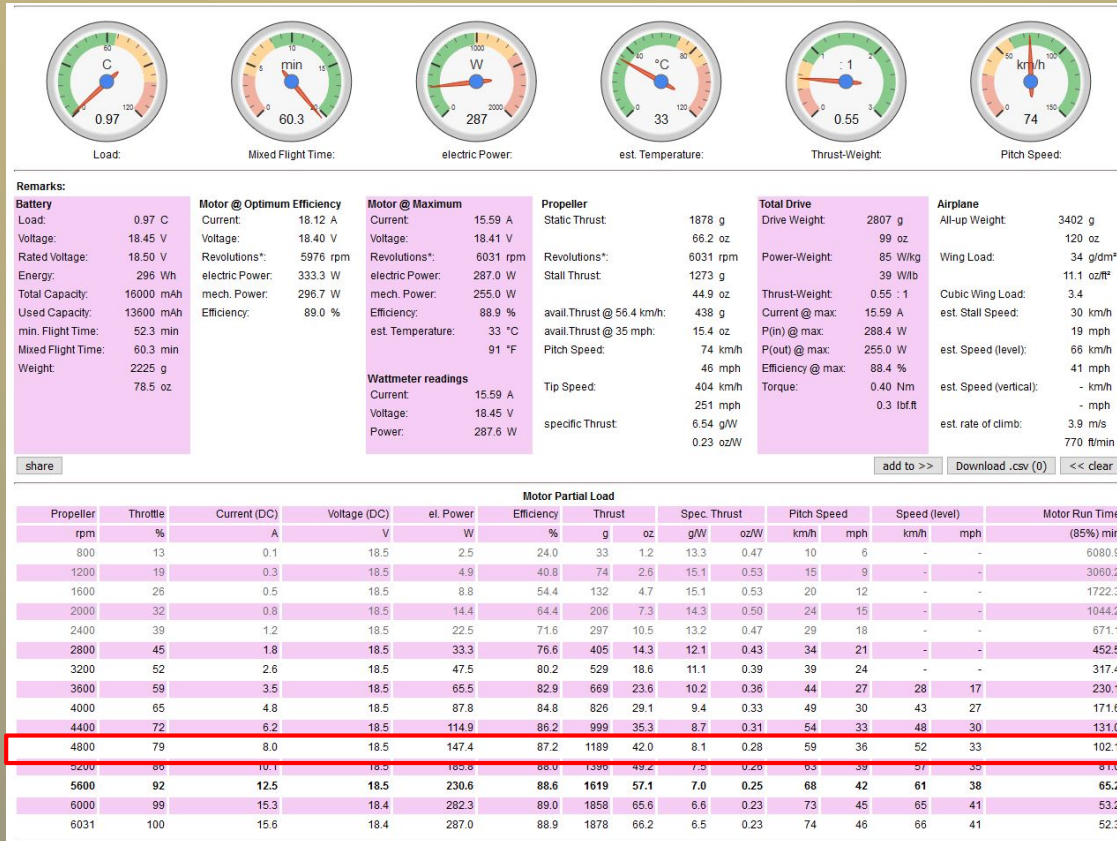
White: propeller with most thrust.  
Yellow: best choice for direct-drive.

Prop Type	Dia (in)	Pitch (in)	RPM	Vpitch (mph)	Thrust (Oz)	Thrust Change	Approx Gear ratio
APC-TE	18.0	10.0	3437	32.7	56.4	-10.0	0.85
APC-TE	18.0	12.0	3235	37.0	60.0	-6.5	0.91
APC-TE	19.0	12.0	3010	34.4	61.0	-5.4	0.98
APC-TE	20.0	12.0	2811	32.1	62.1	-4.3	1.05
APC-TE	20.0	13.0	2737	33.9	63.8	-2.7	1.07
APC-TE	20.0	15.0	2609	37.3	59.8	-6.7	1.13
APC-TE	21.0	13.0	2564	31.7	64.8	-1.6	1.15
APC-TE	21.0	14.0	2502	33.4	66.4	0.0	1.17

# Propulsion: ECalc Results - Extra



## Sample Ecalc Output





# Propulsion: Calculations - Extra

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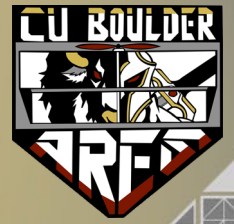


$$P_r = W(T/W)(0.00017K_v + 0.09)$$

$$T_{\min, \text{steady}} = 0.5\rho V^2 C_d S = W / (L/D)_{\max}$$

- For required thrust,  $C_d = 0.02$  from wing design data



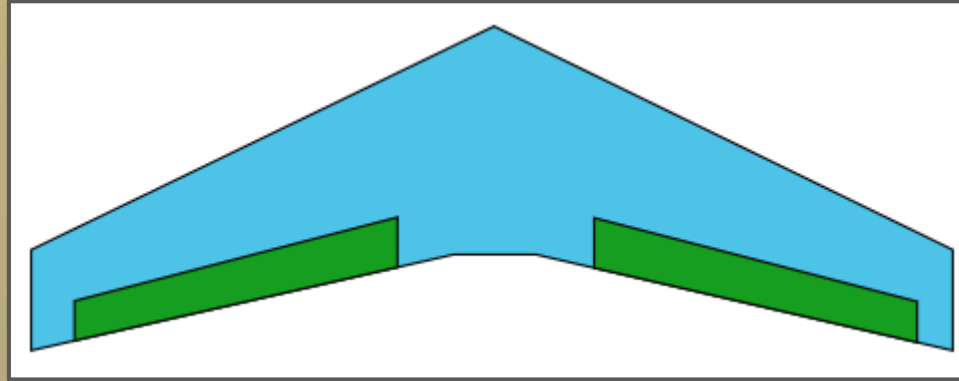


# Autopilot Backup Slides





# Control Surfaces



- Aircraft will use elevons as control surfaces
- Flight heritage and resources on controlling flying wings with elevons
- Elevons on the top wing (farther from c.g.) = larger moment.
- Control surfaces moved physically using servo (same as Eagle Owl and SCUA)
- Most flying wings are swept for yaw stiffness
  - if additional stability is necessary, static or controlled split rudders can be installed on the sides.



