



# A.C.E.S.

*Air-breathing Cold Engine Start*



## Preliminary design Review



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# Outline



- Project Description
- Baseline Design
- Initial Energy Feasibility
- Fuel Delivery System (FDS) Heating Feasibility
- Electronic Heating Feasibility
- Project Summary





# Project Description



- Design, build, and test a system to facilitate starting a JetCat P90-SXi jet engine at a temperature of  $-50^{\circ}\text{F}$  by:
  - Providing fuel to the engine at a mass flow rate of  $4.8 \text{ g/s} \pm 5\%$
  - Ensuring that the engine electronics are within their operating temperature range
  - Ensuring that the heating system has sufficient power to heat the fuel delivery system and engine electronics
- Motivation
  - Air Force Research Lab (AFRL) competition
  - Proof of concept for high-altitude (cold-temperature) restart for jet-powered UAS

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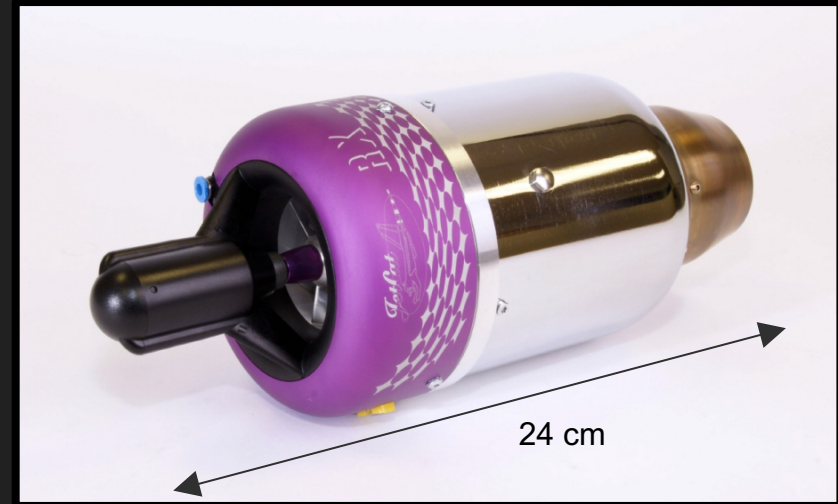




# Engine: JetCat P90-SXi



- Miniature Jet Engine
- Fuel: Jet-A, Kerosene/Oil Mixture
- Specifications:
  - Maximum Thrust: 105 N
  - Maximum RPM: 130,000
  - Idle Fuel Flow Rate: 0.8 g/s
  - Maximum Fuel Flow Rate: 4.8 g/s
- Dimensions:
  - Length: 240 mm
  - Diameter: 97 mm
  - Weight: 1050 g







# New Project Scope

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- The project scope has been narrowed
- Original project involved fuel delivery, keeping electronics operational, creating a custom engine control unit (ECU) and engine sensor board (ESB)
- Starting the engine for the AFRL competition is no longer part of the project requirements
- The course design will focus on delivering the fuel to the engine at a specified flow rate and keeping the electronics operational

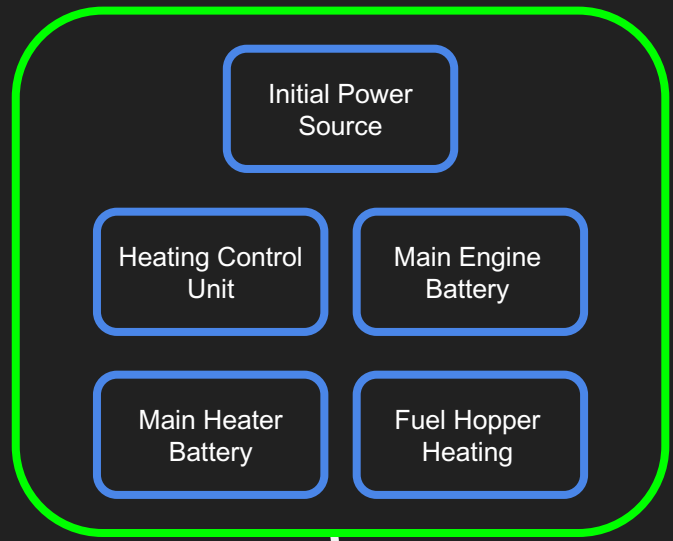




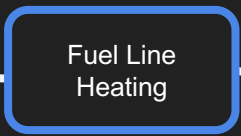
# New Project Scope



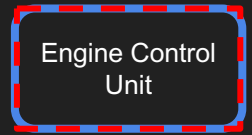
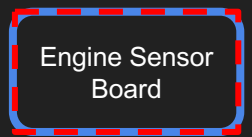
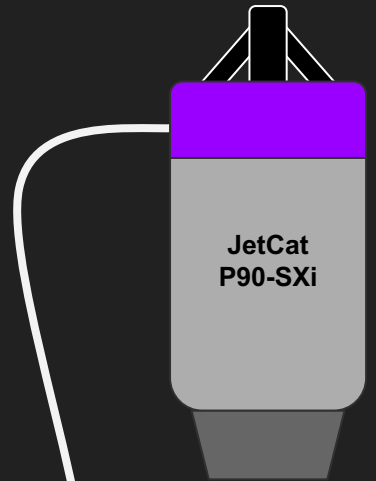
## Course Design Items



Insulated Electronics Housing



## AFRL Design Items





# Motivation



- **Fuel ignition redesigns are too difficult**
  - Ensure droplet size is in the micron range
  - Spray pattern must closely resemble nominal conditions
  - Nominal spray pattern is difficult to quantify
- **Modifications to the JetCat engine are notoriously difficult**
  - Our Engine Sensor Board has already broken when operating the engine
  - Original project would have been impossible to complete without working engine
- **No other undergraduate group has succeeded with custom engine electronics**
  - REAPER, SABRE, MEDUSA





# Critical Project Elements

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- Provide a source of initial electrical energy to heat main heater battery to operational temperature (30°F).
- Heat the fuel lines and hopper to 60°F in order to decrease the viscosity of the fuel and allow it to flow at 4.8 g/s.
- Heat the engine electronics (ECU and receiver) to their standard operating temperatures (60°F).
- Construct a Heating Control Unit (HCU) which will control the fuel and electronics heating systems.





# Course Project Objectives



	Fuel Delivery System (FDS) Heating	Electronics Heating	Time	AFRL Competition
<b>Level 1</b>	Fuel delivery system will regulate Jet-A fuel at the flow rate of 4.8 g/s when initially cold soaked to -30°F.	The electronics will be heated to operational temperature when cold soaked to -30°F.	The fuel delivery and electronics heating systems objectives will be completed in less than 3 hours.	
<b>Level 2</b>	Fuel delivery system will regulate Jet-A fuel at the flow rate of 4.8 g/s when initially cold soaked to -40°F.	The electronics will be heated to operational temperature when cold soaked to -40°F.	The fuel delivery and electronics heating systems objectives will be completed in less than 1.5 hours.	
<b>Level 3</b>	Fuel delivery system will regulate Jet-A fuel at the flow rate of 4.8 g/s when initially cold soaked to -50°F.	The electronics will be heated to operational temperature when cold soaked to -50°F.	The fuel delivery and electronics heating systems objectives will be completed in less than 8 minutes and 42 seconds.	
<b>Level 4</b>				Entire system will be integrated with engine and successfully start within 3 hours.





# Functional Requirements

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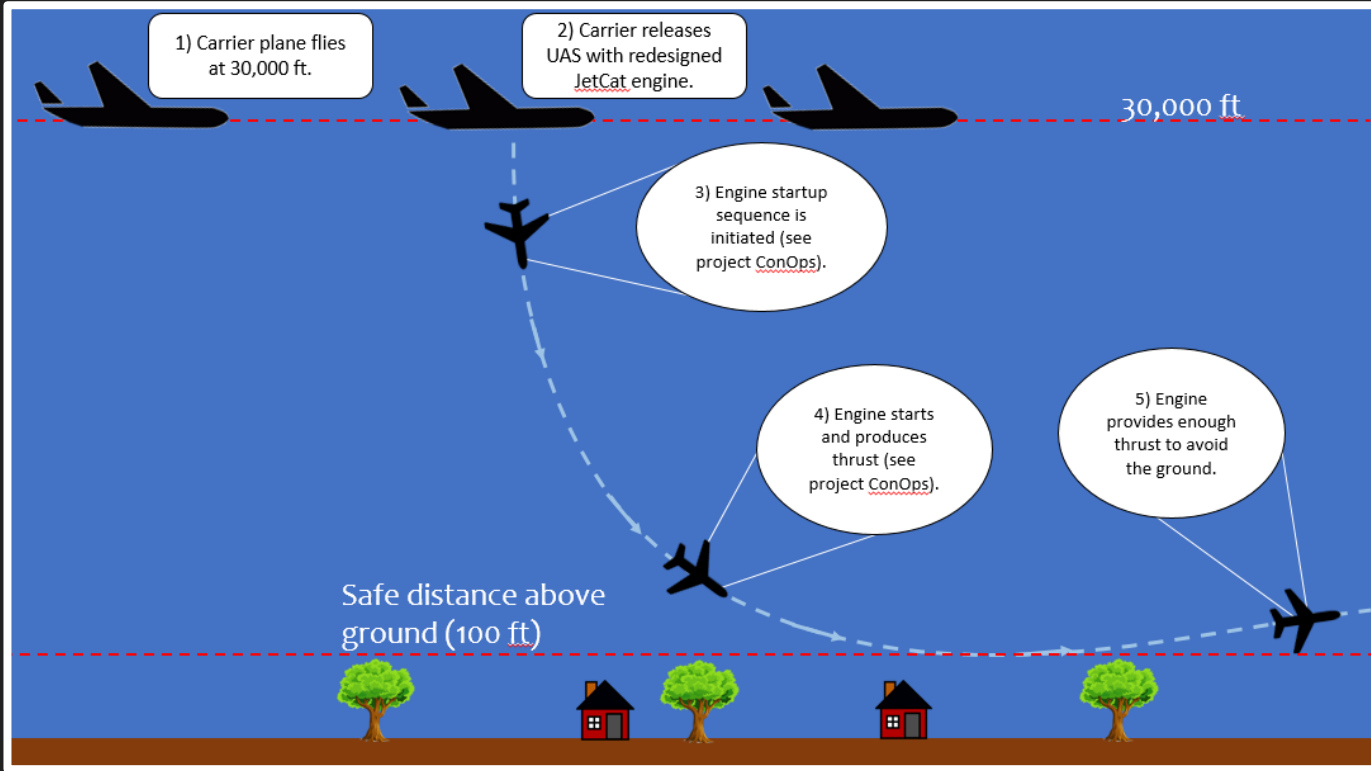


- **HCU:** The Heating Control Unit (HCU) shall monitor and regulate the temperature of the electronic components and fuel delivery heating systems.
- **FDS:** The Fuel Delivery System shall provide adequate fuel flow for a successful start-up sequence and continued operation of the engine. This fuel flow is specified as 4.8 g/s for full throttle.
- **ENERGY:** An initial energy source shall provide adequate power for the fuel delivery system heating and electronics heating.



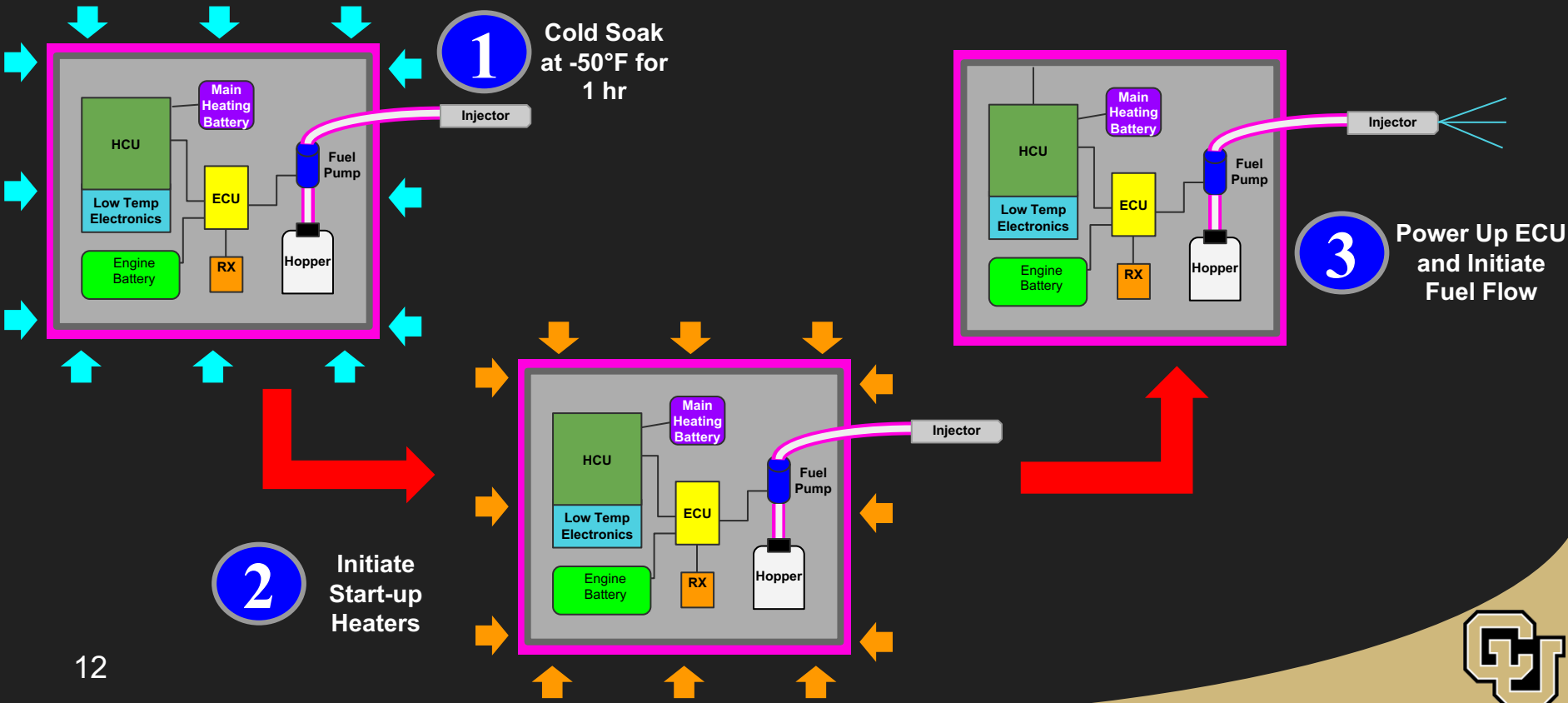


# Mission CONOPS





# Project Conops







# Baseline Design



- Initial Energy: Charged capacitor
  - Stores and discharges energy to heat main battery
- Fuel Delivery System: Resistive heating
  - Resistive heating wire wrapped around fuel delivery components
- Electronics Heating: Resistive heating within insulated box
- Heating Control Unit: Microcontroller powered by start-up batteries
  - Controls temperature of fuel delivery and electronics systems
  - Both components functional at  $-50^{\circ}\text{F}$

