

# 10

## Superelements and Global-Local Analysis

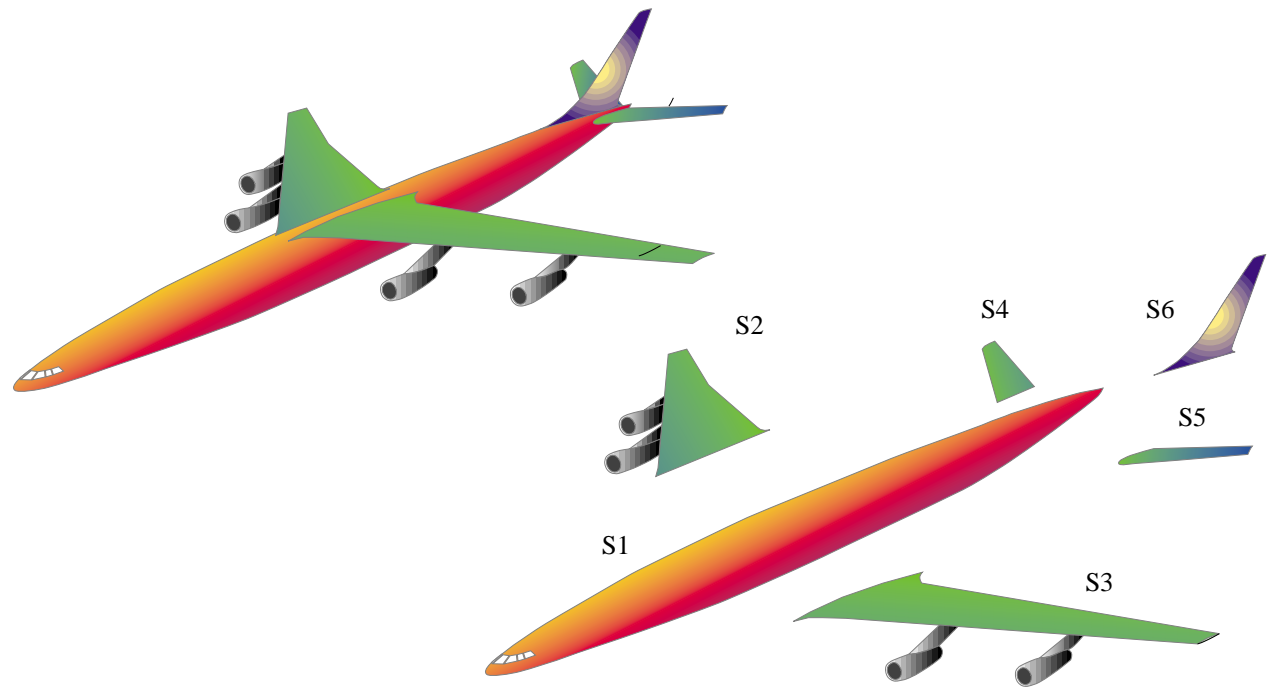
# Superelements

**Two extremes**

**Macroelements**      "bottom up"

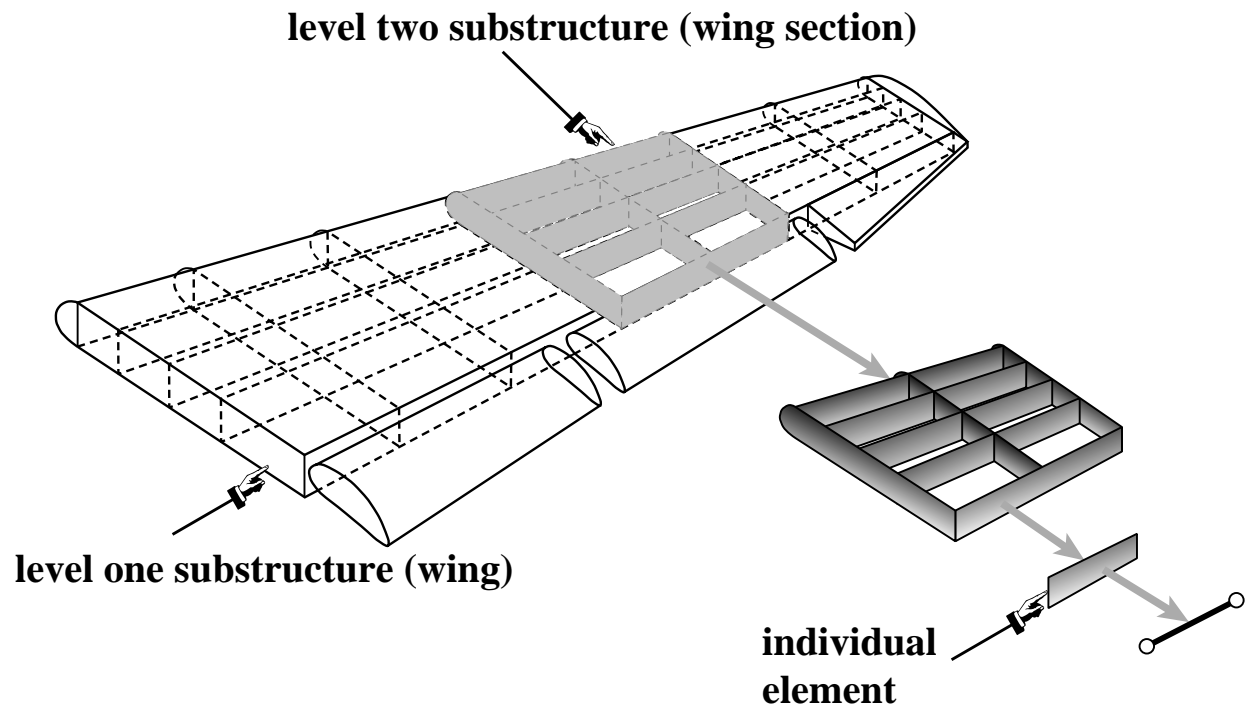
**Substructures**      "top down"

