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MultiFreedom Constraints I

Multifreedom Constraints

Single freedom constraint examples

$$u_{x4} = 0 \quad \text{linear, homogeneous}$$

$$u_{y9} = 0.6 \quad \text{linear, non-homogeneous}$$

Multifreedom constraint examples

$$u_{x2} = \frac{1}{2}u_{y2} \quad \text{linear, homogeneous}$$

$$u_{x2} - 2u_{x4} + u_{x6} = 0.25 \quad \text{linear, non-homogeneous}$$

$$(x_5 + u_{x5} - x_3 - u_{x3})^2 + (y_5 + u_{y5} - y_3 - u_{y3})^2 = 0$$

nonlinear, homogeneous

Sources of Multifreedom Constraints

"Skew" displacement BCs

Coupling nonmatched FEM meshes

Global-local and multiscale analysis

Incompressibility

Model reduction

MFC Application Methods

Master-Slave Elimination

Chapter 8

Penalty Function Augmentation

Lagrange Multiplier Adjunction



Chapter 9

Procedure Summary in **Static** Analysis Valid for the Three Methods

Unmodified master stiffness equations $\mathbf{K} \mathbf{u} = \mathbf{f}$ before applying MFCs

Apply MFCs

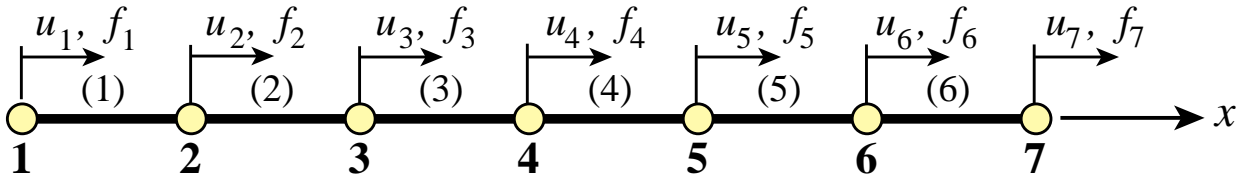
{ master slave
penalty function
Lagrange multiplier

Modified stiffness equations $\hat{\mathbf{K}} \hat{\mathbf{u}} = \hat{\mathbf{f}}$

Equation solver gives $\hat{\mathbf{u}}$

Recover \mathbf{u} if necessary

Example 1D Structure to Illustrate MFCs

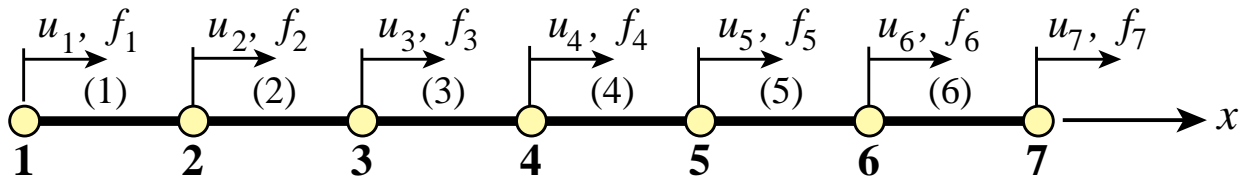


Multifreedom constraint:

$$u_2 = u_6 \quad \text{or} \quad u_2 - u_6 = 0$$

Linear homogeneous MFC

Example 1D Structure (Cont'd)