# Autopilot



FR 4.0: The aircraft shall be piloted by an autopilot during the steady flight regime of the mission

- Flight Heritage
- Open-source software with custom airframe support
- Power
  - Accepts 4.9-5.5 V input power
  - Servo rail input: 0-36 V
  - Power management board included
  - Need 5V BEC (6.2 g) to power servos
- Weight: 15.8 g
- Size: 44x84x12 mm



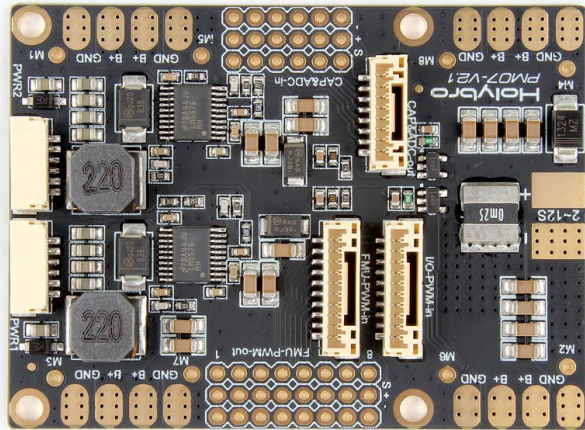
# Autopilot

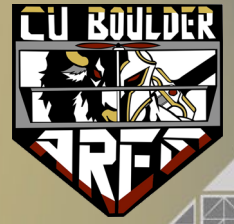


- Built-in Sensors
  - Accelerometers/Gyros (ICM-20689 & BMI055)
  - Magnetometers (IST8310)
  - Barometer (MS5611)
  - GPS (ublox Neo-M8N)
- External Sensor
  - Airspeed sensor to detect stall
- Speed controller between Pixhawk and propeller motor
- Handles RC input with external receiver
- Downlinks data to ground station receiver
- Control templates for flying wings with elevons
- SD Card slot to store data