Project  
Description

Baseline  
Design

Initial  
Energy  
Feasibility

FDS  
Feasibility

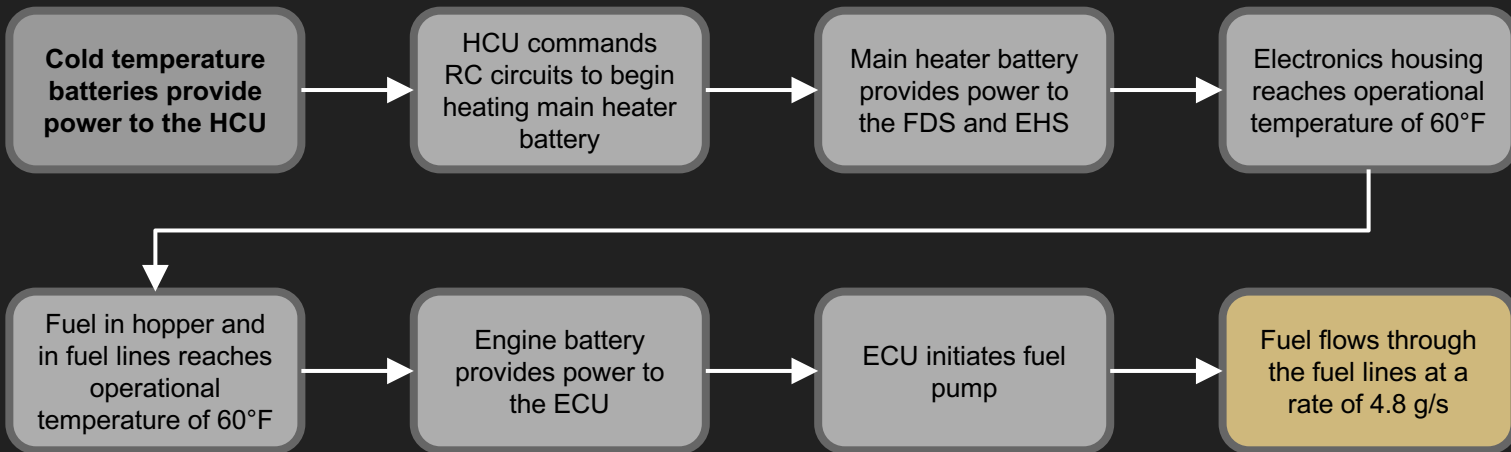
Electronic  
Heating  
Feasibility

Project  
Summary



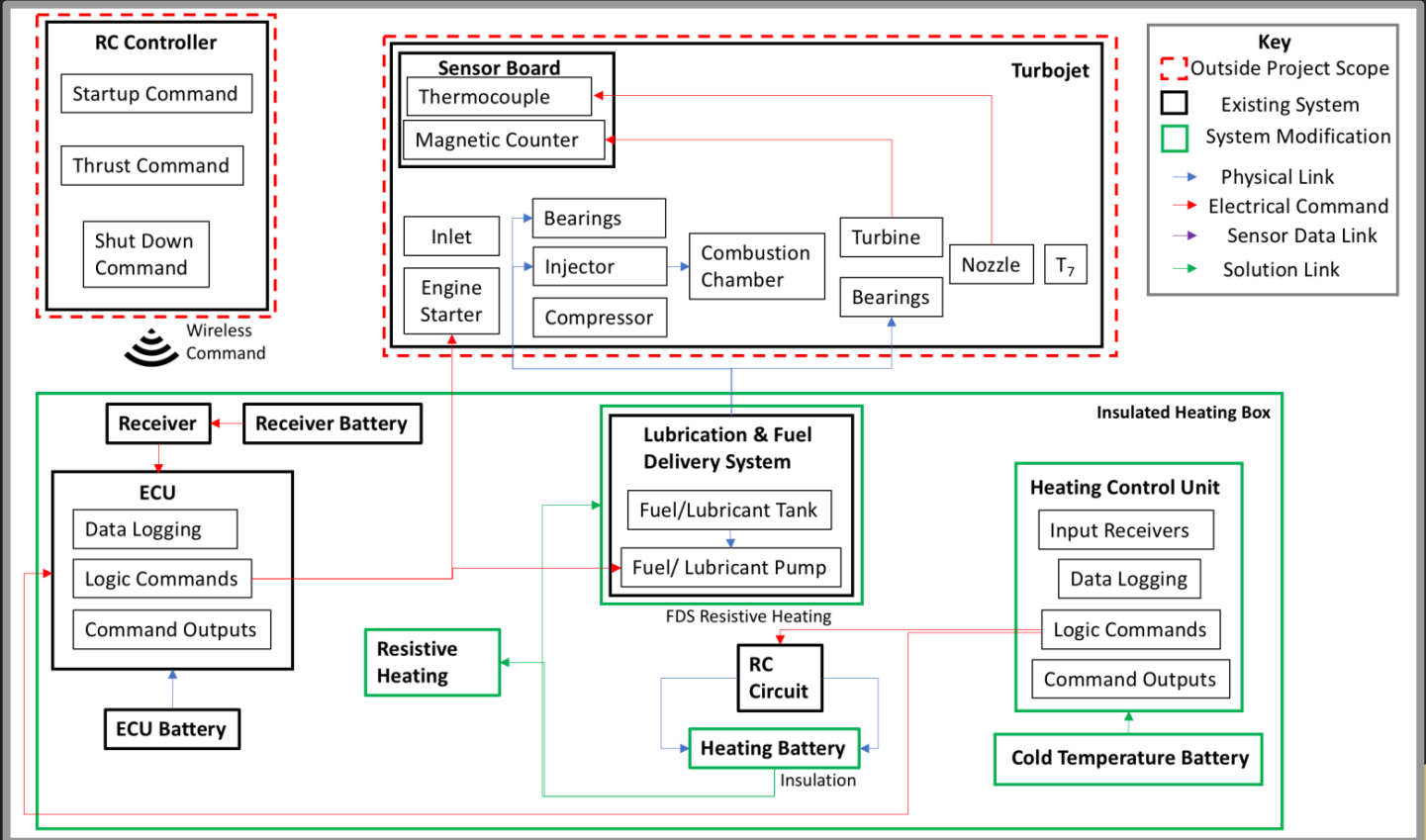


# Process Flow Diagram





# Functional Block Diagram





# Initial Energy Feasibility

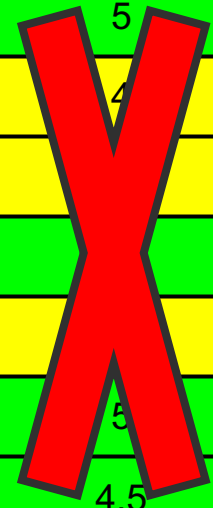




# Initial Energy Trade Study

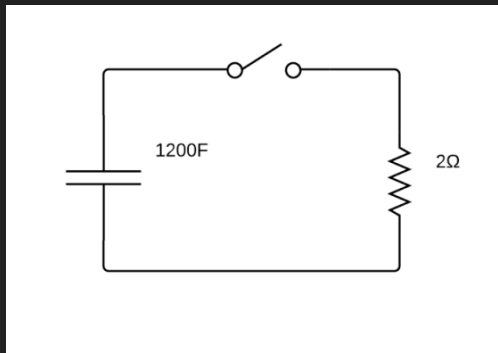
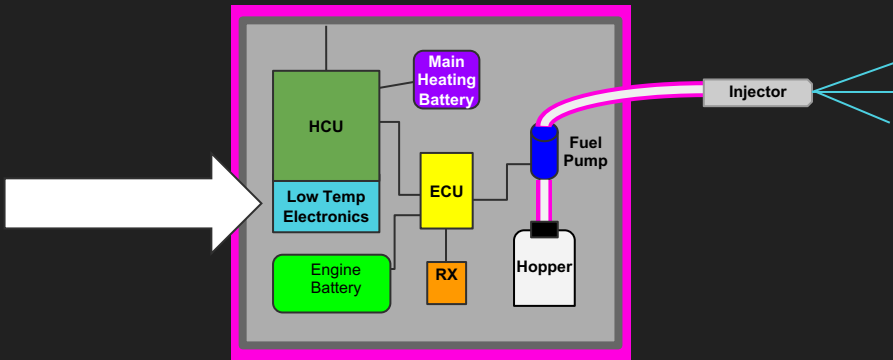


Factor	Weights	Chemical	Mechanical	Low-Temp Electronics	Cold Soak Active Heater
Reliability	0.3	4	2	5	5
Manufacturability	0.25	3	2	5	4
Safety	0.15	1	4	4	4
Start-up Time	0.15	4	3	5	5
Team Experience	0.1	1	3	4	4
Cost	0.05	4	2	4	5
Total	1	3.1	2.5	4.7	4.5



# Initial Energy Design

- 7 individual RC circuits, each with...
  - A 1200 Farad supercapacitor
  - $2\Omega$  Resistive wire wrapped around the main heater battery

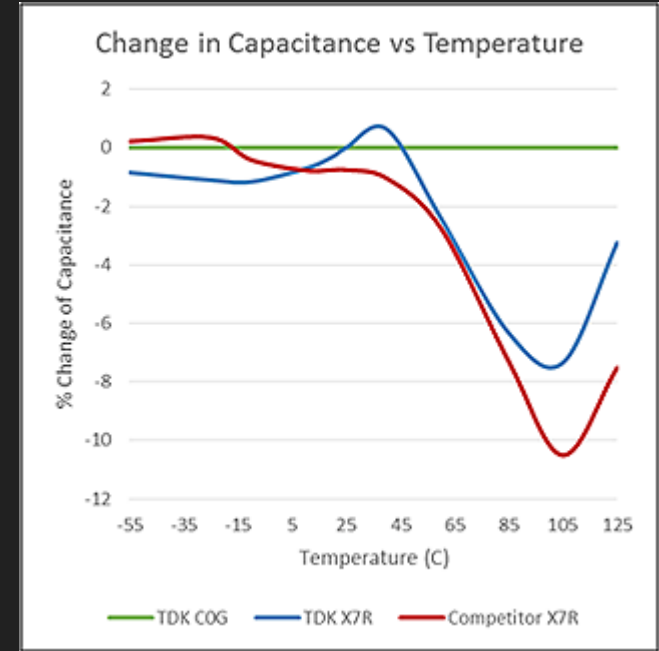




# Initial Energy Feasibility



- Capacitor performance does not degrade at low temperatures
- Chosen 1200F capacitors can provide 3W with 2Ω resistive load
  - 7 RC circuits provide necessary power to warm batteries
- Chosen capacitors are cheaper, smaller, and more powerful than low temperature batteries



Credit to product.TDK.com





# Initial Energy Capacitor Model



The performance of our capacitor system is modeled as a simple RC circuit

- To heat batteries at a safe temperature takes 8 minutes
- In the 8 minute heating window, each circuit releases 1,442J, at an **average 3W**
  - 7 circuits will release about 10,094J, at 21W
  - Peak wattage will be 3.65W

$$V(t) = V_0(e^{-t/(RC)})$$

$V(t)$  = Voltage (V)

$V_0$  = Initial Voltage (V)

$t$  = Time (sec)

$R$  = Resistance ( $\Omega$ )

$C$  = Capacitance (F)

$$I(t) = \frac{V_0}{R} e^{-t/(RC)}$$

$I(t)$  = Current (A)

$V_0$  = Initial Voltage (V)

$t$  = Time (sec)

$R$  = Resistance ( $\Omega$ )

$C$  = Capacitance (F)







# Risk of Supercapacitors

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- Never charge a capacitor past its rated voltage.
- Shorting a capacitor will create a large amount of heat
  - Can burn wire leads and fry other components
  - Potential injury to personnel
- Capacitors retain voltage for a long time after disconnected from circuit
  - From hours up to days