Unconstrained master stiffness equations

$$\begin{bmatrix}
 K_{11} & K_{12} & 0 & 0 & 0 & 0 & 0 \\
 K_{12} & K_{22} & K_{23} & 0 & 0 & 0 & 0 \\
 0 & K_{23} & K_{33} & K_{34} & 0 & 0 & 0 \\
 0 & 0 & K_{34} & K_{44} & K_{45} & 0 & 0 \\
 0 & 0 & 0 & K_{45} & K_{55} & K_{56} & 0 \\
 0 & 0 & 0 & 0 & K_{56} & K_{66} & K_{67} \\
 0 & 0 & 0 & 0 & 0 & K_{67} & K_{77}
 \end{bmatrix}
 \begin{bmatrix}
 u_1 \\
 u_2 \\
 u_3 \\
 u_4 \\
 u_5 \\
 u_6 \\
 u_7
 \end{bmatrix}
 =
 \begin{bmatrix}
 f_1 \\
 f_2 \\
 f_3 \\
 f_4 \\
 f_5 \\
 f_6 \\
 f_7
 \end{bmatrix}$$

or

$$\mathbf{K} \mathbf{u} = \mathbf{f}$$

Master-Slave Method for Example Structure

Recall: $u_2 = u_6$ or $u_2 - u_6 = 0$

Taking u_2 as master and u_6 as slave

$$\begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \\ u_7 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \\ u_7 \end{bmatrix}$$

or

$$\mathbf{u} = \mathbf{T} \hat{\mathbf{u}}$$

Forming the Modified Stiffness Equations

Unconstrained master
stiffness equations:

$$\mathbf{K} \mathbf{u} = \mathbf{f}$$

Master-slave transformation:

$$\mathbf{u} = \mathbf{T} \hat{\mathbf{u}}$$

Replace \mathbf{u} & premultiply
both sides by \mathbf{T}^T :

$$\mathbf{K} \mathbf{T} \hat{\mathbf{u}} = \mathbf{f}$$

$$\mathbf{T}^T \mathbf{K} \mathbf{T} \hat{\mathbf{u}} = \mathbf{T}^T \mathbf{f}$$

On renaming $\hat{\mathbf{K}} = \mathbf{T}^T \mathbf{K} \mathbf{T}$ and $\hat{\mathbf{f}} = \mathbf{T}^T \mathbf{f}$
we get the modified stiffness equations:

$$\hat{\mathbf{K}} \hat{\mathbf{u}} = \hat{\mathbf{f}}$$

Modified Stiffness Equations for Example Structure

$$\hat{\mathbf{K}} \hat{\mathbf{u}} = \hat{\mathbf{f}}$$

In full

$$\begin{bmatrix} K_{11} & K_{12} & 0 & 0 & 0 & 0 \\ K_{12} & K_{22} + K_{66} & K_{23} & 0 & K_{56} & K_{67} \\ 0 & K_{23} & K_{33} & K_{34} & 0 & 0 \\ 0 & 0 & K_{34} & K_{44} & K_{45} & 0 \\ 0 & K_{56} & 0 & K_{45} & K_{55} & 0 \\ 0 & K_{67} & 0 & 0 & 0 & K_{77} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_7 \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 + f_6 \\ f_3 \\ f_4 \\ f_5 \\ f_7 \end{bmatrix}$$

Solve for $\hat{\mathbf{u}}$, then recover $\mathbf{u} = \mathbf{T} \hat{\mathbf{u}}$

Multiple MFCs

Suppose

$$u_2 - u_6 = 0, \quad u_1 + 4u_4 = 0, \quad 2u_3 + u_4 + u_5 = 0$$

Pick 3, 4 and 6 as slaves while 1, 2, 5 and 7 are masters

$$u_6 = u_2 \quad u_4 = -\frac{1}{4}u_1 \quad u_3 = -\frac{1}{2}(u_4 + u_5) = \frac{1}{8}u_1 - \frac{1}{2}u_5$$

Put in matrix form:

$$\begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \\ u_7 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ \frac{1}{8} & 0 & -\frac{1}{2} & 0 \\ -\frac{1}{4} & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_5 \\ u_7 \end{bmatrix}$$

This is $\mathbf{u} = \mathbf{T} \hat{\mathbf{u}}$ - then proceed as before

Non-homogeneous MFCs

$$u_2 - u_6 = 0.2$$

Pick again u_6 as slave, put into matrix form:

$$\begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \\ u_7 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_6 \\ u_7 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ -0.2 \\ 0 \end{bmatrix}$$