# Autopilot: Pixhawk Connections

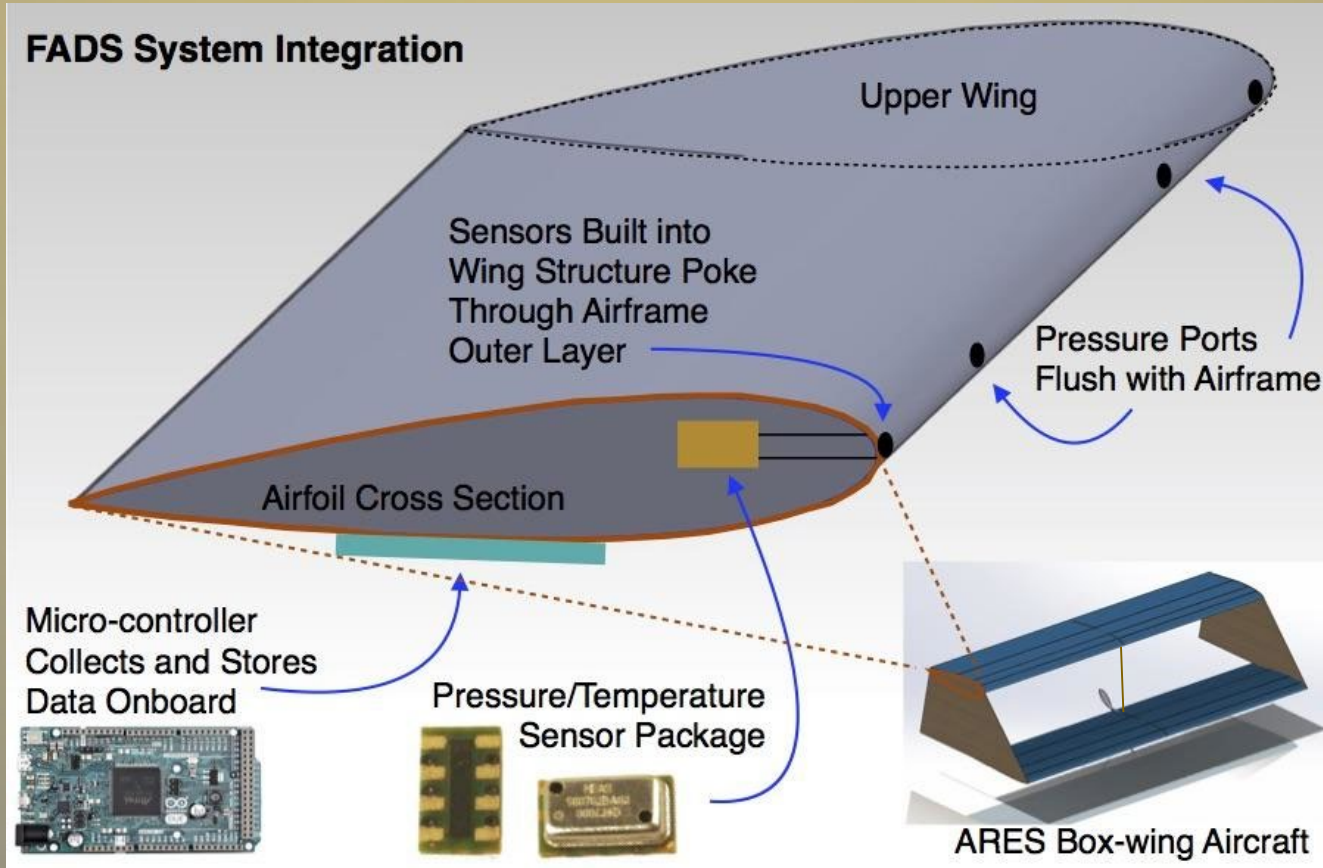




# Science Backup Slides



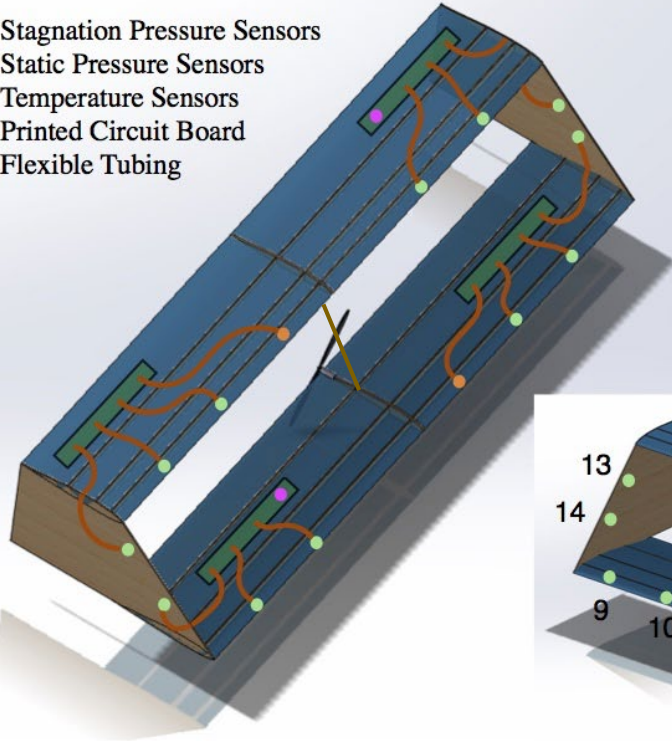
# Science Baseline Design



# Science: Sensor Locations

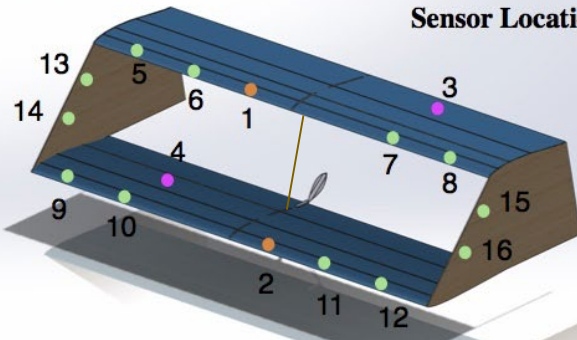
## Board Locations with Sensor Connections:

- Stagnation Pressure Sensors
- Static Pressure Sensors
- Temperature Sensors
- Printed Circuit Board
- Flexible Tubing

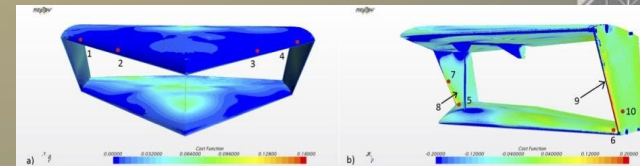


- Located on the leading edge of the wings and sidewalls
- Embedded in the structure so that the sensor is flush with the airframe
- Ideally where pressure changes the most
- 2 stagnation ports at center and 14 static ports along wings

## Sensor Locations:



Optimal Locations from Wind Tunnel Testing the Eagle Owl





# Science: Calibration - Extra



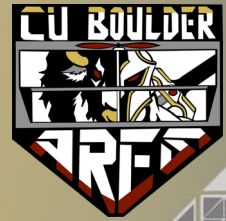
## Calibration Techniques for Finding “True” Values:

- Multi-hole Probe
  - Compare calculated angle of attack and sideslip with multi-hole probe measured angle of attack and sideslip.
  - Cons: \$12,000 piece of equipment, extremely breakable
- Pitot Probe
  - Compare FADS measured pressure with pitot probe measured pressure.
  - Cons: can only compare pressures, extremely breakable
- Computational Fluid Dynamics Analysis
  - Set angle of attack and sideslip in simulation in order to calculate an expected pressure that FADS system should see. Compare to measured results.
  - Cons: need accurate model of pressure sensor locations





# Science: Microcontroller



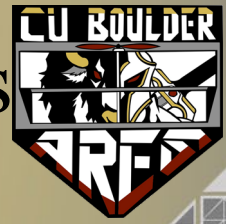
- Design specifications:
  - Memory: 1.5 Mb (factor of safety of 2)
  - Pins: 16 digital I/O pins
    - 16 pressure/temperature transducers
  - Input voltage: 7.4 V
    - 2S LiPo battery for power
  - Processing speed:
    - 48 Kb a second is not a concern
- Feasibility
  - A microcontroller following specifications can be purchased online
  - Mass and power does not exceed expectations
  - Memory can be achieved through MicroSD shield
  - Integration is shown in the power system section





# Science: Microcontroller Calculations

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- Storage
  - Pressure and temperature bits  $(48) * 16 \text{ sensors} * 3600 \text{ s} * 2 \text{ hrs} / 8$  bits per byte
- Pins
  - 16 pins are required as 16 pressure/temperature sensors will be used on the aircraft. Pressure and temperature are given as 24 bit digital.
- Voltage
  - Defined by the power management board of the Pixhawk 4
- Processing Speed: ????



From CU FADS expert, Roger Laurence on his dissertation work with the Skywalker.

Holes can be drilled in wing material to ensure tubing is flush with leading edge



Paths can be carved in wing material to fit flexible tubing

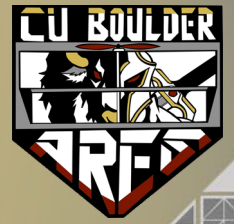
# Science: Logistics



Component	Cost (\$)	Mass (g)	Power (Wh)
Sensor Boards	300	20	.0042
Microcontroller	20-50	10-50	0.15 - 0.35
Housing (tube, acrylic, brass)	40	20	0

Scheduling: All parts can be ordered online with normal shipping times. The manufacturing is expected to take 1 week once the aircraft structure is complete. The calibration simulation is expected to take 2 weeks and can begin as soon as an accurate CAD model of the aircraft exists. Calibration testing and comparison is expected to take 1 week once the FADS is integrated.