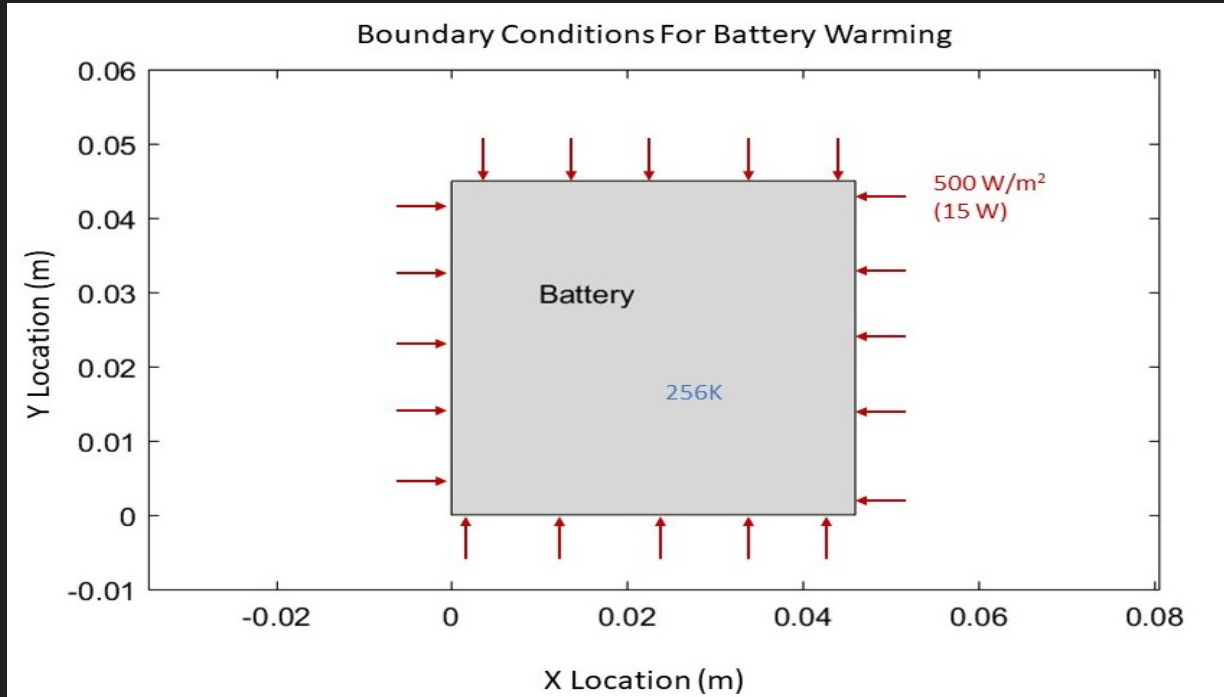




# Initial Energy Feasibility



- Main Heating Battery

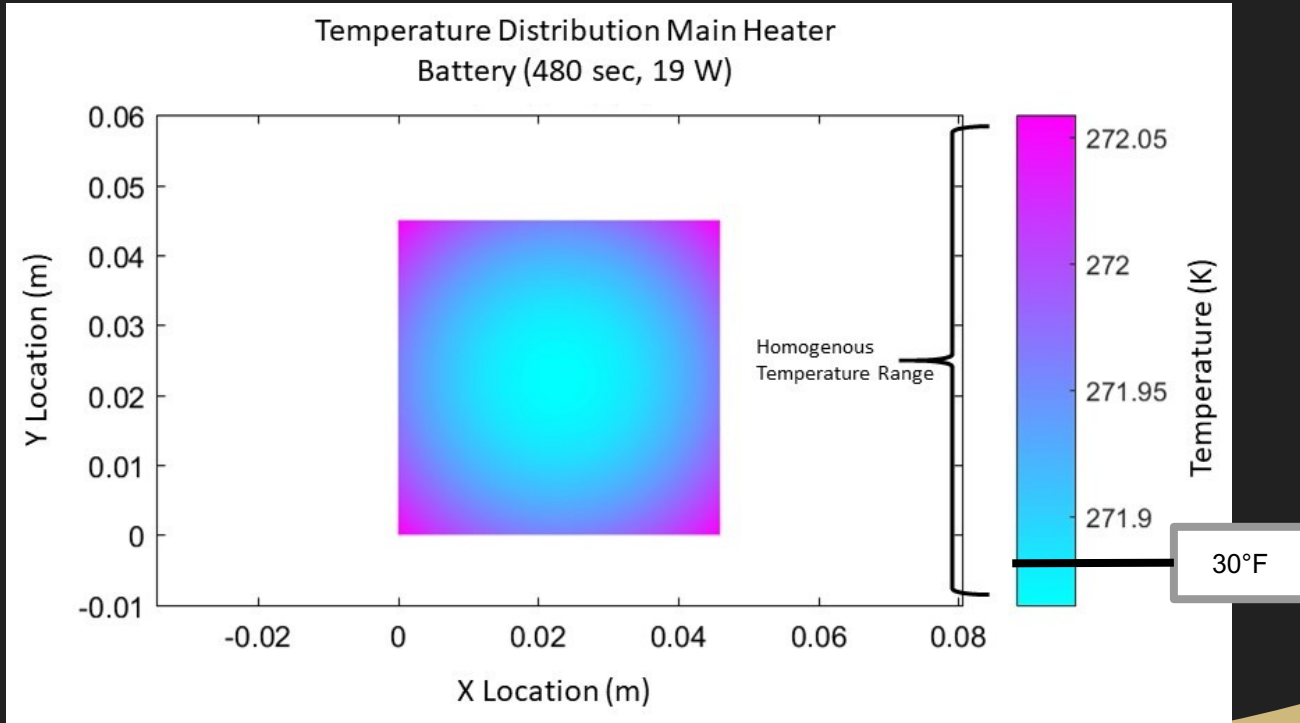




# InITIAL ENERGY Feasibility



- Main Heating Battery



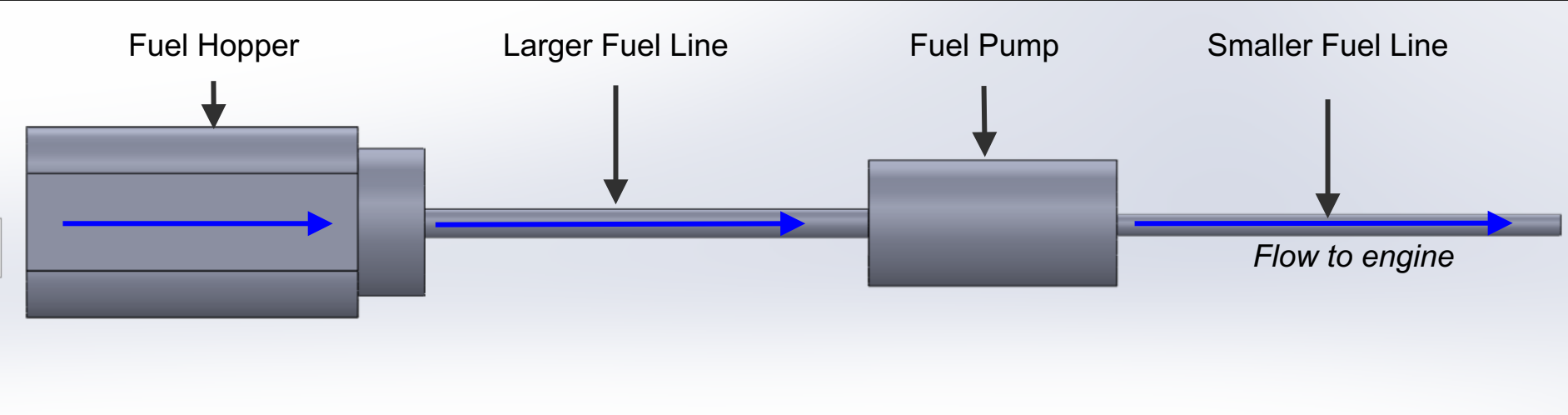


# Fuel Delivery System





# System Layout





# Fuel System Trade Study

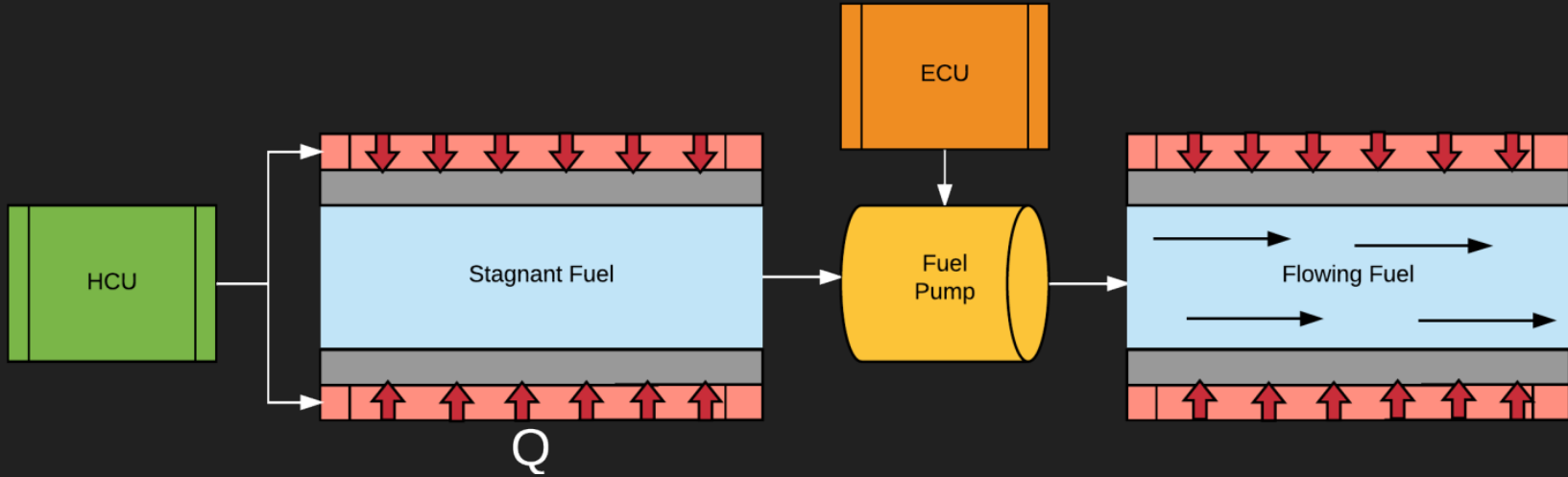


Factor	Weights	Resistive Heating	Fuel Additive	Circulating Fluid	Pressurized Fuel
Manufacturability	0.3	4	4	2	2
Reliability	0.25	4	3	2	2
Power Consumption	0.15	3	5	3	3
Safety	0.1	4	3	4	2
Start-up Time	0.1	4	5	2	4
Cost	0.1	5	3	4	3
Final Score	~	<b>3.85</b>	<b>4.05</b>	2.8	2.65