Nonhomogeneous MFCs (cont'd)

$$\mathbf{u} = \mathbf{T} \hat{\mathbf{u}} + \mathbf{g} \quad \mathbf{g}: \text{"gap" vector}$$

Premultiply both sides by $\mathbf{T}^T \mathbf{K}$, replace $\mathbf{K} \mathbf{u} = \mathbf{f}$ and pass data to RHS. This gives

$$\hat{\mathbf{K}} \hat{\mathbf{u}} = \hat{\mathbf{f}}$$

with $\hat{\mathbf{K}} = \mathbf{T}^T \mathbf{K} \mathbf{T}$ and $\hat{\mathbf{f}} = \mathbf{T}^T (\mathbf{f} - \mathbf{K} \mathbf{g})$

a modified force vector

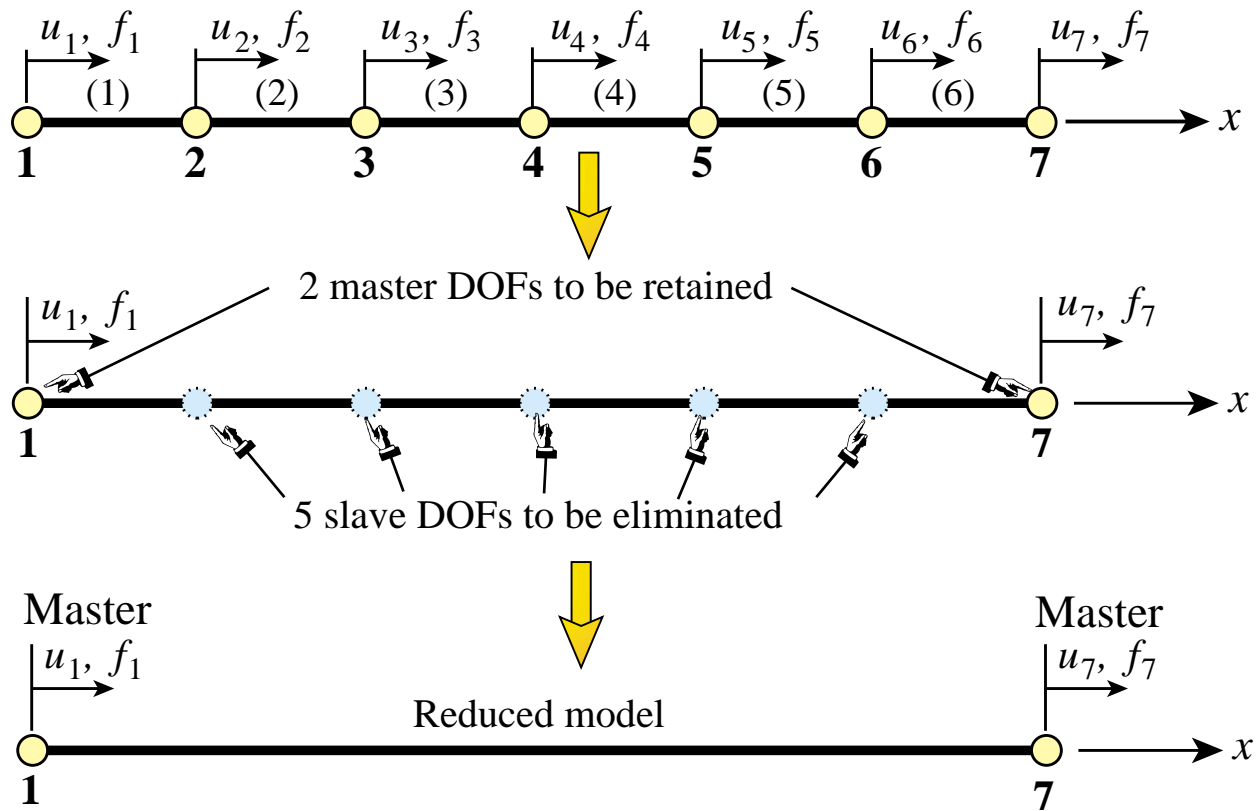
Nonhomogeneous MFCs (cont'd)