## Substructuring was Invented in the Aerospace Industry (early 1960s)



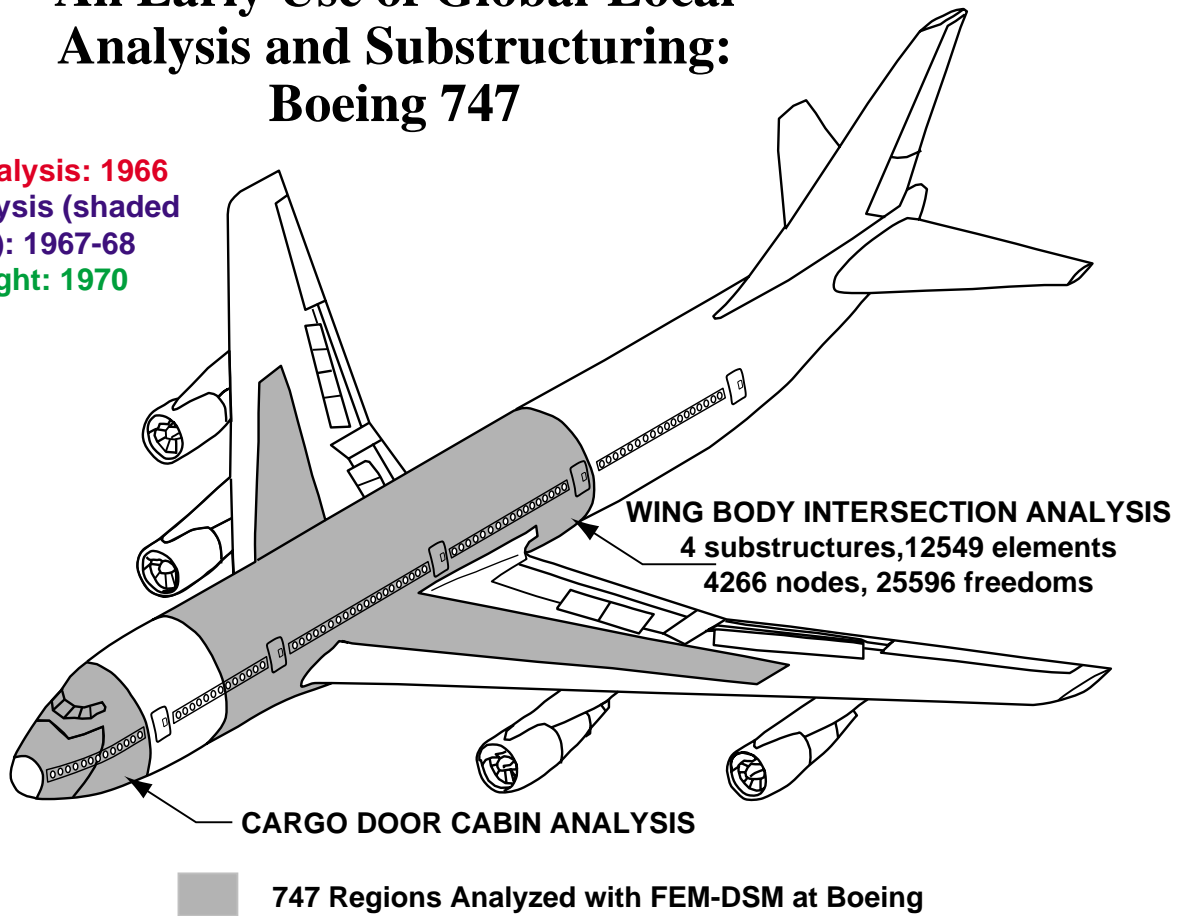
**First level substructuring**

## Substructures (cont'd)

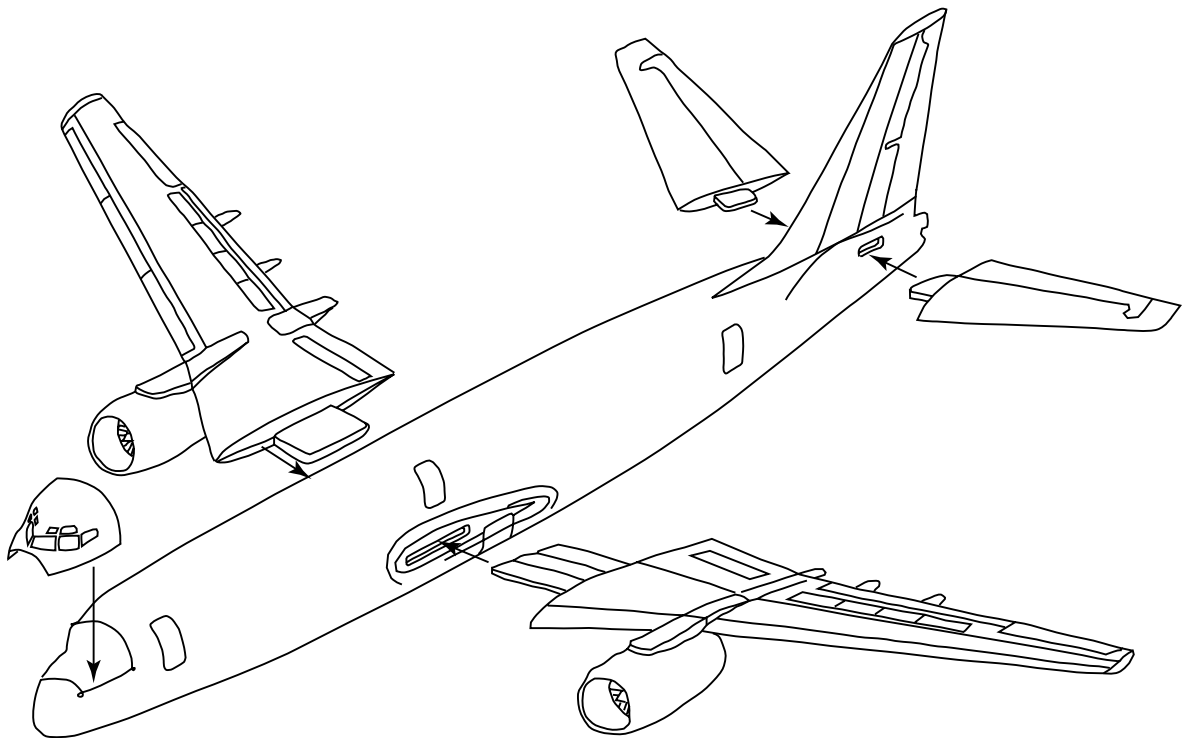