# How the Fuel Line Solution Works

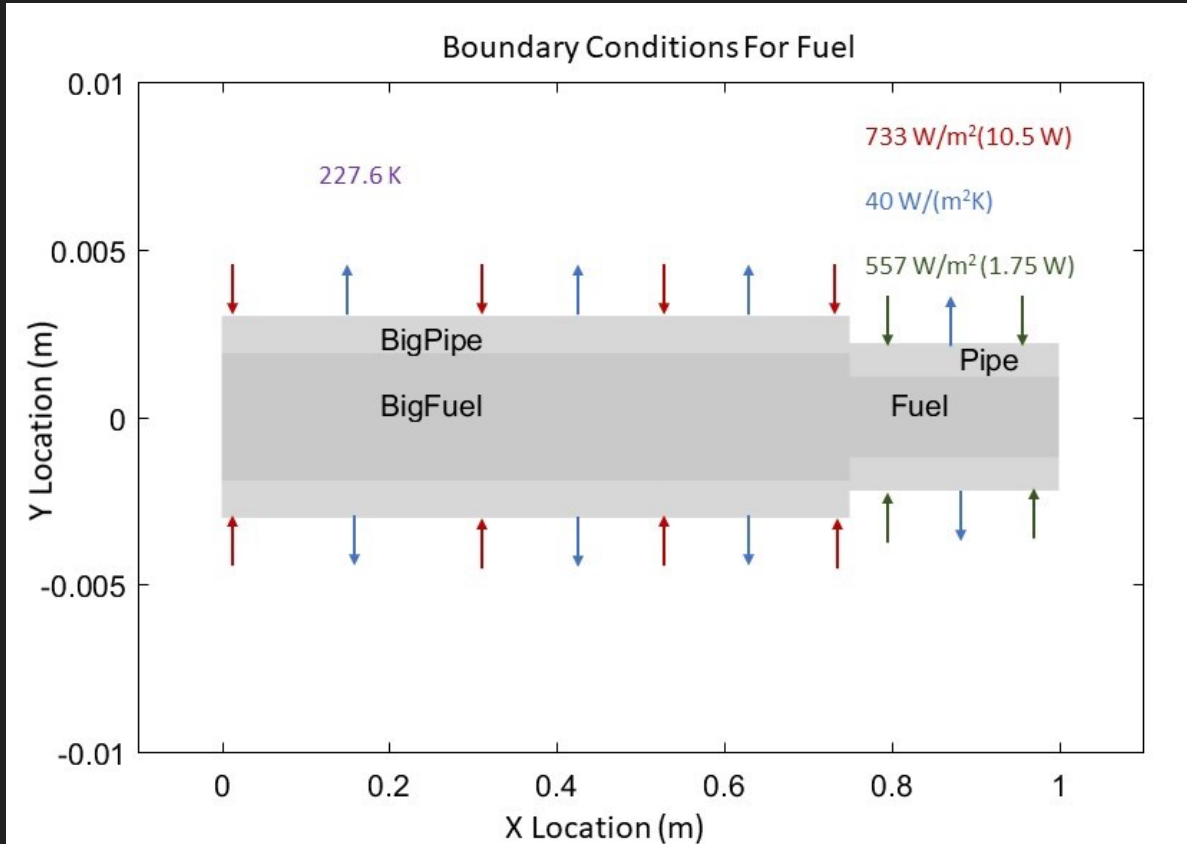


- **Light Red** - Resistive Heating Wire
- **Grey** - Polyurethane Fuel Line





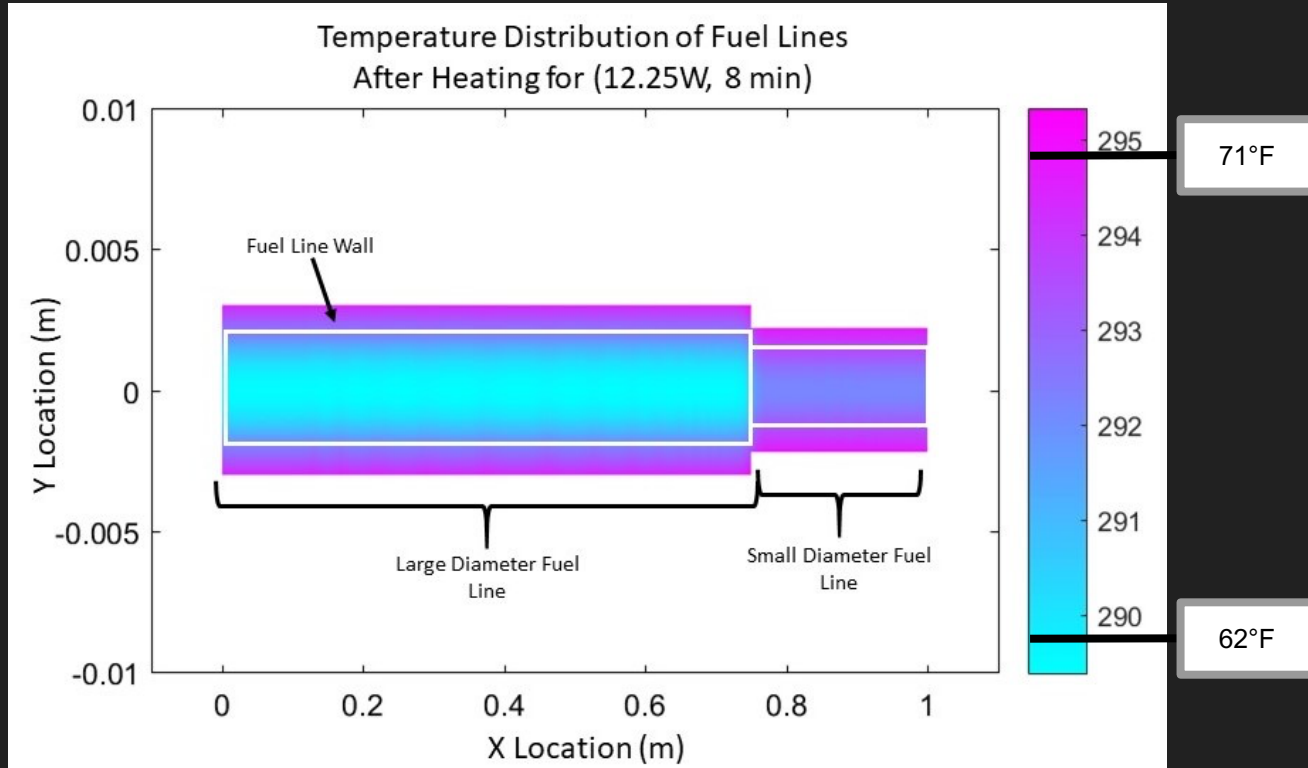
# Fuel Line Heating Feasibility





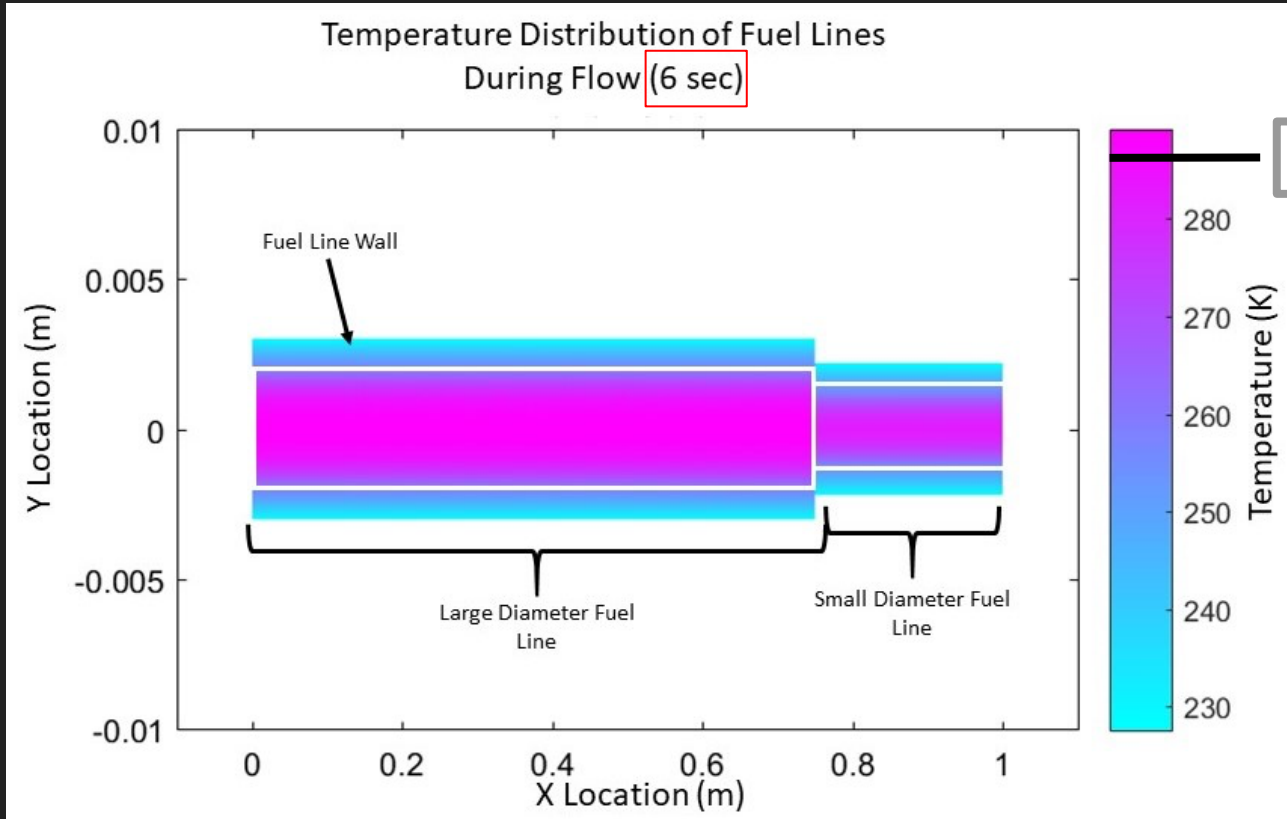


# Fuel Line Heating Feasibility



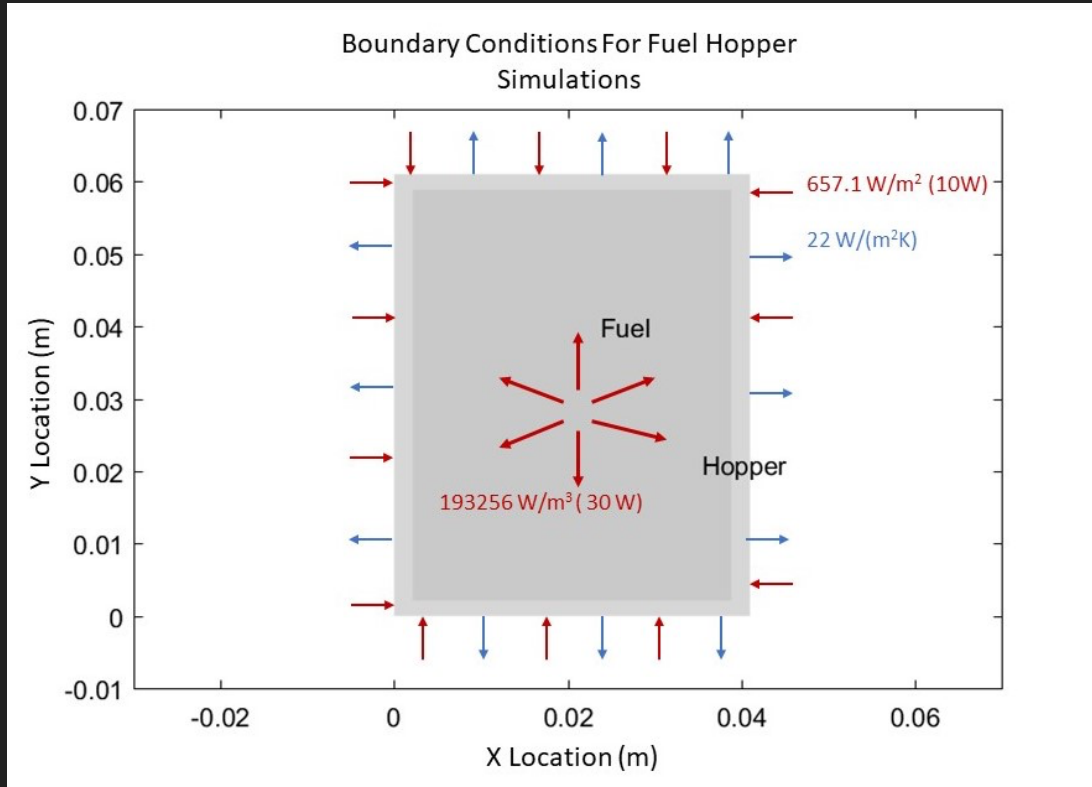


# Fuel Line Heating Feasibility



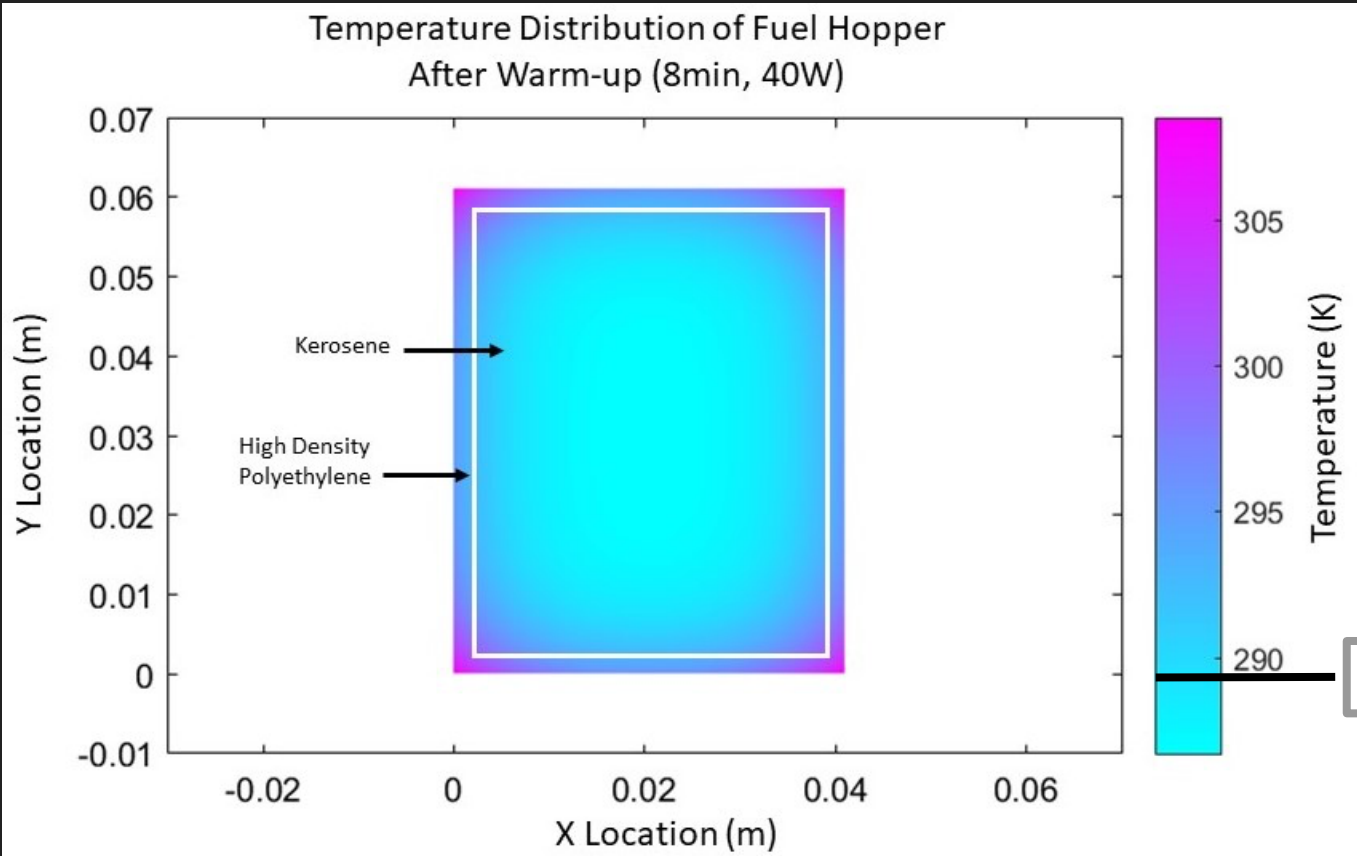


# Fuel Hopper Heating Analysis





# Fuel Hopper Heating Analysis





# Electronics Heating System





# Electronics Heating Trade Study



Factor	Weights	Conductive Heating Element	Radiative Ceramic Resistor	Fluid Heating
Safety	0.3	4	3	2
Reliability	0.2	5	5	3
Start-Up Time	0.2	5	4	3
Power Consumption	0.15	3	2	4
Manufacturability	0.1	4	4	2
Cost	0.05	5	5	4
Total	1	4.45	4.1	2.9