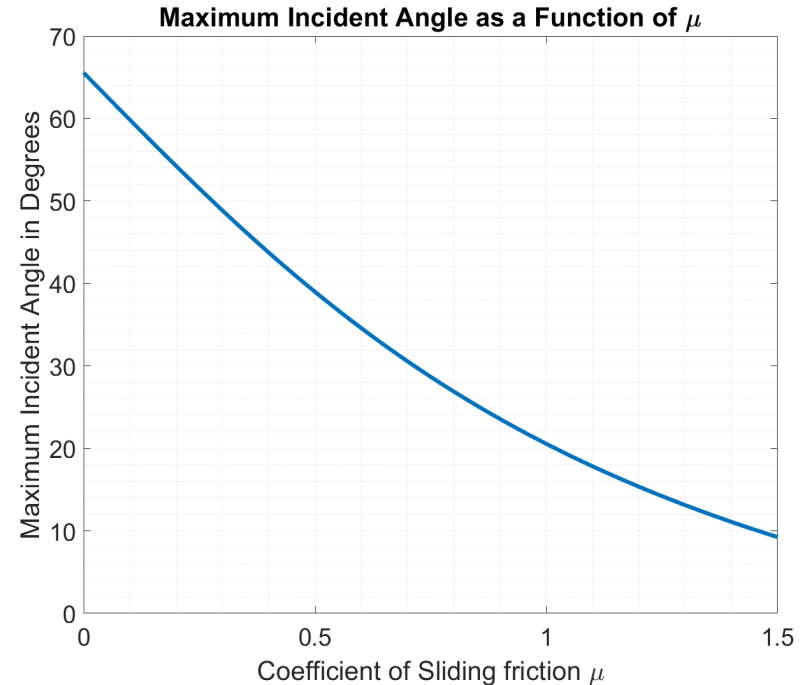
# Landing Backup Slides



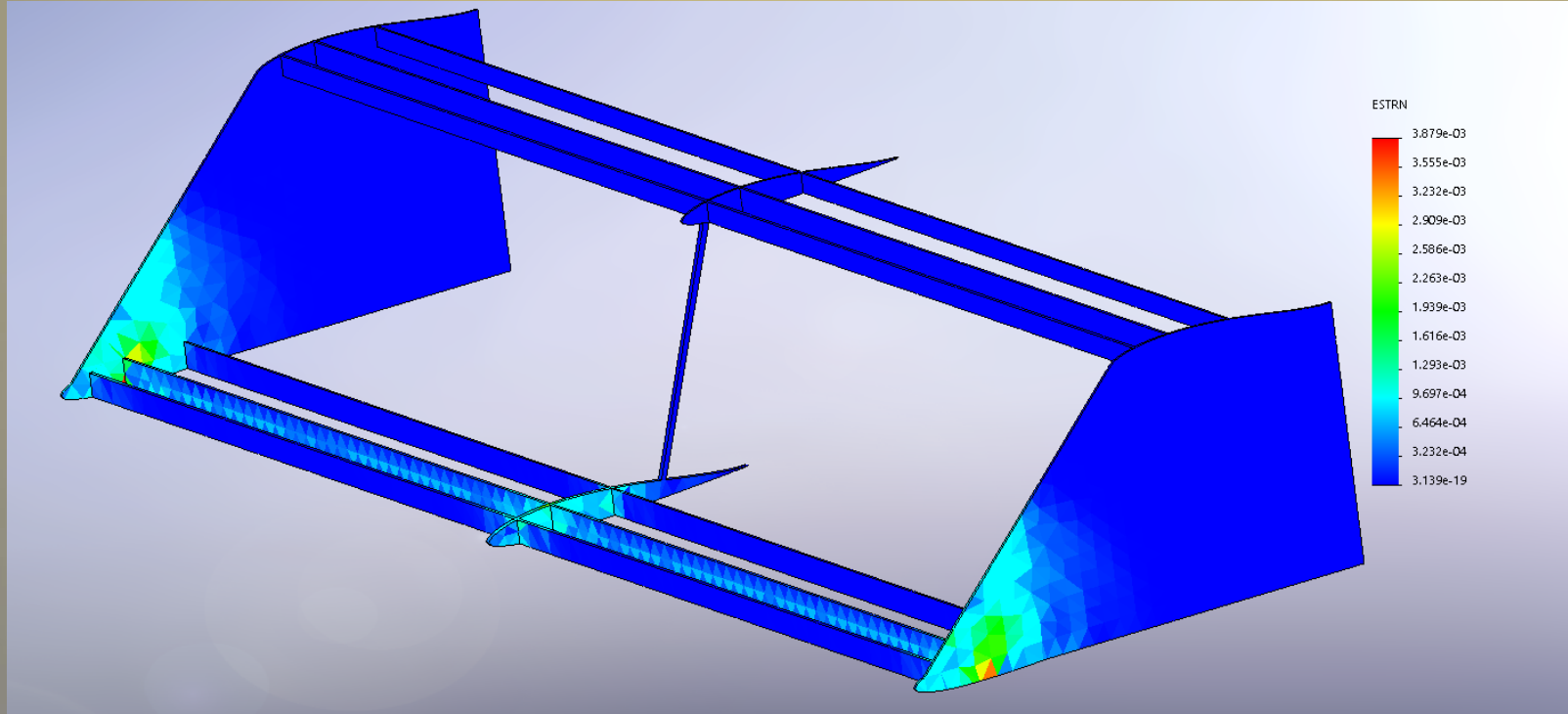
# Landing Feasibility: Sliding



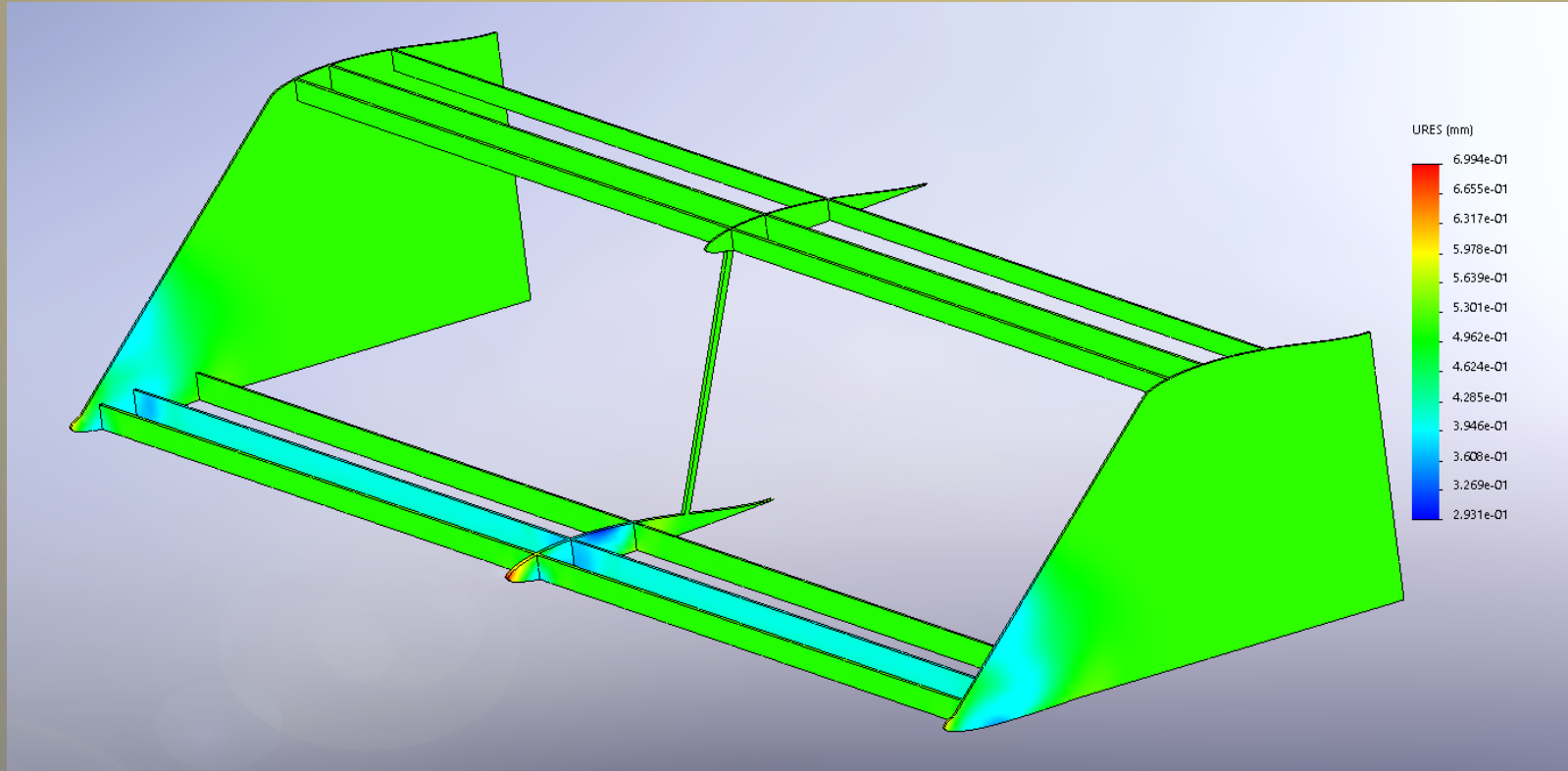
$$\begin{aligned}
 x &= -.1 * \sin(\alpha) + .22 * \cos(\alpha) \\
 y &= .22 * \sin(\alpha) + .1 * \cos(\alpha) \\
 0 &\leq \sum M_{cg} = x * N - y * \mu * N \\
 0 &\leq N * ((.22 * \cos(\alpha) - .1 * \sin(\alpha)) - \mu * (.22 * \sin(\alpha) + .1 * \cos(\alpha))) \\
 0 &\leq \cos(\alpha) * (.22 - .1 * \mu) + \sin(\alpha) * (-.1 - \mu * .22) \\
 \sin(\alpha) * (.1 + \mu * .22) &\leq \cos(\alpha) * (.22 - .1 * \mu) \\
 \tan(\alpha) &\leq \frac{.22 - .1 * \mu}{.1 + \mu * .22}
 \end{aligned}$$



# Landing Extra: Strain



# Landing Extra: Displacement



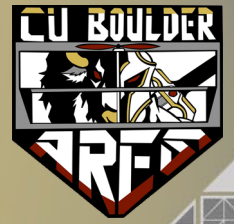




# Landing Extra: Displacement

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# Power Backup Slides

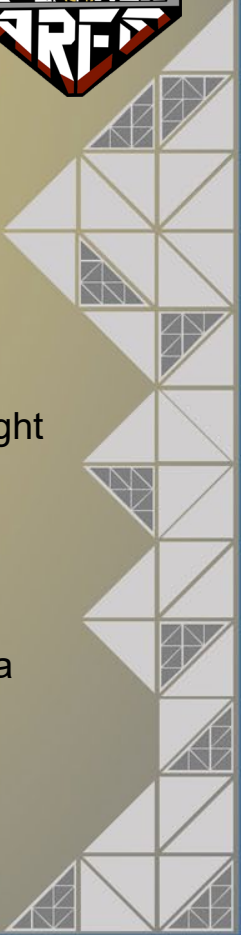


# Propulsion: power budgeting calc.



$$E = Rt^{1-n} \left[ \frac{\mu_{tot} VC}{\frac{1}{2} \rho U^3 SC_{D0} + \frac{2W^2 k}{\rho U S}} \right]^n$$