# An Early Use of Global-Local Analysis and Substructuring: Boeing 747

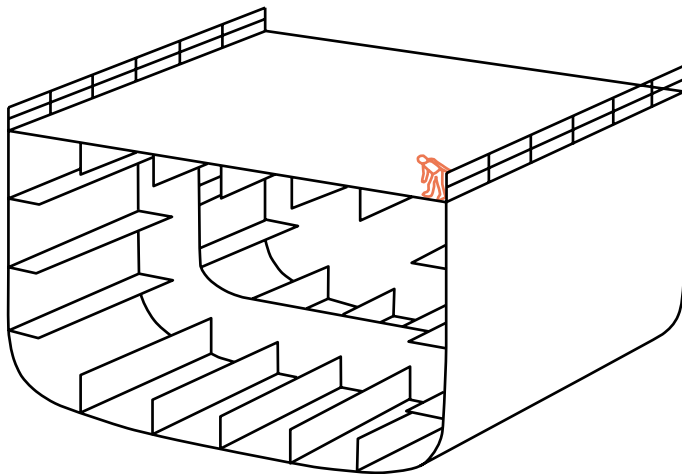
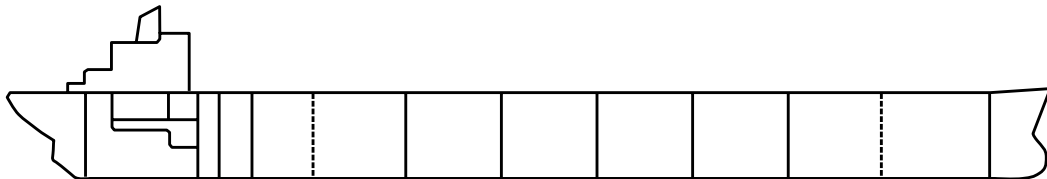