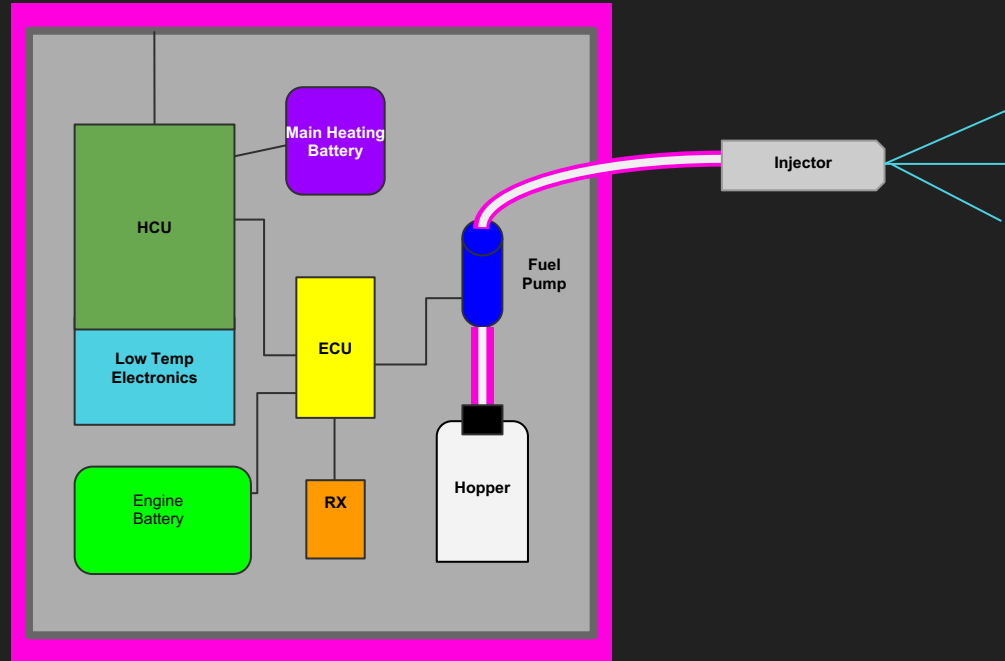




# Electronics Housing

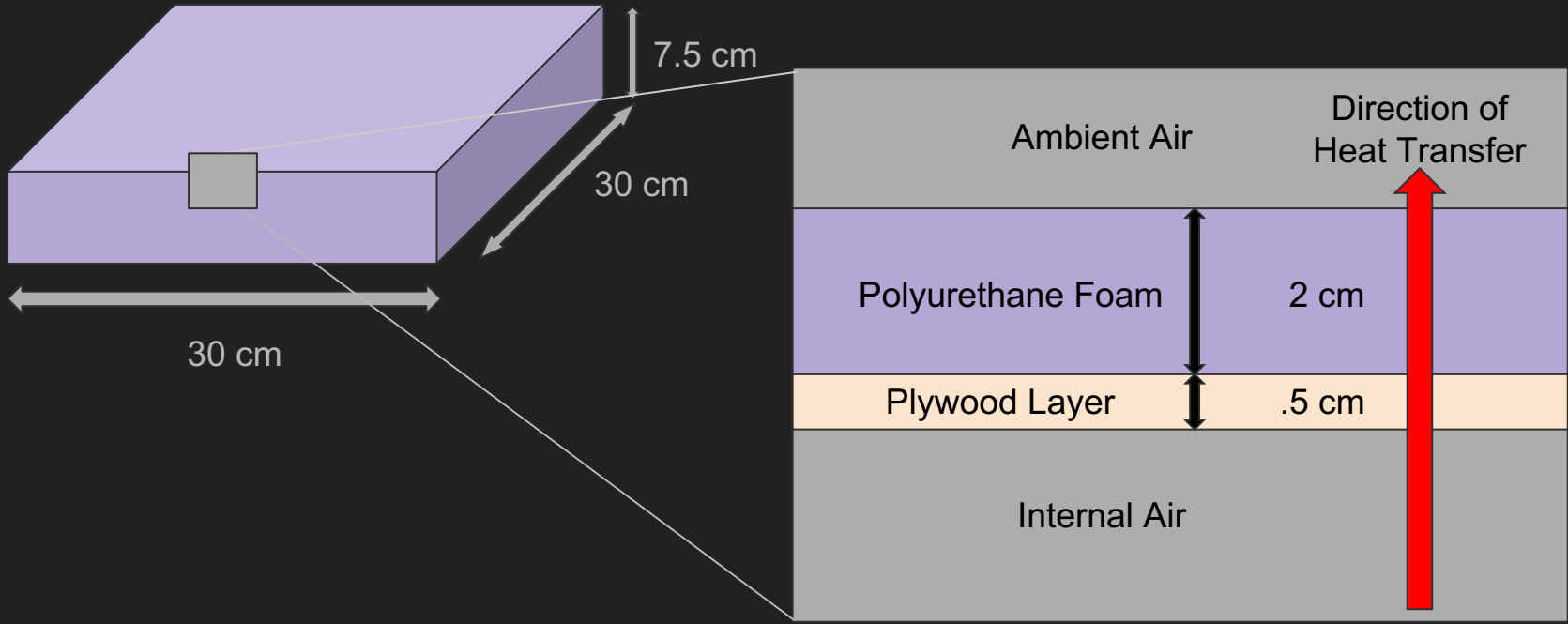


## Electronics Housing (Top View)





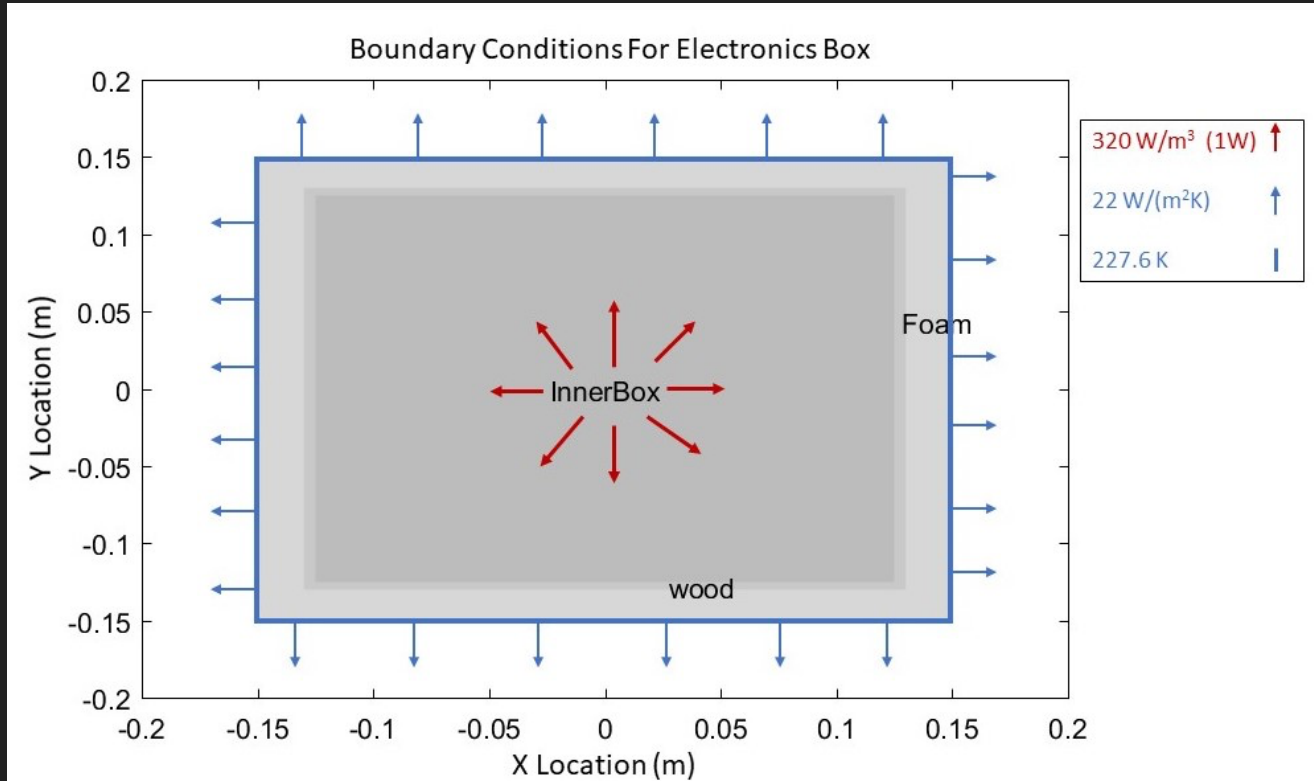
# Electronics Housing Dimensions





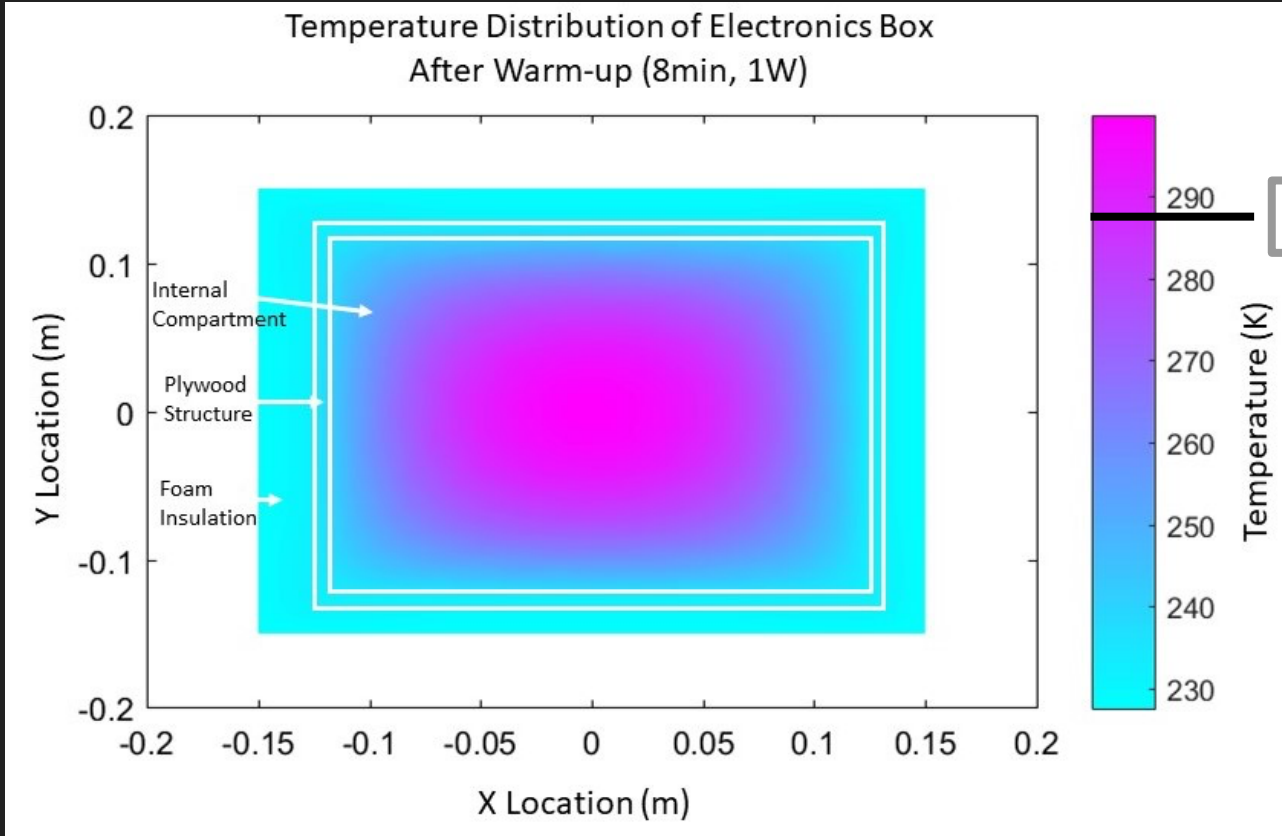


# Transient ELelectronics Heating





# Transient ELelectronics Heating



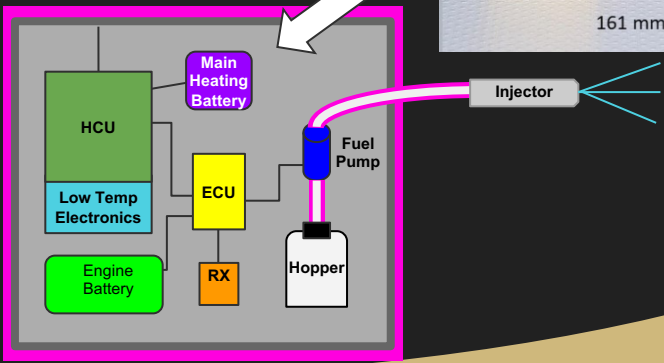
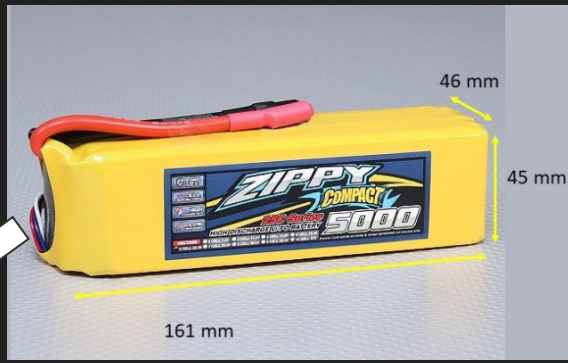