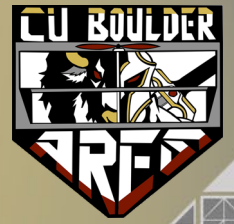
Endurance  $\rightarrow E$   
 Total efficiency  $\rightarrow \mu_{tot}$   
 Voltage  $\rightarrow V$   
 Capacity  $\rightarrow C$   
 Time for capacity  $\rightarrow t$   
 Air density  $\rightarrow \rho$   
 Flight velocity  $\rightarrow U$   
 Minimum Cl/Cd  $\rightarrow C_{D0}$   
 Weight  $\rightarrow W$   
 Wing area  $\rightarrow S$





# Propulsion: Power calculations cont.

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E: Dependent variable

$R_t = 1$  hour

U: Independent variable

$\mu_{Tot} = 0.5$

S:  $1.333 \text{ m}^2$   
(function of C)

Weight:  $1.6 + \text{battery}$

Rho:  $1.056 \text{ kg/m}^3$

$CD_0 = 0.015$

Voltage:  $11.1-14.8 \text{ V}$

$n = 1.3$  (for LiPo batteries)

Capacity: Independent variable  $k = .13$  (experimental)



# Power: Battery Types Trade Study

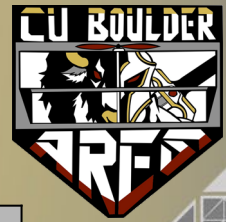


- Common RC batteries: Lithium Polymer (LiPo), Nickel Cadmium (NiCad), Nickel Metal Hydride (NiMH).