**Global Analysis: 1966**  
**Local Analysis (shaded regions): 1967-68**  
**First flight: 1970**



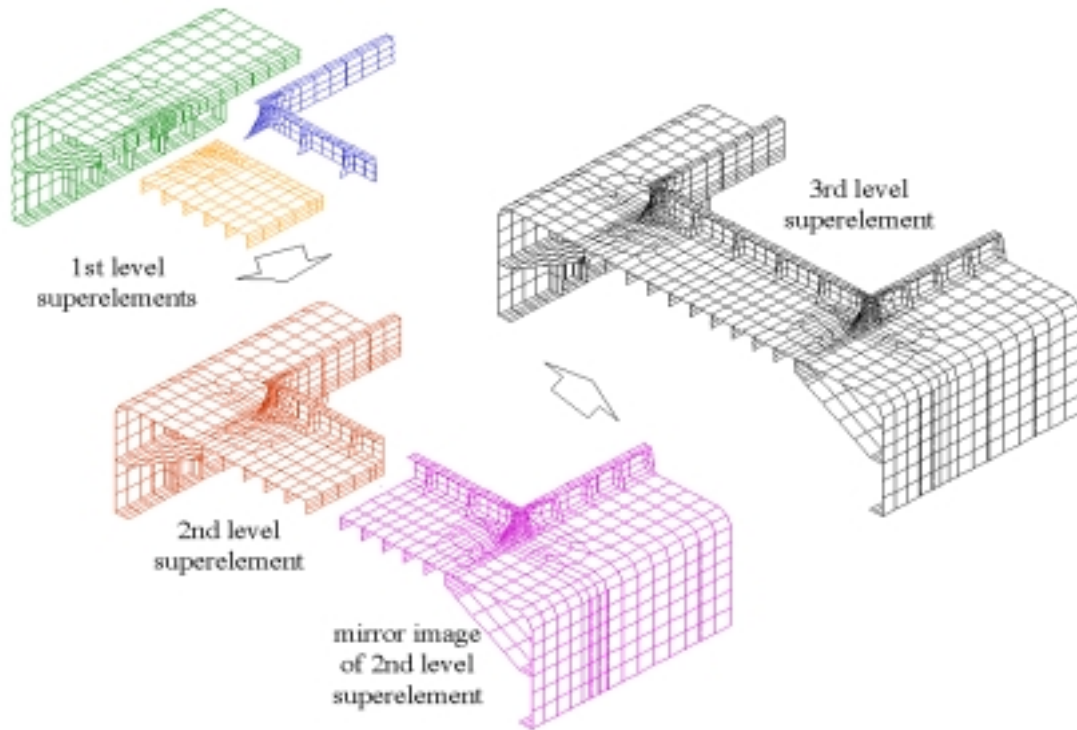
## **Another Example (McDonnell-Douglas DC-10, ca 1968)**