# Main Heater Battery Feasibility



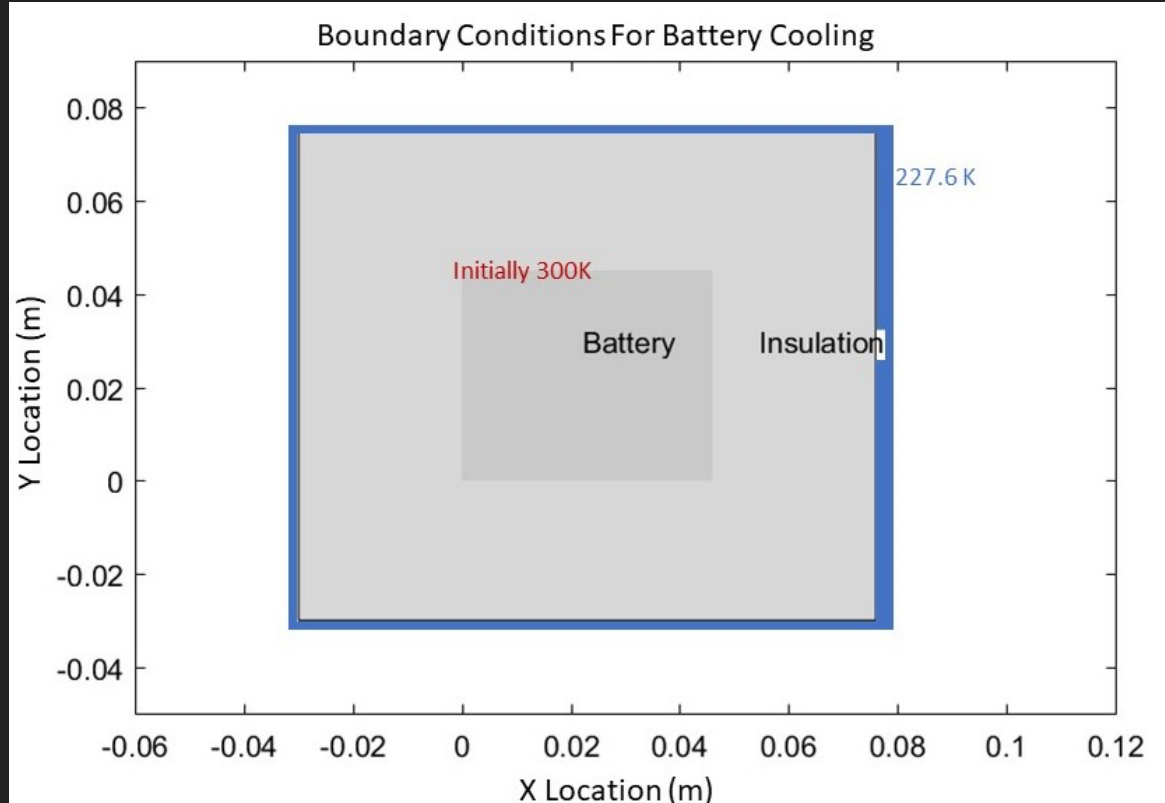
Heating Power Requirements	
Model Type	Transient
FDS Fuel Lines	12.25 W
FDS Fuel Hopper	40 W
Electronics Box	20 W
<b>Total</b>	<b>72.25 W</b>

- 5000 mAh, 22.6 V, 25 C Lipo Battery
- For 30min of discharge, this battery can provide 226 W.



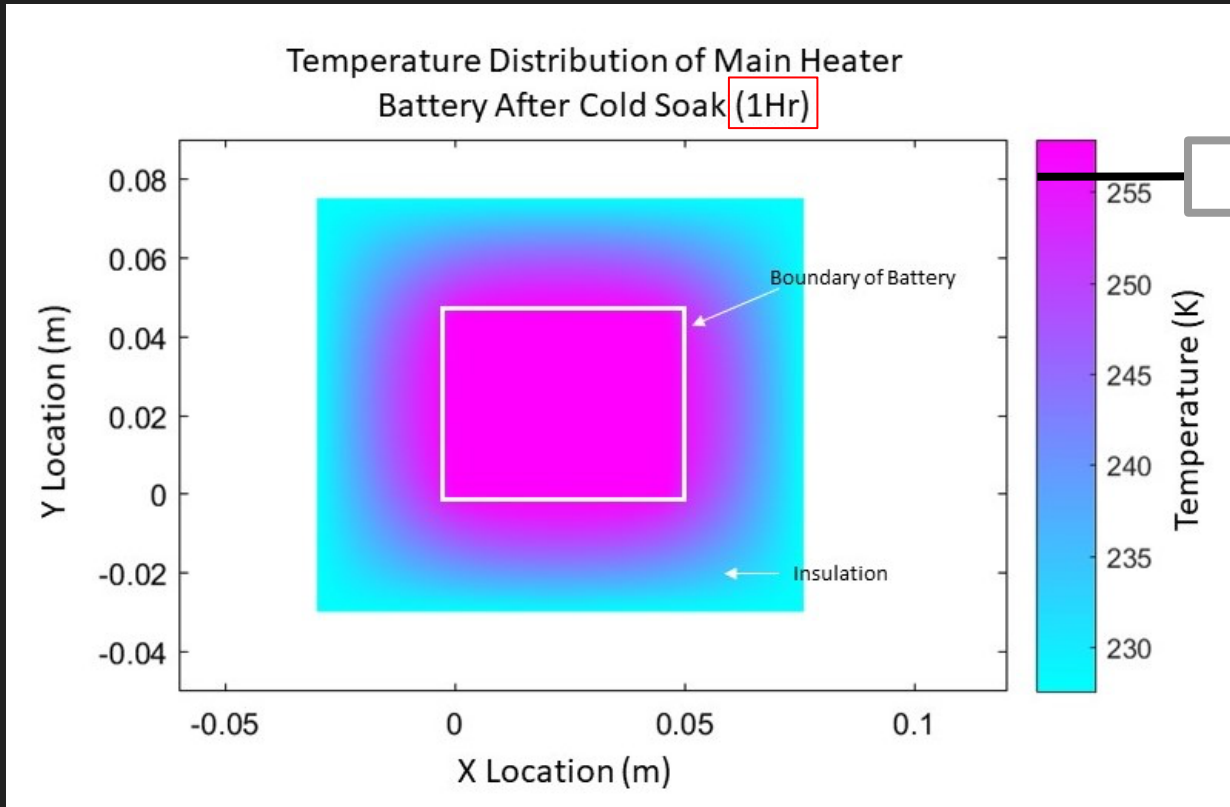


# Main Heater Battery Feasibility





# Main Heater Battery Feasibility





# Heating Control Unit

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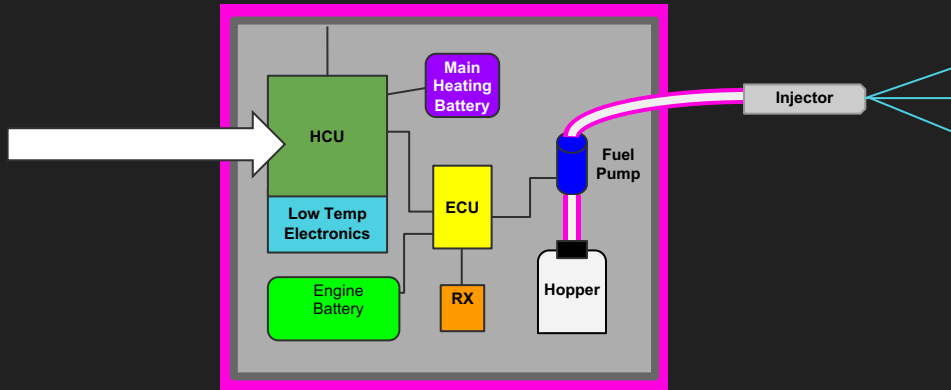


# HEating Control Unit (HCU)



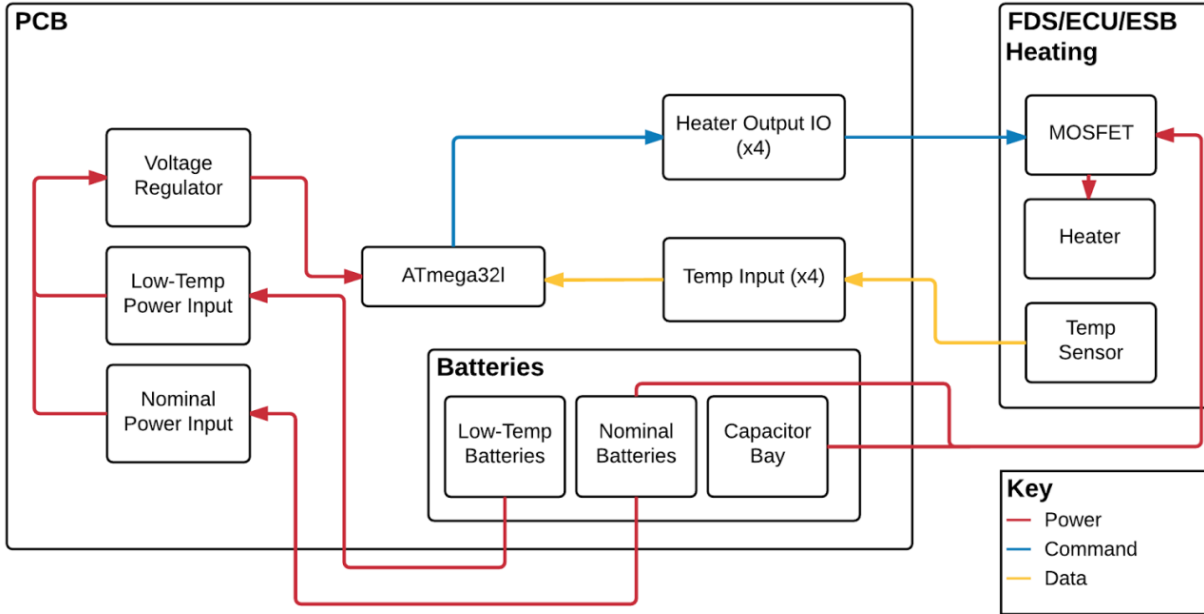
## The Heating Control Unit will be designed to:

- Monitor the temperatures of the electronic and FDS components
- Regulate these temperatures through the use of resistive heaters
- Provide a start-up signal to the ECU once fuel viscosity has been decreased
- Responsible for closing the RC Circuits





# HEating Control Unit (HCU)







# pPROJECT SUMMARY

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# Feasibility Overview

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## CPE:

Provide a source of initial electrical energy to heat main batteries to operational temperature (30°F):

- RC circuits can provide 21W in 8 minutes
- The main heater battery requires 19W to be heated to 30°F
- Power available: 21W > 19W power required

**FEASIBLE**





# Feasibility Overview



## CPE:

Heat the fuel lines and hopper to decrease the viscosity of the fuel and allow it to flow at 4.8 g/s

- Since increasing temperature decreases viscosity, the temperature must be increased to nominal (60°F) so that nominal viscosity and therefore nominal flow rate can be reached
- It takes 12.25W to heat the fuel lines and 40W to heat the fuel hopper to 60°F
- $12.25W + 40W = 52.25W$  - Chosen battery provides 226W.  $52.25W < 226W$

**FEASIBLE**





# Feasibility Overview



## CPE:

Heat the engine electronics (ECU and receiver) to their standard operating temperatures (60°F)

- It takes 20W to heat the air in the electronics housing along with the engine battery to 62°F in 8 minutes
- The main heater battery's insulation never allows its temperature to drop below 0°F
- $52.25\text{W}$  (for fuel heating) +  $20\text{W} = 72.25\text{W}$
- $72.25\text{W} < 226\text{W}$  provided by main heater battery

**FEASIBLE**





# Feasibility Overview

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## **CPE:**

Construct a Heating Control Unit (HCU) which will control the fuel and electronics heating systems