Battery	LiPo	NiCad	NiMH
<b>Pros</b>	<ul style="list-style-type: none"> <li>High discharge rate</li> <li>Highest power to weight ratio</li> <li>Highest capacity</li> </ul>	<ul style="list-style-type: none"> <li>Low self-discharge</li> <li>Low internal resistance (high current)</li> </ul>	<ul style="list-style-type: none"> <li>No voltage depression effect</li> <li>Long lifespan (1000 cycles)</li> </ul>
<b>Cons</b>	<ul style="list-style-type: none"> <li>Short lifespan (150-250 cycles)</li> <li>Fire risk</li> </ul>	<ul style="list-style-type: none"> <li>Heavy and bulky</li> <li>Voltage depression effects</li> </ul>	<ul style="list-style-type: none"> <li>Lower average capacity</li> <li>Heavier than LiPo</li> </ul>



# Power: Subsystem Battery Trade



Propulsion power	Seperate batteries	Single battery
Pros	<ul style="list-style-type: none"> <li>● Redundancy as systems are separated</li> <li>● No conditioning is necessary</li> <li>● Lighter than single battery</li> </ul>	<ul style="list-style-type: none"> <li>● None</li> </ul>
Cons	<ul style="list-style-type: none"> <li>● Weight distribution complications</li> </ul>	<ul style="list-style-type: none"> <li>● Voltage must be conditioned for the Science subsystem</li> <li>● Heavier due to additional capacity needed for single battery at higher voltage</li> </ul>

- Should the aircraft's flight battery/batteries also be used to power the science subsystem



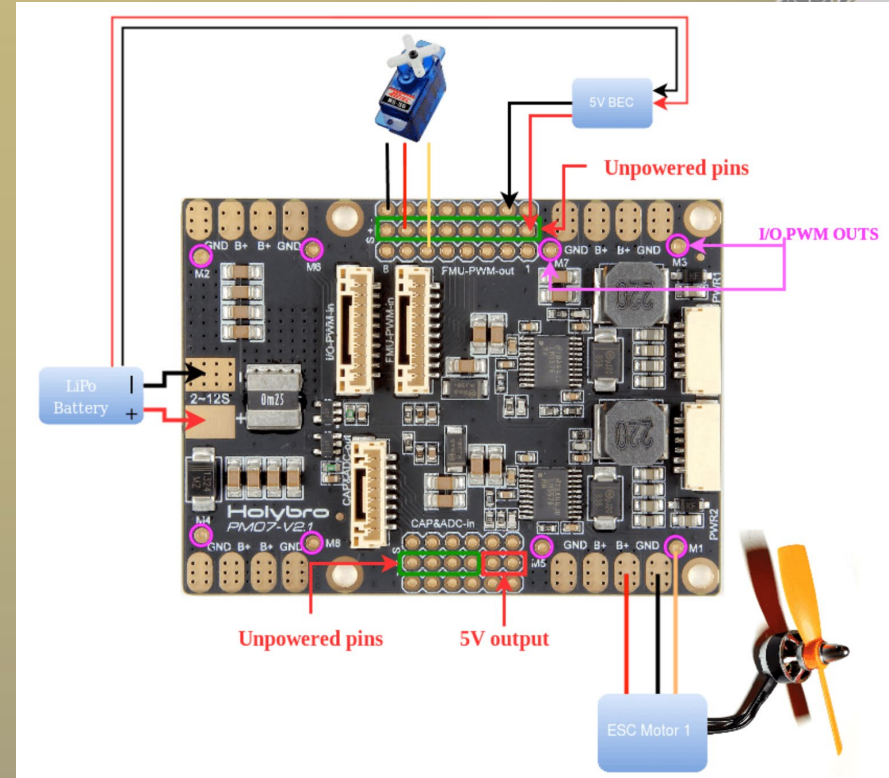
Propulsion power	Multiple batteries in parallel	Single battery
<b>Pros</b>	<ul style="list-style-type: none"> <li>• Distribution of loading along the wing</li> <li>• Significant flight heritage</li> </ul>	<ul style="list-style-type: none"> <li>• Low integration complexity</li> </ul>
<b>Cons</b>	<ul style="list-style-type: none"> <li>• Risky and more complex to integrate batteries in parallel</li> </ul>	<ul style="list-style-type: none"> <li>• Challenging to find really high capacity LiPo batteries</li> <li>• Increased wing loading near battery</li> </ul>

- Similar weight and cost between the two options



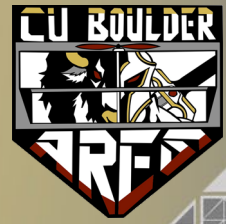
# Power: Conditioning

- Pixhawk power conditioning board takes in a 2-12s battery
- Creates 2 5V outputs for the autopilot power ports
- A 5V BEC will power the servos
- An electronic speed controller will connect to the board and to the motor from the board



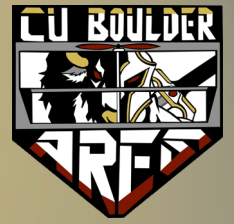


# Preliminary Testing Plan



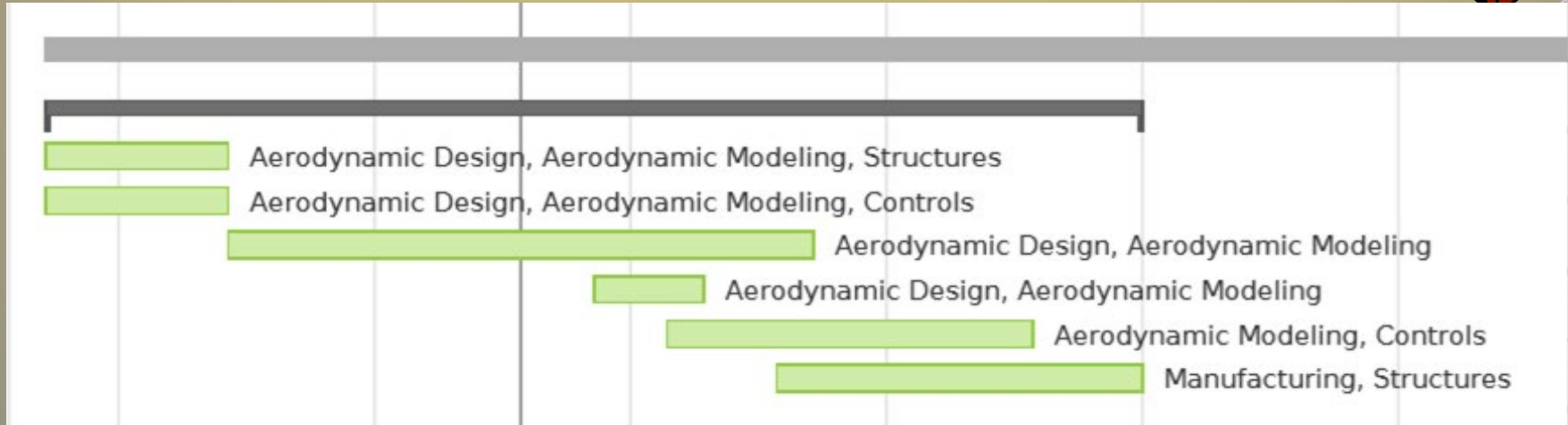
- Plans for testing/verifying difficult requirements
  - FADs - Cold Temperature Plugged Tube Testing
  - Takeoff - Launch a Simulated Mass to Calculate Rail Exit Velocity
  - Landing - Simulate an Expected Force on the Body
  - Propulsion - Static and Dynamic Propulsion Thrust Testing (wind tunnel)
  - Battery - Full System Power Draw Testing (Battery Life Testing)
- Pilot training plan (potential for outside pilot options)
- 2 Battery Flight Testing
  - Two different testing scenarios
    - First Set of Batteries is for running all Avionic and Propulsions Sub-systems for some flight time
    - Second Set of Batteries is for only running Propulsions system for 2+ hours
      - Dynamic testing - Wind tunnel experimentation