# **Multilevel FEM Substructuring** was Invented in the Norwegian Offshore Industry in the mid/late 60s



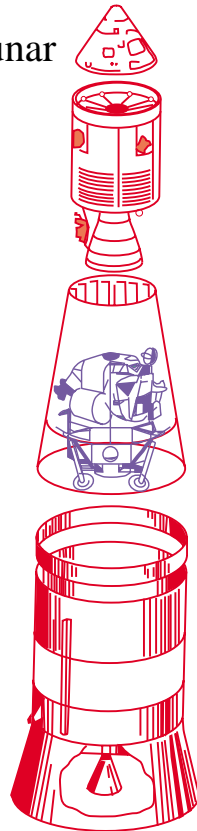
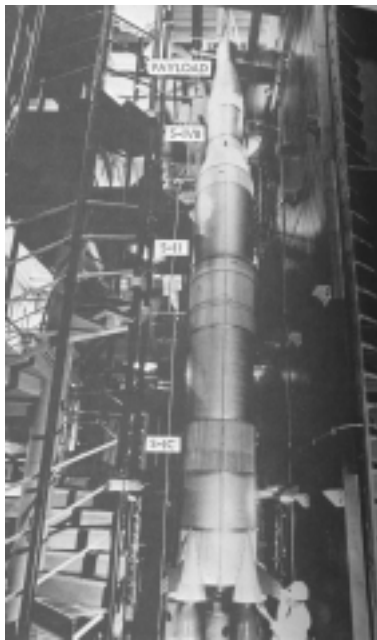
## Among Other Things, to Take Advantage of Repetition



From DNV (Det Norske Veritas) web-posted brochure.  
Permission requested for inclusion in book proper.