- All HCU components are readily obtainable
- All HCU components can operate at  $-50^{\circ}\text{F}$

**FEASIBLE**

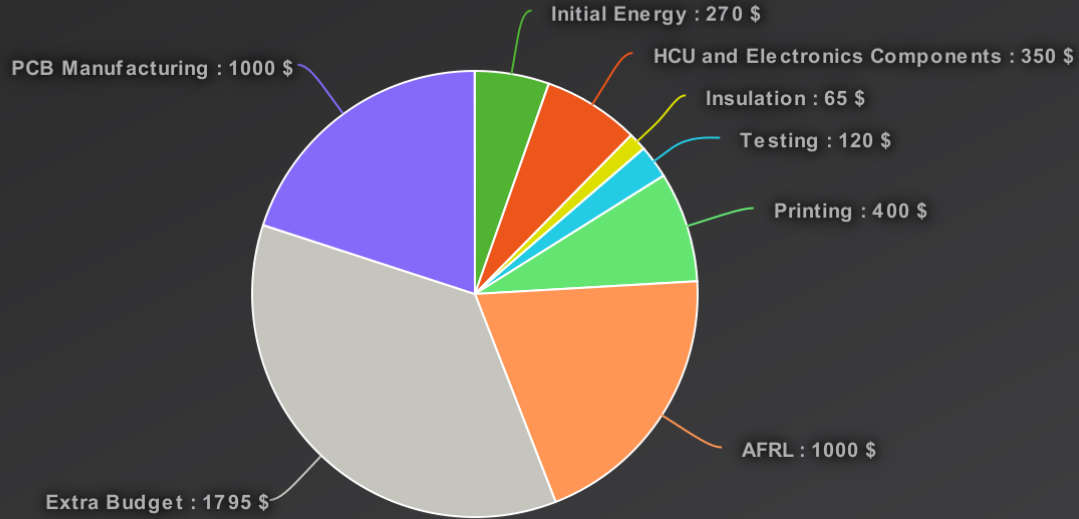




# Projected Budget



## ACES BUDGET



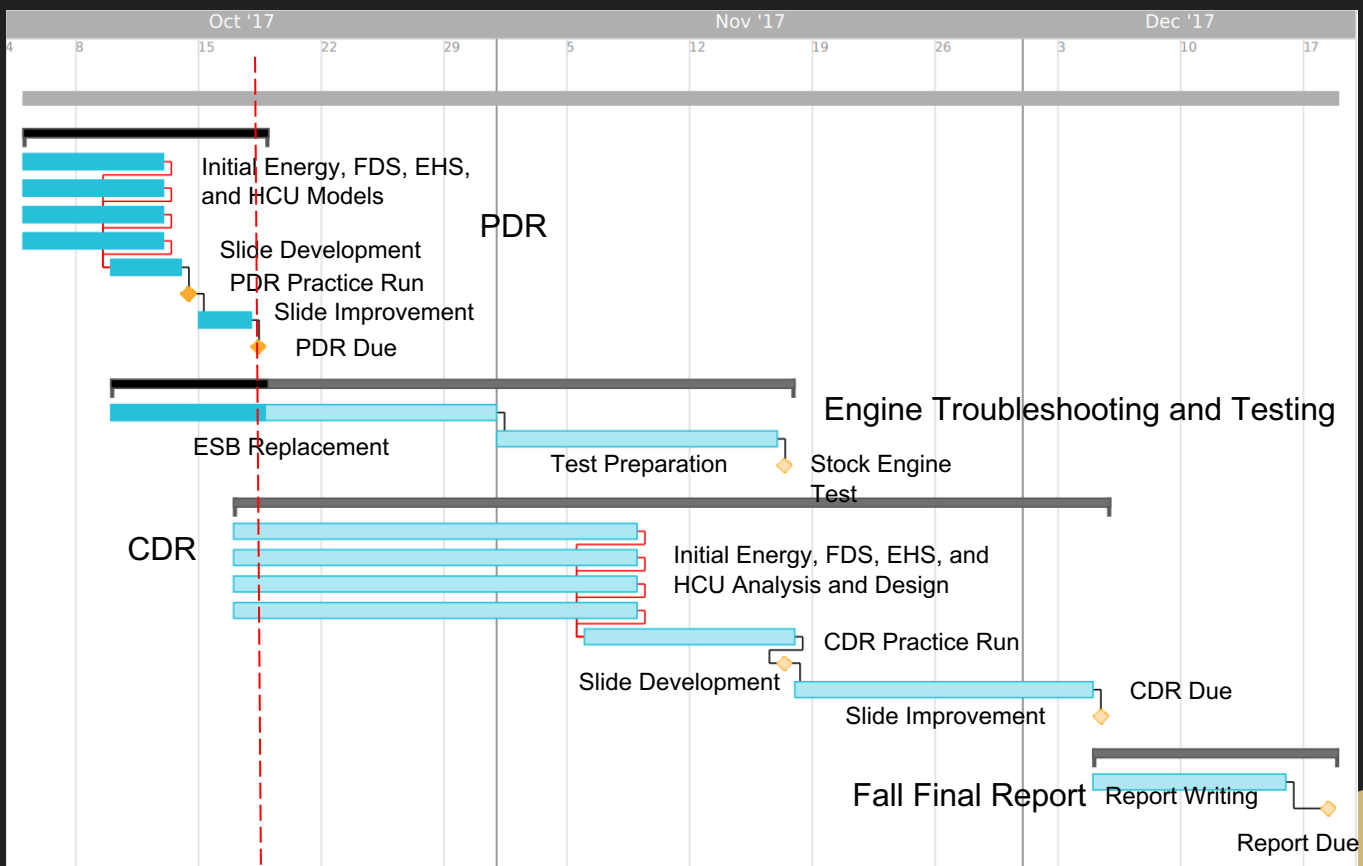
Initial Energy HCU and Electronics Component Insulation Testing Printing  
AFRL Extra Budget PCB Manufacturing

meta-chart.com





# Gantt Chart





# Acknowledgements

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The team would like thank the following people for their assistance in this project.

- John Evans
- Donna Gerren
- Bobby Hodgkinson
- Dale Lawrence
- James Nabity
- Matt Rhode
- Trudy Schwartz







# Sources



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- Coordinating Research Council, “HANDBOOK OF AVIATION FUEL PROPERTIES,” 1983





Questions?





# Backup Slides





## BACK of The Envelope Calculations



### Basic Change in Heat Equation for Warming of System Components

- Equation Used:  $\dot{Q}_{req} = \frac{mc_p(Temp_{final} - Temp_{initial})}{Time}$ 
  - Time = 8 minutes
  - Temp final = 290 K (62 °F)
  - Temp Initial = 227.6 K (-50 °F)

Results:

$$\dot{Q}_{tubing} = 2.242 W$$

$$\dot{Q}_{Hopper} = 32.9 W$$

$$\dot{Q}_{Electronics\ Box} = 0.47 W$$

$$\dot{Q}_{Battery} = 16.95 W$$





# HCU BackUP Slides



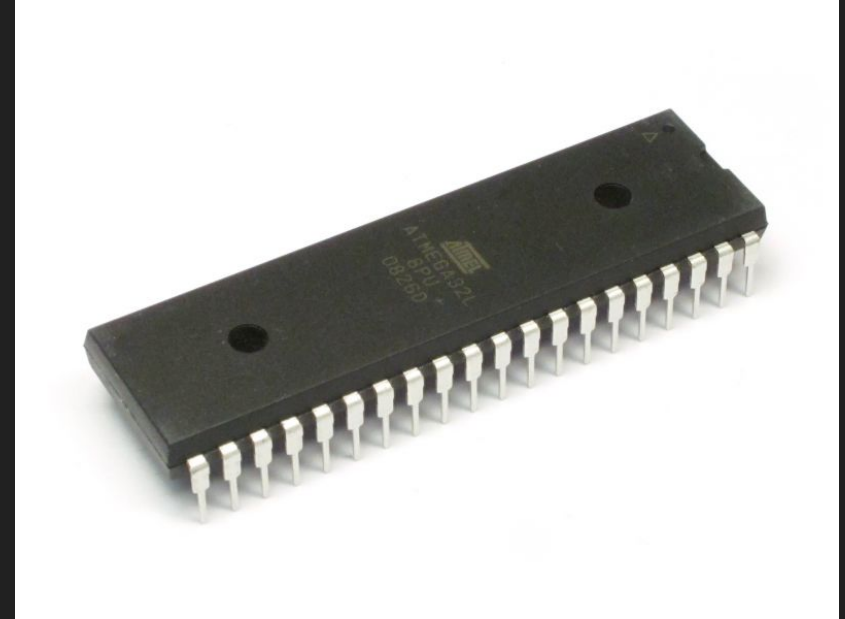


# HCU Components



## ATmega32/L Microprocessor

- Operational Temperature Range:  $-55^{\circ}\text{C}$  to  $125^{\circ}\text{C}$
- Operational Voltage Range: 2.7V to 5.5V
- DC Current per I/O pin: 40 mA
- Data Processing:
  - 9600 Baud Rate (0.2% Error)
  - 8 Channel, 10-bit ADC
  - 4 PWM Channels





# HCU Components



## LM35 Temperature Sensor

Operational Temperature Range:  $-55^{\circ}\text{C}$  to  $150^{\circ}\text{C}$

Operational Voltage Range: 4V to 30V

Current Draw:  $60\mu\text{A}$

Accuracy:  $\pm 0.25^{\circ}\text{C}$

## MOSFET (RFP30N06LE)

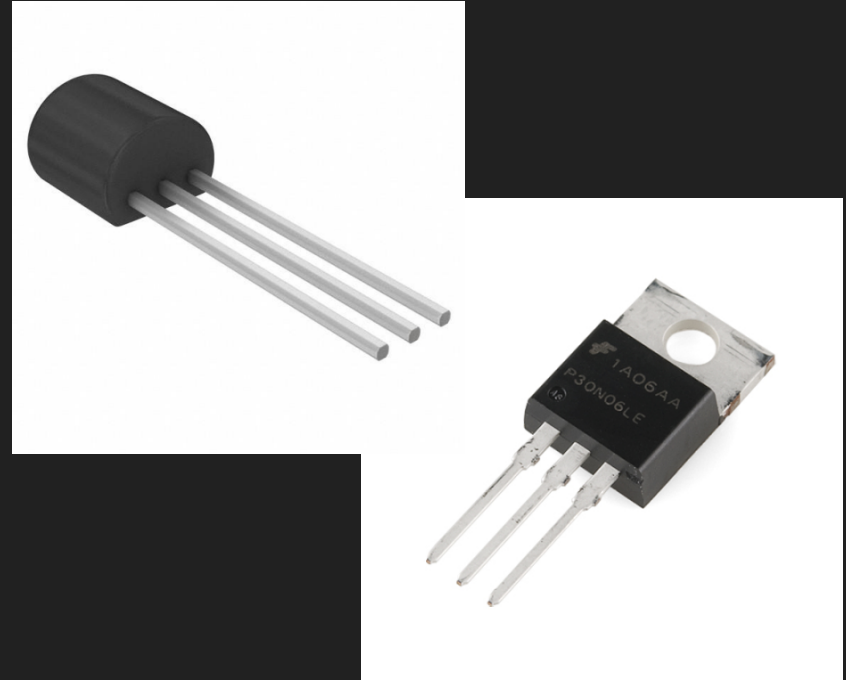
Operational Temperature Range:  $-55^{\circ}\text{C}$  to  $75^{\circ}\text{C}$

Start Time: 140 ns                      Rise

Time: 88 ns

Delay Time: 11 ns                      Fall

Time: 40n ns





# Initial Energy BackUP Slides







# Trade Study Result Analysis



## Low Temperature Batteries

- 3.6V, 19Ah Primary Lithium chosen
- *PROS:*
  - Operating Temperature: -55C to 85C, well within our operating envelope
  - High power capacity and density
- *CONS:*
  - Non-rechargeable
  - Voltage is approximately 2.5V at -50F
  - Can only source <150mA before cells are damaged
    - 375mW per battery
  - Would require 54 batteries to get the necessary power
    - Very costly ( $\$20.00 \times 54 + \text{shipping} + \text{tax} > \$1080.00$ )





# RC Circuit Equations



- Battery heat transfer

$$\dot{Q}_{in} = mc_p\Delta T$$
$$q_{in} = mc_p\Delta T dt$$

$\dot{Q}_{in}$  = power in (W or J/s)  
 $q_{in}$  = energy in (J)  
 $m$  = mass(kg)

$c_p$  = coefficient of temperature (J/kgK)

$\Delta T$  = change in temperature (K)

$dt$  = change in time (s)