Critical Project Elements	Description	Solutions
Surviving Impacts	Landings that do not break the aircraft or propeller	Utilize a foldable propeller system
Endurance	2 hour flight endurance	Descope to 1 hour and use 3S batteries in parallel with a strong motor used at low power
Reusability	Ability to take-off and land 10+ times	Utilize materials such as EPP foam and carbon fiber honeycomb
Power	Weight of the battery for the propulsion system	Using 3-4 3S batteries for propulsion and a separate power system for FADS



# Scheduling Backup Slides

# Schedule Close View

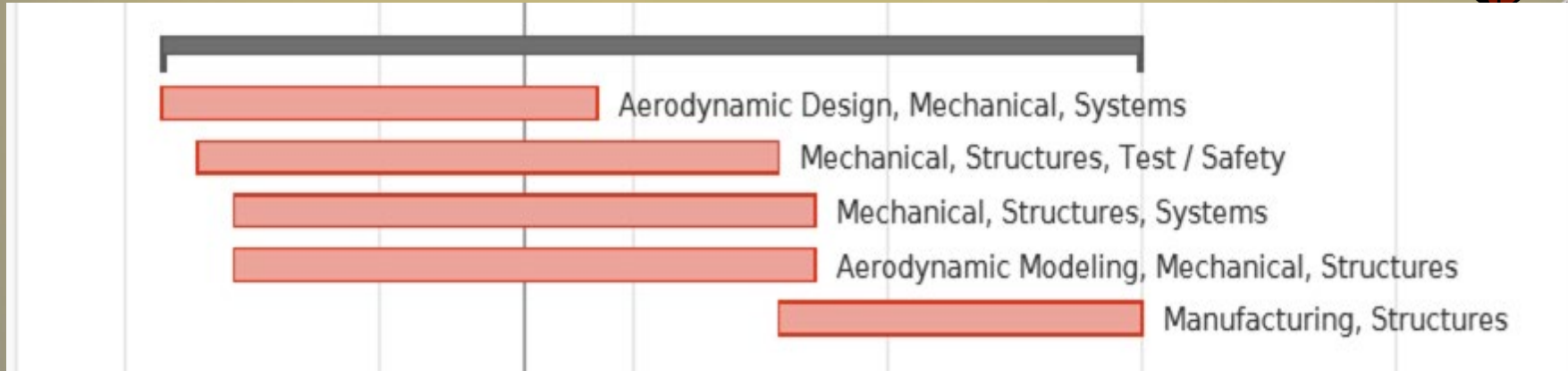


## ARES CDR Schedule

### Wing Design

- Create Model with Full Dimensions
- Choose Airfoil for Wings
- Create CAD Model
- Integrate Takeoff System
- Calculate Stability Coefficients & Flig...
- Choose Construction Materials

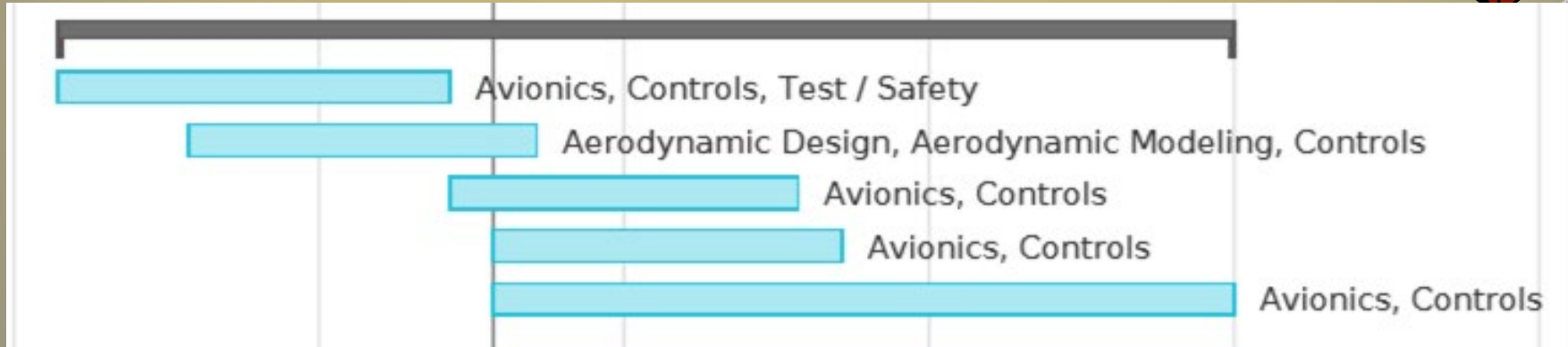
# Schedule Close View



## Takeoff

- Design Aircraft Attachment to Takeoff...
- Determine Minimum Rail Length
- Full CAD Model of Takeoff System
- Model Takeoff Impulses and Forces o...
- Choose Materials for Takeoff System