# Multistage Rockets Naturally Decompose into Substructures

Short stack  
Apollo/Saturn lunar  
rocket



COMMAND MODULE

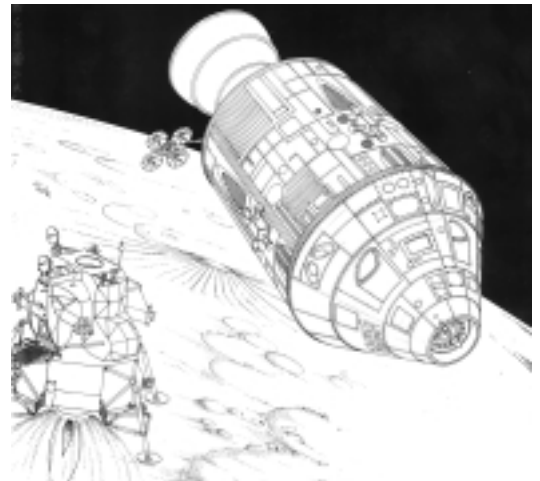
SERVICE MODULE

ADAPTER

LUNAR MODULE

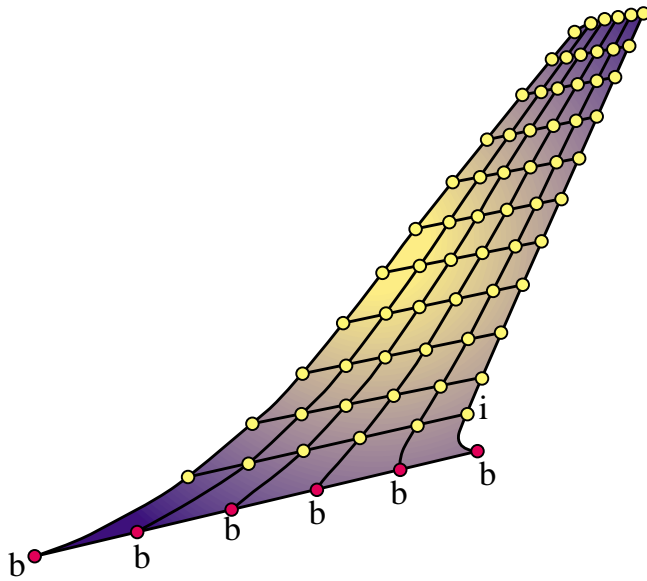
INSTRUMENT UNIT

THIRD STAGE  
SIV-B

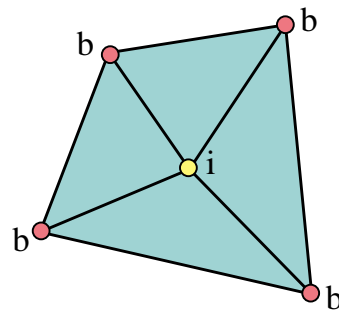


# Static Condensation

A universal way to eliminate internal DOFs



**Substructure**



**Macroelement**

## Static Condensation by Matrix Algebra

Partition 
$$\begin{bmatrix} \mathbf{K}_{bb} & \mathbf{K}_{bi} \\ \mathbf{K}_{ib} & \mathbf{K}_{ii} \end{bmatrix} \begin{bmatrix} \mathbf{u}_b \\ \mathbf{u}_i \end{bmatrix} = \begin{bmatrix} \mathbf{f}_b \\ \mathbf{f}_i \end{bmatrix}$$

Solve for interior displacements from 2nd matrix equation

$$\mathbf{u}_i = \mathbf{K}_{ii}^{-1} (\mathbf{f}_i - \mathbf{K}_{ib} \mathbf{u}_b)$$

replace into first matrix equation

$$\tilde{\mathbf{K}}_{bb} \mathbf{u}_b = \tilde{\mathbf{f}}_b$$

*Condensed  
stiffness equations*

where

$$\tilde{\mathbf{K}}_{bb} = \mathbf{K}_{bb} - \mathbf{K}_{bi} \mathbf{K}_{ii}^{-1} \mathbf{K}_{ib}$$

$$\tilde{\mathbf{f}}_b = \mathbf{f}_b - \mathbf{K}_{bi} \mathbf{K}_{ii}^{-1} \mathbf{f}_i$$

# Static Condensation by Symmetric Gauss Elimination

$$\begin{bmatrix} 6 & -2 & -1 & -3 \\ -2 & 5 & -2 & -1 \\ -1 & -2 & 7 & -4 \\ -3 & -1 & -4 & 8 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} = \begin{bmatrix} 3 \\ 6 \\ 4 \\ 0 \end{bmatrix}$$

8 is called the *pivot*

Task: eliminate  $u_4$

$$\begin{bmatrix} 6 & -2 & -1 & -3 \\ -2 & 5 & -2 & -1 \\ -1 & -2 & 7 & -4 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} 3 \\ 6 \\ 4 \end{bmatrix}$$

$\frac{(-3) \times (-3)}{8}$      $\frac{(-1) \times (-3)}{8}$      $\frac{(-4) \times (-3)}{8}$   
 $\frac{(-3) \times (-1)}{8}$      $\frac{(-1) \times (-1)}{8}$      $\frac{(-4) \times (-1)}{8}$   
 $\frac{(-3) \times (-4)}{8}$      $\frac{(-1) \times (-4)}{8}$      $\frac{(-4) \times (-4)}{8}$

$$\begin{bmatrix} \frac{39}{8} & -\frac{19}{8} & -\frac{5}{2} \\ -\frac{19}{8} & \frac{39}{8} & -\frac{5}{2} \\ -\frac{5}{2} & -\frac{5}{2} & 5 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} 3 \\ 6 \\ 4 \end{bmatrix}$$