For the example structure

$$\begin{bmatrix} K_{11} & K_{12} & 0 & 0 & 0 & 0 \\ K_{12} & K_{22} + K_{66} & K_{23} & 0 & K_{56} & K_{67} \\ 0 & K_{23} & K_{33} & K_{34} & 0 & 0 \\ 0 & 0 & K_{34} & K_{44} & K_{45} & 0 \\ 0 & K_{56} & 0 & K_{45} & K_{55} & 0 \\ 0 & K_{67} & 0 & 0 & 0 & K_{77} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \\ u_5 \\ u_7 \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 + f_6 - 0.2K_{66} \\ f_3 \\ f_4 \\ f_5 - 0.2K_{56} \\ f_7 - 0.2K_{67} \end{bmatrix}$$

Solve for $\hat{\mathbf{u}}$, then recover $\mathbf{u} = \mathbf{T} \hat{\mathbf{u}} + \mathbf{g}$

Model Reduction Example



Model Reduction Example: Mathematica Script

```
(* Model Reduction Example *)
ClearAll[K11,K12,K22,K23,K33,K34,K44,K45,K55,K56,K66,
         f1,f2,f3,f4,f5,f6];
K={{K11,K12,0,0,0,0,0},{K12,K22,K23,0,0,0,0},
   {0,K23,K33,K34,0,0,0},{0,0,K34,K44,K45,0,0},
   {0,0,0,K45,K55,K56,0},{0,0,0,0,K56,K66,K67},
   {0,0,0,0,0,K67,K77}}; Print["K=",K//MatrixForm];
f={f1,f2,f3,f4,f5,f6,f7}; Print["f=",f];
T={{6,0},{5,1},{4,2},{3,3},{2,4},{1,5},{0,6}}/6;
Print["Transformation matrix T=",T//MatrixForm];
Khat=Simplify[Transpose[T].K.T];
fhat=Simplify[Transpose[T].f];
Print["Modified Stiffness:"];
Print["Khat(1,1)=",Khat[[1,1]],"\nKhat(1,2)=",Khat[[1,2]],
      "\nKhat(2,2)=",Khat[[2,2]] ];
Print["Modified Force:"];
Print["fhat(1)=",fhat[[1]]," fhat(2)=",fhat[[2]] ];
```

Modified Stiffness:

(Some print output removed so slide fits)

$$\text{Khat}(1,1) = \frac{1}{36} (36 K11 + 60 K12 + 25 K22 + 40 K23 + 16 K33 + 24 K34 + 9 K44 + 12 K45 + 4 K55 + 4 K56 + K66)$$

$$\text{Khat}(1,2) = \frac{1}{36} (6 K12 + 5 K22 + 14 K23 + 8 K33 + 18 K34 + 9 K44 + 18 K45 + 8 K55 + 14 K56 + 5 K66 + 6 K67)$$

$$\text{Khat}(2,2) = \frac{1}{36} (K22 + 4 K23 + 4 K33 + 12 K34 + 9 K44 + 24 K45 + 16 K55 + 40 K56 + 25 K66 + 60 K67 + 36 K77)$$

Modified Force:

$$\text{fhat}(1) = \frac{1}{6} (6 f1 + 5 f2 + 4 f3 + 3 f4 + 2 f5 + f6) \quad \text{fhat}(2) = \frac{1}{6} (f2 + 2 f3 + 3 f4 + 4 f5 + 5 f6 + 6 f7)$$

Assessment of Master-Slave Method



ADVANTAGES

- exact if precautions taken**
- easy to understand**
- retains positive definiteness**
- important applications to model reduction**



DISADVANTAGES

- requires user decisions**
- messy implementation for general MFCs**
- hinders sparsity of master stiffness equations**
- sensitive to constraint dependence**
- restricted to linear constraints**