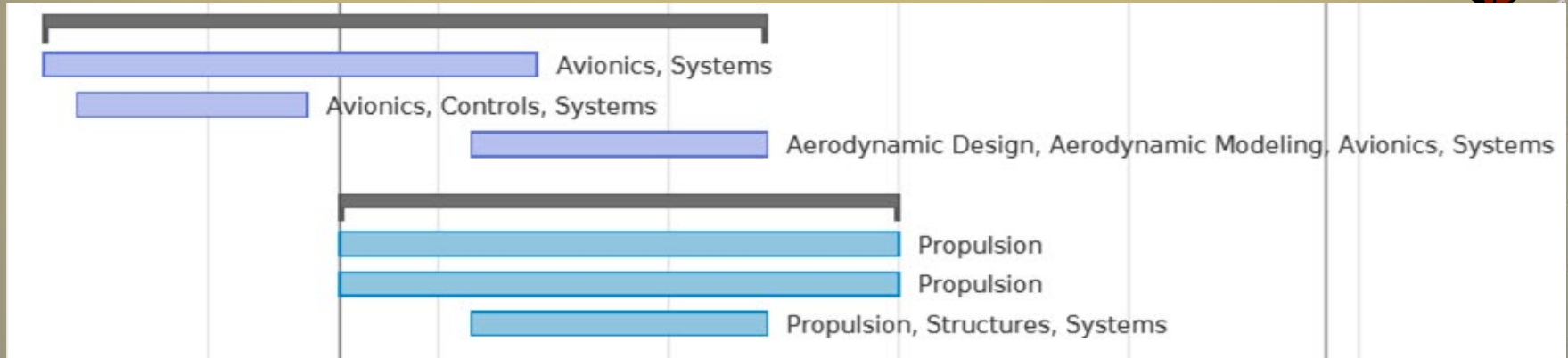
# Schedule Close View



## Flight

- Design Ground Station
- Size and Range of Control Surfaces
- Communication System Plan
- Determine Servos Needed for Control...
- Control Algorithm for PixHawk

# Schedule Close View



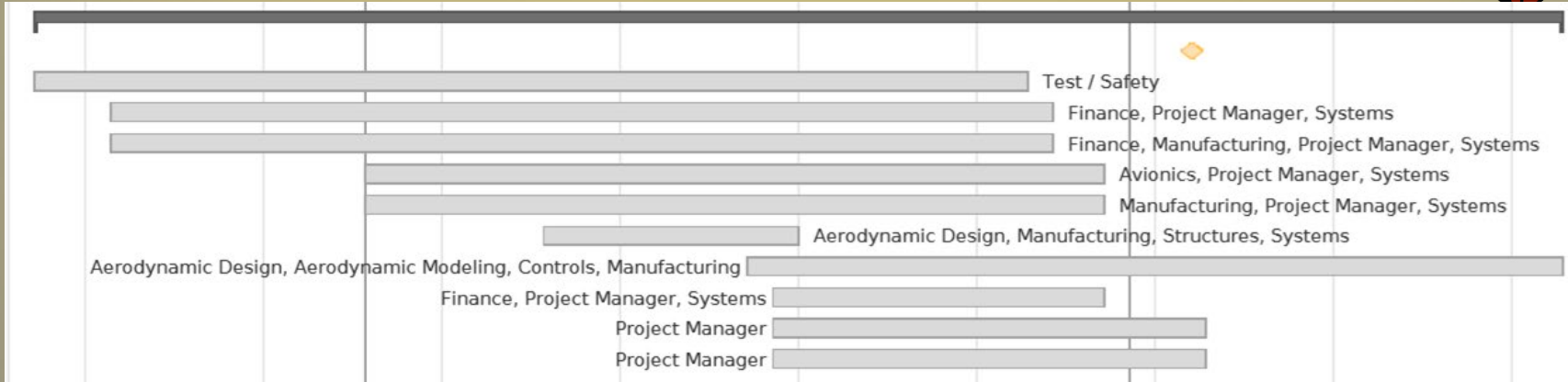
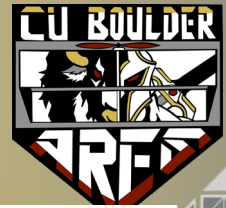
## Science

- Design FADS Pressure Collection
- Design FADS Integration to Wing
- Calibration Plan for FADS Data

## Propulsion

- Select Motor
- Select Propeller
- Determine Mounting Plan

# Schedule Close View

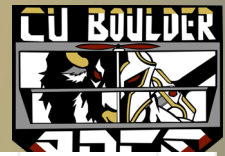


## General

- Present CDR
- Testing Plan for Each System
- List of COTS Products
- List of Products to Manufacture
- Power Budget
- Weight Budget
- Determine Placement of All Compon...
- Build Prototype Aircraft
- Cost Budget
- Create CDR Presentation
- Determine Schedule



# Schedule Dependency Organization



## ARES CDR Schedule

### No Dependency

Task	start	end
Create Airframe Model with Full Dim...	10/19	10/23
Choose Airfoil for Wings	10/19	10/23
Testing Plan for Each System	10/19	11/26
Design Aircraft Attachment to Takeof...	10/22	11/02
Design Ground Station	10/22	10/30
Design FADS Data Collection	10/23	11/06

### First Level Dependency

Task	start	end
Determine Minimum Rail Length	10/23	11/07
Design FADS Integration to Wing	10/24	10/30
Model Landing Impulses and Forces ...	10/24	10/30
Size and Range of Control Surfaces	10/25	11/01
Communication System Plan	10/31	11/07
Integrate Takeoff System	11/03	11/05
Calibration Plan for FADS Data	11/05	11/13

### Second Level Dependency

Task	start	end
Full CAD Model of Aircraft	10/24	11/08
Full CAD Model of Takeoff System	10/24	11/08
Model Takeoff Impulses and Forces o...	10/24	11/08
Design Aircraft to Survive Landing	10/30	11/06
Determine Servos Needed for Control...	11/01	11/08
Control Algorithm for PixHawk	11/01	11/17

### Third Level Dependency

Task	start	end
Determine Mounting Plan	11/05	11/13
Calculate Stability Coefficients & Flig...	11/05	11/14
Choose Wing Construction Materials	11/08	11/17
Choose Materials for Takeoff System	11/08	11/17
Determine Placement of All Compon...	11/08	11/17

### Fourth Level Dependency

Task	start	end
Select Motor	11/01	11/17
Select Propeller	11/01	11/17
Power Budget	11/01	11/29
Weight Budget	11/01	11/29
Build Prototype Aircraft	11/16	12/17
Cost Budget	11/17	11/29

### Ongoing/Non-Dependent Tasks

Task	start	end
Present CDR	12/03	12/03
List of COTS Products	10/22	11/27
List of Products to Manufacture	10/22	11/27
Create CDR Presentation	11/17	12/03
Determine Schedule	11/17	12/03
Work on FRR	12/04	12/17
FFR Due	12/17	12/17