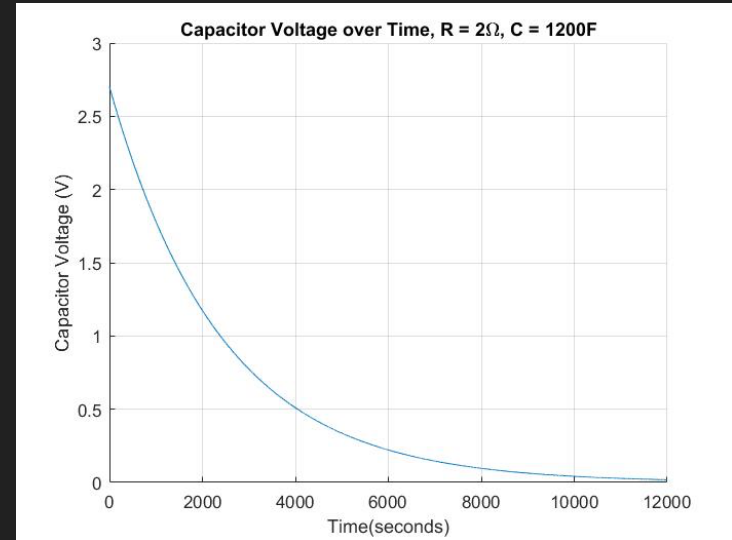




# Management of Supercapacitors



1. The team will never charge the capacitor with higher voltage than 2.7 V.
1. The team will never handle a charged capacitor without proper safety equipment
  - a. Thermal and electrical insulation will need to be worn.
1. Capacitors retain voltage for a long time after disconnected from circuit
  - a. Our capacitor will take 3 hours to fully discharge



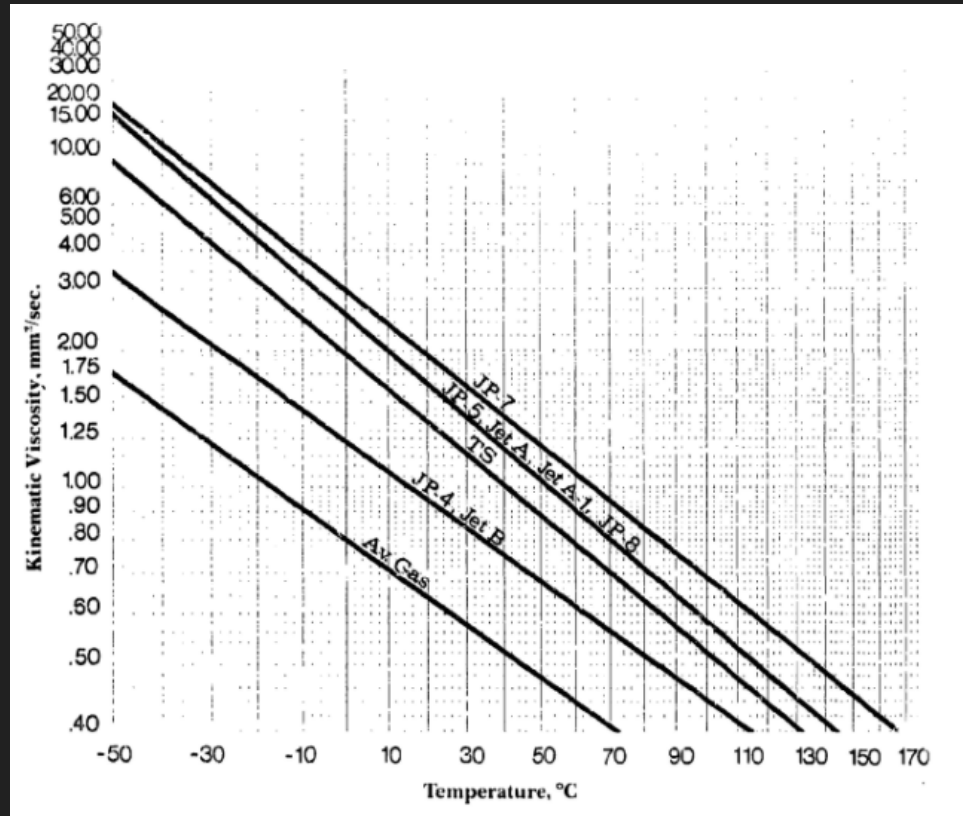


# Fuel Delivery System Backup Slides





# Viscosity vs Temperature





# Structures BackUP Slides





# Engine Structural Feasibility - Blade Tolerances



## Compressor Blade Clearances

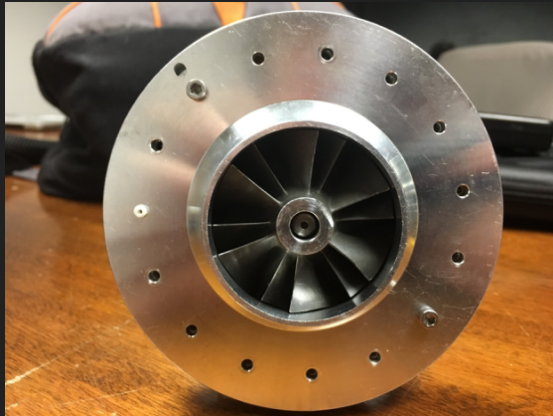
Blade material: Inconel

Housing material: 6061 Aluminum

Blade radius:  $23.385 \pm 0.0005$  mm

Housing radius:  $23.400 \pm 0.0005$  mm

Clearance:  $0.1905 \pm 0.01275$  mm



## Turbine Blade Clearances

Blade material: Inconel

Housing material: Inconel

Blade radius:  $33.235 \pm 0.0005$  mm

Housing radius:  $33.550 \pm 0.0005$  mm

Clearance:  $0.1397 \pm 0.01275$  mm





# Engine Structural Feasibility -Blade Tolerances (Cont.)



	$r_n$ (mm) [Housing radius]	$\ell_n$ (mm) [Blade length]
Compressor	23.3825	23.3494
Turbine	33.5249	33.2102

Thermal expansion for 1D material (blade):  $\ell_n = \ell_0 \cdot (1 + \alpha \cdot \Delta T)$

Thermal expansion for a ring (housing):  $r_n = r_o \cdot (1 + \alpha \cdot \Delta T)$

- $\Delta T = -65 \text{ C}$
- $\alpha_{\text{inc}} = 23.4 \cdot 10^{-6} [\text{C}^{-1}]$   
(for Inconel)
- $\alpha_{\text{Al}} = 11.5 \cdot 10^{-6} [\text{C}^{-1}]$   
(for Al-6061)

For structural integrity:  $r_n > \ell_n$







# Engine Structural Feasibility -Bearing Analysis



## Bearing and Housing radii [mm]:

- Material: Stainless Austenitic Steel 304 \*
- Housing material: Aluminum 6061
- Ball material: Silicon Nitride ( $\text{Si}_3\text{N}_4$ )
- Bearing diameter: 21.98 +/- 0.01
- Housing diameter: 21.92 +/- 0.01





# Engine Structural Feasibility -Bearing Analysis (Cont.)



- Because bearing and shaft have same material properties, will contract at same rate
  - Concern: shaft casing

	$r_n$ (mm) [housing radius]	$l_n$ (mm) [bearing radius]
Ball Bearing	21.9036	21.9553

Thermal expansion for 1D material (bearing):  $l_n = l_0 \cdot (1 + \alpha \cdot \Delta T)$

Thermal expansion for a ring (housing):  $r_n = r_0 \cdot (1 + \alpha \cdot \Delta T)$

For structural integrity of ball bearing in housing:  $r_n < l_n$

- $\Delta T = -65 \text{ C}$
- $\alpha_{\text{Steel}} = 17.3 \cdot 10^{-6} [\text{C}^{-1}]$   
(for Stainless Steel Austenitic 304)
- $\alpha_{\text{Al}} = 11.5 \cdot 10^{-6} [\text{C}^{-1}]$   
(for Al- 6061)



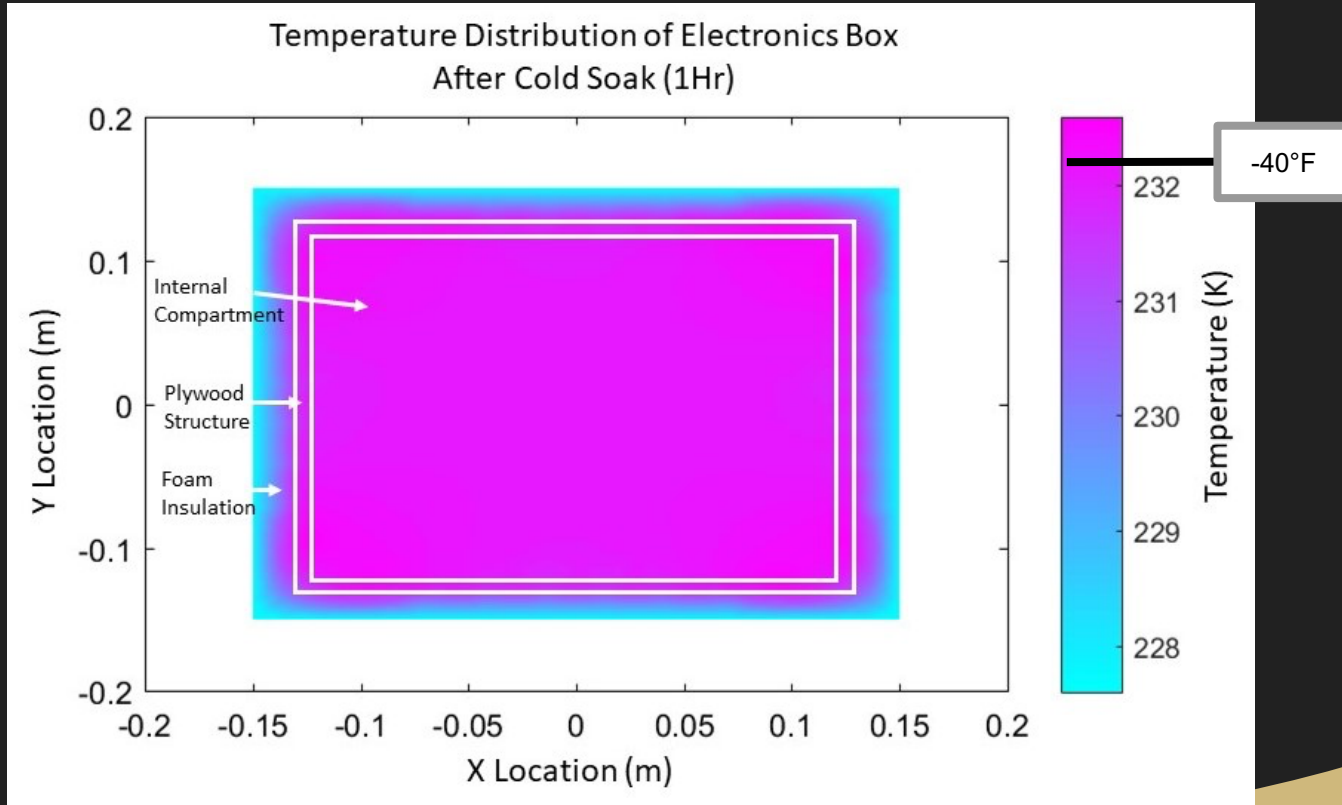


# Electronics Heating BackUP Slides





# Cooling of Electronics Box





# BUDGET BACKUP SLIDES





# Projected Budget



1. Initial power and batteries ~\$270
  - a. About 6 cold temperature batteries at \$20 each plus \$10 shipping=\$135
  - b. 2 LifePo batteries at \$65 each plus \$5 shipping=\$135
  - c. 2 LiPo batteries at \$50 each plus \$5 shipping=\$105
2. HCU and Electronic Components ~ \$1350
  - a. 10 supercapacitors at \$27 each plus \$5 shipping=\$275
  - b. 100 ft of insulated resistive heating wire at \$10/100ft plus \$5 shipping=\$15
  - c. Development and Printing PCB \$1000
3. Insulation ~ \$65
  - a. 2"x24"x82" Polyurethane foam at \$50 plus \$5 shipping=\$55
  - b. Plywood <\$10
4. Testing ~ \$120
  - a. Dry Ice at \$1-3 per pound, 10 pounds per test, 4 tests= \$120

Known Total: \$805





# FEM Setup Slides





# Fuel Line Parameters



- Used MATLAB's built in PDE tool
  - Numerical FEM Solver

## Material Properties

Material	Polyurethane	Kerosene
Density (kg/m <sup>3</sup> )	1100	862.4
Specific Heat (J/kg*k)	1800	2010
Thermal Conductivity (W/m*k)	0.29	0.15
Coefficient of Heat Transfer (W/m <sup>2</sup> *k)	22	N/A







# Fuel Hopper Feasibility



- Used MATLAB's built in PDE tool
  - Numerical FEM Solver

## Material Properties

Material	High Density Polyethylene	Kerosene
Density (kg/m <sup>3</sup> )	960	862.4
Specific Heat (J/kg*k)	2250	2010
Thermal Conductivity (W/m*k)	0.47	0.15
Internal Heat Generation (W/m <sup>3</sup> )	0	193256 TS, 64419 SS
Coefficient of Heat Transfer (W/m <sup>2</sup> *k)	22	N/A





# Electronic Box Feasibility



- Used MATLAB's built in PDE tool.
  - Numerical FEM Solver

Material Properties			
Material	Polyurethane	Plywood	Air
Density (kg/m <sup>3</sup> )	1100	680	1.569
Specific Heat (J/kg*k)	1800	1215	715.6
Thermal Conductivity (W/m*k)	0.29	0.12	0.0202
Coefficient of Heat Transfer (W/m <sup>2</sup> *k)	22	N/A	N/A





# Main Heater Parameters



- Used MATLAB's built in PDE tool.
  - Numerical FEM Solver

Material Properties		
Material	Lithium Polymer	Polyurethane
Density (kg/m <sup>3</sup> )	2109.4	1100
Specific Heat (J/kg*k)	795	1800
Thermal Conductivity (W/m*k)	73.98	0.29
Coefficient of Heat Transfer (W/m <sup>2</sup> *k)	N/A	40