*Condensed equations*

## Static Condensation by Symmetric Gauss Elimination (cont'd)

$$\begin{bmatrix} \frac{39}{8} & -\frac{19}{8} & -\frac{5}{2} \\ -\frac{19}{8} & \frac{39}{8} & -\frac{5}{2} \\ -\frac{5}{2} & -\frac{5}{2} & 5 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} 3 \\ 6 \\ 4 \end{bmatrix}$$

Now eliminate  $u_3$

$$\begin{bmatrix} \frac{39}{8} - \frac{(-5/2) \times (-5/2)}{5} & -\frac{19}{8} - \frac{(-5/2) \times (-5/2)}{5} \\ -\frac{19}{8} - \frac{(-5/2) \times (-5/2)}{5} & \frac{39}{8} - \frac{(-5/2) \times (-5/2)}{5} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} 3 - \frac{4 \times (-5/2)}{5} \\ 6 - \frac{4 \times (-5/2)}{5} \end{bmatrix}$$

$$\begin{bmatrix} \frac{29}{8} & -\frac{29}{8} \\ -\frac{29}{8} & \frac{29}{8} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} 5 \\ 8 \end{bmatrix}$$

**Condensed equations**

## Static Condensation Module (posted on web site)

```

CondenseLastFreedom[K_,f_]:=Module[{pivot,c,Kc,fc,
  n=Length[K]}, If [n<=1,Return[{K,f}]];
  Kc=Table[0,{n-1},{n-1}]; fc=Table[0,{n-1}];
  pivot=K[[n,n]]; If [pivot==0, Print["CondenseLastFreedom:",
    " Singular Matrix"]; Return[{K,f}]];
  For [i=1,i<=n-1,i++, c=K[[i,n]]/pivot;
    fc[[i]]=f[[i]]-c*f[[n]];
    For [j=1,j<=i,j++,
      Kc[[j,i]]=Kc[[i,j]]=K[[i,j]]-c*K[[n,j]]
    ];
  ];
  Return[Simplify[{Kc,fc}]]
];

ClearAll[K,f];
K={{6,-2,-1,-3},{-2,5,-2,-1},{-1,-2,7,-4},{-3,-1,-4,8}};
f={3,6,4,0};
Print["Before condensation:", " K=",K//MatrixForm," f=",f//MatrixForm];
{K,f}=CondenseLastFreedom[K,f];Print["Upon condensing DOF 4:",
  " K=",K//MatrixForm," f=",f//MatrixForm];
{K,f}=CondenseLastFreedom[K,f];Print["Upon condensing DOF 3:",
  " K=",K//MatrixForm," f=",f//MatrixForm];

```

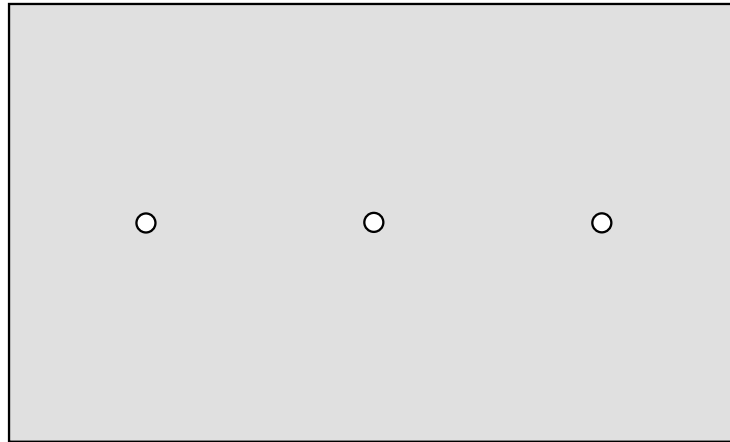
## Static Condensation Module Results on Notes Example

$$\text{Before condensation: } K = \begin{pmatrix} 6 & -2 & -1 & -3 \\ -2 & 5 & -2 & -1 \\ -1 & -2 & 7 & -4 \\ -3 & -1 & -4 & 8 \end{pmatrix} \quad f = \begin{pmatrix} 3 \\ 6 \\ 4 \\ 0 \end{pmatrix}$$

$$\text{Upon condensing DOF 4: } K = \begin{pmatrix} \frac{39}{8} & -\frac{19}{8} & -\frac{5}{2} \\ -\frac{19}{8} & \frac{39}{8} & -\frac{5}{2} \\ -\frac{5}{2} & -\frac{5}{2} & 5 \end{pmatrix} \quad f = \begin{pmatrix} 3 \\ 6 \\ 4 \end{pmatrix}$$

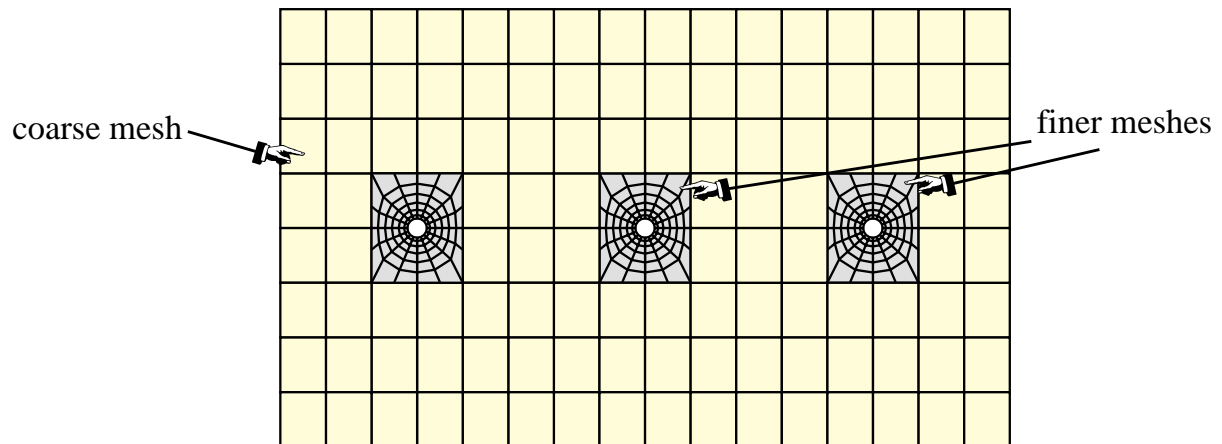
$$\text{Upon condensing DOF 3: } K = \begin{pmatrix} \frac{29}{8} & -\frac{29}{8} \\ -\frac{29}{8} & \frac{29}{8} \end{pmatrix} \quad f = \begin{pmatrix} 5 \\ 8 \end{pmatrix}$$

## **Global-Local Analysis (an instance of Multiscale Analysis)**

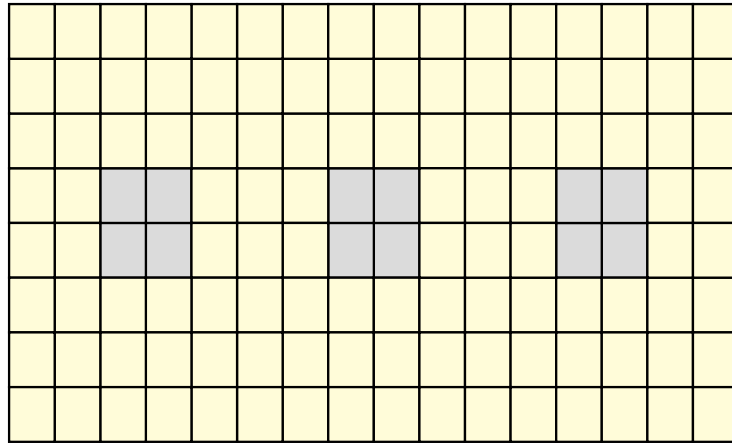


**Example structure: panel with small holes**

## Standard (one-stage) FEM Analysis



## **Global-Local (two-stage) FEM Analysis**



Global analysis with a coarse mesh, ignoring holes, followed by local analysis of the vicinity of the holes with finer meshes (next slide)

## **Local Analysis**

**BCs of displacement or (better) of force type  
using results extracted from the global analysis**

